

Combustion Targets for Low Emissions and High Efficiency

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September, 2005



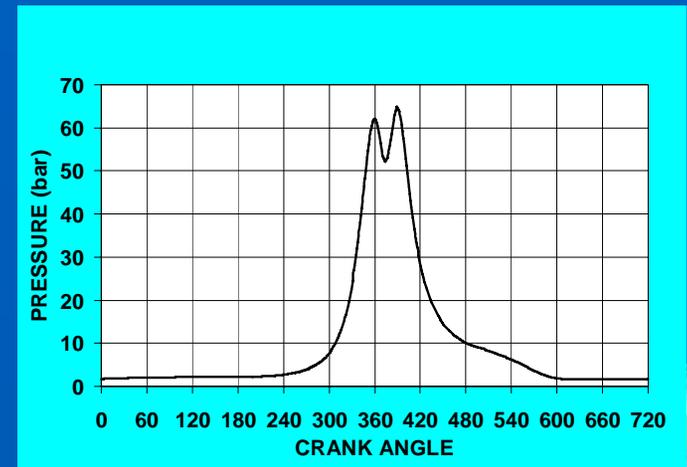
Three Combustion Modes

- Flame Propagation (SI Gasoline)
 - ◆ Stoichiometric Combustion
 - ◆ Thin Reaction Zone
 - ◆ High Temperature and High NO_x
- Diffusion Burning (Conventional Diesel)
 - ◆ Stoichiometric Reaction Zone
 - ◆ Thin Reaction Zone
 - ◆ High Temperature and High NO_x
 - ◆ Rich Zones at High T Leading to Soot Formation
- Homogeneous Reaction (HCCI)
 - ◆ Dilute Mixtures
 - ◆ Low Temperature Reactions and Low NO_x
 - ◆ Homogeneous Mixture at Low Temperature



Background

- Engine Combustion Technologies are Apparently Converging to the same General Characteristics
 - ◆ Delayed Ignition and Rapid Burn Rate
- Engine Technologies are also Converging
 - ◆ Highly Boosted
 - ◆ High BMEP
 - ◆ High EGR



New Combustion Modes

- HEDGE, HCCI, CAI, PCCI, LTC, PCI, and CSI are some of the Acronyms used to Describe the Recent Developments for Modified Fuel Reaction Approaches
 - ▣ HEDGE - High Efficiency Dilute Gasoline Engine
 - ▣ HCCI - Homogeneous Charge Compression Ignition
 - ▣ CAI - Controlled Auto Ignition
 - ▣ PCCI - Premixed Charge Compression Ignition
 - ▣ LTC - Low Temperature Combustion
 - ▣ PCI - Premixed Compression Ignition
 - ▣ CSI - Compression and Spark Ignition



HEDGE, HCCI, CAI, PCCI, LTC, PCI, and CSI

- Common Factors include:
 - ◆ Thick Flames
 - ◆ Part or all of the Fuel is Premixed
 - ◆ All Use EGR
 - ◆ All have Lower NO_x
 - ◆ All have Higher HC and CO
- Differences Include:
 - ◆ Degree of Premixing
 - ◆ PM Emissions
 - ◆ Overall Equivalence Ratio
 - ◆ Initiation of Reaction
 - ◆ Purpose/Application
 - Low Emissions
 - Exhaust Gas Composition and Temperature Control



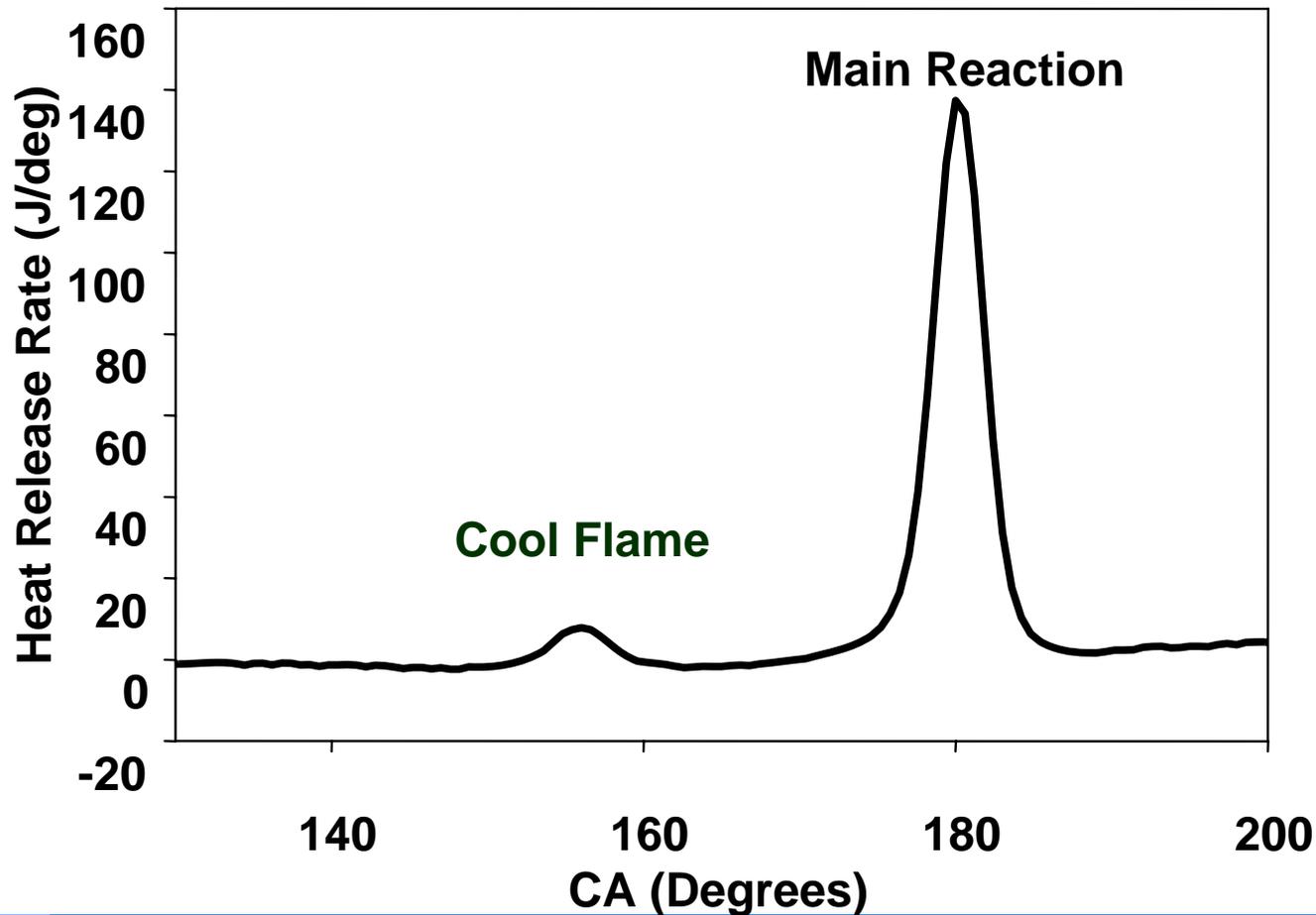
Best Combustion Phasing

- Theoretical vs Practical

- Thermodynamically Ideal Cycles Produce Highest Efficiency with Instantaneous Heat Release at TDC
- Practical Limitations Include
 - ◆ Noise due to Rapid Rates of Heat Release
 - ◆ Increases in Friction due to Higher Bearing Loads and Small $dV/d\theta$ Effects
 - ◆ Peak Firing Pressure Limits
 - ◆ Pressure Oscillations (maybe Knock)



Typical Advanced Heat Release Rate



Approach

- Use Cycle Simulation to Determine the Effects of Changing the Heat Release Rate Characteristics on the Emissions and the Efficiency
 - ◆ Mainly Concerned with NO_x and BTE



HEDGE Performance Predictions Tools

- Alamo Engine (A_E)
 - ◆ Phenomenological, Zero Dimensional Models
 - ◆ Gas Exchange
 - ▣ Steady State Emptying & Filling (Checks With Steady State 1D Flow Code)
 - ◆ TC
 - ▣ Energy and Flow Balance for Selected Efficiencies, Wastegating (Vs Engine Speed)
 - ◆ Combustion
 - ▣ Watson and Wiebe
 - ◆ Friction
 - ▣ Chenn-flynn
 - ◆ Aftertreatment
 - ▣ Fixed Converter Efficiencies



