

Boosted HCCI for High Power without Engine Knock, and with Ultra-Low NO_x Emissions using a Conventional Fuel

John Dec and Yi Yang
Sandia National Laboratories



15th Directions in Engine-Efficiency & Emissions Research Conference
August 3 – 6, 2009, Dearborn, MI

Sponsor:

U.S. DOE, Office of FreedomCAR & Vehicle Technologies
Program Manager: Gurpreet Singh





- Advanced engines using HCCI or HCCI-like combustion can provide both high efficiencies and very low emissions of NO_x and PM.
- Limited max. power is a significant limitation to implementation of HCCI.
- Intake boosting is well-known as a method for increasing power.
 - Application to HCCI challenging because increased P_{in} enhances autoignition \Rightarrow combustion becomes overly advanced \Rightarrow knock.
 - Reduced CR and/or special fuels (natural gas, ethanol) often required.
- Previous work on boosted HCCI.
 1. Christensen & Johansson \Rightarrow 16 bar IMEP using natural gas.
 2. Olsson *et al.* \Rightarrow 16 bar BMEP using ethanol and *n*-heptane.
 3. Bessonette *et al.* \Rightarrow 16 bar BMEP using low ON gasoline & low CN diesel, CR = 12.
 4. Kalghatgi *et al.* \Rightarrow 16 bar IMEP using gasoline in a DI diesel, but $\text{NO}_x = 0.58 \text{ g/kWh}$, well above US 2010 limits.

● IMEP or BMEP ~ 16 bar, but used special fuels or other changes.

Objective and Approach



- Desirable to use a conventional fuel and to keep NO_x below US 2010 limits without aftertreatment.
 - Maintain a relatively high CR for high efficiency/low fuel consumption.

● **Objective:** Determine the potential boosted HCCI using conventional gasoline \Rightarrow with no engine knock and $\text{NO}_x < \text{US2010}$.

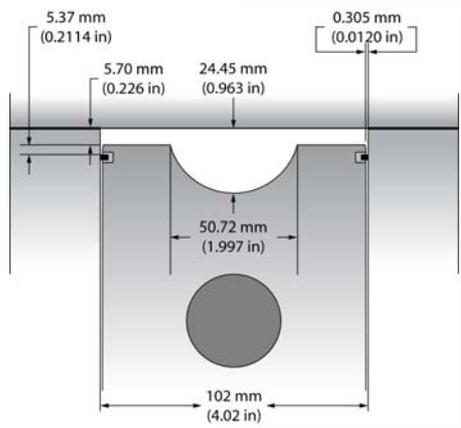
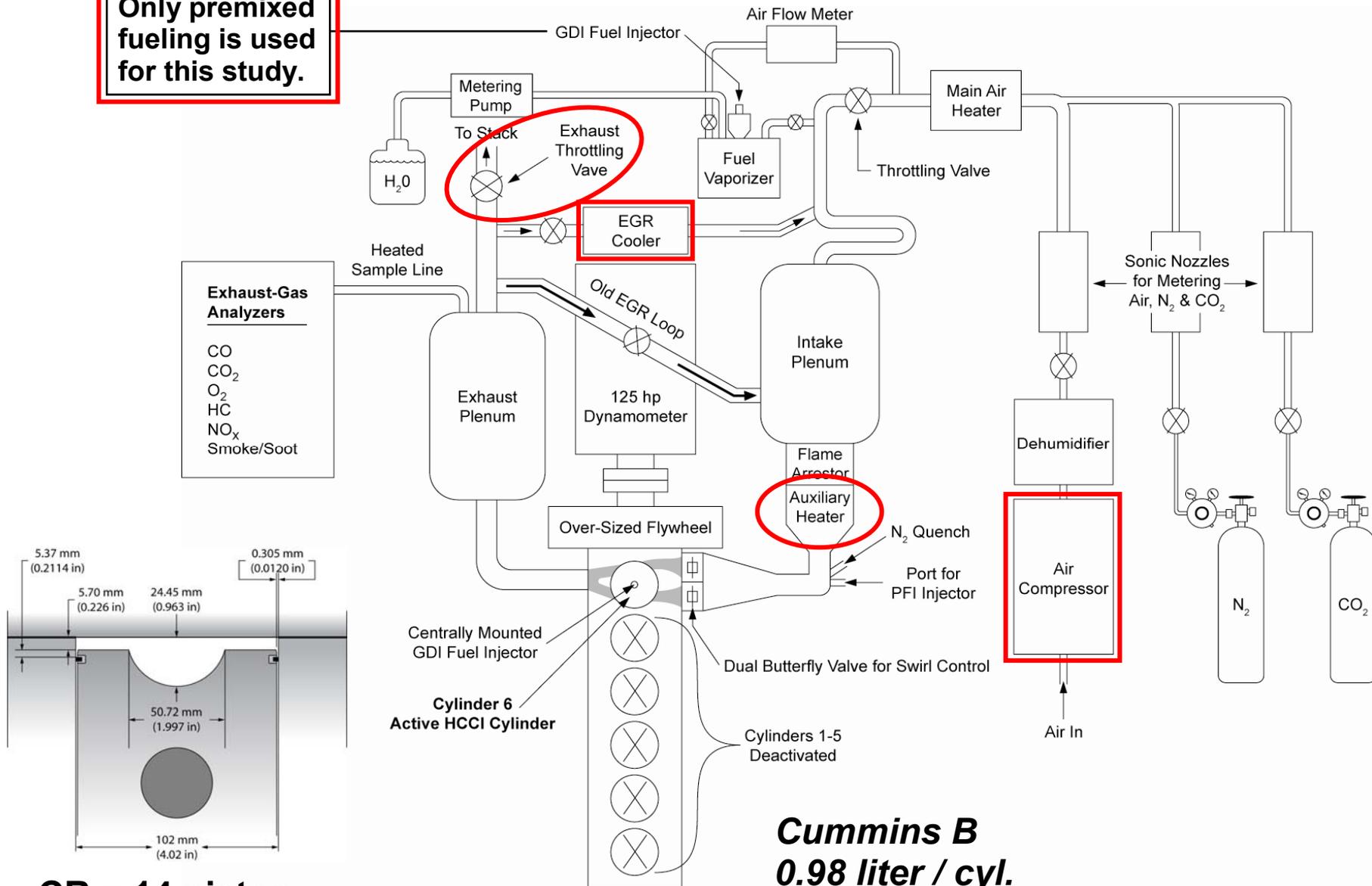
● Approach:

