

ICME Guided Development of Advanced Cast Aluminum Alloys For Automotive Engine Applications

Project ID: PM060

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2015 DOE VEHICLE TECHNOLOGY PROGRAM REVIEW



Overview

Timeline

- Project start date: February 2013
- Project end date: February 2016
- Percent complete: 30%

Barrier

- High temperature performance
- Design data & modeling tools
- Manufacturability
- Cost

Budget

- Total project funding
 - DOE share: \$3.24M
 - Contractor share: \$1.39M
- Funding received in FY14
 - \$579K
- Funding for FY15
 - \$1.3M

Partners

- Alcoa Inc.
- Nemak
- MAGMA Foundry Technologies, Inc.
- University of Michigan



Project Objectives

- To develop a new class of advanced, cost competitive aluminum casting alloys providing a 25% improvement in component strength relative to components made with A319 or A356 alloys for high-performance engine applications.
- To demonstrate the power of Integrated Computational Materials Engineering (ICME) tools for accelerating the development of new materials and processing techniques, as well as to identify the gaps in ICME capabilities.
- To develop comprehensive cost models to ensure that components manufactured with these new alloys do not exceed 110% of the cost using incumbent alloys A319 or A356.
- To develop a technology transfer and commercialization plan for deployment of these new alloys in automotive engine applications.



Approach

Task 1.0 – Project Management and Planning

Task 2.0 – ICME Guided Alloy Development

Task 3.0 – ICME Tools Gap Analysis

**Task 4.0 – Demonstration and Validation of New Alloys
on Engine Components**

Task 5.0 – Cost Model Development and Planning



Deliverables and Timeline

| Tasks | Year 1 | | | | Year 2 | | | | Year 3 | | | |
|--|--------|---|---|---|--------|---|---|---|--------|----|----|----|
| | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 |
| Task 1: Project Management and Planning | | | | | | | | | | | | |
| 1.1 Update Project Management Plan | | | | | | | | | | | | |
| 1.2 Project Management | | | | | | | | | | | | |
| Task 2: ICME Guided Alloy Development | | | | | | | | | | | | |
| 2.1 Initial Alloy Design | | | | | | | | | | | | |
| 2.2 Microstructural Characterization and Property Quantification | | | | | | | | | | | | |
| 2.3 Alloy Optimization | | | | | | | | | | | | |
| Task 3: ICME Tools Gap Analysis | | | | | | | | | | | | |
| 3.1 CALPHD tools gap analysis | | | | | | | | | | | | |
| 3.2 Process modeling gap analysis | | | | | | | | | | | | |
| 3.3 Microstructure model gap analysis | | | | | | | | | | | | |
| 3.4 Mechanical property models gap analysis | | | | | | | | | | | | |
| Task 4: Demonstration and Validation of New Alloys on Engine Components | | | | | | | | | | | | |
| 4.1 Demonstration on Engine Components | | | | | | | | | | | | |
| 4.2 Validation on Engine Components | | | | | | | | | | | | |
| Task 5: Cost Model Development | | | | | | | | | | | | |
| 5.1 Evaluation of Existing Cost Model | | | | | | | | | | | | |
| 5.2 Development of Predictive Cost Model for the New Alloys | | | | | | | | | | | | |
| 5.3 Establishment of Technology Transfer and Commercialization Plan | | | | | | | | | | | | |



Targeted Properties

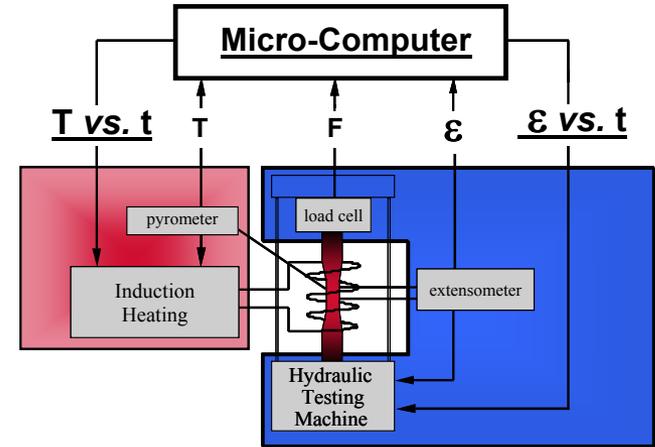
| Property | Cast Aluminum Baseline | Cast Lightweight Alloy Targets | Key Properties |
|---|------------------------|--------------------------------|----------------|
| Tensile Strength (Ksi) | 33 KSI | 40 KSI | Key |
| Yield Strength (Ksi) | 24 KSI | 30 KSI | Key |
| Density | 2.7 g/cm ³ | < 6.4 g/cm ³ | Key |
| Elongation (%) | 3.50% | 3.50% | |
| Shear Strength | 26 KSI | 30 KSI | |
| Endurance Limit | 8.5 KSI | 11 KSI | |
| Fluidity (Die Filling Capacity/Spiral Test) | Excellent | Excellent | Key |
| Hot Tearing Resistance | Excellent | Excellent | Key |
| High Temperature Performance | @ 250C | @ 300 C | |
| Tensile Strength (KSI) | 7.5KSI @ 250 C | 9.5 KSI @ 300 C | Key |
| Yield Strength (KSI) | 5 KSI @ 250 C | 6.5 KSI @ 300 C | Key |
| Elongation in 2" | 20% @ 250 C | < 20% @ 300 C | |



Casting and Testing Facility



Electric melting furnaces and flux unit
Sand mixer and sand mold



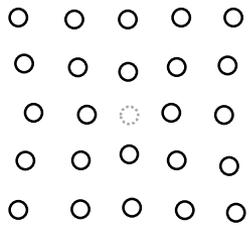
Schematic representation of the TMF
test setup implemented at Ford R&A



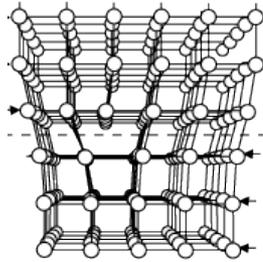
Drop bottom HT furnace and
Quenching basket



Alloy Design Strengthening Mechanism



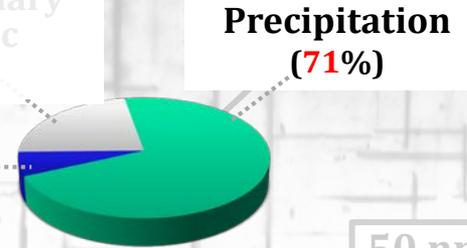
• Vacancy



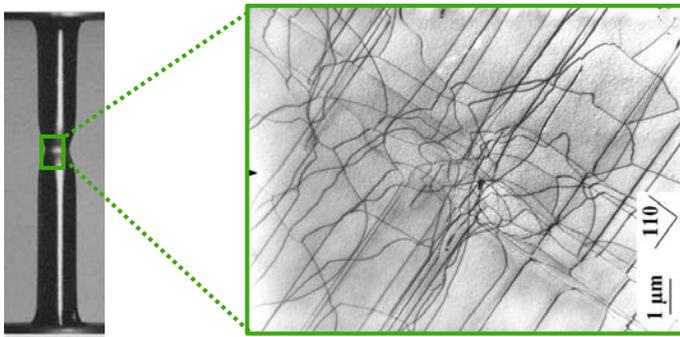
--- Dislocation

Yield Strength of W319 (230°C10hr): 310 MPa

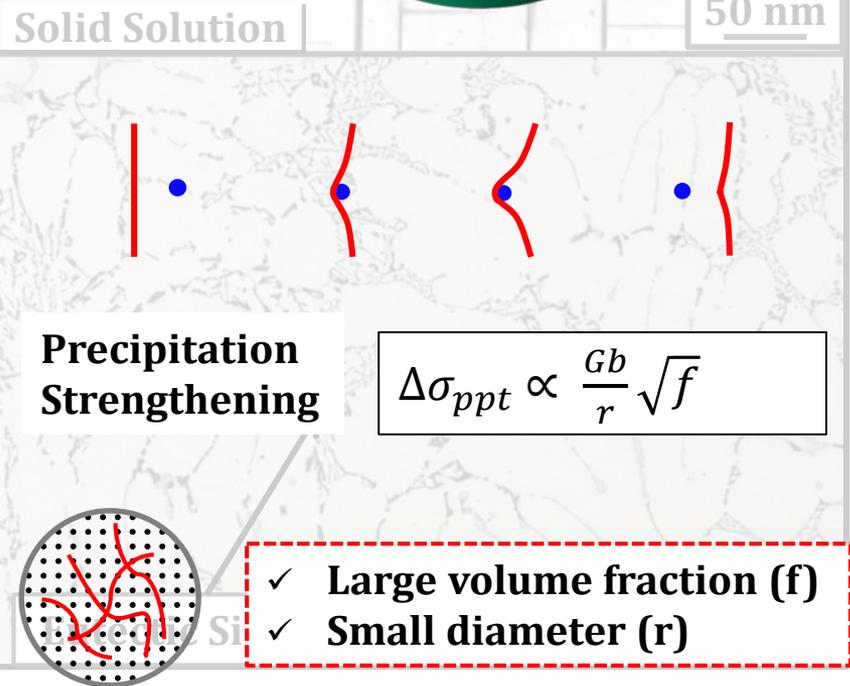
Precipitation is KEY!