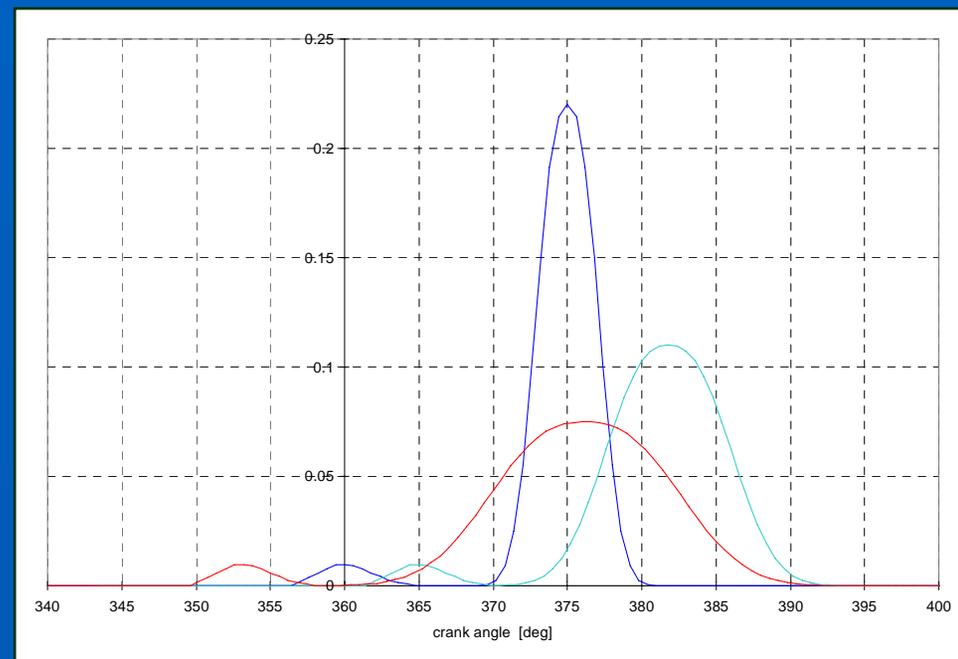
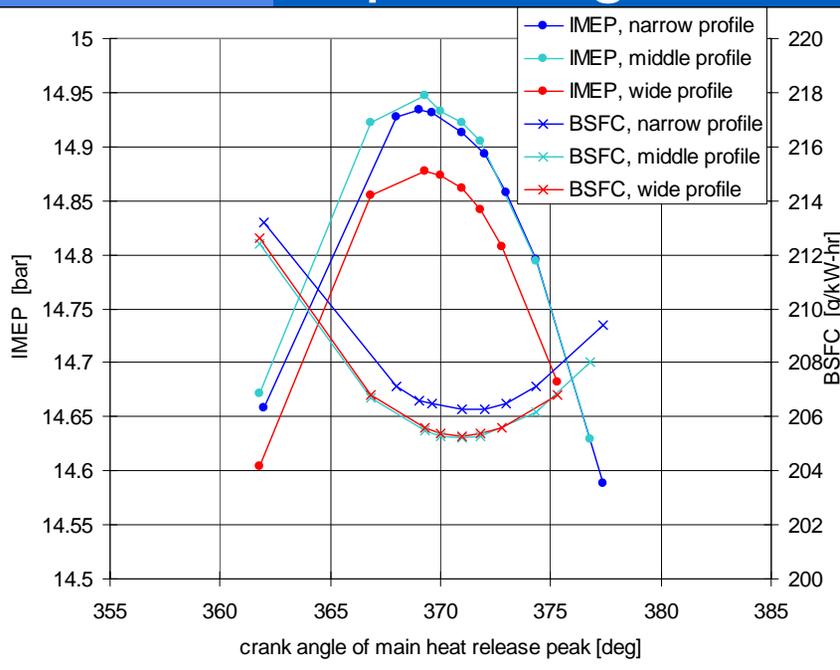
Assumption for All Calculations

- Engine Configuration
 - ◆ 130X160 mm BoreXStroke
 - ◆ 16:1 CR
 - ◆ Turbocharged
- Engine Conditions
 - ◆ 1800 rpm
 - ◆ A/F 24:1
 - ◆ 40% EGR
 - ◆ 240 kPa MAP
- Only Changes, Shape and Timing of the HRR Diagrams



Details on Shape and Timing Effect

- Peak Efficiency Occurs in All Cases as 12° ATDC
- Rapid to Slow Heat Release (Duration 10 to 30°) Results in 0.5% Change in BSFC
- Corresponding IMEP Drop of 0.5%



Future Diesel Engines



Areas of Greatest Potential

- Fuel Management
 - ◆ High Pressure Injection Essential
 - ◆ Injection Rate Control Essential
 - ◆ Air Utilization Essential
 - ◆ Liquid Fuel Wall Interactions must be Avoided
- Gas Management
 - ◆ High Density Essential
 - ◆ High EGR Levels Essential
 - Outcome is High Boost Pressure
 - ◆ Uniform EGR Distribution Essential
 - ◆ Intake Cooling is Desirable
 - ◆ High Efficiency Turbocharger Systems Essential
 - ◆ In-Cylinder Flow Management Essential
- Combustion Chambers
 - ◆ Matched to Nozzle Spray Capabilities
 - ◆ Design for Maximum Mixing Rates
 - ◆ Premixed Combustion Considerations
 - Surface-to-Volume Ratio Minimized
 - Quench Volume Minimized



Premise

- Lowest Possible Emissions and Highest Efficiency in Diesel Engines Achieved Using:
 - ◆ Ultra High Injection Pressure and Small Holes
 - ◆ Massive EGR
 - ◆ Ultra High Boost
 - ◆ Well Designed Pistons and Intake



High Injection Pressure and Small Holes

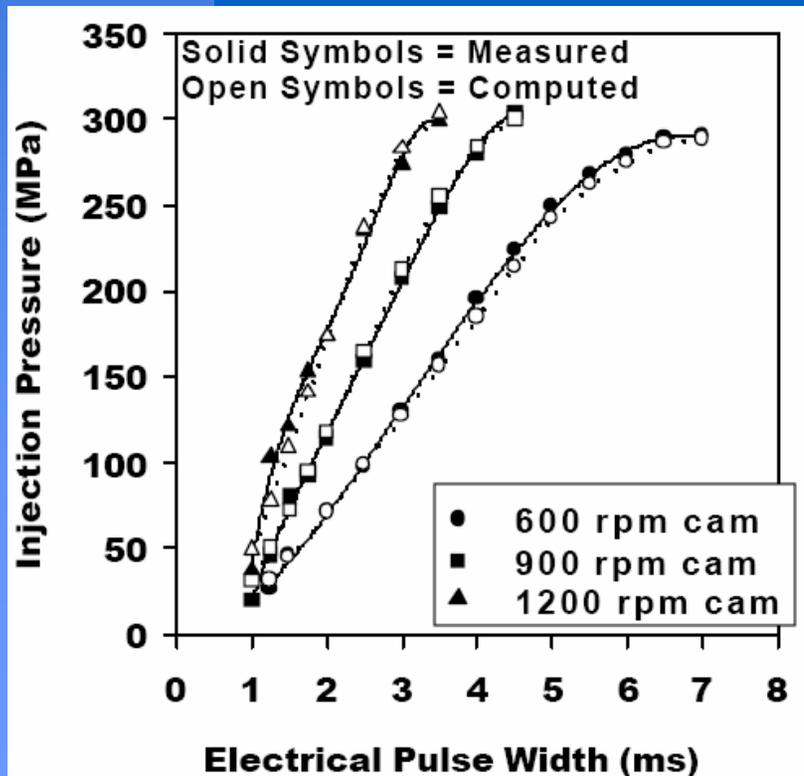


Fuel Injection - High Pressure

SwRI Results SAE 2002-01-0494

High Pressure Electronic Unit Injector Operating on a Fixed Cam at Constant Speeds

- Single Hole Nozzles 0.086 to 0.18 mm Dia
- Peak Injection Pressures from 254 to 283 MPa
- Higher Mixing Rates and Smaller Drops