1. Conventional Gasoline: $(R+M)/2 = 87$, RON = 90.8, MON = 83.2.
Aromatics 23%, Olefins 4.2%, Alkanes 73%
2. Piston: CR = 14, open combustion chamber.
3. Current data at 1200 rpm.
4. Control pressure-induced enhancement of autoignition with a combination of:
 - \Rightarrow Intake temperature control
 - \Rightarrow Cooled EGR
5. Maintain $P_{\text{exhaust}} \approx P_{\text{in}} + 2 \text{ kPa}$. (P_{in} = intake pressure)

HCCI Engine and Subsystems



Only premixed fueling is used for this study.



CR = 14 piston

Test Procedure



- Systematically increase P_{in} and determine maximum attainable IMEP_g.
 - Overly advanced combustion can cause knock and reduced efficiency.
 - Control pressure-induced enhancement of autoignition using a combination of T_{in} adjustment and cooled EGR.
- Retard combustion to prevent knock \Rightarrow eventually reach stability limit.
- For each P_{in} , load is limited by knock/stability limit.

- Knock-limit criterion: **Ringing $\leq 5 \text{ MW/m}^2$** $= \frac{1}{2\gamma} \cdot \frac{\left(0.05 \cdot \frac{dP}{dt, \max}\right)^2}{P_{\max}} \cdot \sqrt{\gamma RT_{\max}}$

