

DOE/EIS-0360

**FINAL ENVIRONMENTAL IMPACT  
STATEMENT FOR CONSTRUCTION  
AND OPERATION OF A DEPLETED URANIUM  
HEXAFLUORIDE CONVERSION FACILITY  
AT THE PORTSMOUTH, OHIO, SITE**

Volume 1: Main Text and Appendixes A–H

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U.S. Department of Energy  
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## COVER SHEET\*

**RESPONSIBLE FEDERAL AGENCY:** U.S. Department of Energy (DOE)

**TITLE:** Final Environmental Impact Statement for Construction and Operation of a Depleted Uranium Hexafluoride Conversion Facility at the Portsmouth, Ohio, Site (DOE/EIS-0360)

**CONTACT:** For further information on this environmental impact statement (EIS), contact:

Gary S. Hartman  
DOE-ORO Cultural Resources Management Coordinator  
U.S. Department of Energy-Oak Ridge Operations  
P.O. Box 2001  
Oak Ridge, TN 37831  
e-mail: Ports\_DUF6@anl.gov  
phone: 1-866-530-0944  
fax: 1-866-530-0943

For general information on the DOE National Environmental Policy Act (NEPA) process, contact:

Carol Borgstrom, Director  
Office of NEPA Policy and Compliance (EH-42)  
U.S. Department of Energy  
1000 Independence Avenue, SW  
Washington, DC 20585  
202-586-4600, or leave message at 1-800-472-2756

**ABSTRACT:** The U.S. Department of Energy (DOE) proposes, via a contract awarded at the direction of Congress (Public Law 107-206), to design, construct, and operate two conversion facilities for converting depleted uranium hexafluoride (commonly referred to as DUF<sub>6</sub>): one at Portsmouth, Ohio, and one at Paducah, Kentucky. DOE intends to use the proposed facilities to convert its inventory of DUF<sub>6</sub> to a more stable chemical form suitable for beneficial use or disposal. This site-specific EIS analyzes the construction, operation, maintenance, and decontamination and decommissioning (D&D) of the proposed DUF<sub>6</sub> conversion facility at three alternative locations within the Portsmouth site; transportation of all cylinders (DUF<sub>6</sub>, enriched, and empty) currently stored at the East Tennessee Technology Park (ETTP) near Oak Ridge, Tennessee, to Portsmouth; construction of a new cylinder storage yard at Portsmouth (if required) for ETTP cylinders; transportation of depleted uranium conversion products and waste materials to a disposal facility; transportation and sale of the hydrogen fluoride (HF) produced as a conversion co-product; and neutralization of HF to calcium fluoride (CaF<sub>2</sub>) and its sale or disposal in the event that the HF product is not sold. This EIS also considers a no action alternative that assumes continued storage of DUF<sub>6</sub> at the Portsmouth and ETTP sites. A separate EIS has been prepared for the proposed facility at Paducah (DOE/EIS-0359). DOE's preferred alternative is to construct and operate the conversion facility at Location A within the Portsmouth site. DOE plans to decide where to dispose of depleted U<sub>3</sub>O<sub>8</sub> conversion product after additional appropriate NEPA review.

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\* Vertical lines in the right margin of this cover sheet and in the remainder of this EIS document indicate changes that have been added after the public comment period.

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## NOTATION

The following is a list of acronyms and abbreviations, chemical names, and units of measure used in this document. Some acronyms used only in tables may be defined only in those tables.

### GENERAL ACRONYMS AND ABBREVIATIONS

AEA	Atomic Energy Act of 1954
AEC	U.S. Atomic Energy Commission
AIHA	American Industrial Hygiene Association
ALARA	as low as reasonably achievable
ANL	Argonne National Laboratory
ANP	Advanced Nuclear Power (Framatome ANP, Inc.)
ANSI	American National Standards Institute
AQCR	Air Quality Control Region
BLS	Bureau of Labor Statistics
CAA	Clean Air Act
CEQ	Council on Environmental Quality
CERCLA	Comprehensive Environmental Response, Compensation, and Liability Act of 1980
CFR	<i>Code of Federal Regulations</i>
CRMP	cultural resource management plan
CROET	Community Reuse Organization of East Tennessee
CWA	Clean Water Act
D&D	decontamination and decommissioning
DNFSB	Defense Nuclear Facilities Safety Board
DNL	day-night average sound level
DOE	U.S. Department of Energy
DOT	U.S. Department of Transportation
DU	depleted uranium
DUF <sub>6</sub>	depleted uranium hexafluoride
EA	environmental assessment
EBE	evaluation basis earthquake
EIS	environmental impact statement
EM	Office of Environmental Management (DOE)
EPA	U.S. Environmental Protection Agency
ERDA	Energy Research and Development Administration
ERPG	Emergency Response Planning Guideline
ETTP	East Tennessee Technology Park (formerly K-25 site)

FONSI	Finding of No Significant Impact
FR	<i>Federal Register</i>
FTE	full-time equivalent
FY	fiscal year
GDP	gaseous diffusion plant
GIS	geographic information system
HEPA	high-efficiency particulate air
HMMH	Harris Miller Miller & Hanson, Inc.
HMR	hazardous materials regulation
HMTA	Hazardous Materials Transportation Act
ICRP	International Commission on Radiological Protection
IHE	irreversible health effect
ISC	Industrial Source Complex
LCF	latent cancer fatality
L <sub>eq</sub>	equivalent steady sound level
LLMW	low-level radioactive mixed waste
LLW	low-level radioactive waste
LMES	Lockheed Martin Energy Systems, Inc.
MCL	maximum concentration limit
MEI	maximally exposed individual
MMES	Martin Marietta Energy Systems, Inc.
MOA	memorandum of agreement
NAAQS	National Ambient Air Quality Standard(s)
NCRP	National Council on Radiation Protection and Measurements
NEPA	National Environmental Policy Act of 1969
NESHAPs	National Emission Standards for Hazardous Air Pollutants
NHPA	National Historic Preservation Act
NOI	Notice of Intent
non-DUF <sub>6</sub>	non-depleted uranium hexafluoride
NOV	Notice of Violation
NPDES	National Pollutant Discharge Elimination System
NRC	U.S. Nuclear Regulatory Commission
NRHP	<i>National Register of Historic Places</i>
NTS	Nevada Test Site
OEPA	Ohio Environmental Protection Agency
OIG	Office of Inspector General (DOE)
ORNL	Oak Ridge National Laboratory
ORR	Oak Ridge Reservation
OSHA	Occupational Safety and Health Administration

PA	preliminary assessment
PEA	programmatic environmental assessment
PEIS	programmatic environmental impact statement
PEL	permissible exposure limit
P.L.	Public Law
PM	particulate matter
PM <sub>10</sub>	particulate matter with a mean aerodynamic diameter of 10 μm or less
PM <sub>2.5</sub>	particulate matter with a mean aerodynamic diameter of 2.5 μm or less
PORTS	Portsmouth Gaseous Diffusion Plant
PSD	prevention of significant deterioration
R&D	research and development
RCRA	Resource Conservation and Recovery Act
RFP	Request for Proposal(s)
ROD	Record of Decision
ROI	region of influence
SAAQS	State Ambient Air Quality Standard(s)
SAR	safety analysis report
SHPO	State Historic Preservation Officer
SVOC	semivolatile organic compound
TDEC	Tennessee Department of Environment and Conservation
TEDE	total effective dose equivalent
TLD	thermoluminescence dosimeter
TRU	transuranic(s)
TSCA	Toxic Substances Control Act
TUS	Termoelectrica U.S., LLC
TVA	Tennessee Valley Authority
UDS	Uranium Disposition Services, LLC
USACE	U.S. Army Corps of Engineers
USC	<i>United States Code</i>
USDA	U.S. Department of Agriculture
USEC	United States Enrichment Corporation
USFWS	U.S. Fish and Wildlife Service
USGS	U.S. Geological Survey
VOC	volatile organic compound
WM PEIS	Waste Management Programmatic Environmental Impact Statement