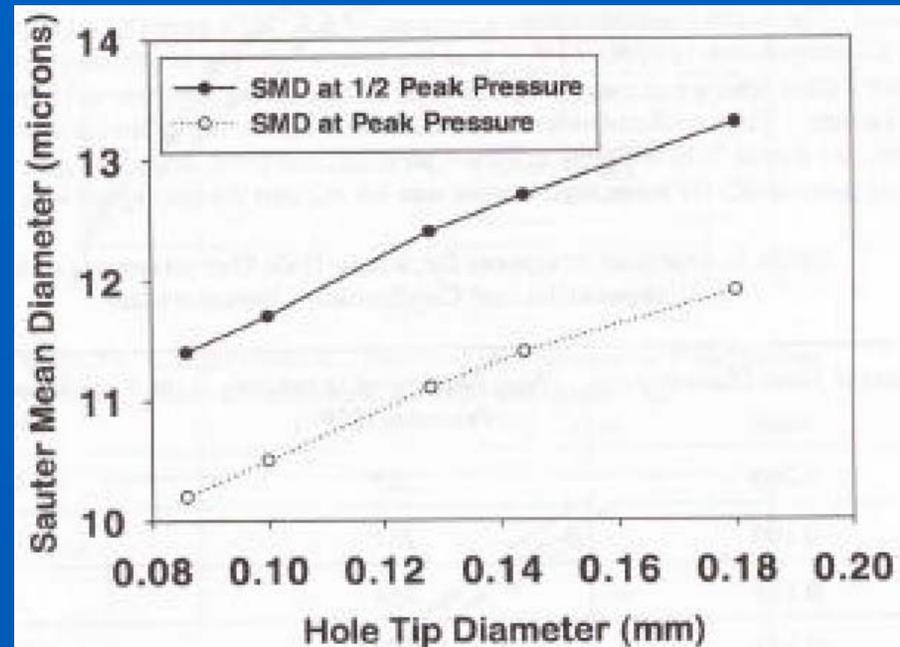
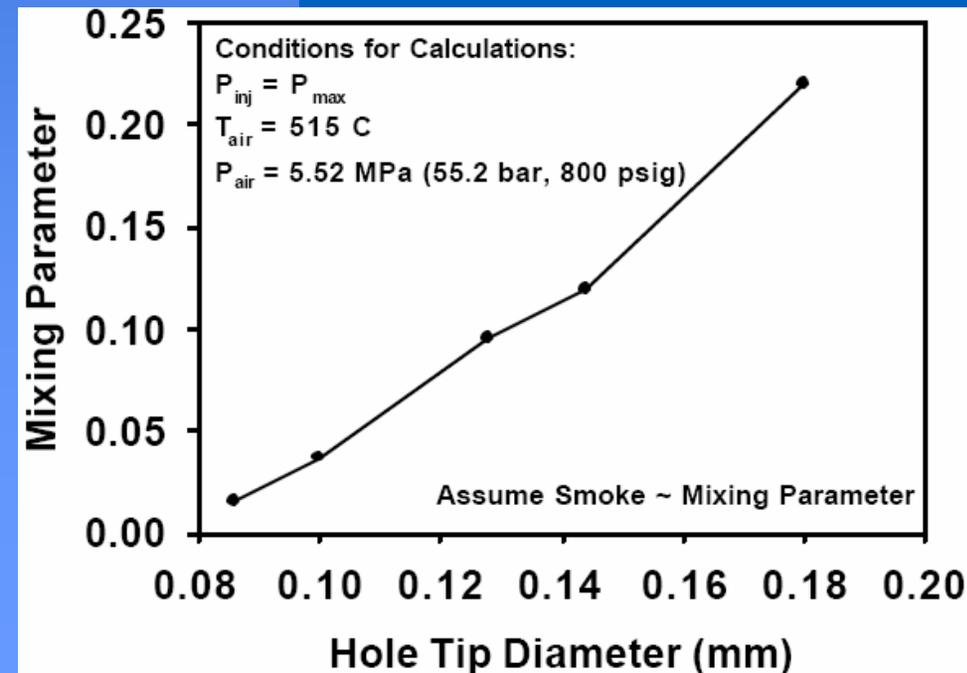


Injection Hole Diameter (mm)	Peak Injection Pressure (MPa)	1/2 Peak Injection Pressure (MPa)
0.086	283	142
0.100	281	141
0.128	266	133
0.144	267	134
0.18	254	127

Fuel Injection - High Pressure

1. Mixing Rates Quantified in Terms of SwRI Defined Mixing Parameter
2. Mixing Parameter Defines the Mass of Fuel at Phi Greater Than 1.0 for than 0.6 ms
3. Rich Regions Mean More Soot

- Mixing Parameter and Drop Size both Decrease with Smaller Holes
- P_{inj} Increases with Smaller Holes



Fuel Injection - High Pressure



0.144 mm

0.128 mm

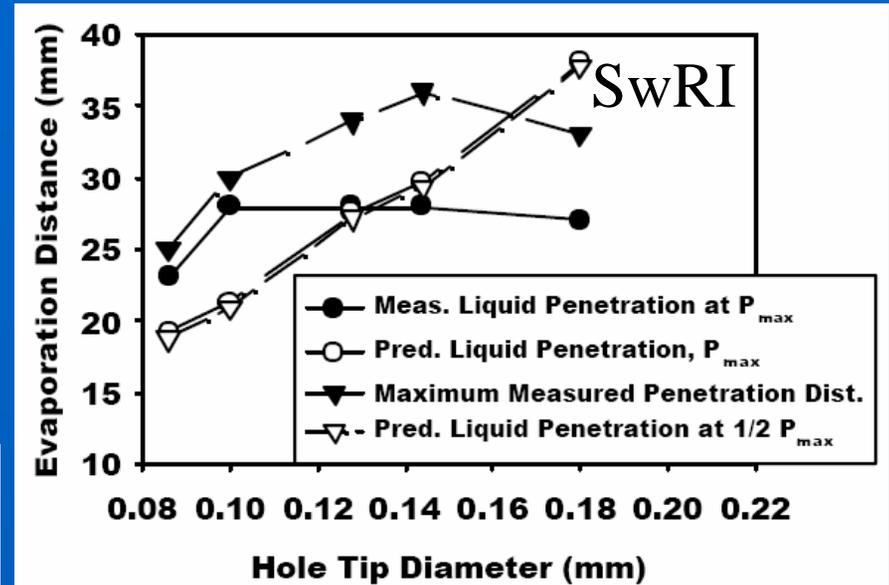
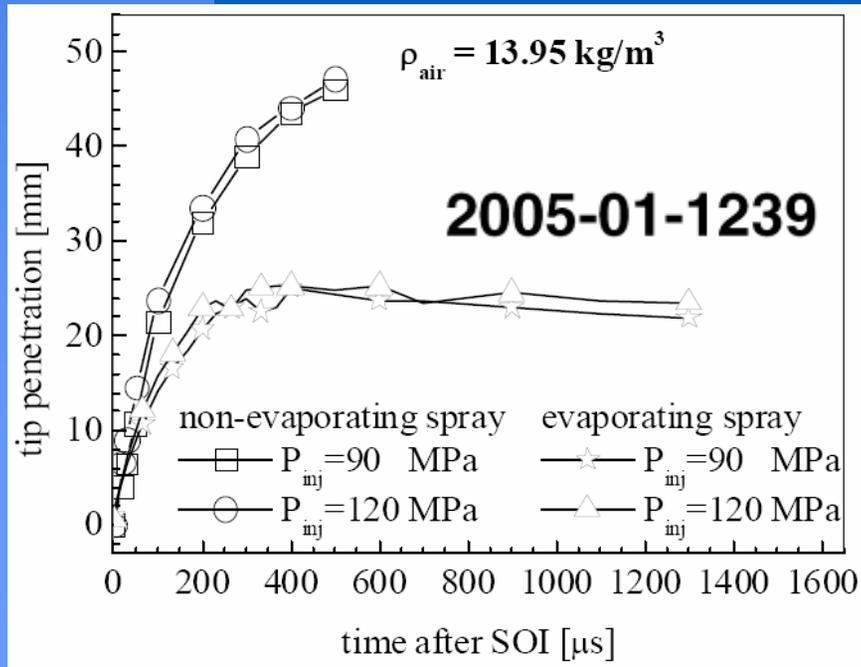
0.086 mm

- Small Holes Produce High Pressure, Small SMD, High Mixing Rates and Low Soot Formation Rates