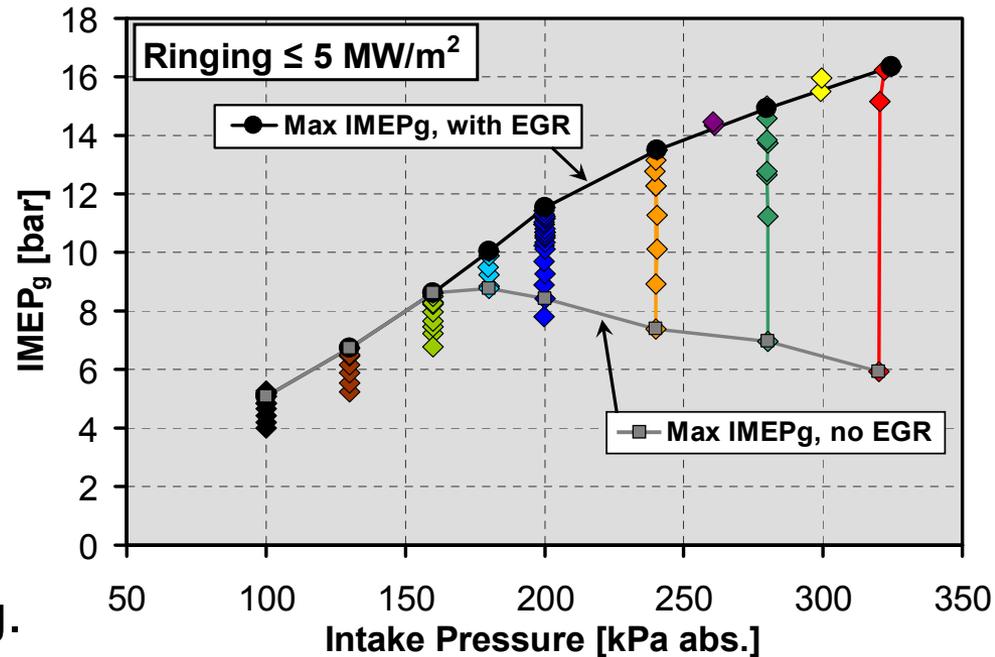
Jim Eng, SAE 2002-01-2859

- Corresponds to 8 bar/°CA at 1200 rpm, $P_{in} = 100\text{kPa}$ absolute.
- Increase in P_{\max} helps $\Rightarrow dP/d\theta > 8 \text{ bar/}^\circ\text{CA}$ is OK with boost.