**CHEMICALS**

Am	americium
CaF <sub>2</sub>	calcium fluoride
Co	cobalt
CO	carbon monoxide
H <sub>2</sub>	hydrogen
HF	hydrogen fluoride (slag); hydrofluoric acid
H <sub>2</sub> O	water
KF	potassium fluoride
KOH	potassium hydroxide
NH <sub>3</sub>	ammonia
NO	nitrogen oxide
NO <sub>2</sub>	nitrogen dioxide
NO <sub>x</sub>	nitrogen oxides
Np	neptunium
O <sub>3</sub>	ozone
PAH	polycyclic aromatic hydrocarbon
Pb	lead
PCB	polychlorinated biphenyl
Pu	plutonium
SO <sub>2</sub>	sulfur dioxide
SO <sub>x</sub>	sulfur oxides
Tc	technetium
TCE	trichloroethylene
U	uranium
UF <sub>4</sub>	uranium tetrafluoride
UF <sub>6</sub>	uranium hexafluoride
UO <sub>2</sub>	uranium dioxide
UO <sub>3</sub>	uranium trioxide
UO <sub>2</sub> F <sub>2</sub>	uranyl fluoride
U <sub>3</sub> O <sub>8</sub>	triuranium octaoxide

**UNITS OF MEASURE**

°C	degree(s) Celsius	mi <sup>2</sup>	square mile(s)
Ci	curie(s)	min	minute(s)
cm	centimeter(s)	mL	milliliter(s)
		mph	mile(s) per hour
d	day(s)	mrem	millirem(s)
dB	decibel(s)	mSv	millisievert(s)
dB(A)	A-weighted decibel(s)	MVA	megavolt-ampere(s)
		MW	megawatt(s)
°F	degree(s) Fahrenheit	MWh	megawatt-hour(s)
ft	foot (feet)		
ft <sup>2</sup>	square foot (feet)	nCi	nanocurie(s)
g	gram(s)	oz	ounce
gal	gallon(s)		
		pCi	picocurie(s)
h	hour(s)	ppb	part(s) per billion
ha	hectare(s)	ppm	part(s) per million
		psia	pound(s) per square inch absolute
in.	inch(es)	psig	pound(s) per square inch gauge
in. <sup>2</sup>	square inch(es)		
		rem	roentgen equivalent man
kg	kilogram(s)		
km	kilometer(s)	s	second(s)
km <sup>2</sup>	square kilometer(s)	Sv	sievert(s)
kPa	kilopascal(s)		
		t	metric ton(s)
L	liter(s)	ton(s)	short ton(s)
lb	pound(s)		
		wt%	percent by weight
m	meter(s)		
m <sup>2</sup>	square meter(s)	yd <sup>3</sup>	cubic yard(s)
m <sup>3</sup>	cubic meter(s)	yr	year(s)
MeV	million electron volts		
mg	milligram(s)	µg	microgram(s)
mi	mile(s)	µm	micrometer(s)

**ENGLISH/METRIC AND METRIC/ENGLISH EQUIVALENTS**

Multiply	By	To Obtain
<i>English/Metric Equivalents</i>		
acres	0.4047	hectares (ha)
cubic feet (ft <sup>3</sup> )	0.02832	cubic meters (m <sup>3</sup> )
cubic yards (yd <sup>3</sup> )	0.7646	cubic meters (m <sup>3</sup> )
degrees Fahrenheit (°F) -32	0.5555	degrees Celsius (°C)
feet (ft)	0.3048	meters (m)
gallons (gal)	3.785	liters (L)
gallons (gal)	0.003785	cubic meters (m <sup>3</sup> )
inches (in.)	2.540	centimeters (cm)
miles (mi)	1.609	kilometers (km)
pounds (lb)	0.4536	kilograms (kg)
short tons (tons)	907.2	kilograms (kg)
short tons (tons)	0.9072	metric tons (t)
square feet (ft <sup>2</sup> )	0.09290	square meters (m <sup>2</sup> )
square yards (yd <sup>2</sup> )	0.8361	square meters (m <sup>2</sup> )
square miles (mi <sup>2</sup> )	2.590	square kilometers (km <sup>2</sup> )
yards (yd)	0.9144	meters (m)
<hr style="border-top: 1px dashed black;"/>		
<i>Metric/English Equivalents</i>		
centimeters (cm)	0.3937	inches (in.)
cubic meters (m <sup>3</sup> )	35.31	cubic feet (ft <sup>3</sup> )
cubic meters (m <sup>3</sup> )	1.308	cubic yards (yd <sup>3</sup> )
cubic meters (m <sup>3</sup> )	264.2	gallons (gal)
degrees Celsius (°C) +17.78	1.8	degrees Fahrenheit (°F)
hectares (ha)	2.471	acres
kilograms (kg)	2.205	pounds (lb)
kilograms (kg)	0.001102	short tons (tons)
kilometers (km)	0.6214	miles (mi)
liters (L)	0.2642	gallons (gal)
meters (m)	3.281	feet (ft)
meters (m)	1.094	yards (yd)
metric tons (t)	1.102	short tons (tons)
square kilometers (km <sup>2</sup> )	0.3861	square miles (mi <sup>2</sup> )
square meters (m <sup>2</sup> )	10.76	square feet (ft <sup>2</sup> )
square meters (m <sup>2</sup> )	1.196	square yards (yd <sup>2</sup> )

## SUMMARY<sup>1</sup>

### S.1 INTRODUCTION

This document is a site-specific environmental impact statement (EIS) for construction and operation of a proposed depleted uranium hexafluoride (DUF<sub>6</sub>) conversion facility at the U.S. Department of Energy (DOE) Portsmouth site in Ohio (Figure S-1). The proposed facility would convert the DUF<sub>6</sub> stored at Portsmouth to a more stable chemical form suitable for use or disposal. The facility would also convert the DUF<sub>6</sub> from the East Tennessee Technology Park (ETTP) site near Oak Ridge, Tennessee.

In a Notice of Intent (NOI) published in the *Federal Register* on September 18, 2001 (*Federal Register*, Volume 66, page 48123 [66 FR 48123]), DOE announced its intention to prepare a single EIS for a proposal to construct, operate, maintain, and decontaminate and decommission two DUF<sub>6</sub> conversion facilities at Portsmouth, Ohio, and Paducah, Kentucky, in accordance with the National Environmental Policy Act of 1969 (NEPA) (*United States Code*, Title 42, Section 4321 et seq. [42 USC 4321 et seq.]) and DOE's NEPA implementing procedures (*Code of Federal Regulations*, Title 10, Part 1021 [10 CFR Part 1021]). Subsequent to award of a contract on August 29, 2002, to Uranium Disposition Services, LLC (hereafter referred to as UDS), for design, construction, and operation of DUF<sub>6</sub> conversion facilities at Portsmouth and Paducah, DOE reevaluated its approach to the NEPA process and decided to prepare separate site-specific EISs. This change was announced in a *Federal Register* Notice of Change in NEPA Compliance Approach published on April 28, 2003 (68 FR 22368); the Notice is included as Attachment B to Appendix C of this EIS.

This EIS addresses the potential environmental impacts from the construction, operation, maintenance, and decontamination and decommissioning (D&D) of the proposed conversion facility at three alternative locations within the Portsmouth site; from the transportation of all ETTP cylinders (DUF<sub>6</sub>, normal and enriched UF<sub>6</sub>, and empty) to Portsmouth; from the transportation of depleted uranium conversion products to a disposal facility; and from the transportation, sale, use, or disposal of the fluoride-containing conversion products (hydrogen fluoride [HF] or calcium fluoride [CaF<sub>2</sub>]). An option of shipping the ETTP cylinders to Paducah is also considered, as is an option of expanding operations. In addition, this EIS evaluates a no action alternative, which assumes continued storage of DUF<sub>6</sub> in cylinders at the Portsmouth and ETTP sites. A separate EIS (DOE/EIS-0359) evaluates potential environmental impacts for the proposed Paducah conversion facility.