Plastic Deformation: Motion of Dislocation



Strengthening Mechanism: Grain Boundary, Eutectic, Precipitation, Solid Solution...



Alloy Design The Problem

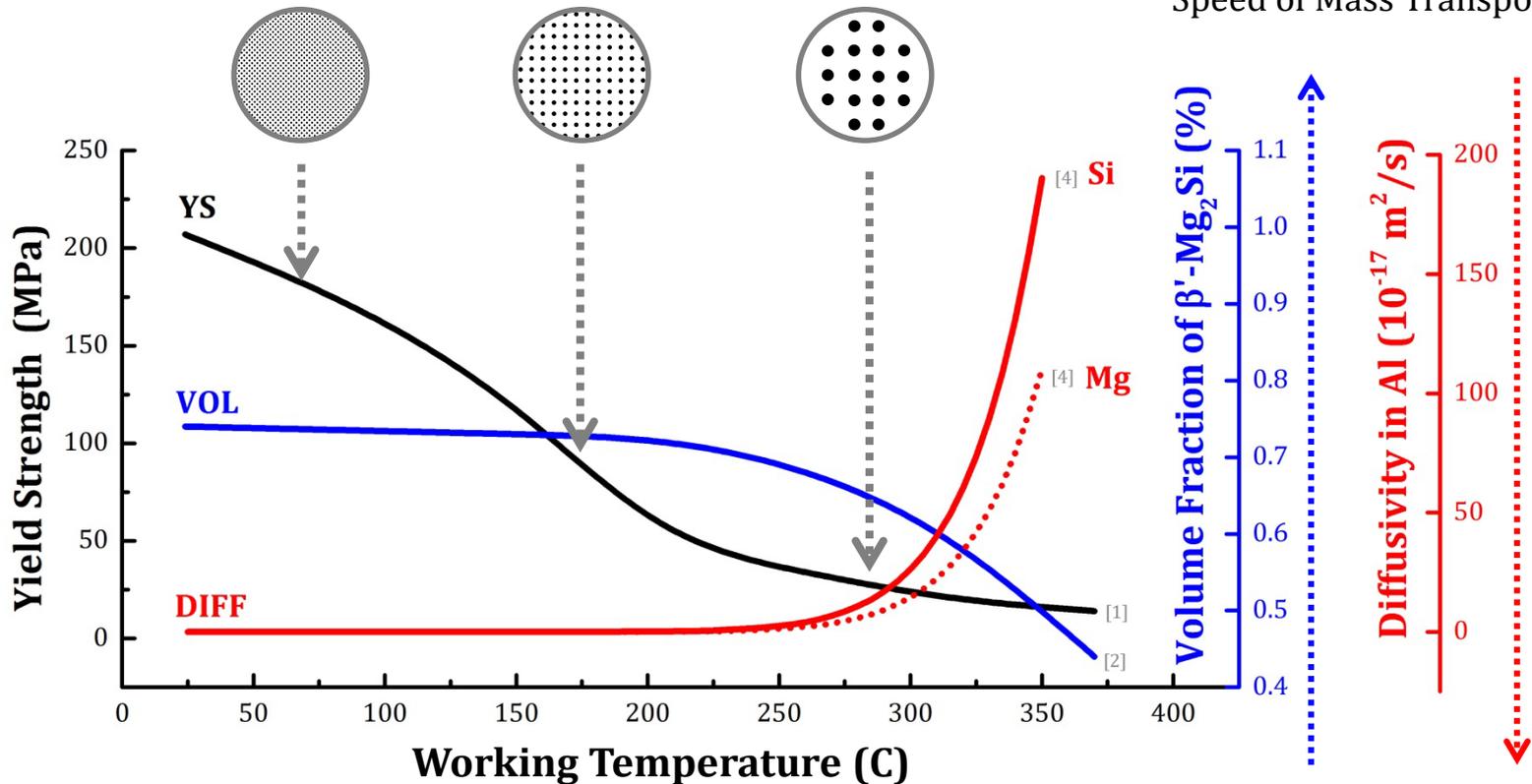
(A356-T61 Permanent Mold)

✓ Large volume fraction (f) + Small diameter (r)

$$r^3 = k \cdot t$$

$$k \propto D\gamma C_e$$

Diffusivity:
Speed of Mass Transportation



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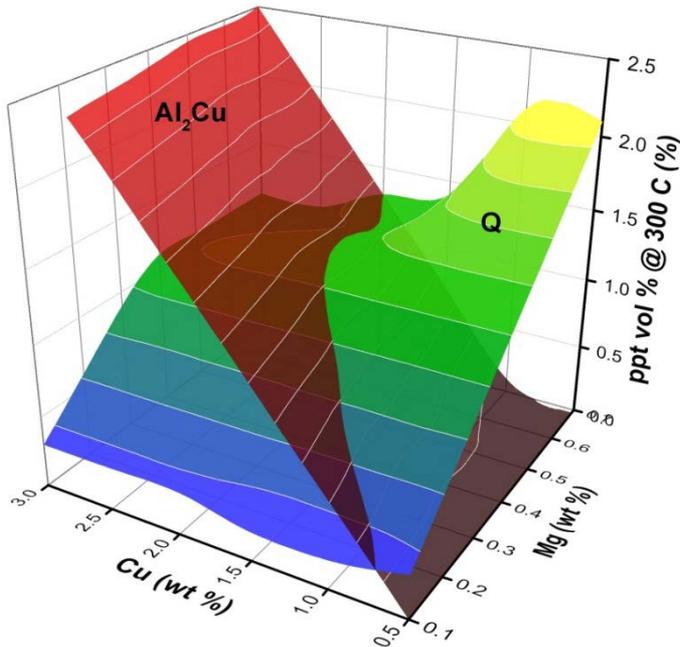
Alloy Design Composition

Matrix:

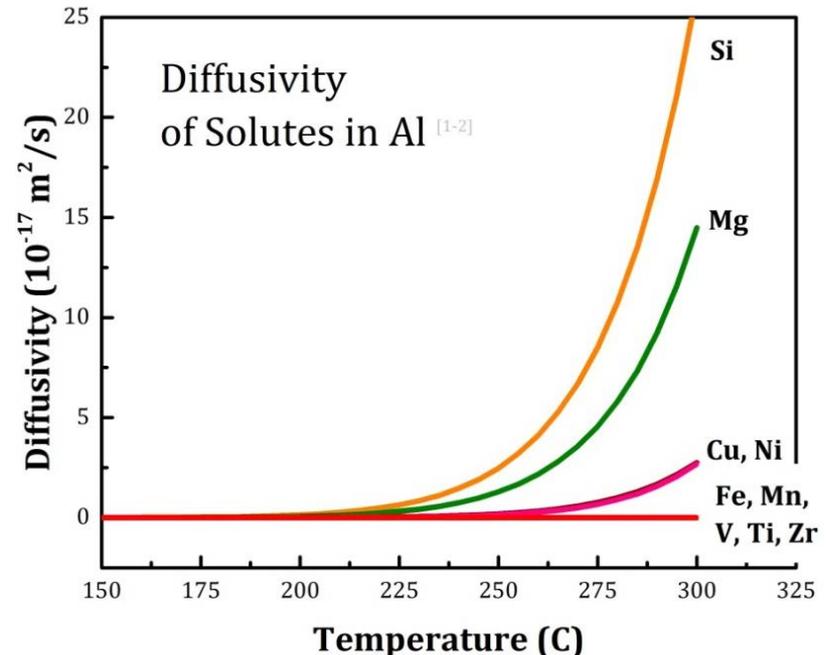
Al5.0-10.0Si0-4.0Cu0-0.4Mg was chosen as the baseline because of its good castability and strength.