High-Load Limits with Boost



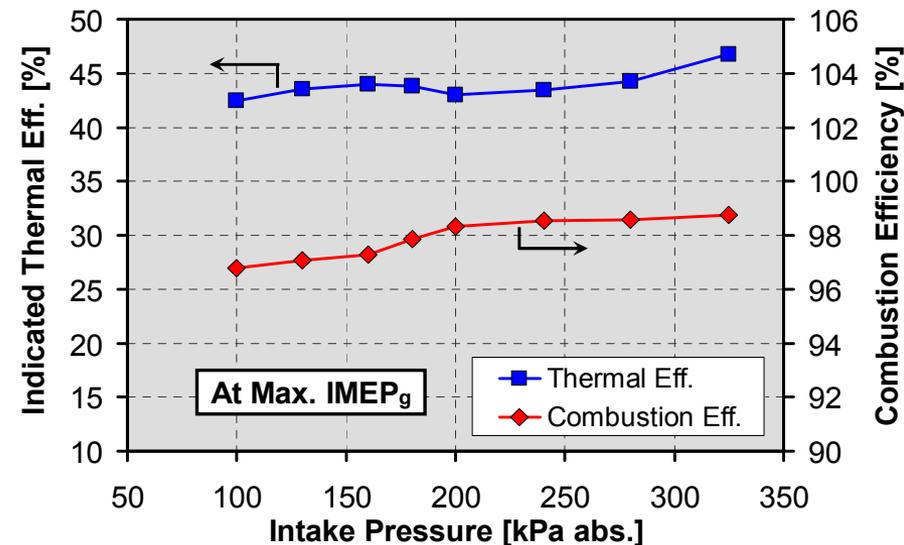
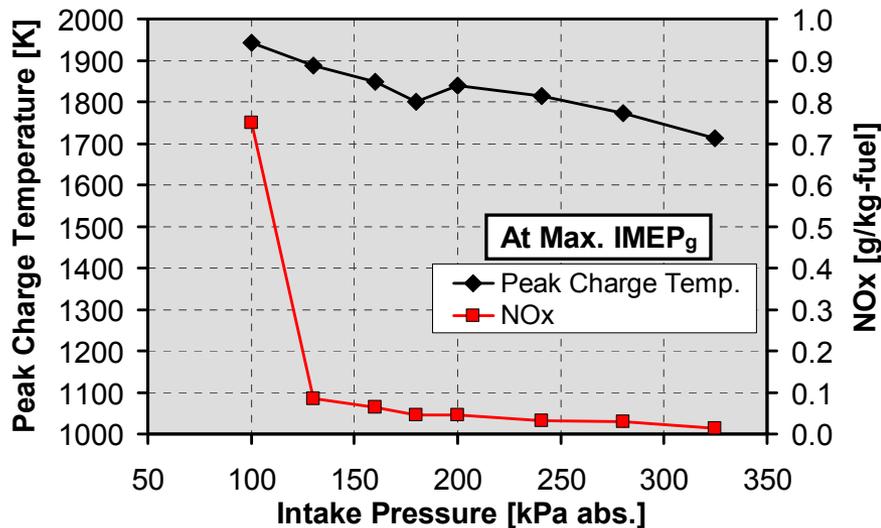
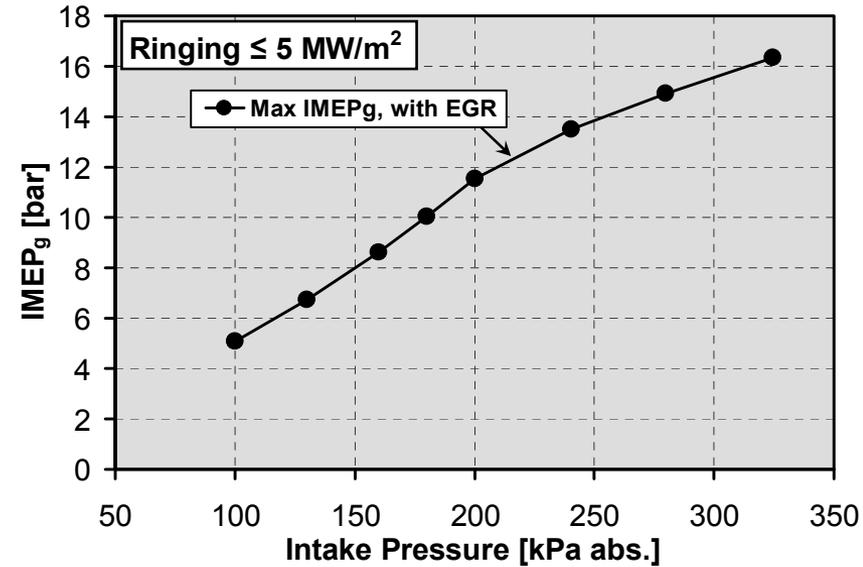
- Naturally aspirated, requires $T_{in} \approx 130^\circ\text{C}$ (or hot residuals).
- Reduce T_{in} with boost to maintain sufficient combustion retard.
 - For $P_{in} > 160$ kPa, $T_{in} \rightarrow T_{amb} \Rightarrow$ limits allowable fueling.
 - Max. $\text{IMEP}_g = 8.8$ bar at $P_{in} = 180$ kPa.
- Cooled EGR to further slow autoig.
- Maintain $T_{in} = 60^\circ\text{C} \Rightarrow$ allows substantial timing retard w/o significant LTHR.
 - Allows a large increase in fueling \Rightarrow Max. IMEP_g increased to 16.3 bar at 324 kPa.
- For $P_{in} \geq 260$ kPa, EGR levels are so high that the mixture is stoichiometric.
 - Mass-fraction of reactants must be reduced as P_{in} is increased above 260 kPa.
- Therefore, higher loads require proportionally more boost.
 - Currently limited by max. allowable cylinder press. ~ 170 bar.
 - 100-cycle avg. peak pressure at max.-load point is 150 bar.