#### S.1.1 Background Information

The current DUF<sub>6</sub> conversion facility project is the culmination of a long history of DUF<sub>6</sub> management activities and events. To put the current project into context and provide

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<sup>1</sup> Vertical lines in the right margin of this summary and the remainder of this EIS document indicate changes that have been added after the public comment period.

perspective, this section briefly discusses the origin and size of the DOE cylinder inventory considered in this EIS and then summarizes the management history.

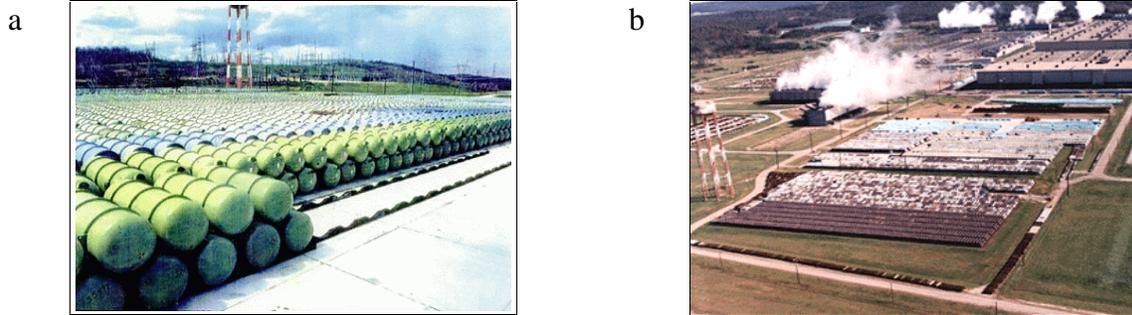
Uranium enrichment in the United States began as part of the atomic bomb development by the Manhattan Project during World War II. Enrichment for both civilian and military uses continued after the war under the auspices of the U.S. Atomic Energy Commission and its successor agencies, including DOE. Three large gaseous diffusion plants (GDPs) were constructed to produce enriched uranium, first at the K-25 site (now called ETTP) and subsequently at Paducah and Portsmouth. The K-25 plant ceased operations in 1985, and the Portsmouth plant ceased operations in 2001. The Paducah GDP continues to operate.

The DUF<sub>6</sub> produced during enrichment has been stored in large steel cylinders at all three gaseous diffusion plant sites since the 1950s. The cylinders are typically stacked two high and are stored outdoors on concrete or gravel yards. Figure S-2 shows typical arrangements for storing cylinders.

DOE is currently responsible for the management of a total of approximately 700,000 metric tons (t) (770,000 short tons [tons])<sup>2</sup> of DUF<sub>6</sub> stored in about 60,000 cylinders at three storage sites. The cylinder inventory considered in this EIS is provided in Table S-1. This EIS considers the conversion of the approximately 250,000 t (275,000 tons) of DUF<sub>6</sub> stored in about 16,000 cylinders at Portsmouth and about 4,800 cylinders at ETTP. In addition, approximately 3,200 cylinders at Portsmouth and 1,100 cylinders at ETTP contain

<b>DUF<sub>6</sub> Management Time Line</b>	
1950–1993	DOE generates DUF <sub>6</sub> stored in cylinders at the ETTP, Portsmouth, and Paducah sites.
1985	K-25 (ETTP) GDP ceases operations.
1992	Ohio EPA issues Notice of Violation (NOV) to Portsmouth.
1993	USEC is created by P.L. 102-186.
1994	DOE initiates DUF <sub>6</sub> PEIS.
1995	DNFSB issues Recommendation 95-1, Safety of Cylinders Containing Depleted Uranium. DOE initiates UF <sub>6</sub> Cylinder Project Management Plan.
1996	USEC Privatization Act (P.L. 104-134) is enacted.
1997	DOE issues Draft DUF <sub>6</sub> PEIS.
1998	DOE and Ohio EPA reach agreement on NOV. Two DOE-USEC MOAs transfer 11,400 DUF <sub>6</sub> cylinders to DOE. P.L. 105-204 is enacted.
1999	DOE and TDEC enter consent order. DOE issues Final DUF <sub>6</sub> PEIS and Record of Decision. DOE issues conversion plan in response to P.L. 105-204. DNFSB closes Recommendation 95-1. DOE issues Draft RFP for conversion services.
2000	DOE issues Final RFP for conversion services.
2001	DOE receives five proposals in response to RFP. DOE identifies three proposals in competitive range. DOE publishes NOI for site-specific DUF <sub>6</sub> Conversion EIS. DOE prepares environmental critique to support conversion services procurement process. Portsmouth GDP ceases operations. DOE holds public scoping meetings for the site-specific DUF <sub>6</sub> Conversion EIS.
2002	DOE-USEC agreement transfers 23,000 t (25,684 tons) of DUF <sub>6</sub> to DOE. P.L. 107-206 is enacted. DOE awards conversion services contract to UDS. DOE prepares environmental synopsis to support conversion services procurement process.
2003	DOE announces Notice of Change in NEPA Compliance Approach and issues the draft EIS. DOE issues draft site-specific conversion facility EISs.
2004	Final site-specific conversion facility EISs issued.

<sup>2</sup> In general, in this EIS, values in English units are presented first, followed by metric units in parentheses. However, when values are routinely reported in metric units, the metric units are presented first, followed by English units in parentheses.



**FIGURE S-2 Storage of DUF<sub>6</sub> Cylinders: (a) Cylinders stacked two high. (b) Cylinder storage yards at the Portsmouth site.**

**TABLE S-1 Inventory of DOE UF<sub>6</sub> Cylinders Considered in This EIS<sup>a</sup>**

Location	No. of Cylinders	Weight of UF <sub>6</sub> (t)
Portsmouth – DUF <sub>6</sub>	16,109	195,800
Non-DUF <sub>6</sub>		
Enriched UF <sub>6</sub>	1,444	19
Normal UF <sub>6</sub>	1,249	13,500
Empty	485	0
ETTP <sup>b</sup> – DUF <sub>6</sub>	4,822	54,300
Non-DUF <sub>6</sub>		
Enriched UF <sub>6</sub>	881	7
Normal UF <sub>6</sub>	221	19
Empty	20	0
<b>Total</b>		
DUF <sub>6</sub>	20,931	250,100
Non-DUF <sub>6</sub>	3,795	13,544
Empty	505	0

<sup>a</sup> As of January 26, 2004.

<sup>b</sup> The proposed action calls for shipment of the ETTP cylinders to Portsmouth.

enriched UF<sub>6</sub> or normal UF<sub>6</sub> (collectively called “non-DUF<sub>6</sub>” cylinders in this EIS) or are empty. This EIS considers the shipment of all ETTP cylinders to Portsmouth, as well as the management of both the Portsmouth and ETTP non-DUF<sub>6</sub> cylinders at Portsmouth. The non-DUF<sub>6</sub> cylinders would not be processed in the conversion facility.

### S.1.1.1 Creation of USEC

In 1993, the U.S. government began the process of privatizing uranium enrichment services by creating the United States Enrichment Corporation (USEC), a wholly owned government corporation, pursuant to the *Energy Policy Act of 1992* (Public Law [P.L.] 102-186). The Paducah and Portsmouth GDPs were leased to USEC, but DOE retained responsibility for storage, maintenance, and disposition of 46,422 DUF<sub>6</sub> cylinders produced before 1993 and located at the three gaseous diffusion plant sites (28,351 at Paducah, 13,388 at Portsmouth, and 4,683 at K-25). In 1996, the *USEC Privatization Act* (P.L. 104-134) transferred ownership of USEC from the government to private investors. This act provided for the allocation of USEC's liabilities between the U.S. government (including DOE) and the new private corporation, including liabilities for DUF<sub>6</sub> cylinders generated by USEC before privatization.

In May and June of 1998, USEC and DOE signed two memoranda of agreement (MOAs) regarding the allocation of responsibilities for depleted uranium generated by USEC after 1993. The two MOAs transferred ownership of a total of 11,400 DUF<sub>6</sub> cylinders from USEC to DOE.