Precipitates:

Optimize volume fraction of (θ' +Q')



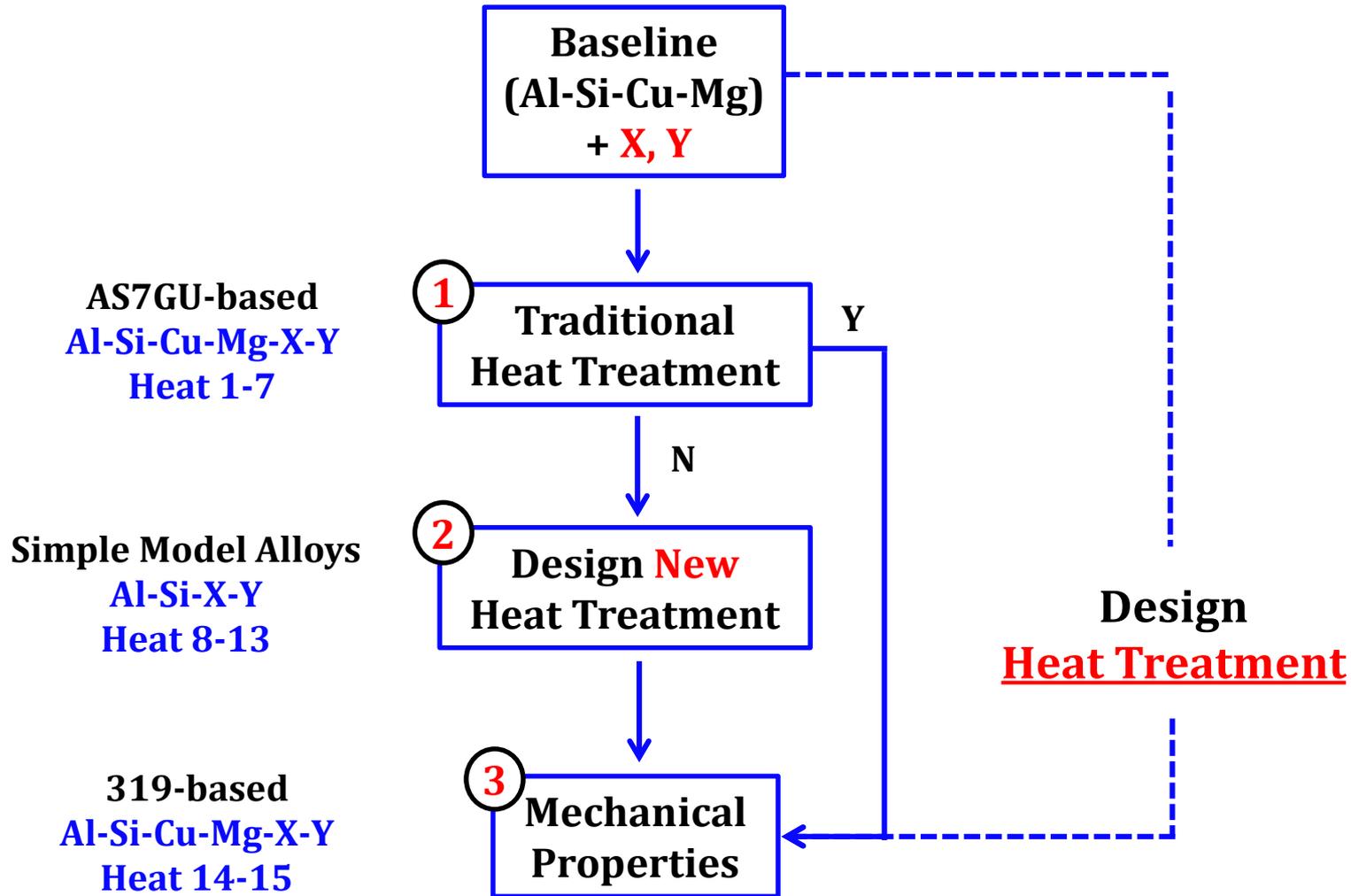
Introduce Heat-resistant Precipitates



15 different heats of alloys were proposed to pursue the optimal alloy composition.



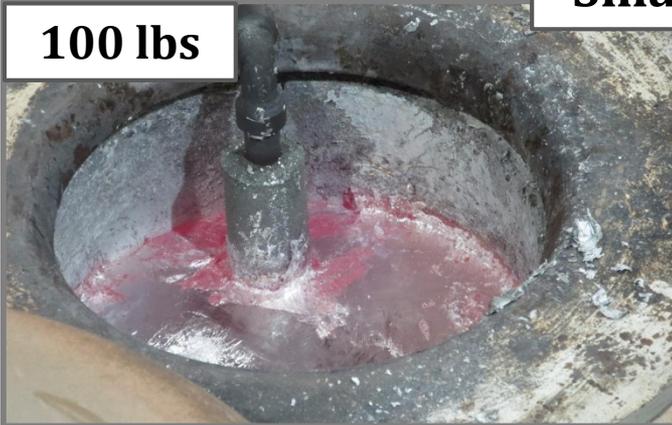
Alloy Design Heat Treatment



Experiment Casting

Small Batch

100 lbs



(a) Melting raw materials @ 750 C.

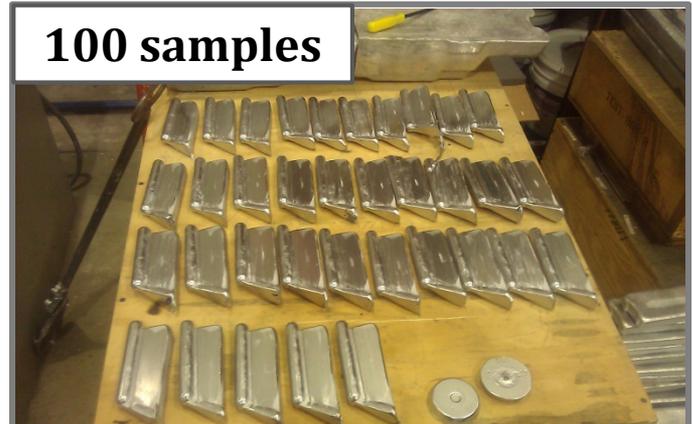


(b) Pouring spectrometer disk.



(c) Pouring torpedo shape sample.

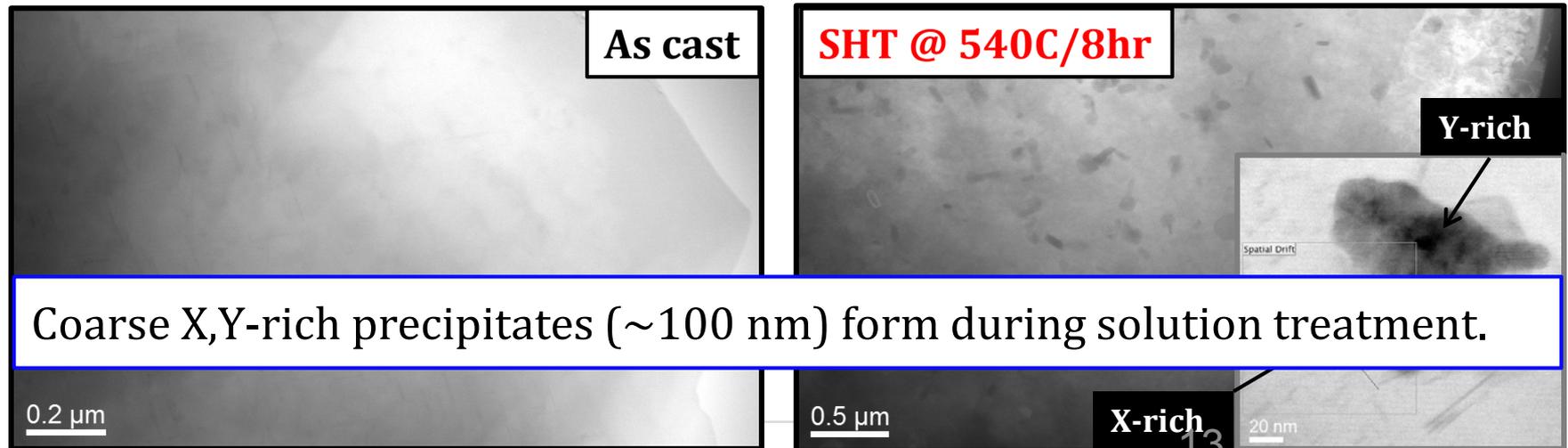
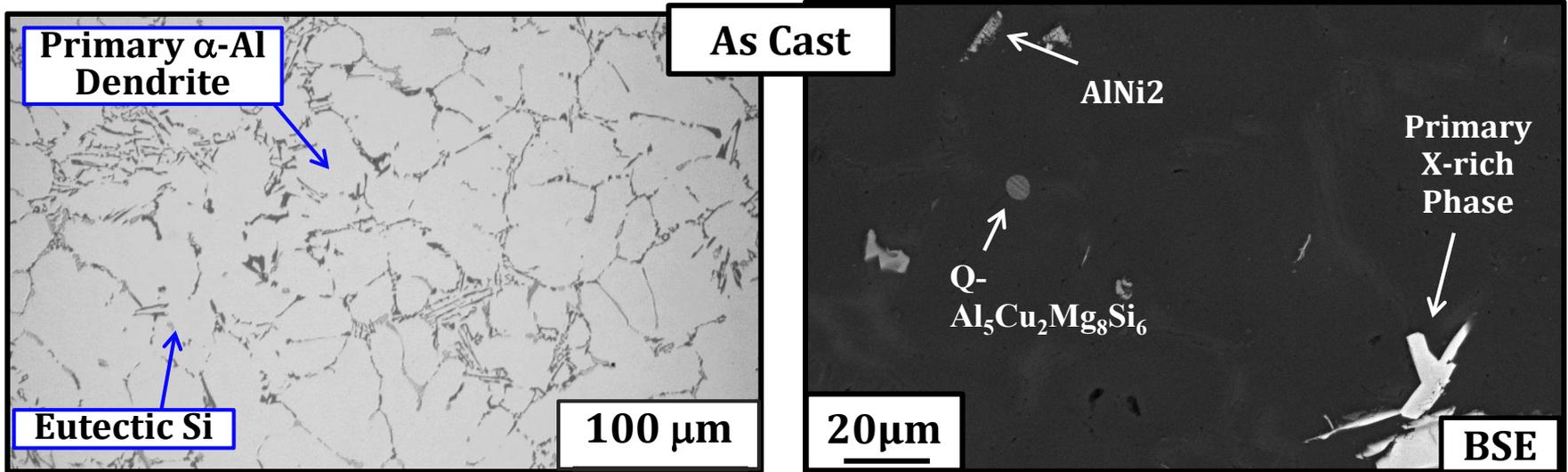
100 samples