Performance at Maximum IMEP_g Points



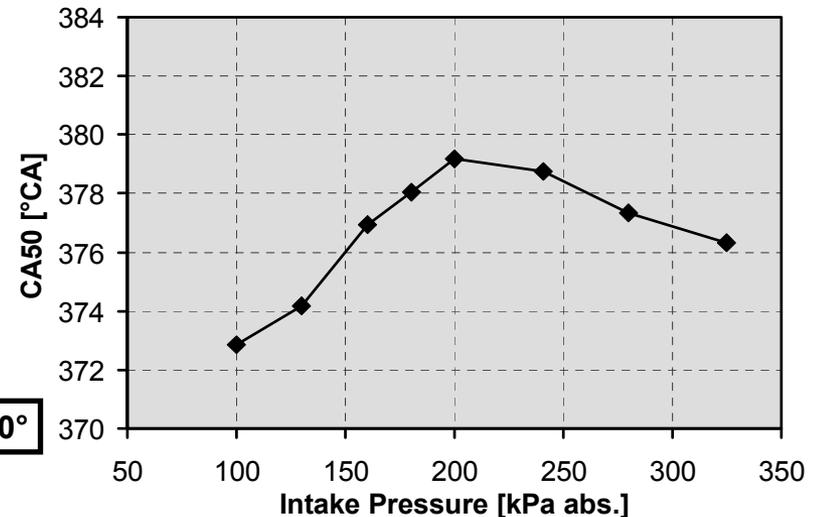
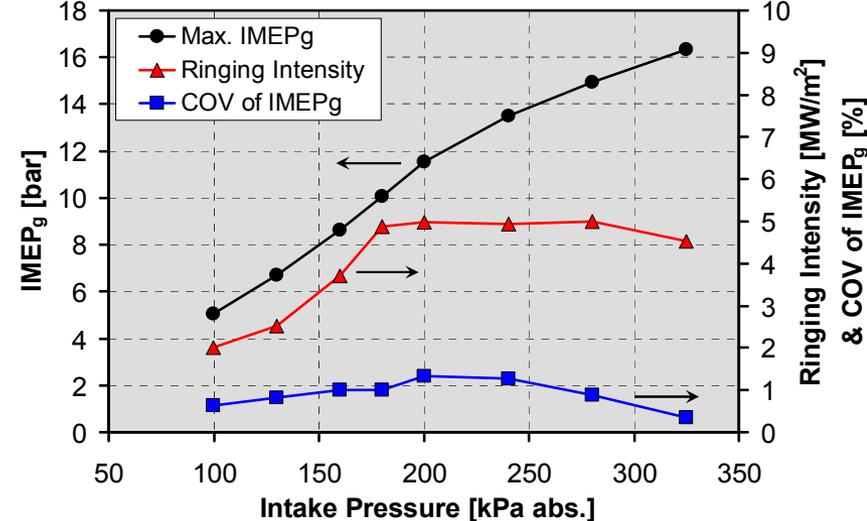
- Indicated thermal efficiency ~45%.
 - Increases slightly with boost → 47%.
- Combustion eff. increases, 97 → 99%.
 - Higher wall temps. ⇒ improve combst.
 - Increased EGR reduces HC & CO emiss.
- NO_x emissions extremely low for all boosted cases, < 0.1 g/kg-fuel.
- Correlates with low peak charge temp.
 - NO_x higher for $P_{in} = 100$, $T_{peak} > 1900K$.



Maximum IMEP_g Point – Stability and Knock



- Achieved **IMEP_g = 16.3 bar**, $P_{in} = 324$.
 - Stoichiometric C/F = 38.5, EGR = 60%,
 $T_{exhaust} = 407^{\circ}\text{C}$.
- COV of IMEP_g ≤ 1%, VG stability.
- Ringing ≤ 5 MW/m², No Knocking.
 - Ringing increases $P_{in} = 100 - 180$ kPa.
 - $P_{in} \geq 180$ kPa, Ringing held at 5 by substantially retarding combustion timing.
- Allowable combustion retard (CA50) increases greatly with increased P_{in} .
 - Less retard required, $P_{in} > 200$ kPa.