Fuel Injection - High Pressure

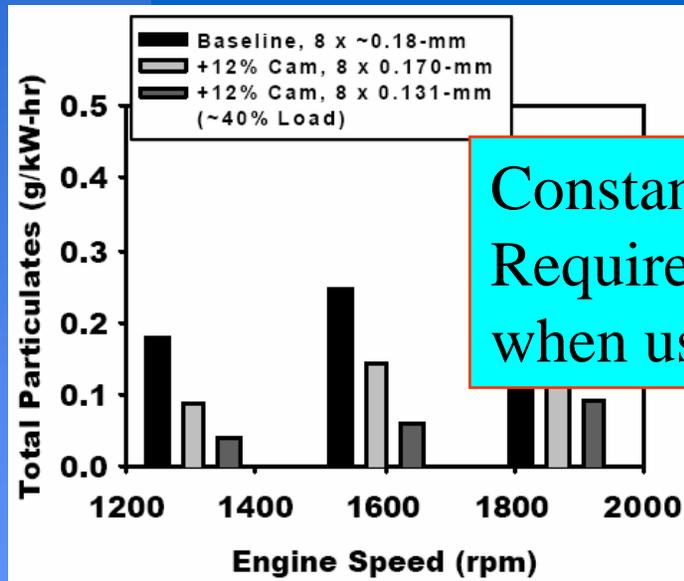
- High Pressure does not Affect the Jet Penetration Rate in either Evaporating or Non-Evaporating Sprays



- Small Holes do Affect the Evaporation Rate and the Liquid Length in Evaporating Sprays

Fuel Injection - High Pressure

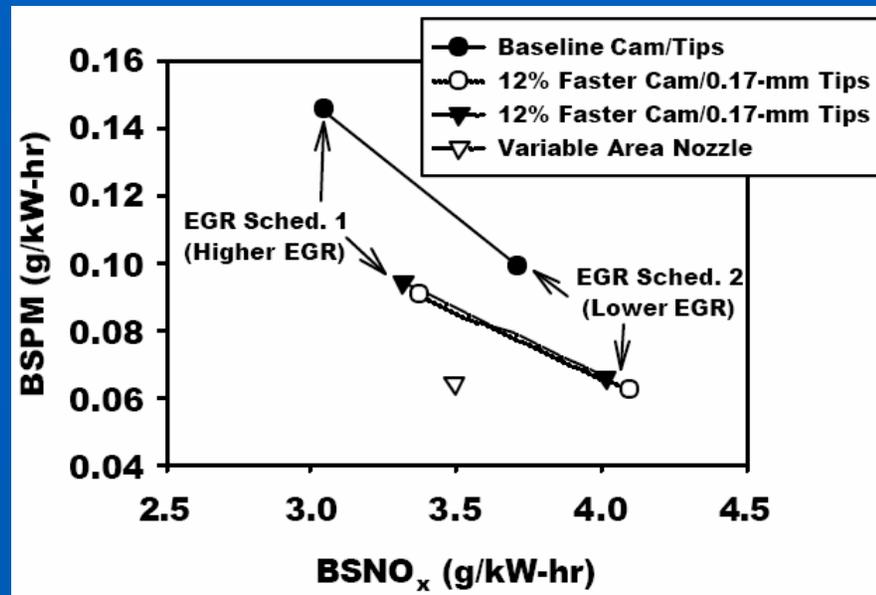
- Variable Area Nozzle (0.17 to 0.131 mm) Gives a Significant Improvement



Constant Injection Duration Requires Higher Pressure when using Small Holes

- 12% Cam and 0.17 mm Nozzle Give same Duration as Baseline
- 12% Cam and 0.131 mm Nozzle Give Higher Rates

used for Light Loads
ed for High Loads
Liquid Length, and
e are Important

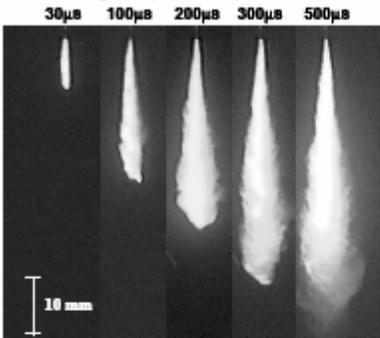


High Boost

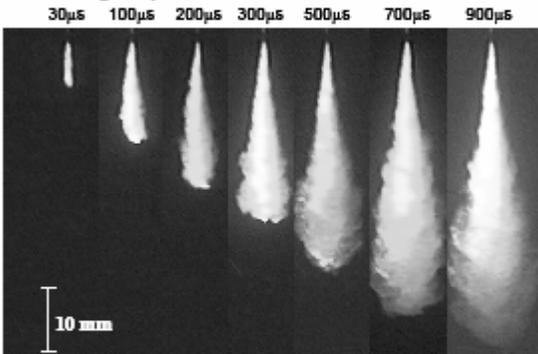


Fuel Injection - High Density

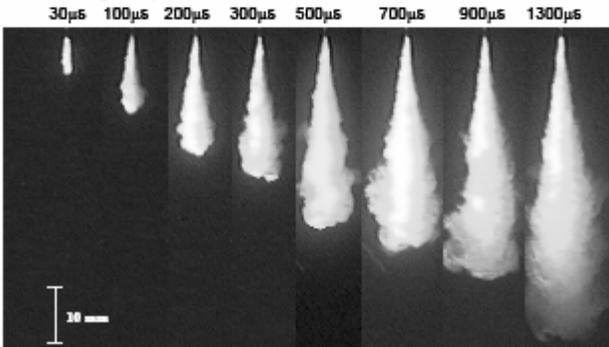
Vessel gas pressure = 1.2 MPa



Vessel gas pressure = 3.0 MPa



Vessel gas pressure = 5.0 MPa



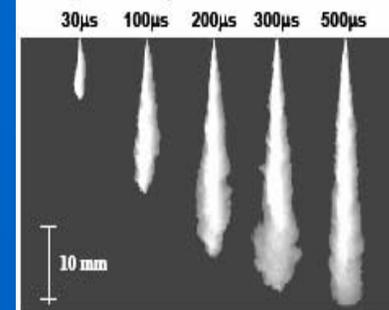
- Liquid Length Affected most Strongly by Hole Size and the Ambient Density

- ◆ Smaller Holes
- ◆ Higher Density

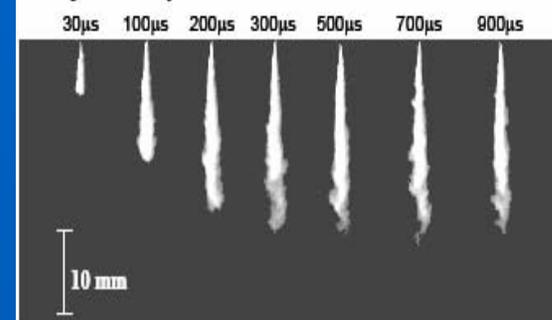
- Gas Jet Always Interacts with Combustion Chamber

- ◆ Wall Jet Mixing Important
- ◆ Air Motion

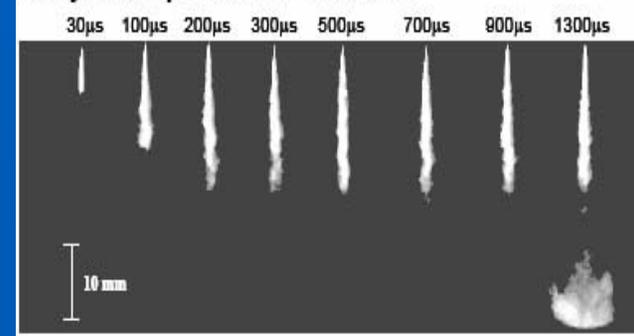
In-cylinder pressure = 1.2 MPa



In-cylinder pressure = 3.0 MPa



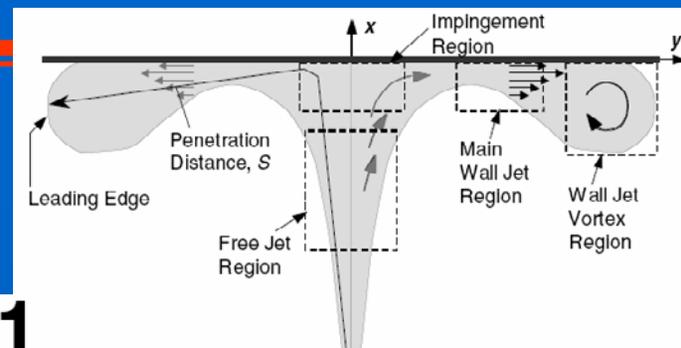
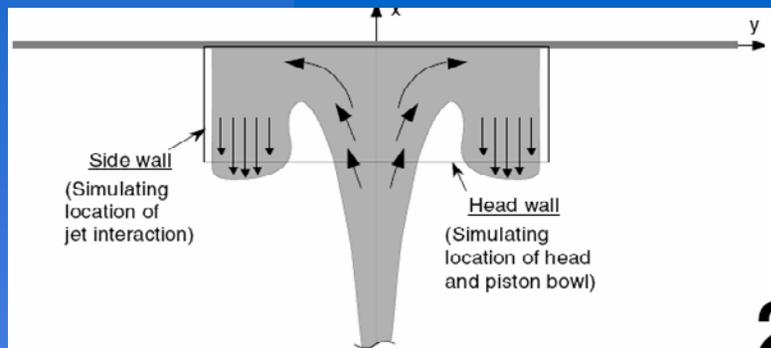
In-cylinder pressure = 5.0 MPa