(d) Torpedo samples for analysis.

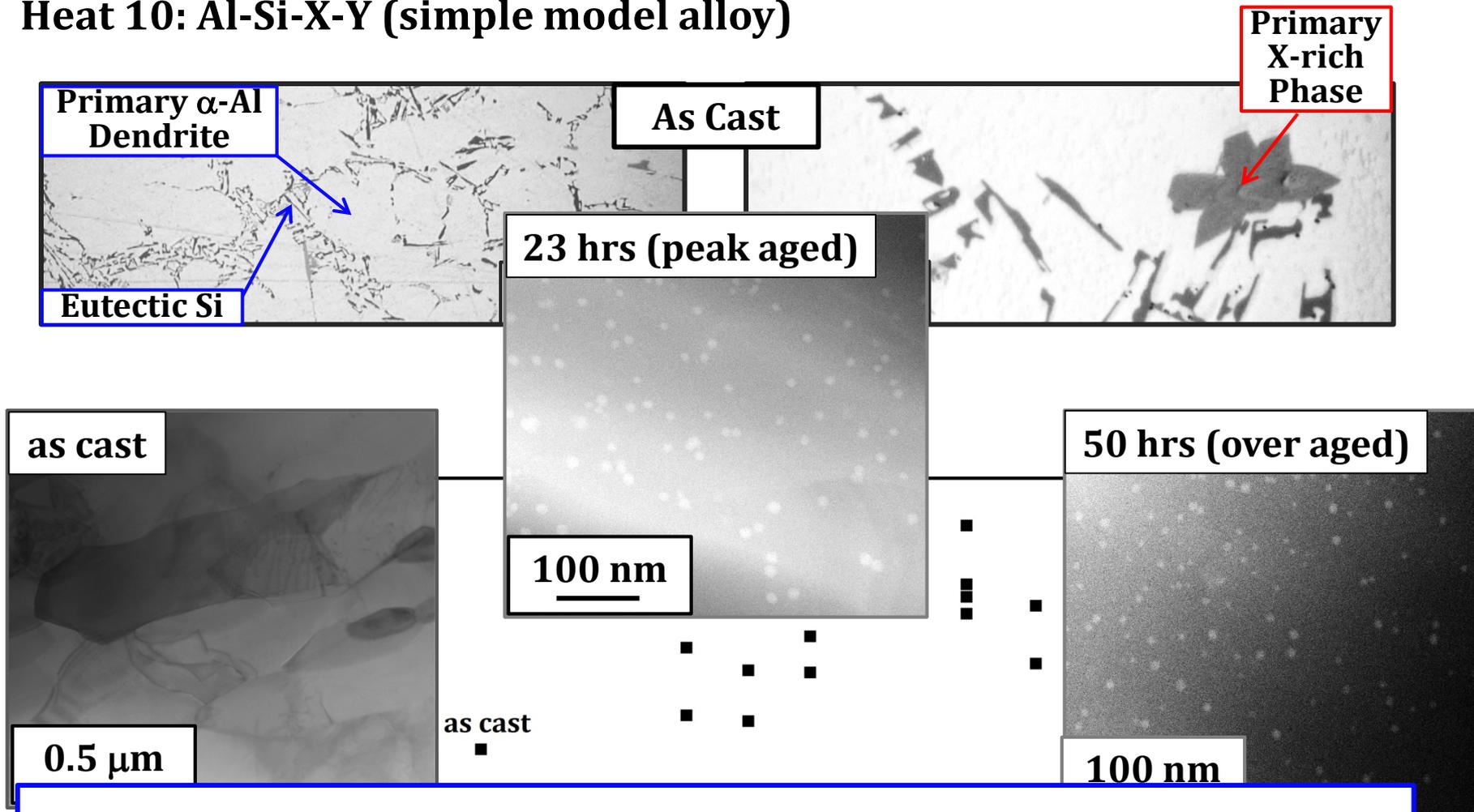
Step 1: Traditional Heat Treatment

Heat 7H: Al-Si-Cu-Mg-X-Y (AS7GU based)



Step 2 New Heat Treatment

Heat 10: Al-Si-X-Y (simple model alloy)



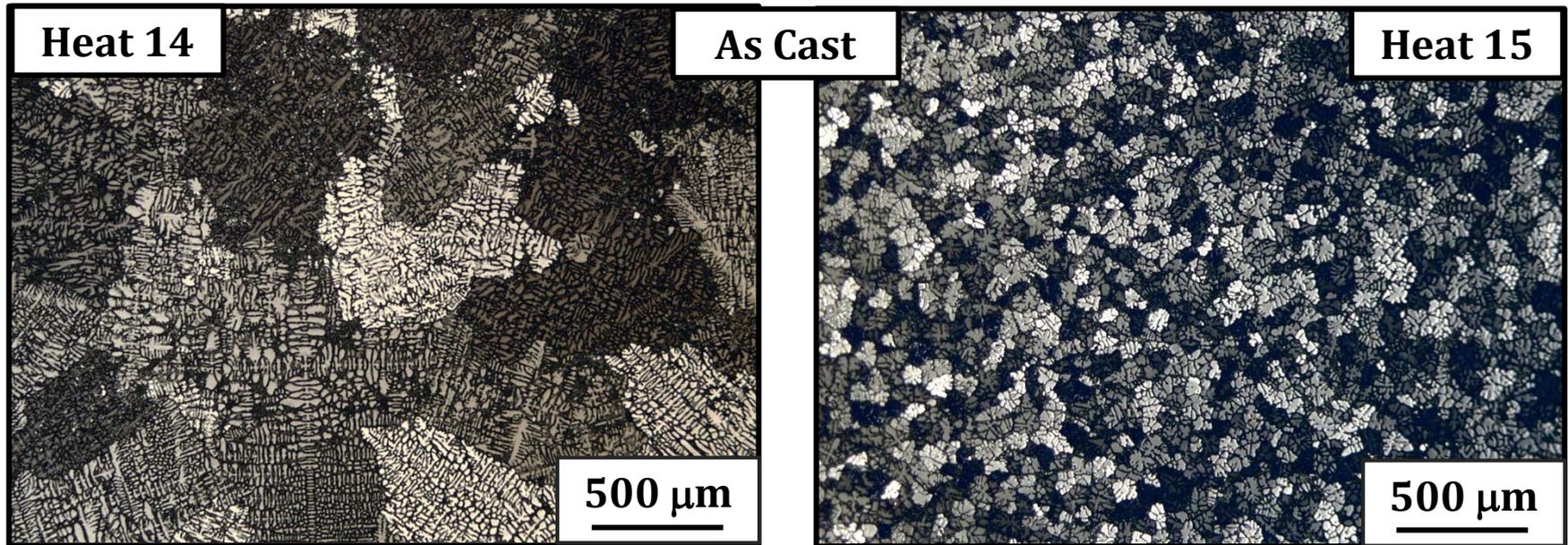
Aging generates nano-scale precipitates that \uparrow RT YS by ~ 20 MPa and are coarsening resistant at this temperature.