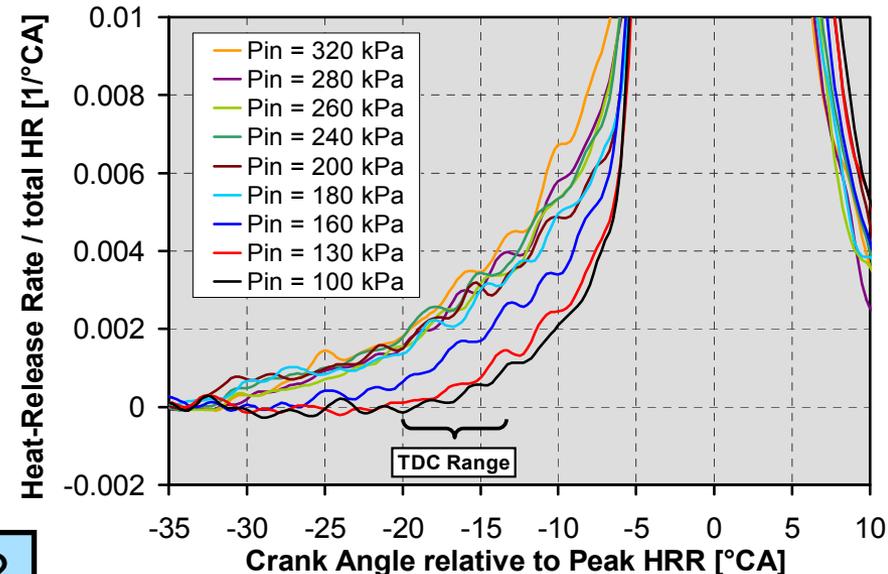
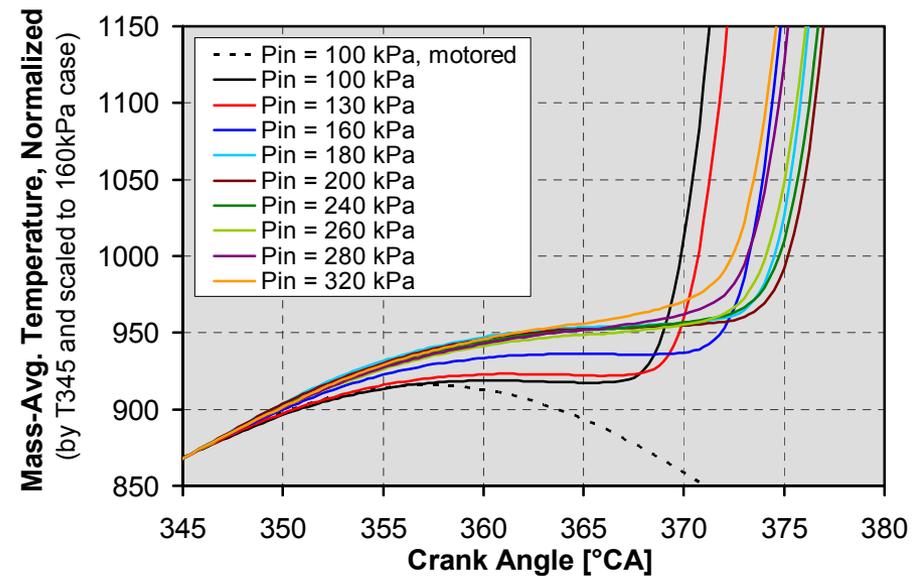
TDC = 360°

● Substantial timing retard with good stability is the key to controlling knock.

Retarding Combustion for Boosted Operation



- Retard combst. to reduce max. PRR.
 - Sjöberg *et al.*, SAE 2005-01-0113.
- Stability depends on $dT/d\theta$ prior to onset of main combustion.
 - Sjöberg & Dec, P. Comb. Inst. 2006.
- $dT/d\theta$ increases with intake boost.
 - Allows more retard with good stability.
- Compare HRR curves \Rightarrow align by peak HRR & normalize by total HR.
- Shows that the cause is increased ITHR (intermediate-temperature heat release) at higher boost.
 - Increases greatly $P_{in} = 100 - 180$ kPa,
> T_{in} is reduced from 130 \rightarrow 60°C.
 - Little change for $P_{in} > 180$, $T_{in} = 60$ °C.