Combustion Chamber Design



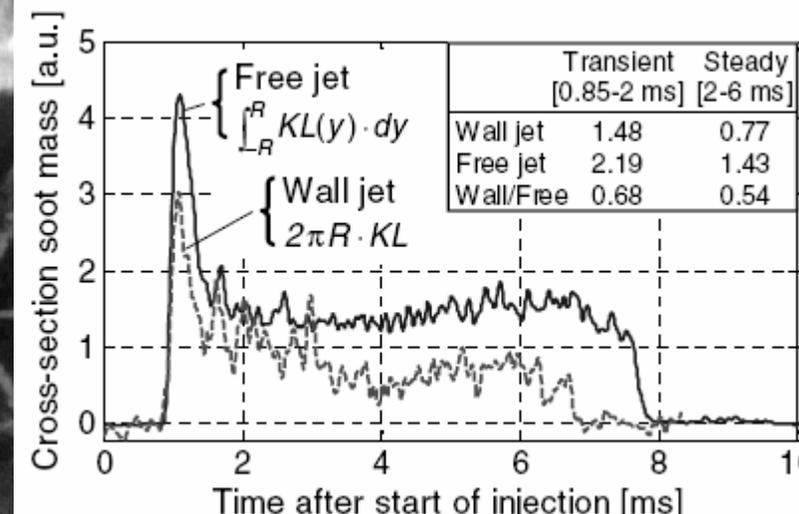
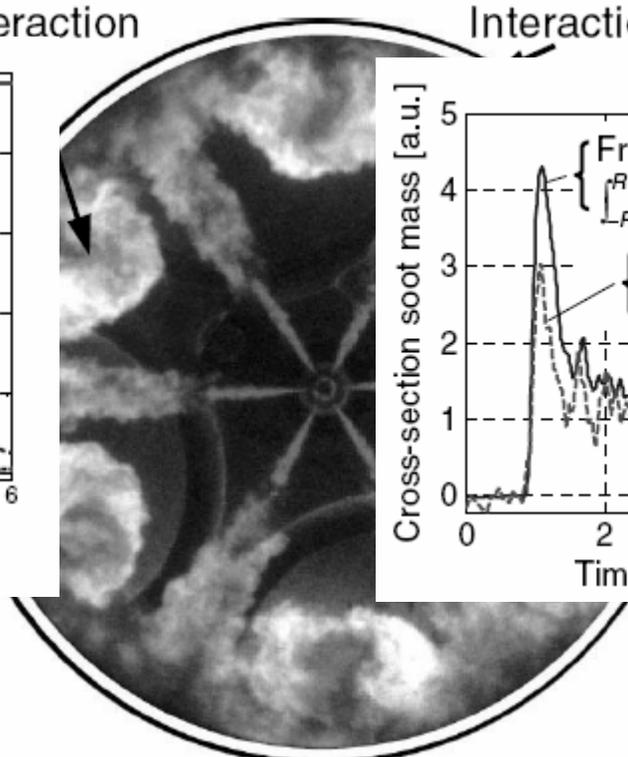
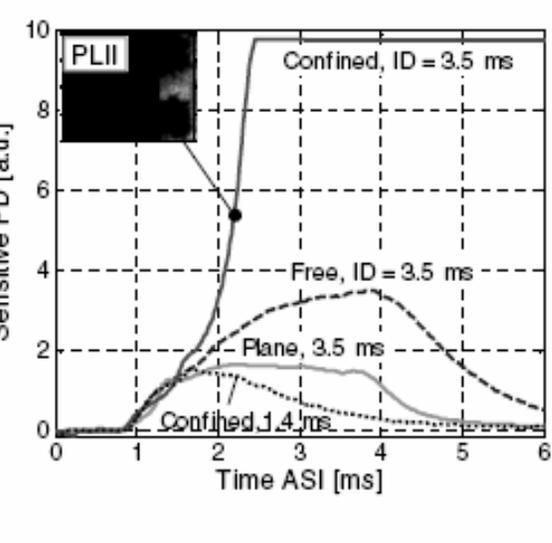
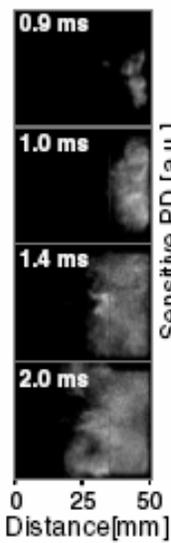
Fuel Injection - Jet-Wall Interaction



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Jet-Jet
Interaction

Jet-Wall
Interaction



Combustion Chamber Design



Man D20



Cat C9



Cat C15



Volvo D12



ISX



DDC S60

- Spray Wall Interactions are Unavoidable
 - ◆ Avoid Liquid Impingement
 - ◆ Take Advantage of Jet Break-up and Wall Jet Opportunities
- Pilot and Post Injections Change the Bowl Shape and Spray Angle Requirements
 - ◆ Cat uses Pilot at Almost all Conditions
 - Spray Angle Narrower



Fuel Injection Wall-Wetting Issues



Background Is Liquid Impingement and Oil Dilution a Concern?

- Concerned with both Early Pre- Injection for Emissions and Noise Control and Late Post - Injection Strategies for DPF and LNT Regeneration
 - ◆ Fuel Jet Penetration Increases during Late Injection Due to the Lower Density
 - ▣ Decreasing Pressure and High Temperature
 - ◆ Liquid Fuel can Impinge on the Wall and Some can Adhere and Enter the Lubricant
- Approach
 - ▣ Developed an empirical based model for estimation of the relative quantity of injected fuel that becomes associated with, or adheres, to the combustion chamber walls



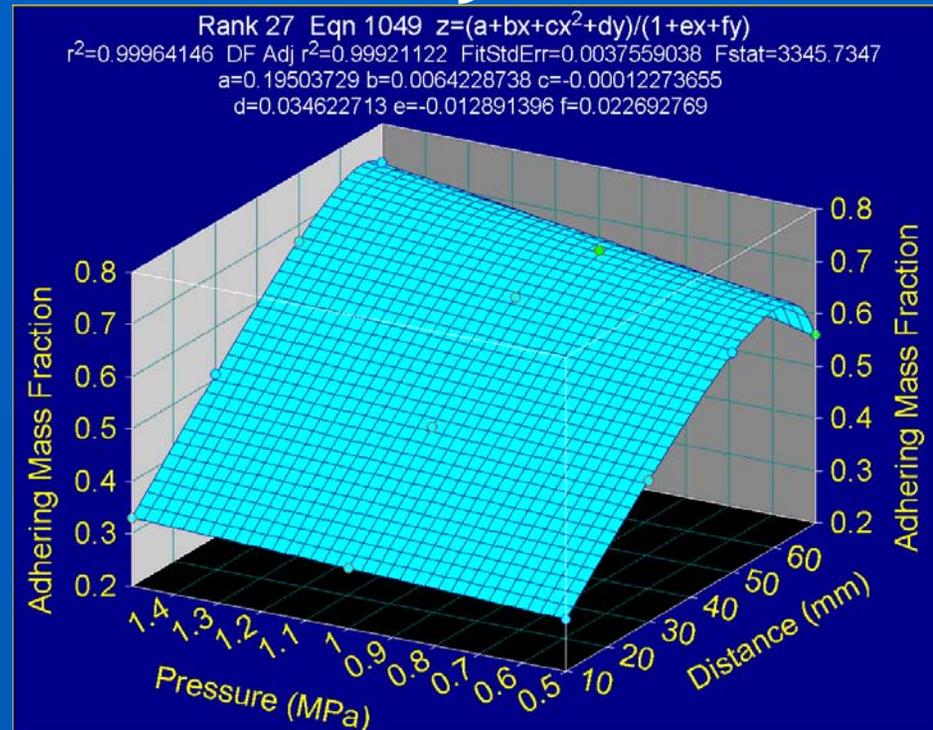
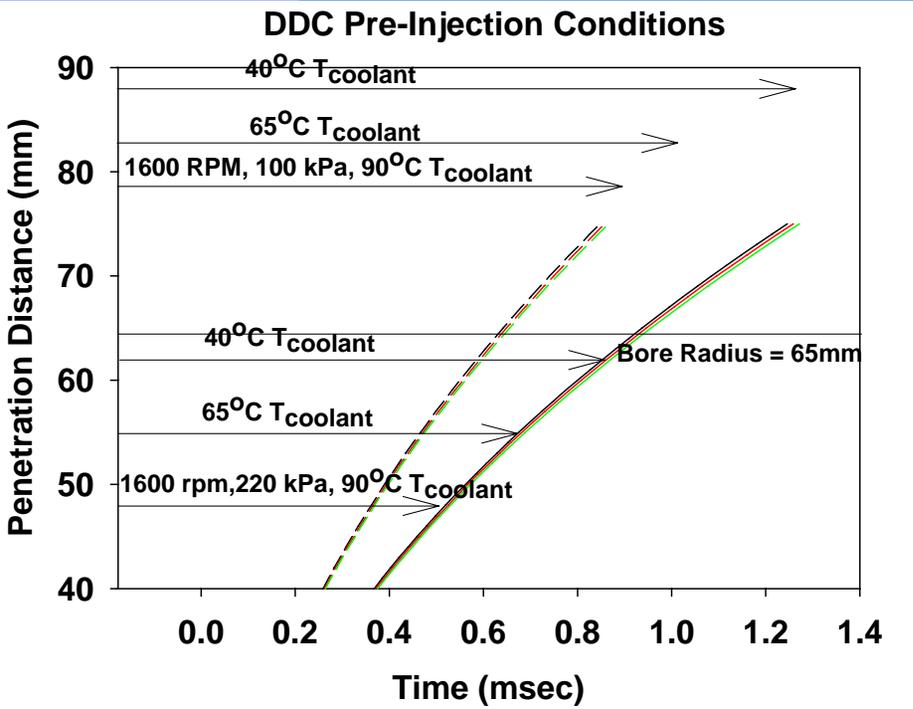
DDC Series 60, 1600 rpm, Pilot