Step 3 Multi-Step Heat Treatment

H14: Al-Si-Cu-Mg

H15: Al-Si-Cu-Mg-X-Y

Electrolytic Etching: 5 mL HBF₄ (48%) + 200 mL water (Barker's) 20 V, 90 seconds. (polarized light)



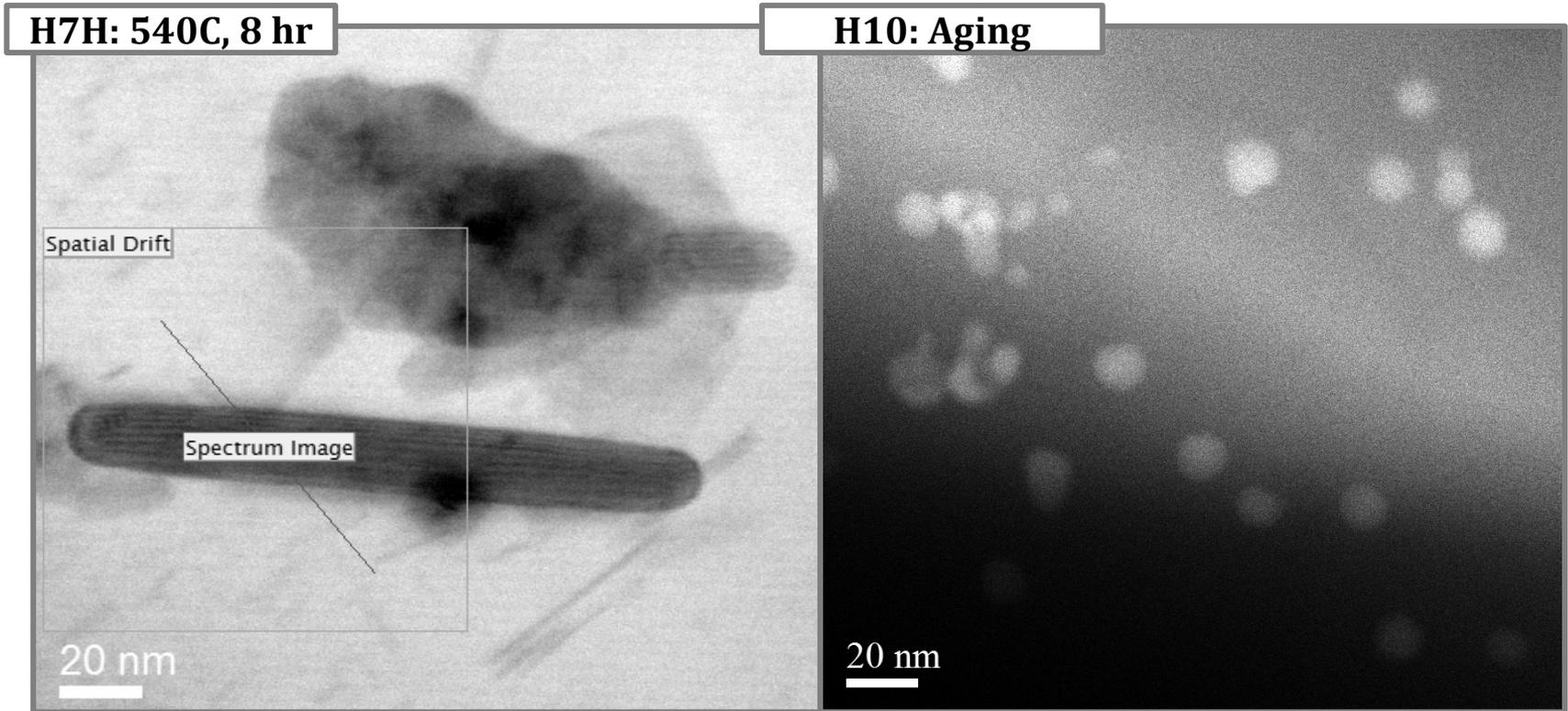
Grain Size: >500 μm

Grain Size: 70 μm

Significant grain refinement with X, Y additions !!

Step 3 New Heat Treatment

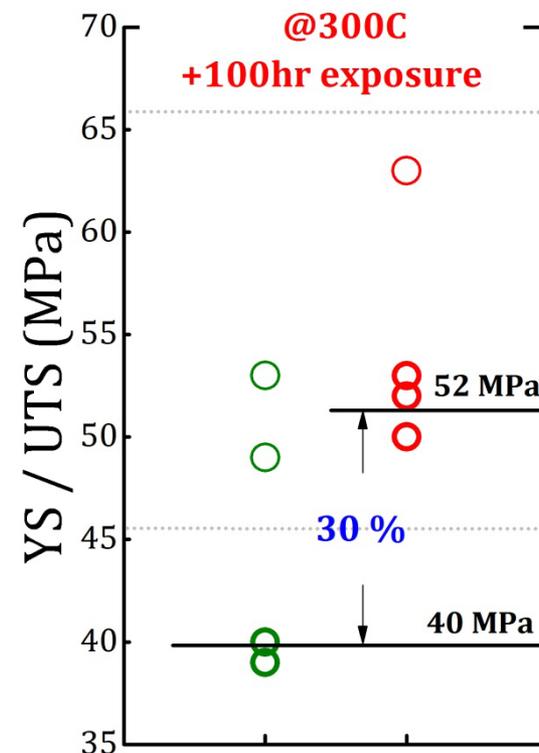
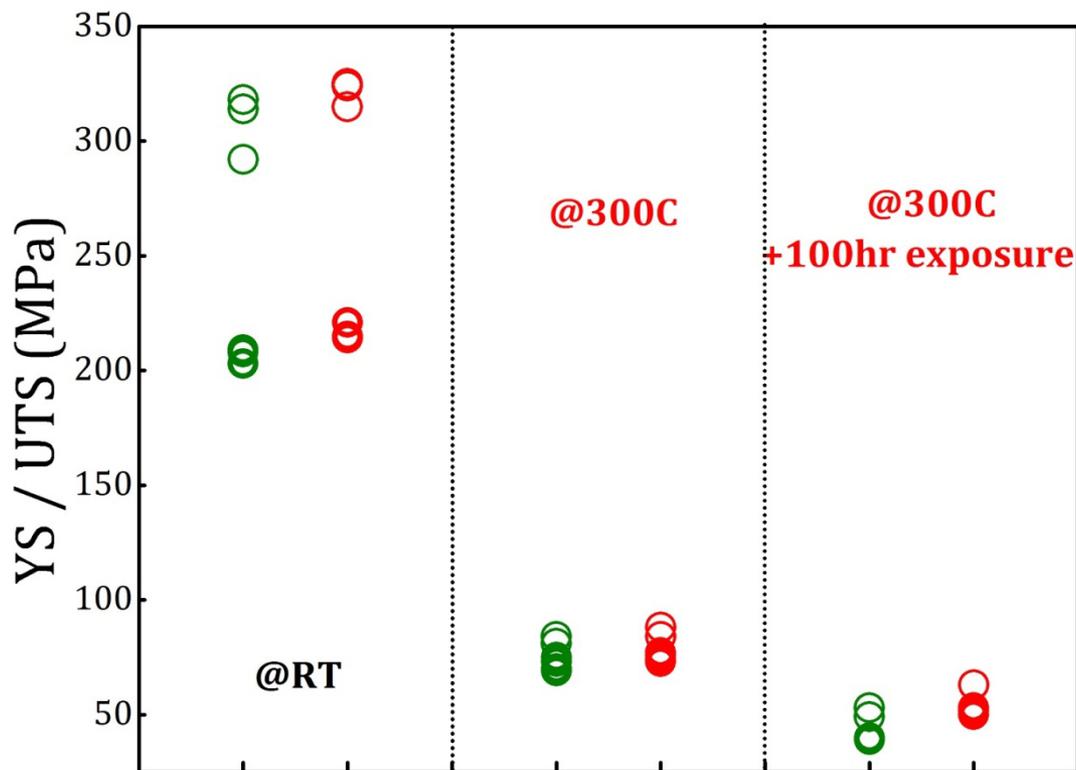
Apply the knowledge gained from Heat7H and Heat 10 on heat treatment to Heat 15 (Al-Si-Cu-Mg-X-Y, 319-based).