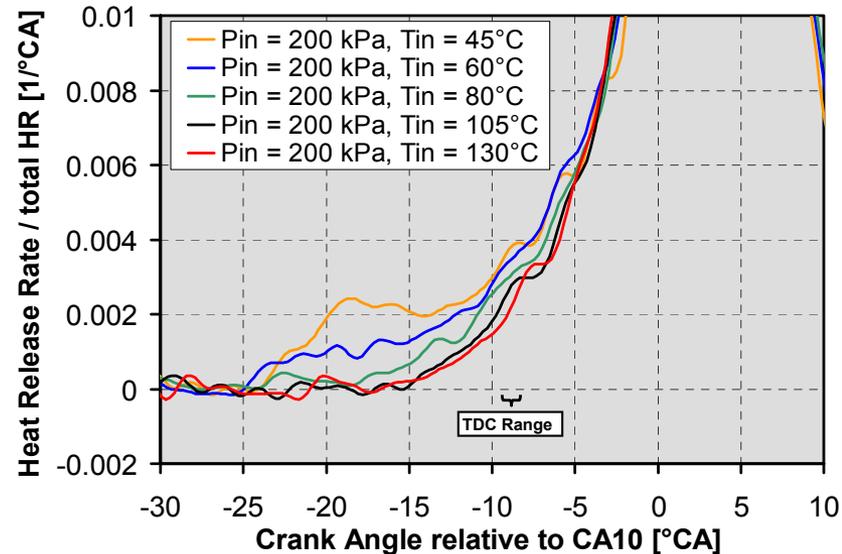
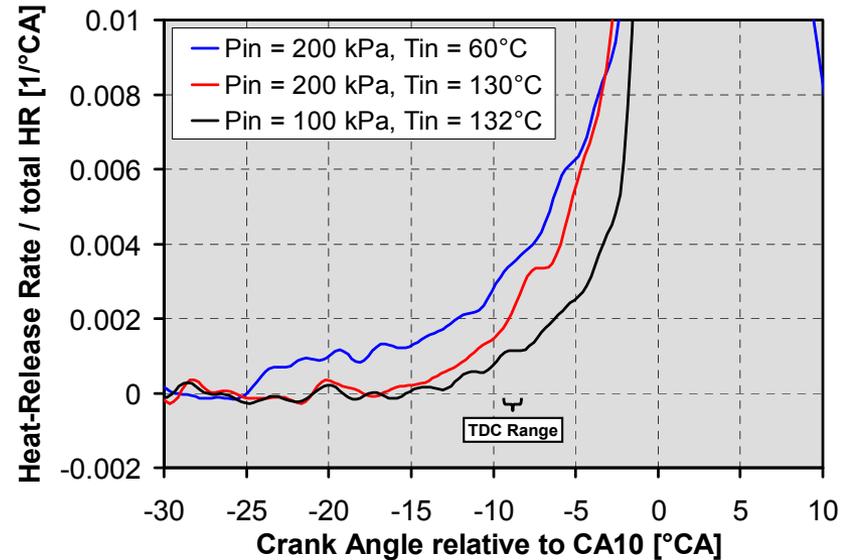
- Is increased ITHR due to $\uparrow P_{in}$ or $\downarrow T_{in}$?

P_{in} and T_{in} Effects on ITHR with Boost



- T_{in} fixed at $130^{\circ}\text{C} \Rightarrow$ Increase P_{in} from 100 \rightarrow 200 kPa, ITHR \uparrow significantly.
 - Mainly late ITHR \Rightarrow most important.
- Reduce T_{in} 130 \rightarrow $60^{\circ}\text{C} \Rightarrow$ more ITHR.
 - Mainly early ITHR; and onset of LTTHR.
 - Further decr. T_{in} to 45°C , more LTTHR.
 - Less important for stability.

- Temp. reduction contributes to the increase in ITHR.
- Pressure-induced increase in the ITHR is the more important effect.



Concluding Remarks



- Intake boosting allowed high $\text{IMEP}_g = 16.3$ bar with 87-ON gasoline fuel.
 - No ringing, very good stability, high efficiency, and ultra-low NO_x .
 - Higher IMEP_g should be possible with greater boost \Rightarrow max. cyl. press?
- The key to this success was the ability to substantially retard combustion.
 \Rightarrow CA50 to 379°CA (19°aTDC) with good stability.
 - This is possible because the ITHR increases significantly with boost \Rightarrow keeps bulk-gas temperatures rising despite late CA50.
 - Detailed investigation showed that enhancement of ITHR by increased P_{in} is most important, but the enhancement by the reduction of T_{in} also contributes.
- For all data, $P_{\text{exhaust}} \approx P_{in} + 2$ kPa
 - Also tested $P_{\text{exhaust}} = 250$ for $P_{in} = 200$ kPa \Rightarrow little effect on performance.
 - For max. IMEP_g points, $T_{\text{exhaust}} = 407 - 470$ K \Rightarrow OK for turbo-charger.
- Study suggests that boosting has good potential as a viable approach for extending the load of gasoline-fueled HCCI.
- Future studies are planned to investigate boosted HCCI over a wider range of operating conditions.