On June 17, 2002, DOE and USEC signed a third agreement to transfer up to 23,300 t (25,684 tons) of DUF<sub>6</sub> from USEC to DOE between 2002 and 2006. The exact number of cylinders was not specified. Transfer of ownership of all the material will take place at Paducah. While title to the DUF<sub>6</sub> is transferred to DOE under this agreement, custody and cylinder management responsibility remains with USEC until DOE requests that USEC deliver the cylinders for processing in the conversion facility.

### Cylinder-Related Terms Used in This EIS

#### Types of UF<sub>6</sub>

UF <sub>6</sub>	A chemical composed of one atom of uranium combined with six atoms of fluorine. UF <sub>6</sub> is a volatile white crystalline solid at ambient conditions.
Normal UF <sub>6</sub>	UF <sub>6</sub> made with uranium that contains the isotope uranium-235 at a concentration equal to that found in nature, that is, 0.7% uranium-235.
DUF <sub>6</sub>	UF <sub>6</sub> made with uranium that contains the isotope uranium-235 in concentrations less than the 0.7% found in nature. In general, the DOE DUF <sub>6</sub> contains between 0.2% and 0.4% uranium-235.
Enriched UF <sub>6</sub>	UF <sub>6</sub> made with uranium containing more than 0.7% uranium-235. In general, DOE enriched UF <sub>6</sub> considered in this EIS contains less than 5% uranium-235.
Reprocessed UF <sub>6</sub>	UF <sub>6</sub> made with uranium that was previously irradiated in a nuclear reactor and chemically separated during reprocessing.

#### Types of Cylinders

Full DUF <sub>6</sub>	Cylinders filled to 62% of their volume with DUF <sub>6</sub> (some cylinders are slightly overfilled).
Partially Full	Cylinders that contain more than 50 lb (23 kg) of DUF <sub>6</sub> but less than 62% of their volume.
Heel	Cylinders that contain less than 50 lb (23 kg) of residual nonvolatile material left after the DUF <sub>6</sub> has been removed.
Empty	Cylinders that have had the DUF <sub>6</sub> and heel material removed and contain essentially no residual material.
Feed	Cylinders used to supply UF <sub>6</sub> into the enrichment process. Most feed cylinders contain natural UF <sub>6</sub> , although some historically contained reprocessed UF <sub>6</sub> .
Non-DUF <sub>6</sub>	A term used in this EIS to refer to cylinders that contain enriched UF <sub>6</sub> or normal UF <sub>6</sub> .

### S.1.1.2 Growing Concern over the DUF<sub>6</sub> Inventory

In May 1995, the Defense Nuclear Facilities Safety Board (DNFSB), an independent DOE oversight organization within the Executive Branch, issued Recommendation 95-1 regarding storage of the DUF<sub>6</sub> cylinders. This document advised that DOE should take three actions: (1) start an early program to renew the protective coating on cylinders containing DUF<sub>6</sub> from the historical production of enriched uranium, (2) explore the possibility of additional measures to protect the cylinders from the damaging effects of exposure to the elements as well as any additional handling that might be called for, and (3) institute a study to determine whether a more suitable chemical form should be selected for long-term storage of depleted uranium.

In response to Recommendation 95-1, DOE began an aggressive effort to better manage its DUF<sub>6</sub> cylinders, known as the *UF<sub>6</sub> Cylinder Project Management Plan*. This plan incorporated more rigorous and more frequent inspections, a multiyear schedule for painting and refurbishing cylinders, and construction of concrete-pad cylinder yards. In December 1999, the DNFSB determined that DOE's implementation of the *UF<sub>6</sub> Cylinder Project Management Plan* was successful, and, as a result, on December 16, 1999, it closed Recommendation 95-1.

Several affected states also expressed concern over the DOE DUF<sub>6</sub> inventory. In October 1992, the Ohio Environmental Protection Agency (OEPA) issued a Notice of Violation (NOV) alleging that DUF<sub>6</sub> stored at the Portsmouth facility is subject to regulation under state hazardous waste laws. The NOV stated that the OEPA had determined DUF<sub>6</sub> to be a solid waste and that DOE had violated Ohio laws and regulations by not evaluating whether such waste was hazardous. DOE disagreed with this assessment and entered into discussions with the OEPA that continued through February 1998, when an agreement was reached. Ultimately, in February 1998, DOE and the OEPA agreed to set aside the issue of whether the DUF<sub>6</sub> is subject to state hazardous waste regulation and instituted a negotiated management plan governing the storage of the Portsmouth DUF<sub>6</sub>. The agreement also requires DOE to continue its efforts to evaluate the potential use or reuse of the material. The agreement expires in 2008.

Similarly, in February 1999, DOE and the Tennessee Department of Environment and Conservation (TDEC) entered into a consent order that included a requirement for the performance of two environmentally beneficial projects: the implementation of a negotiated management plan governing the storage of the small inventory (relative to other sites) of all UF<sub>6</sub> (depleted, enriched, and natural) cylinders stored at the ETTP site and the removal of the DUF<sub>6</sub> from the ETTP site or the conversion of the material by December 31, 2009. The consent order further requires DOE to submit a plan, within 60 days of completing NEPA review of its long-term DUF<sub>6</sub> management strategy, that contains schedules for activities related to removal of cylinders from the ETTP site.

In Kentucky, a final Agreed Order between DOE and the Kentucky Natural Resources and Environmental Protection Cabinet concerning DUF<sub>6</sub> cylinder management was entered in October 2003. This Agreed Order requires that DOE provide the Kentucky Department of Environmental Protection with an inventory of all DUF<sub>6</sub> cylinders for which DOE has management responsibility at the Paducah site and, with regard to that inventory, that DOE implement the DUF<sub>6</sub> Cylinder Management Plan, which is Attachment 1 to the Agreed Order.

### S.1.1.3 Programmatic NEPA Review and Congressional Interest

In 1994, DOE began work on a *Programmatic Environmental Impact Statement for Alternative Strategies for the Long-Term Management and Use of Depleted Uranium Hexafluoride* (DUF<sub>6</sub> PEIS) (DOE/EIS-0269) to evaluate potential broad management options for DOE's DUF<sub>6</sub> inventory. Alternatives considered included continued storage of DUF<sub>6</sub> in cylinders at the gaseous diffusion plant sites or at a consolidated site, and the use of technologies for converting the DUF<sub>6</sub> to a more stable chemical form for long-term storage, use, or disposal. DOE issued the draft DUF<sub>6</sub> PEIS for public review and comment in December 1997 and held hearings near each of the three sites where DUF<sub>6</sub> is currently stored (Paducah, Kentucky; Oak Ridge, Tennessee; and Portsmouth, Ohio) and in Washington, D.C. In response to its efforts, DOE received some 600 comments.

In July 1998, while the PEIS was being prepared, the President signed into law P.L. 105-204. The text of P.L. 105-204 pertinent to the management of DUF<sub>6</sub> is as follows:

(a) *PLAN.* – *The Secretary of Energy shall prepare, and the President shall include in the budget request for fiscal year 2000, a Plan and proposed legislation to ensure that all amounts accrued on the books of the United States Enrichment Corporation for the disposition of depleted uranium hexafluoride will be used to commence construction of, not later than January 31, 2004, and to operate, an onsite facility at each of the gaseous diffusion plants at Paducah, Kentucky, and Portsmouth, Ohio, to treat and recycle depleted uranium hexafluoride consistent with the National Environmental Policy Act.*

DOE began, therefore, to prepare a responsive plan while it proceeded with the PEIS.