Result Yield Strength of Heat 14 & 15

H14: Al-Si-Cu-Mg (T7)

H15: Al-Si-Cu-Mg-X-Y (HT Aging + T7)



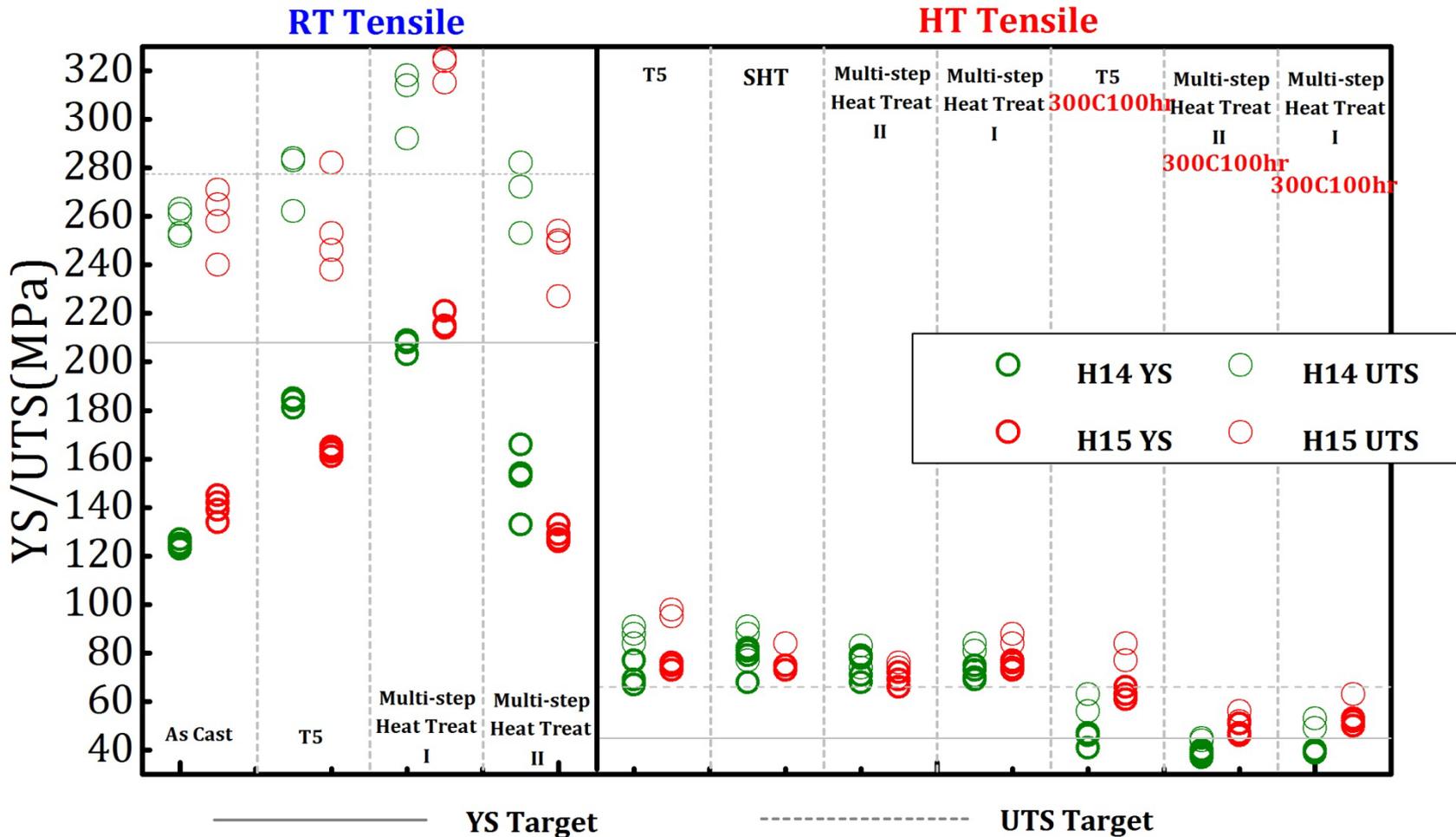
H15 exhibits superior YS @ 300 C than H14 !



Result Other Heat treatment of Heat 14 & 15

H14: Al-Si-Cu-Mg

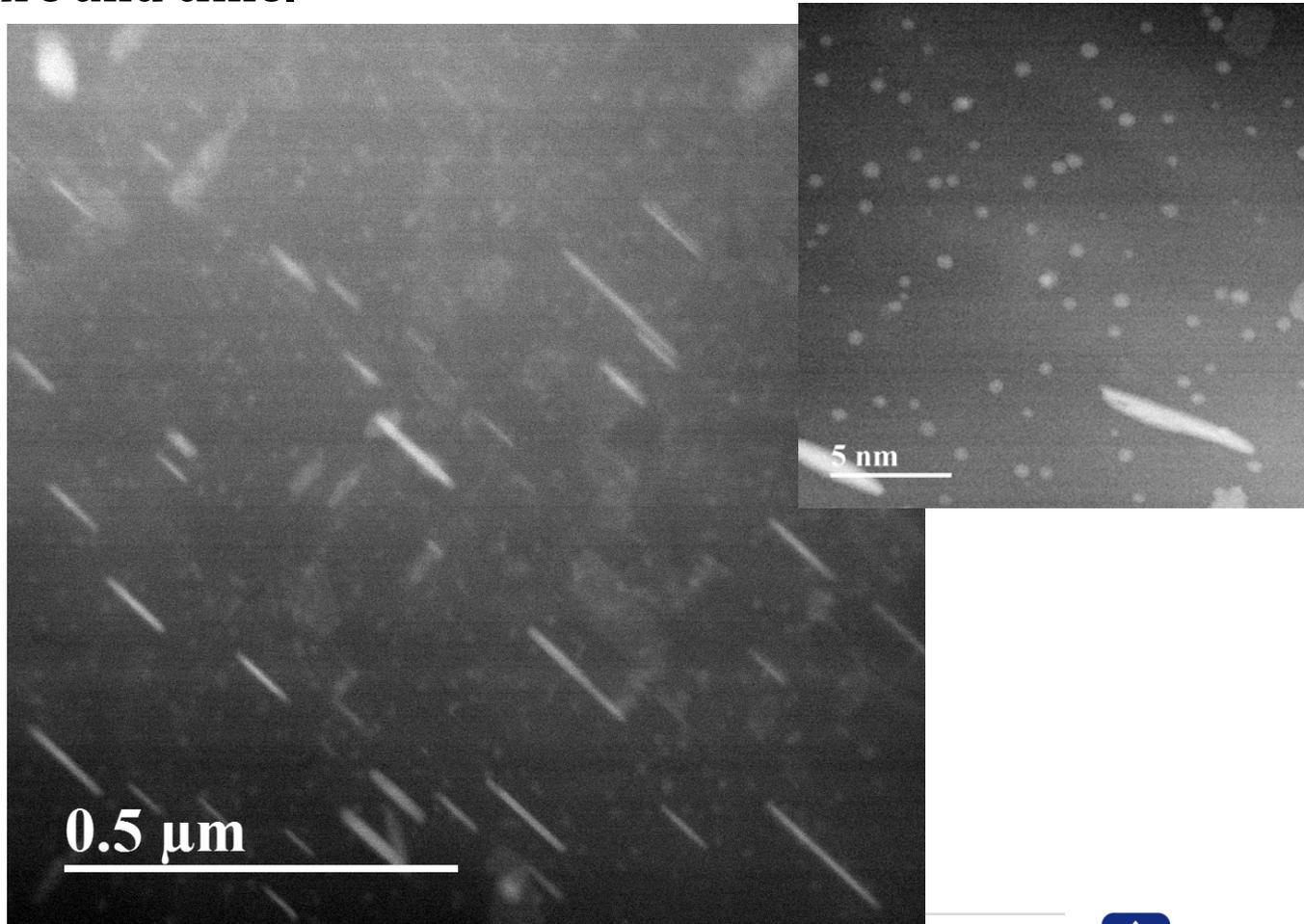
H15: Al-Si-Cu-Mg-X-Y



Result Heat Treatment Optimization

H15: Al-Si-Cu-Mg-X-Y

Duplex precipitation microstructure achieved by ↓ solution treatment temperature and time.



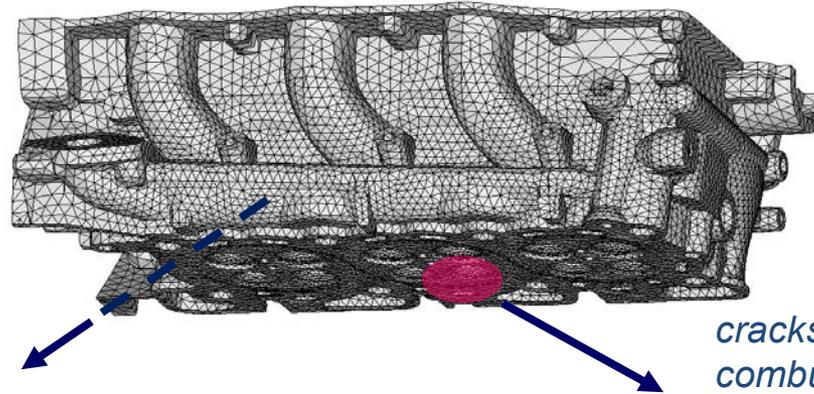
High-cycle Fatigue (HCF) vs. Low-cycle Fatigue (LCF)

HCF

cracks initiate internally
usually from water jacket
infinite life ($>10^7$ cycles)

elastic strains and stresses

property: **Fatigue Strength** (endurance limit)