- Liquid Mass Fractions at Bore

- ◆ 90°C = 31% Liquid
- ◆ 65°C = 37% Liquid
- ◆ 40°C = 43% Liquid

- Adhering Mass Fraction on Bore is 71%

- ◆ 90°C = 22%
 - ◆ 65°C = 26%
 - ◆ 40°C = 31%
- } Liquid



OM 611, 1500 rpm, Pilot

- Liquid Mass Fractions at Bore

- High Load

- 65°C = 22% Liquid
 - 40°C = 34% Liquid

- Low Load

- 90°C = 50% Liquid
 - 65°C = 64% Liquid
 - 40°C = 76% Liquid

- Adhering Mass Fraction 71%

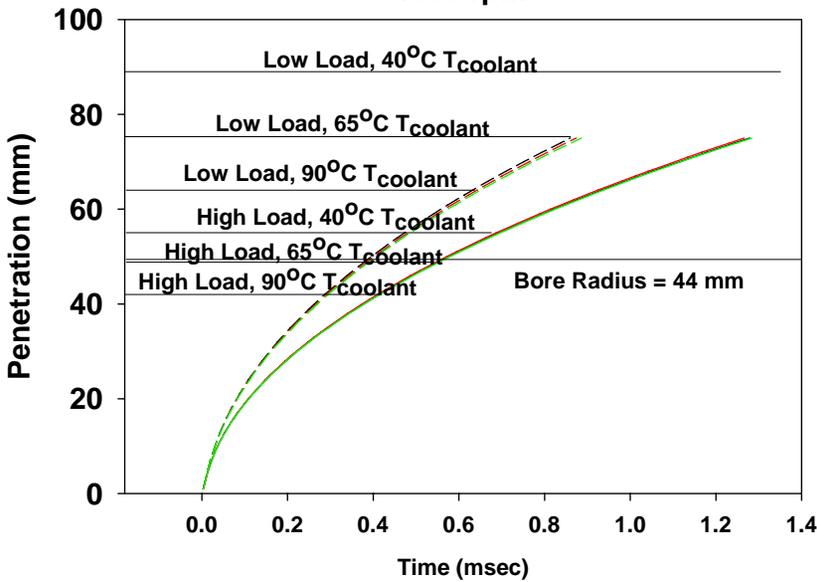
- High Load

- 65°C = 16% Liquid
 - 40°C = 24% Liquid

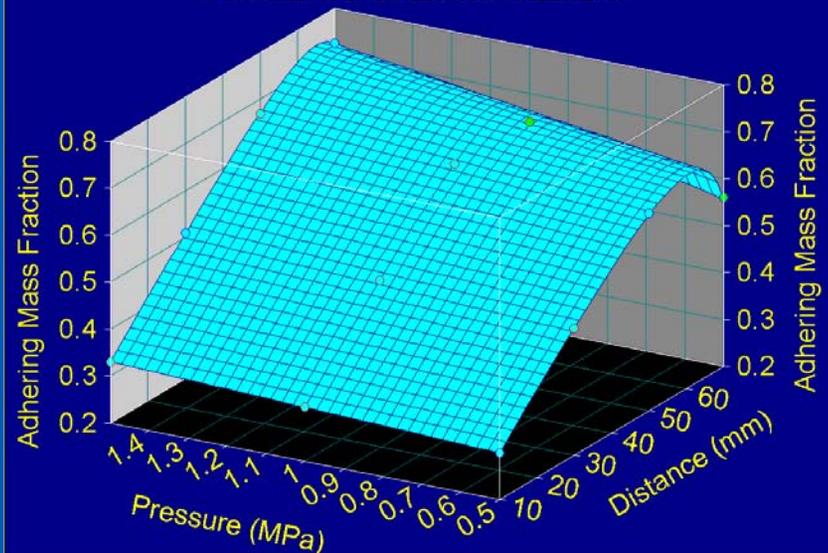
- Low Load

- 90°C = 36% Liquid
 - 65°C = 45% Liquid
 - 40°C = 54% Liquid

OM 611 Pre-Injection
1500 rpm



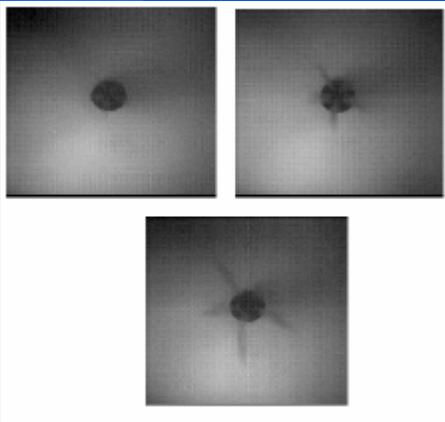
Rank 27 Eqn 1049 $z=(a+bx+cx^2+dy)/(1+ex+fy)$
 $r^2=0.99964146$ DF Adj $r^2=0.99921122$ FitStdErr=0.0037559038 Fstat=3345.7347
 $a=0.19503729$ $b=0.0064228738$ $c=-0.00012273655$
 $d=0.034622713$ $e=-0.012891396$ $f=0.022692769$



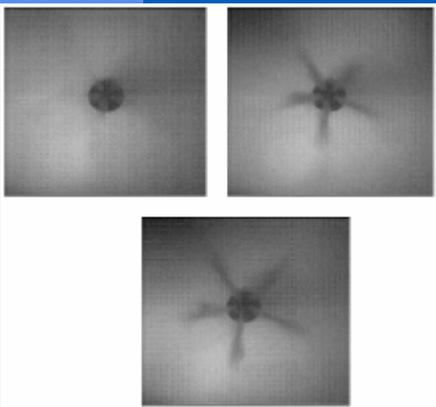
Fuel Injection - Pilot and Post

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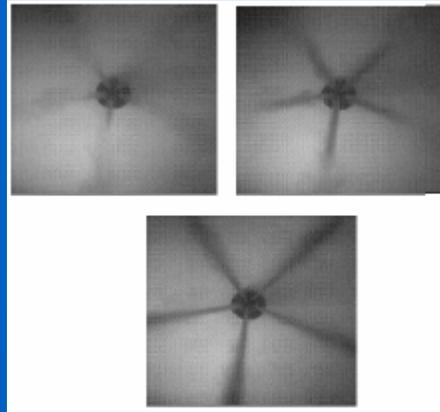
First Pilot, 0.17 ms