On March 12, 1999, DOE submitted the plan to Congress; no legislation was proposed. In April 1999, DOE issued the final DUF<sub>6</sub> PEIS. The PEIS identified conversion of DUF<sub>6</sub> to another chemical form for use or long-term storage as part of the preferred management alternative. In the Record of Decision (ROD) (64 FR 43358, August 10, 1999), DOE decided to promptly convert the DUF<sub>6</sub> inventory to a more stable uranium oxide form. DOE also stated that it would use the depleted uranium oxide as much as possible and store the remaining depleted uranium oxide for potential future uses or disposal, as necessary. In addition, DUF<sub>6</sub> would be converted to depleted uranium metal only if uses for metal were available. DOE did not select a specific site or sites for the conversion facilities but reserved that decision for subsequent NEPA review. (This EIS is that site-specific review.)

Then, in July 1999, DOE issued the *Final Plan for the Conversion of Depleted Uranium Hexafluoride as Required by Public Law 105-204*. The Conversion Plan describes the steps that would allow DOE to convert the DUF<sub>6</sub> inventory to a more stable chemical form. It incorporates information received from the private sector in response to a DOE request for expressions of interest; ideas from members of the affected communities, Congress, and other interested stakeholders; and the results of the analyses for the final DUF<sub>6</sub> PEIS. The Conversion Plan

describes DOE's intent to chemically process the DUF<sub>6</sub> to create products that would present a lower long-term storage hazard and provide a material suitable for use or disposal.

#### **S.1.1.4 DOE Request for Contractor Proposals and Site-Specific NEPA Review**

DOE initiated the Final Conversion Plan on July 30, 1999, and announced the availability of a draft Request for Proposals (RFP) for a contractor to design, construct, and operate DUF<sub>6</sub> conversion facilities at the Paducah and Portsmouth sites.

In early 2000, the RFP was modified to allow for a wider range of potential conversion product forms and process technologies than had been previously reviewed in the DUF<sub>6</sub> PEIS (the PEIS considered conversion to triuranium octaoxide [U<sub>3</sub>O<sub>8</sub>] and uranium dioxide [UO<sub>2</sub>] for disposal and conversion to uranium metal for use). DOE stated that if the selected conversion technology would generate a previously unconsidered product (e.g., depleted uranium tetrafluoride [UF<sub>4</sub>]), DOE would review the potential environmental impacts as part of the site-specific NEPA review.

On October 31, 2000, DOE issued a final RFP to procure a contractor to design, construct, and operate DUF<sub>6</sub> conversion facilities at the Paducah and Portsmouth sites. The RFP stated that any conversion facilities that would be built would have to convert the DUF<sub>6</sub> within a 25-year period to a more stable chemical form that would be suitable for either beneficial use or disposal. The selected contractor would use its proposed technology to design, construct, and operate the conversion facilities for an initial 5-year period. Operation would include (1) maintaining the DUF<sub>6</sub> inventories and conversion product inventories; (2) transporting all UF<sub>6</sub> storage cylinders currently located at ETTP to a conversion facility at the Portsmouth site, as appropriate; and (3) transporting to an appropriate disposal site any conversion product for which no use was found. The selected contractor would also be responsible for preparing such excess material for disposal.

In March 2001, DOE announced the receipt of five proposals in response to the RFP, three of which proposed conversion to U<sub>3</sub>O<sub>8</sub> and two of which proposed conversion to UF<sub>4</sub>. In August 2001, DOE deemed three of these proposals to be within the competitive range; two conversion to U<sub>3</sub>O<sub>8</sub> proposals and one conversion to UF<sub>4</sub> proposal.

On September 18, 2001, DOE published the NOI in the *Federal Register* (66 FR 48123), announcing its intention to prepare an EIS for the proposed action to construct, operate, maintain, and decontaminate and decommission two DUF<sub>6</sub> conversion facilities at Portsmouth, Ohio, and Paducah, Kentucky. DOE held three scoping meetings to provide the public with an opportunity to present comments on the scope of the EIS and to ask questions and discuss concerns with DOE officials regarding the EIS. The scoping meetings were held in Piketon, Ohio, on November 28, 2001; in Oak Ridge, Tennessee, on December 4, 2001; and in Paducah, Kentucky, on December 6, 2001.

The alternatives identified in the NOI included a two-plant alternative (one at the Paducah site and another at the Portsmouth site), a one-plant alternative (only one plant would be

built, at either the Paducah or the Portsmouth site), an alternative using existing UF<sub>6</sub> conversion capacity at commercial nuclear fuel fabrication facilities, and a no action alternative. For alternatives that involved constructing one or two new plants, DOE planned to consider alternative conversion technologies, local siting alternatives within the Paducah and Portsmouth site boundaries, and the shipment of DUF<sub>6</sub> cylinders stored at ETTP to either the Portsmouth site or to the Paducah site. The technologies to be considered in the EIS were those submitted in response to the October 2000 RFP, plus any other technologies that DOE believed must be considered.

#### **S.1.1.5 Public Law 107-206 Passed by Congress**

During the site-specific NEPA review process, Congress acted again regarding DUF<sub>6</sub> management, and on August 2, 2002, the President signed the *2002 Supplemental Appropriations Act for Further Recovery from and Response to Terrorist Attacks on the United States* (P.L. 107-206). The pertinent part of P.L. 107-206 had several requirements: that no later than 30 days after enactment, DOE must select for award of a contract for the scope of work described in the October 2000 RFP, including design, construction, and operation of a DUF<sub>6</sub> conversion facility at each of the Department's Paducah, Kentucky, and Portsmouth, Ohio, gaseous diffusion sites; that the contract require groundbreaking for construction to occur no later than July 31, 2004; that the contract require construction to proceed expeditiously thereafter; that the contract include as an item of performance the transportation, conversion, and disposition of DU contained in cylinders located at ETTP, consistent with environmental agreements between the State of Tennessee and the Secretary of Energy; and that no later than 5 days after the date of groundbreaking for each facility, the Secretary of Energy shall submit to Congress a certification that groundbreaking has occurred. The relevant portions of the Appropriations Act are set forth in Appendix A of this EIS.

In response to P.L. 107-206, on August 29, 2002, DOE awarded a contract to UDS, for construction and operation of two conversion facilities. DOE also reevaluated the appropriate scope of its site-specific NEPA review and decided to prepare two separate EISs, one for the plant proposed for the Paducah site and a second for the Portsmouth site. This change in approach was announced in the *Federal Register* on April 28, 2003 (68 FR 22368).

The two draft site-specific conversion facility EISs were mailed to stakeholders in late November 2003, and a notice of availability was published by the U.S. Environmental Protection Agency (EPA) in the *Federal Register* on November 28, 2003 (68 FR 66824). Comments on the draft EISs were accepted during a 67-day review period, from November 28, 2003, until February 2, 2004. Public hearings on the draft EISs were held near Portsmouth, Ohio, on January 7, 2004; Paducah, Kentucky, on January 13, 2004; and Oak Ridge, Tennessee, on January 15, 2004.

### S.1.1.6 Characteristics of DUF<sub>6</sub>

The gaseous diffusion process uses uranium in the form of UF<sub>6</sub>, primarily because UF<sub>6</sub> can conveniently be used in gaseous form for processing, in liquid form for filling or emptying containers, and in solid form for storage. Solid UF<sub>6</sub> is a white, dense, crystalline material that resembles rock salt. Depleted uranium is uranium that, through the enrichment process, has been stripped of a portion of the uranium-235 that it once contained so that its proportion is lower than the 0.7 percent by weight (wt%) found in nature. The uranium in most of DOE's DUF<sub>6</sub> has between 0.2 wt% and 0.4 wt% uranium-235.

The chemical and physical characteristics of DUF<sub>6</sub> pose potential health risks, and the material is handled accordingly. Uranium and its decay products in DUF<sub>6</sub> emit low levels of alpha, beta, gamma, and neutron radiation. If DUF<sub>6</sub> is released to the atmosphere, it reacts with water vapor in the air to form HF and a uranium oxyfluoride compound called uranyl fluoride (UO<sub>2</sub>F<sub>2</sub>), which can be harmful to human health if inhaled or ingested in sufficient quantities. Uranium is a heavy metal that, in addition to being radioactive, can have toxic chemical effects (primarily on the kidneys) if it enters the bloodstream by means of ingestion or inhalation. HF is an extremely corrosive gas that can damage the lungs and cause death if inhaled at high enough concentrations. In light of such characteristics, DOE stores DUF<sub>6</sub> in a manner designed to minimize the risk to workers, the public, and the environment.