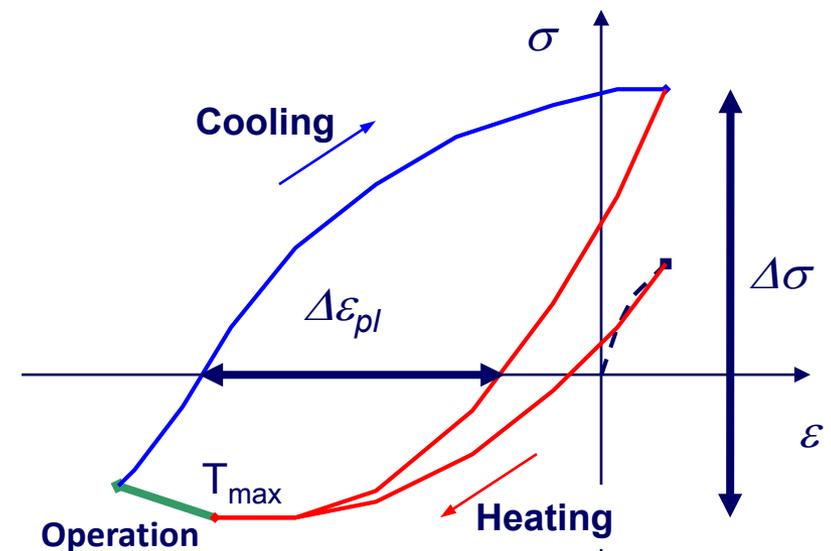
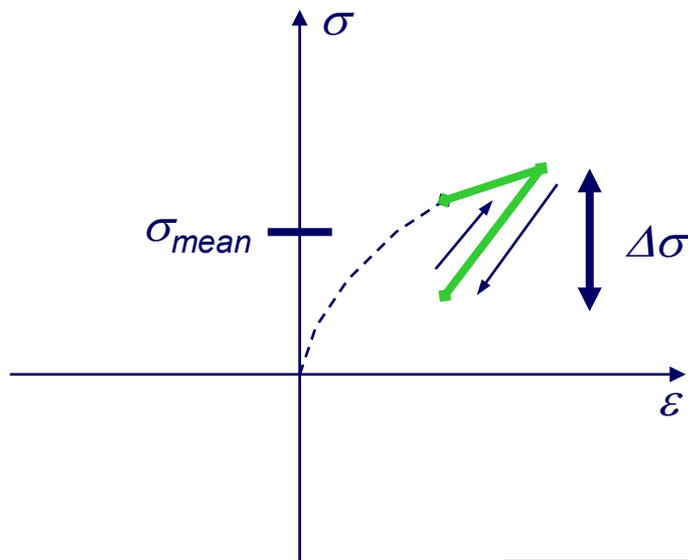


LCF/TMF

cracks usually from
combustion chamber
finite life (target is $\sim 10,000$)

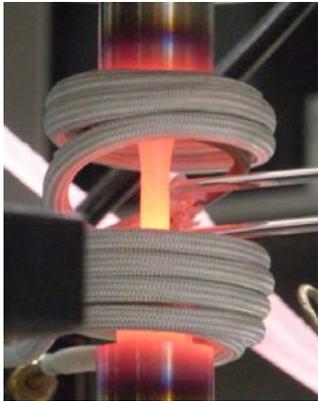
plastic strains

property: **Strain-Life curve**

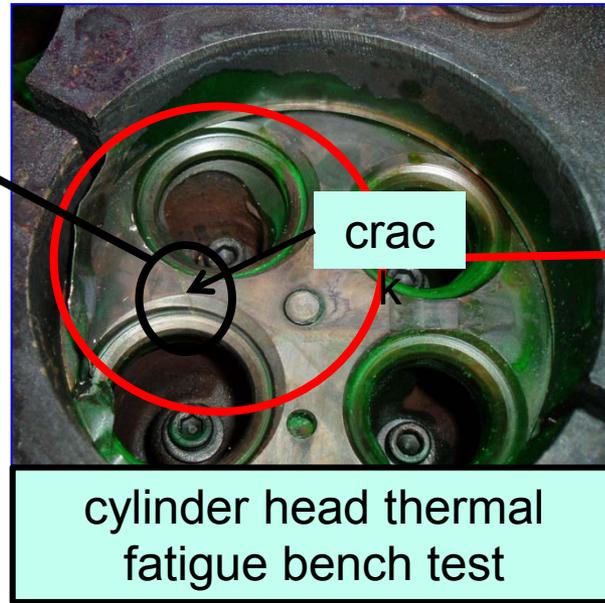
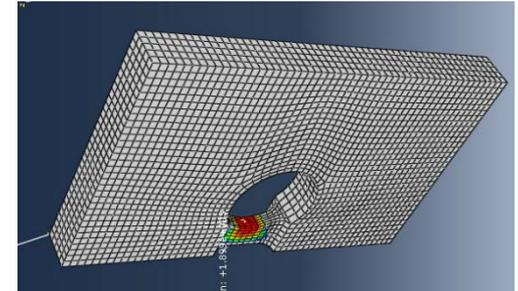


Testing: Thermomechanical vs. Thermal fatigue

TMF Material Test



TF Structural Test



- External strains and stresses (no thermal gradient)
- Essential for assessing intrinsic fatigue properties

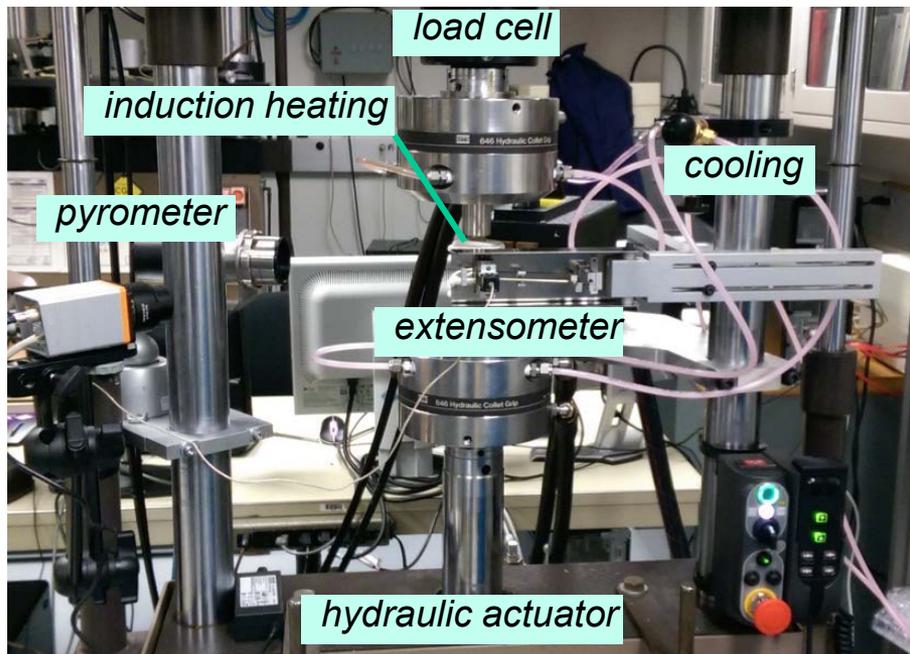
- Internal strains and stresses (due to thermal gradients)
- Ideal for comparing different materials (includes effects of other properties like stiffness, expansion, conductivity, etc.)

Testing: Thermomechanical vs. Thermal fatigue

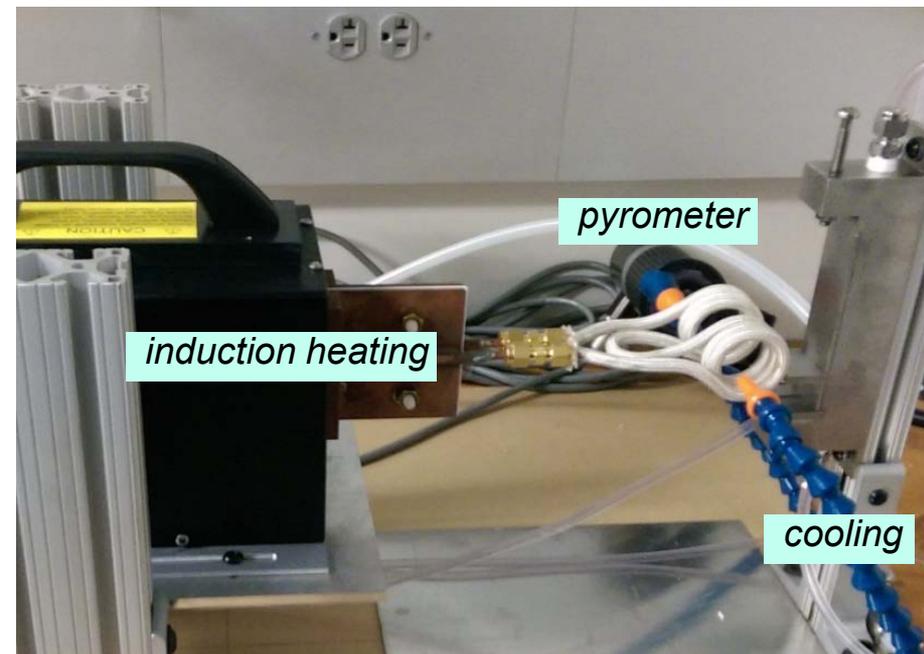
Customized testing systems at Ford Research & Innovation Center:

- Simulation of complex Thermal and Mechanical Fatigue loading
- Determination of properties under non-isothermal loading conditions (start-up / shut down)
- First in Industry (no other OEM has this capability)

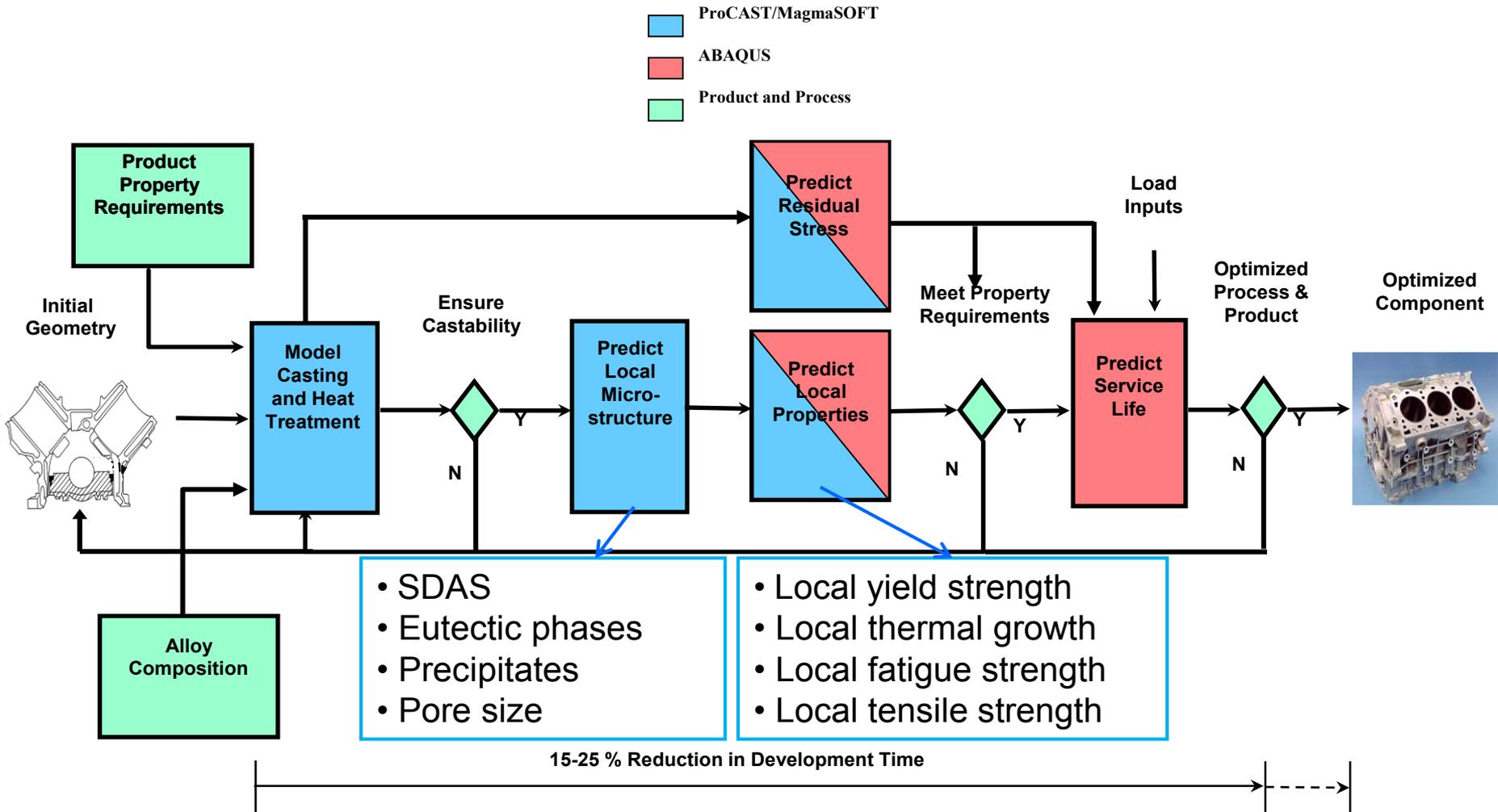
thermomechanical fatigue



thermal fatigue

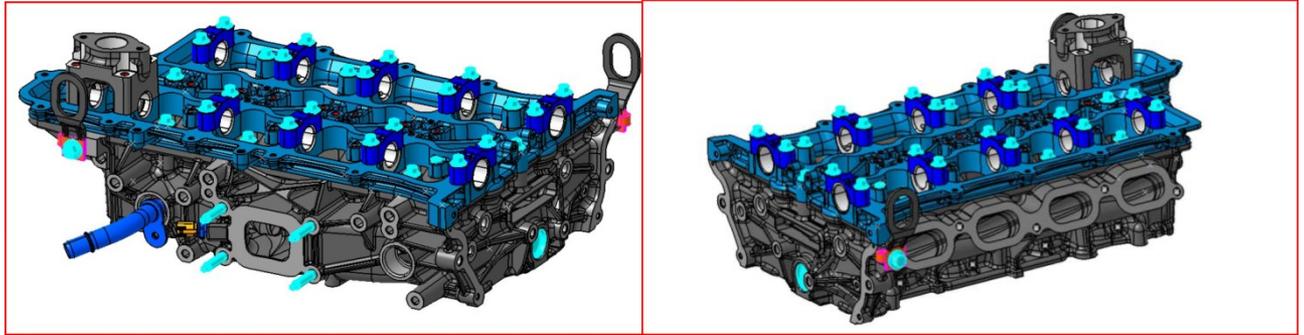


ICME Virtual Aluminum Castings



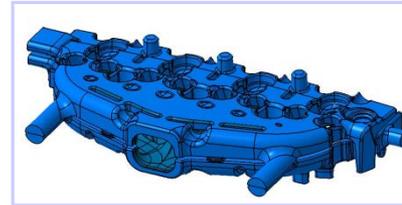
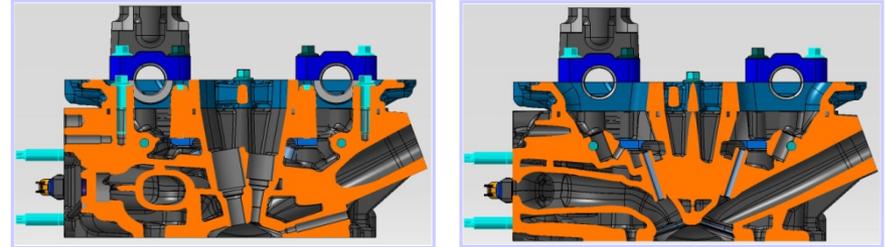
Demonstration on Ford GTDI Engine Program

Under DOE Contract
DE-EE0003332



Design Requirements

- 14 mm spark plug w/transverse fuel injector location
- Bosch and MM fuel injector (protect for both injectors)
- Two piece water jacket (cross / split cooling)
- Cross flow coolant path (lower jacket)
- Longitudinal coolant path (upper jacket)
- 8.5 mm chamber wall w/ additional IEM / chamber support
- AS7GU material
- 10° spark plug angle / 6° injector angle
- 31.8 mm (X2) intake valve diameter at a 18° angle
- 28.5 mm (X2) exhaust valve diameter at a 18.4° angle
- Outboard intake and exhaust HLA



- Based on Ford's large I4 Architecture
- Complete new Cylinder Head Design
- New Feature Content



Accomplishments

- Identified several key alloying elements that could potentially form heat resistant precipitates and enhance the high temperature mechanical properties.
- Designed novel multi-stage heat treatment procedure that generates complex nano-scale precipitation microstructure.
- Optimized alloy composition and heat treatment that could meet the room temperature and high temperature strength criteria.
- Thermo-mechanical fatigue testing frame set up has been completed and is ready for testing candidate alloys.



Accomplishments

- Customer designed a thermal fatigue rig and sample geometry compare candidate alloys under complex thermal and mechanical fatigue loading condition similar to engine working condition.
- Casting process simulation has completed on the selected engine component
- Thermop-hysical properties are being characterized for the new alloys
- Initial cost model has been accessed and the cost associated with the new heat treatment is being incorporated



Future Work

- Complete the design and optimization of the new alloys and the associated casting and heat treatment processes
- Complete the quantification and modeling of phase transformation kinetics during casting, solution treatment and aging treatment
- Complete the quantification and modeling of mechanical properties including yield strength, fatigue strength and thermo-mechanical fatigue properties
- Validate and identify the gaps in microstructural and property models
- Refine the cost model to quantify the cost of new alloys compared with A319 and A356 alloys.