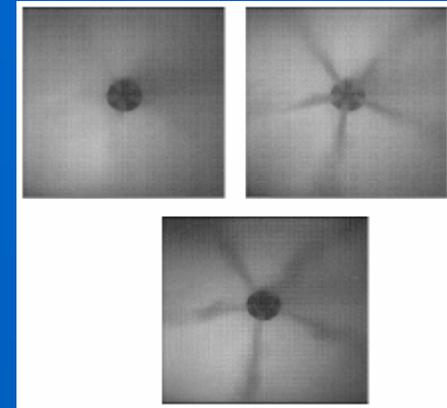
Second Pilot, 0.17 ms



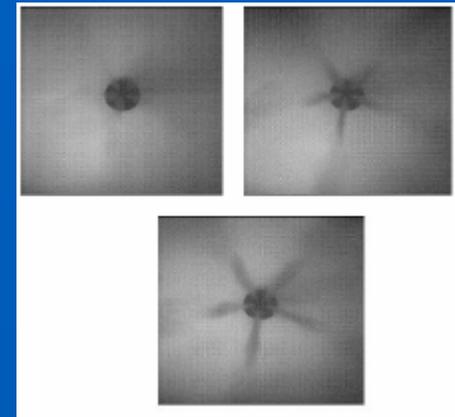
Main, 0.45 ms



First Post, 0.17 ms



Second Post, 0.17 ms



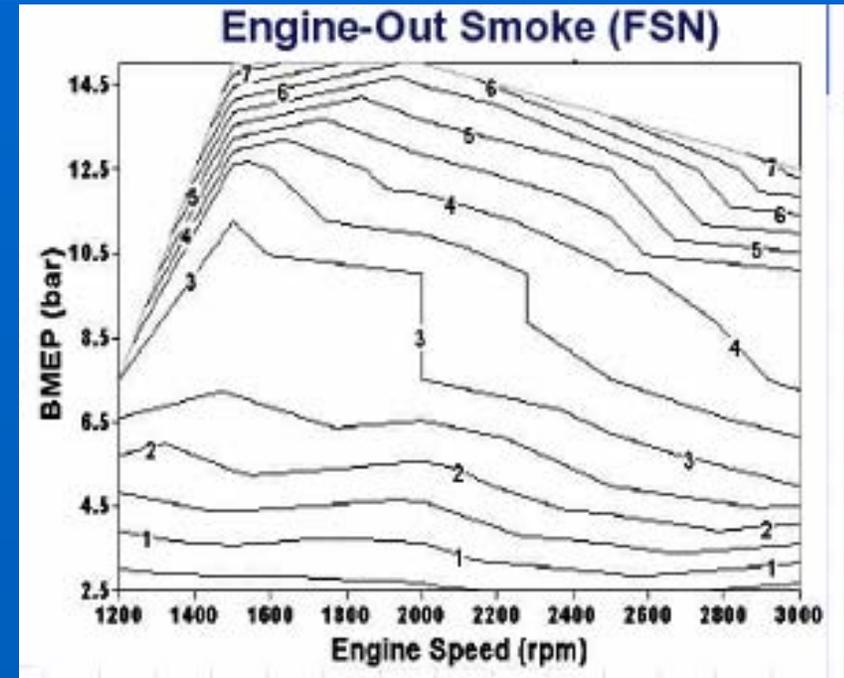
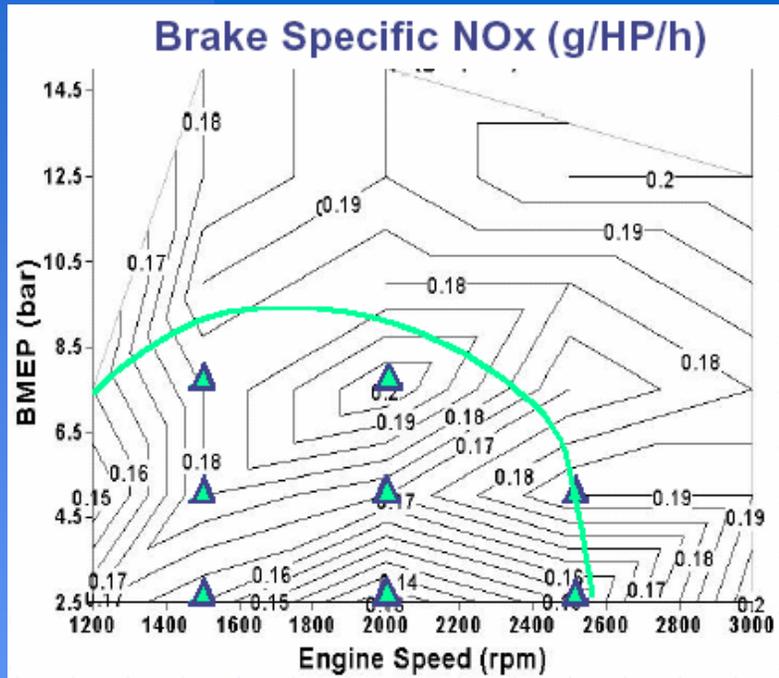
- Split Injection Offers Opportunity to Reduce Liquid Length and Liquid Impingement
- Benefits for both Pre and Post Injection



Massive EGR



Massive EGR Background - EPA-Ford Data



Type	4-cylinder, 2 valve/cyl OHC
Displacement	1896 cm ³
Bore	79.5 mm
Stroke	95.5 mm
Comp. Ratio	19.5:1

EPA Fuel System - Hydraulically Intensified
 Injector Location - 7mm offset w/ 26° Incl.
 Boost Systems - externally supplemented
 ($P_{exh} = P_{int} + 0.1\text{Bar}$)
 - partial map TC matched
 (Initial effort)

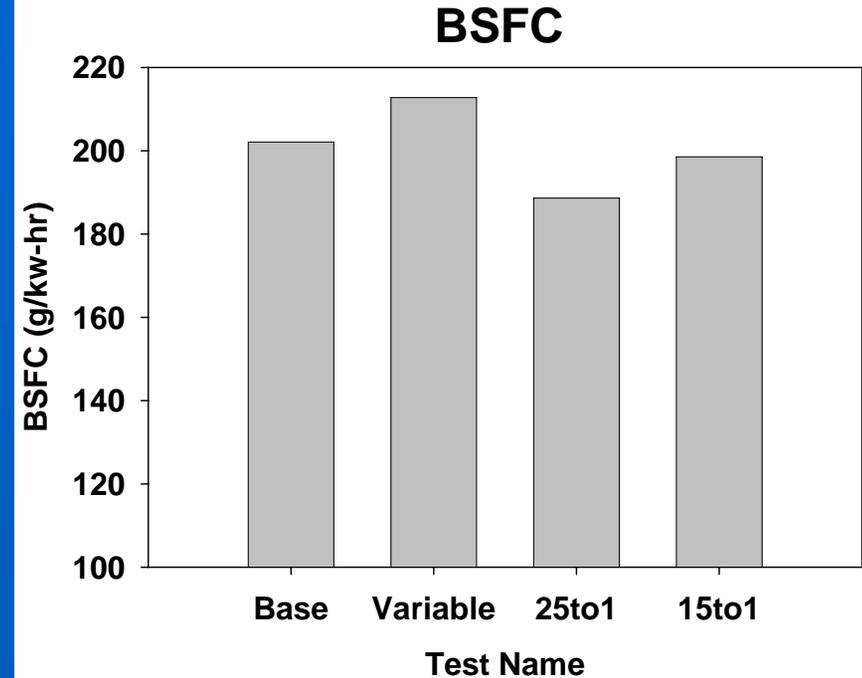
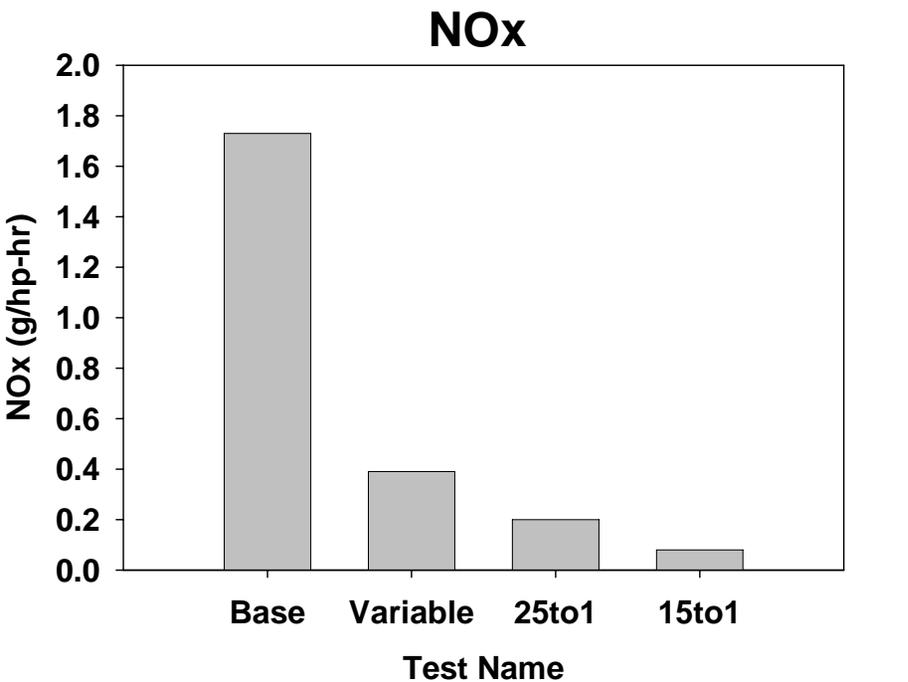