As the inventory of DUF<sub>6</sub> cylinders ages, some cylinders have begun to show evidence of external corrosion. A total of three cylinder breaches have occurred at Portsmouth, five breaches have occurred at ETTP, and three breaches have occurred at Paducah (see text box on next page). However, since DUF<sub>6</sub> is solid at ambient temperatures and pressures, it is not readily released after a cylinder leak or breach due to corrosion. When a hole develops in a cylinder, moist air reacts with the exposed solid DUF<sub>6</sub> and iron, forming a dense plug of solid uranium and iron compounds and a small amount of HF gas. The plug limits the amount of material released from a breached cylinder. When a hole in a cylinder is identified, the cylinder is typically repaired or its contents are transferred to a new cylinder. Following a large release of solid UF<sub>6</sub> (generally only possible if a cylinder is involved in a fire), the UF<sub>6</sub> would slowly react with moisture in the air, forming UO<sub>2</sub>F<sub>2</sub> and HF, which would be dispersed downwind. The presence of a fire can result in a more rapid reaction and a larger release of UO<sub>2</sub>F<sub>2</sub> and HF.

Because reprocessed uranium was enriched in the early years of gaseous diffusion, some of the DUF<sub>6</sub> inventory is contaminated with small amounts of technetium (Tc) and the transuranic (TRU) elements plutonium (Pu), neptunium (Np), and americium (Am). The final RFP for conversion services concluded that any DUF<sub>6</sub> contaminated with TRU elements and Tc at the concentrations expected could be safely handled in a conversion facility. As discussed in this EIS, the risk associated with potential contamination would be relatively small, and those cylinders would be processed in the same manner as cylinders not containing TRU and Tc contamination.

Some of the cylinders manufactured before 1978 were painted with coatings containing polychlorinated biphenyls (PCBs). (Although PCBs are no longer in production in the United States, from the 1950s to the late 1970s, PCBs were added to some paints as fungicides

and to increase durability and flexibility.) The long persistence of PCBs in the environment and the tendency for bioaccumulation in the foodchain has resulted in regulations to prevent their release and distribution in the environment. Potential issues associated with PCB-containing cylinder coatings are addressed in more detail in Appendix B of the EIS. As discussed in Appendix B, the presence of PCBs in the coatings of some cylinders is not expected to result in health and safety risks to workers or the public.

### S.1.2 Purpose and Need

DOE needs to convert its inventory of DUF<sub>6</sub> to a more stable chemical form for use or disposal. This need follows directly from (1) the decision presented in the August 1999 ROD for the PEIS, namely, to begin conversion of the DUF<sub>6</sub> inventory as soon as possible, and (2) P.L. 107-206, which directs DOE to award a contract for construction and operation of conversion facilities at both the Paducah site and the Portsmouth site.

### S.1.3 Proposed Action

The proposed action evaluated in this EIS is to construct and operate a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products. The action includes construction, operation, maintenance, and D&D of the proposed DUF<sub>6</sub> conversion facility at the Portsmouth site; transportation of DUF<sub>6</sub> cylinders from ETTP to Portsmouth for conversion, as well as transportation of the non-DUF<sub>6</sub> cylinders from ETTP to Portsmouth; construction of a new cylinder storage yard at Portsmouth (if required) for ETTP cylinders; transportation of depleted uranium conversion products and waste materials to a disposal facility; transportation and sale of the HF produced as a conversion co-product; and neutralization of HF to CaF<sub>2</sub> and its sale or disposal in

#### Summary Data for Breached Cylinders at the Storage Sites through 2003

##### *Portsmouth Site, three breached cylinders:*

Two identified in 1990 were initiated by mechanical damage during stacking; the damage was not noticed immediately, and subsequent corrosion occurred at the point of damage. The largest breach size was about 9 in. × 18 in. (23 cm × 46 cm); the estimated mass of DUF<sub>6</sub> lost was between 17 and 109 lb (7.7 and 49 kg). The next largest cylinder breach had an area of about 2 in. (5.1 cm) in diameter; the estimated DUF<sub>6</sub> lost was less than 4 lb (1.8 kg). The third breached cylinder occurred in 1996 and was the result of handling equipment knocking off a cylinder plug.

##### *ETTP Site, five breached cylinders:*

Four were identified in 1991 and 1992. Two of these were initiated by mechanical damage during stacking, and two were caused by external corrosion due to prolonged ground contact. The breach areas for these four cylinders were about 2 in. (5.1 cm), 6 in. (15 cm), and 10 in. (25 cm) in diameter for three circular breaches, and 17 in. × 12 in. for a rectangular-shaped breach. The mass of material loss from the cylinders could not be estimated because equipment to weigh the cylinders was not available at the ETTP site. The fifth breach occurred in 1998 and was caused by steel grit blasting, which resulted in a breach at the location of an as-fabricated weld defect (immediately repaired without loss of DUF<sub>6</sub>).

##### *Paducah Site, three breached cylinders:*

One identified in 1992 was initiated by mechanical damage during stacking. The breached area was about 0.06 in. × 2 in. (0.16 cm × 5.1 cm). Estimated material loss was 0. The other two cylinder breaches were identified as breached because of missing cylinder plugs; they were identified between 1998 and 2002. Material loss from these cylinders was not estimated.

the event that the HF product is not sold. The EIS also considers an option of shipping the cylinders stored at ETTP to Paducah rather than to Portsmouth and an option of expanding facility operations.

#### **S.1.4 Scope**

The scope of an EIS refers to the range of actions, alternatives, and impacts it considers. As noted in Section S.1.1.4, on September 18, 2001, DOE published a NOI in the *Federal Register* (66 FR 48123) announcing its intention to prepare an EIS for a proposal to construct, operate, maintain, and decontaminate and decommission two DUF<sub>6</sub> conversion facilities at Portsmouth, Ohio, and Paducah, Kentucky. The NOI announced that the scoping period for the EIS would be open until November 26, 2001. The scoping period was later extended to January 11, 2002. During the scoping process, the public was given six ways to submit comments on the DUF<sub>6</sub> proposal to DOE, including public meetings, mail, facsimile transmission, voice messages, electronic mail, and through a dedicated Web site. DOE held public scoping meetings near Paducah, Kentucky, Portsmouth, Ohio, and Oak Ridge, Tennessee, to give the public an opportunity to present comments on the scope of the EIS and to ask questions and discuss concerns regarding the EIS with DOE officials. The scoping meetings were held in Piketon, Ohio, on November 28, 2001, and in Oak Ridge, Tennessee, on December 4, 2001. Approximately 140 comments were received from about 30 individuals and organizations during the scoping period via all media. These comments were examined to determine the proposed scope of this EIS. Comments were related primarily to five major issues: (1) DOE policy; (2) alternatives; (3) cylinder inventory, maintenance, and surveillance; (4) transportation; and (5) general environmental concerns. Comments received in response to the April 28, 2003, Notice of Change in NEPA Compliance Approach were similar to those made during the public scoping period and were also considered.

The alternatives that are evaluated and compared in this EIS represent reasonable alternatives for converting DUF<sub>6</sub>. Three alternative locations within the Portsmouth site are evaluated in detail in this EIS for the proposed action as well as a no action alternative. In addition, this EIS considers the effects on the Portsmouth conversion facility if an option of shipping the cylinders at ETTP to Paducah is selected (although current proposals call for these cylinders to be shipped to Portsmouth) and an option of expanding the conversion facility operations. These alternatives and options, as well as alternatives considered but not evaluated in detail, are described in more detail in Chapter 2.

#### **S.1.5 Public Review of the Draft EIS**

The two draft site-specific conversion facility EISs were mailed to stakeholders in late November 2003, and a notice of availability was published by the EPA in the *Federal Register* on November 28, 2003 (68 FR 66824). In addition, each EIS was also made available in its entirety on the Internet at the same time, and e-mail notification was sent to those on the project Web site mailing list. Stakeholders were encouraged to provide comments on the draft EISs during a 67-day review period, from November 28, 2003, until February 2, 2004. Comments

could be submitted by calling a toll-free number, by fax, by letter, by e-mail, or through the project Web site. Comments could also be submitted at public hearings held near Portsmouth, Ohio, on January 7, 2004; Paducah, Kentucky, on January 13, 2004; and Oak Ridge, Tennessee, on January 15, 2004. The public hearings were announced on the project Web site and in local newspapers prior to the meetings.

A total of about 210 comments was received during the comment period. The comments received and DOE's responses to those comments are presented in Volume 2 of this EIS. Because of the similarities in the proposed actions and the general applicability of many of the comments to both the Portsmouth and the Paducah site-specific conversion facility EISs, all comments received on both EISs are included in Volume 2. In addition, all comments received were considered in the preparation of both final EISs.

The most common issues raised by reviewers were related to support for the proposed action and preferred alternative, transportation of cylinders, removal of cylinders from the ETTP site, the potential for DOE to accept additional DUF<sub>6</sub> cylinders from other sources, the recently announced USEC American Centrifuge Facility, and general health and safety concerns. Several revisions were made to the two site-specific conversion facility draft EISs on the basis of the comments received (changes are indicated by vertical lines in the right margin of the document). The vast majority of the changes were made to provide clarification and additional detail. Specific responses to each comment received on the draft EISs are presented in Volume 2 of this EIS.

### **S.1.6 Relationship to Other NEPA Reviews**

This DUF<sub>6</sub> Conversion EIS, along with the Paducah conversion facility EIS (DOE/EIS-0359), represent the second level of a tiered environmental review process being used to evaluate and implement DOE's DUF<sub>6</sub> Management Program. The project-level review in these conversion facility EISs incorporates, by reference, the programmatic analysis, as appropriate, from the DUF<sub>6</sub> PEIS published by DOE in 1999.

In addition to the Paducah conversion facility EIS, which is directly related to this EIS, DOE has prepared (or is preparing) other NEPA reviews that are related to the management of DUF<sub>6</sub> or to the current DUF<sub>6</sub> storage sites. These reviews were evaluated and their results taken into consideration in the preparation of this EIS. The related reviews included continued waste management activities, winterization activities associated with cold-standby of the Portsmouth GDP, industrial reuse of sections of the Portsmouth site, long-term management for DOE's inventory of potentially reusable uranium, and waste management activities at the Oak Ridge Reservation.

In addition, DOE prepared a Supplement Analysis for the shipment of up to 1,700 DUF<sub>6</sub> cylinders that meet transportation requirements from ETTP to Portsmouth in fiscal years (FYs) 2003 through 2005. Based on the Supplement Analysis, DOE issued an amended ROD to the PEIS concluding that the estimated impacts for the proposed transport of up to 1,700 cylinders were less than or equal to those considered in the PEIS and that no further NEPA documentation

was required (68 FR 53603). Nonetheless, this EIS considers shipment of all DUF<sub>6</sub> and non-DUF<sub>6</sub> at ETTP to Portsmouth by truck and rail.

### **S.1.7 Organization of This Environmental Impact Statement**

This DUF<sub>6</sub> Conversion EIS consists of two volumes. Volume 1 contains 10 chapters and 8 appendixes. Chapter 1 describes background information, the purpose and need for the DOE action, the scope of the assessment, and related NEPA reviews and other studies. Chapter 2 defines the alternatives and options considered in this EIS. Chapter 3 discusses the environmental setting at the Portsmouth and ETTP sites. Chapter 4 addresses the assumptions, approach, and methods used in the impact analyses. Chapter 5 discusses the potential environmental impacts of the alternatives, and Chapter 6 identifies the major laws, regulations, and other requirements applicable to implementing the alternatives. Chapter 7 lists the cited references used in preparing this EIS, and Chapter 8 lists the names of those who prepared this EIS. Chapter 9 is a glossary of technical terms used in this EIS, and Chapter 10 is a subject matter index.

The eight appendixes in Volume 1 include a summary of the pertinent text from P.L. 107-206 (Appendix A), a discussion of issues associated with potential TRU and Tc contamination (Appendix B), comments received during public scoping and from the Notice of Change in NEPA Compliance Approach (Appendix C), the environmental synopsis prepared to support the DUF<sub>6</sub> conversion procurement process (Appendix D), the potential sale of HF and CaF<sub>2</sub> and estimated health and socioeconomic impacts associated with their use (Appendix E), a description of discipline-specific assessment methodologies (Appendix F), letters of consultation (Appendix G), and the contractor disclosure statement (Appendix H).

Volume 2 of the EIS is the comment response document prepared after the public review of the draft EIS. Volume 2 contains an overview of the public review process, copies of the letters or other documents that contained comments to DOE, and the responses to all comments received.

## **S.2 ALTERNATIVES**

The alternatives considered in this EIS are summarized in Table S-2 and described below.

### **S.2.1 No Action Alternative**

Under the no action alternative, it is assumed that DUF<sub>6</sub> cylinder storage would continue indefinitely at the Portsmouth and ETTP sites. The no action alternative assumes that DOE would continue surveillance and maintenance activities to ensure the continued safe storage of cylinders. Potential environmental impacts are estimated through the year 2039. The year 2039 was selected to be consistent with the PEIS, which evaluated a 40-year cylinder storage period

(1999–2039). In addition, long-term impacts (i.e., occurring after 2039) from potential cylinder breaches are assessed.

Specifically, the activities assumed to occur under no action include routine cylinder inspections, ultrasonic testing of the wall thicknesses of selected cylinders, painting of selected cylinders to prevent corrosion, cylinder yard surveillance and maintenance, and relocation of some cylinders. It was assumed that cylinders would be painted every 10 years. On the basis of these activities, an assessment of the potential impacts on workers, members of the general public, and the environment was conducted.

For assessment purposes in this EIS, two cylinder breach cases were evaluated. In the first case, it was assumed that the planned cylinder maintenance and painting program would maintain the cylinders in a protected condition and control further corrosion. In this case, it was assumed that after the initial painting, some cylinder breaches would occur from handling damage; the total numbers of future breaches estimated to occur through 2039 were 16 for the Portsmouth site and 7 for the ETTP site. In the second case, it was assumed that external corrosion would not be halted by improved storage conditions, cylinder maintenance, and painting. This case was considered in order to account for uncertainties with regard to how effective painting would be in controlling cylinder corrosion and uncertainties in the future painting schedule. In this case, the numbers of future breaches estimated through 2039 were 74 for the Portsmouth site and 213 for the ETTP site.

The estimated numbers of future breaches at the Portsmouth and ETTP sites were used to estimate potential impacts that might occur during the repair of breached cylinders and impacts from releases that might occur during continued cylinder storage.

### S.2.2 Proposed Action Alternatives

The proposed action evaluated in this EIS is to construct and operate a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products. Three alternative locations within the Portsmouth site are evaluated (see Table S-2). The proposed action includes shipping the ETTP cylinders to Portsmouth and construction of a new cylinder storage yard at Portsmouth for the ETTP cylinders, if required. The conversion facility would convert DUF<sub>6</sub> into

#### Alternatives Considered in This EIS

**No Action:** NEPA regulations require evaluation of a no action alternative as a basis for comparing alternatives. In this EIS, the no action alternative is storage of DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders indefinitely in yards at the Portsmouth and ETTP sites, with continued cylinder surveillance and maintenance activities.