Massive EGR Background - Diffusion Burn Engine (Alternative to NO_x After treatment)

- SwRI Has Extensive Data Base of 8-Mode Data for Cat 3176 2.5 g/hp-hr NO_x + HC Engine
- Use Cycle Simulation to Model Different Levels of EGR
- Assumed LP Loop EGR After DPF
- Conditions Examined
 - ◆ Baseline - Good Prediction of Existing Data
 - ◆ Baseline A/F and Timing + EGR + Boost
 - ◆ Baseline Timing + A/F=25:1 + EGR + Boost
 - ◆ A/F=15:1 + EGR + Boost + Timing Advance



Massive EGR



- Baseline Engine Around 2 g/hp-hr
- BSFC Penalty with Variable Due to Back Pressure Increases
- 25:1 A/F Produced Lots of Turbine Energy
- 15:1 A/F Lowered the Air Flow and Boost Requirements



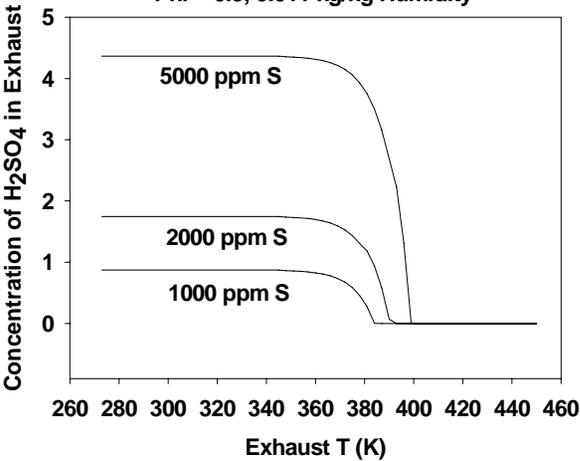
Massive EGR Issue



Cooled EGR

Concentration of H₂SO₄ in Exhaust

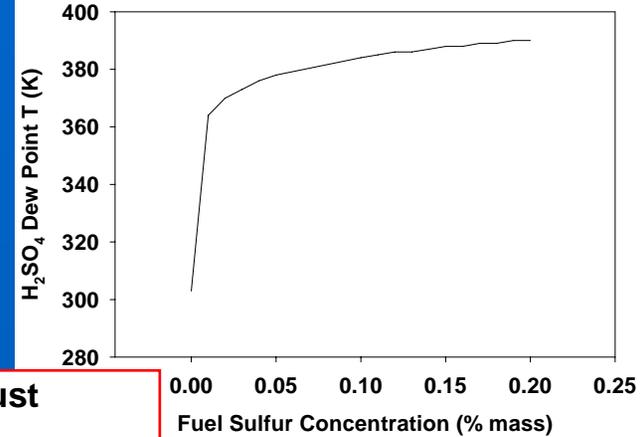
Phi = 0.5, 0.011 kg/kg Humidity



- S in the Fuel Raises the Exhaust Dewpoint
 - ◆ Concentration Determines the Concentration of H₂SO₄ in the Exhaust
- NO in the Exhaust Raises the Exhaust Dewpoint
 - ◆ Concentration Determine the Concentration of HNO₃ in the Exhaust
- H₂SO₄ in the Exhaust is Directly Related to Fuel S Concentration

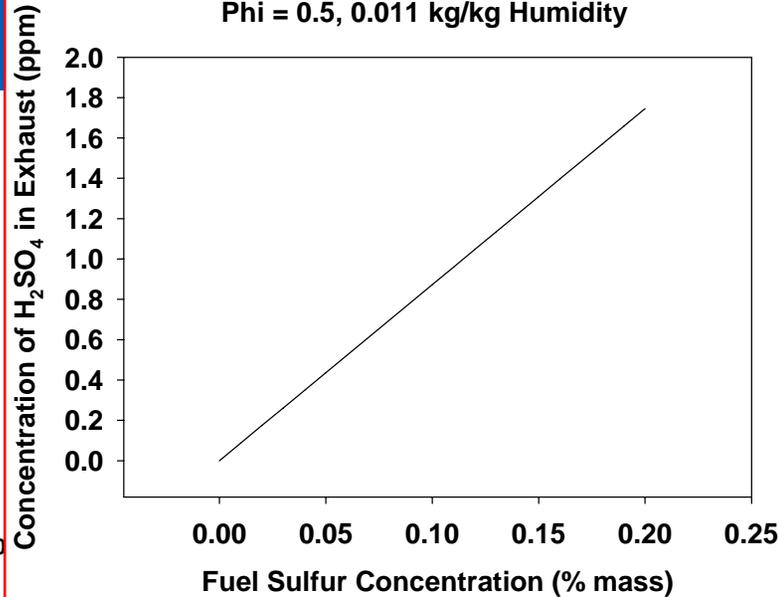
Exhaust Dew Point

P_{exh} = 1 atm, T_{exh} = 40°C
Phi = 0.5, 0.011 kg/kg Humidity



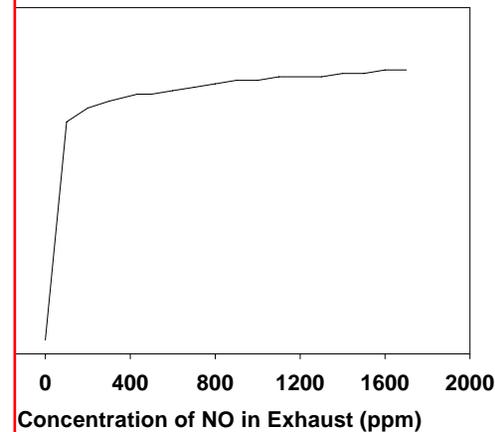
H₂SO₄ Concentration in Exhaust

Phi = 0.5, 0.011 kg/kg Humidity



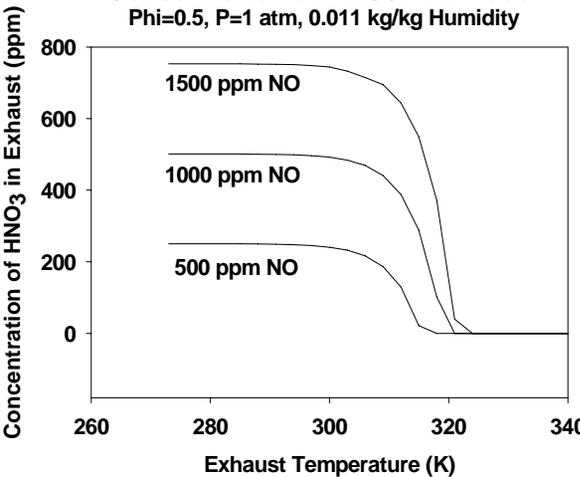
Exhaust Dewpoint

P_{exh} = 1 atm, T_{exh} = 40°C
Phi = 0.5, 0.011 kg/kg Humidity



Concentration of HNO₃ in Exhaust

Phi=0.5, P=1 atm, 0.011 kg/kg Humidity



Diffusion Burn Engine Fuel

- Conventional Current Diesel Engine Fuel Appetite
 - ◆ Low Aromatics (high H/C Ratio)
 - ☒ Lower Flame T and Lower NOx
 - ☒ Lower Propensity for Soot Formation
 - ◆ High Cetane Number
- Advanced Diesel Engine Fuel Appetite
 - ◆ Mixed Mode (Part Time HCCI and LTC)
 - ☒ Low Aromatic
 - ☒ High Cetane Number (at least consistent)



So, Best Diffusion Burn System

- Ultra High Injection Pressure and Small Holes
- Massive EGR
- Ultra High Boost
- Well Designed Pistons and Intake
- High Quality Diesel Fuel



Alternative Approaches

- Full Time HCCI
 - ◆ New Fuel Required
- HEDGE
 - ◆ Could be the Lowest Cost Alternative



Thank You