**Proposed Action:** Construction and operation of a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products.

**Action Alternatives:** Three action alternatives focus on where to construct the conversion facility within the Portsmouth site (Alternative Locations A, B, and C) The preferred alternative is Location A.

a stable chemical form for beneficial use/reuse and/or disposal. The off-gas from the conversion process would yield aqueous HF, which would be processed and marketed or converted to a solid for sale or disposal. To support the conversion operations, the emptied DUF<sub>6</sub> cylinders would be stored, handled, and processed for reuse as uranium oxide disposal containers to the extent practicable. The time period considered is a construction period of approximately 2 years, an operational period of 18 years, and a 3-year period for the D&D of the facility. Current plans call for construction to begin in the summer of 2004. The assessment is based on the conceptual conversion facility design proposed by the selected contractor, UDS (see text box below).

The action alternatives focus on where to site the conversion facility within the Portsmouth site. The Portsmouth site was evaluated to identify alternative locations for a conversion facility. The three alternative locations identified at the Portsmouth site, denoted Locations A, B, and C, are shown in Figure S-3.

#### **S.2.2.1 Alternative Location A (Preferred Alternative)**

Location A is the preferred location for the conversion facility and is located in the west-central portion of the site, encompassing 26 acres (10 ha). This location has three existing structures that were formerly used to store containerized lithium hydroxide monohydrate. The site was rough graded, and storm water ditch systems were installed. Two railroad spurs existed at one time in this area. One has had the track and ties removed, and the other has fallen into disrepair. This location was identified in the RFP for conversion services as the site for which bidders were to design their proposed facilities.

#### **Proposed Action**

The proposed action in this EIS is construction and operation of a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products. DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders would be transported from ETTP to Portsmouth; and a cylinder storage yard would be constructed at Portsmouth for ETTP cylinders, if required. Three alternative locations within the Portsmouth site are evaluated (Locations A, B, and C).

#### **Conversion Facility Design**

This EIS is based on the conversion facility design being developed by UDS, the selected conversion contractor. At the time the draft EIS was prepared, the UDS design was in the 30% conceptual stage, with several facility design options being considered.

Following the public comment period, the draft EIS was revised on the basis of comments received and on the basis of UDS 100% conceptual facility design. This final EIS identifies and evaluates design options to the extent possible.

### **S.2.2.2 Alternative Location B**

Location B is in the southwest portion of the site and encompasses approximately 50 acres (20 ha). The site has two existing structures built as part of the gas centrifuge enrichment project that was begun in the early 1980s and was terminated in 1985. The open field to the east of the buildings was developed during the same time period; it was rough graded, and storm water systems were installed. USEC is currently in the process of developing and demonstrating an advanced enrichment technology based on gas centrifuges. A license for a lead test facility to be operated at the Portsmouth site was issued by the U.S. Nuclear Regulatory Commission (NRC) in February 2004. The lead facility would be located in the existing gas centrifuge buildings within Location B. In addition, USEC announced in January 2004 that it planned to site its American Centrifuge Facility at Portsmouth, although it did not identify an exact location. Therefore, Location B might not be available for construction of the conversion facility.

### **S.2.2.3 Alternative Location C**

Location C is in the southeast portion of the site and has an area of about 78 acres (31 ha). This location consists of a level to very gently rolling grass field. It was graded during the construction of the Portsmouth site and has been maintained as grass fields since then.

### **S.2.2.4 Conversion Process Description**

The proposed conversion system is based on a proven commercial process in operation at the Framatome Advanced Nuclear Power fuel fabrication facility in Richland, Washington. The UDS dry conversion is a continuous process in which DUF<sub>6</sub> is vaporized and converted to a mixture of uranium oxides (primarily U<sub>3</sub>O<sub>8</sub>) by reaction with steam and hydrogen in a fluidized-bed conversion unit. The hydrogen is generated using anhydrous ammonia (NH<sub>3</sub>). Nitrogen is also used as an inert purging gas and is released to the atmosphere through the building stack as part of the clean off-gas stream. The depleted U<sub>3</sub>O<sub>8</sub> powder is collected and packaged for disposition. The process equipment would be arranged in parallel lines. Each line would consist of two autoclaves, two conversion units, a HF recovery system, and process off-gas scrubbers. The Portsmouth facility would have three parallel conversion lines. Equipment would also be installed to collect the HF co-product and process it into any combination of several marketable products. A backup HF acid neutralization system would be provided to convert up to 100% of the HF acid to CaF<sub>2</sub> for storage, sale, or disposal in the future, if necessary. Figure S-4 is an overall material flow diagram for the conversion facility; Figure S-5 is a conceptual facility site plan. A summary of key facility characteristics is presented in Table S-3.

The conversion facility will be designed to convert 13,500 t (15,000 tons) of DUF<sub>6</sub> per year, requiring 18 years to convert the Portsmouth and ETTP inventories. The footprint of the Portsmouth process building would be approximately 148 ft × 271 ft (45 m × 83 m). The conversion facility would occupy a total of approximately 10 acres (4 ha), with up to 65 acres

**TABLE S-3 Summary of Portsmouth Conversion Facility Parameters**

Parameter/Characteristic	Value
Construction start	2004
Construction period	2 years
Start of operations	2006
Operational period	18 years
Facility footprint	10 acres (4 ha)
Facility throughput	13,500 t/yr (15,000 tons/yr) DUF <sub>6</sub> (≈1,000 cylinders/yr)
Conversion products	
Depleted U <sub>3</sub> O <sub>8</sub>	10,800 t/yr (11,800 tons/yr)
CaF <sub>2</sub>	18 t/yr (20 tons/yr)
70% HF acid	2,500 t/yr (2,800 tons/yr)
49% HF acid	5,800 t/yr (6,300 tons/yr)
Steel (emptied cylinders, if not used as disposal containers)	1,177 t/yr (1,300 tons/yr)

(26 ha) of land disturbed during construction (including temporary construction lay-down areas and utility access). Some of the disturbed areas would be areas cleared for railroad or utility access, not adjacent to the construction area.

The conversion process would generate four conversion products that have a potential use or reuse: depleted U<sub>3</sub>O<sub>8</sub>, HF, CaF<sub>2</sub>, and steel from emptied DUF<sub>6</sub> cylinders (if not used as disposal containers). DOE has been working with industrial and academic researchers for several years to identify potential uses for these products. Some potential uses for depleted uranium exist or are being developed, and DOE believes that a viable market exists for the HF generated during conversion. To take advantage of these to the extent possible, DOE requested in the RFP that the bidders for conversion services investigate and propose viable uses. Table S-4 summarizes the probable disposition paths identified by UDS for each of the conversion products.

### S.2.2.5 Preparation and Transportation of ETTP Cylinders to Portsmouth

DOE proposes to ship the DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders at ETTP to Portsmouth. All shipments of ETTP cylinders would have to be made consistent with U.S. Department of Transportation (DOT) regulations for the shipment of radioactive materials as specified in Title 49 of the CFR (see text box on page S-24). A large number of the ETTP DUF<sub>6</sub> cylinders do not meet the DOT requirements intended to maintain the safety of shipments during both routine and accident conditions. Some cylinders have physically deteriorated such that they no longer meet the DOT requirements. Currently, it is estimated that 1,700 cylinders are DOT compliant.

**TABLE S-4 Summary of Proposed Conversion Product Treatment and Disposition**

Conversion Product	Packaging/Storage	Proposed Disposition	Optional Disposition
Depleted U <sub>3</sub> O <sub>8</sub>	Packaged in emptied cylinders for disposal (bulk bags are an option).	Disposal at Envirocare of Utah, Inc. <sup>a</sup>	Disposal at Nevada Test Site (NTS). <sup>a</sup>
CaF <sub>2</sub>	Packaged for sale or disposal.	Commercial sale pending DOE approval of authorized release limits, as appropriate.	Disposal at Envirocare of Utah, Inc. <sup>a</sup>
HF acid (70% and 49%)	HF would be commercial grade and stored on site until loaded into rail tank cars.	Sale to commercial HF acid supplier pending DOE approval of authorized release limits, as appropriate.	Neutralization of HF to CaF <sub>2</sub> for use or disposal.
Steel (emptied cylinders)	If bulk bags were used for U <sub>3</sub> O <sub>8</sub> disposal, emptied cylinders would be processed for disposal; otherwise used for disposal of U <sub>3</sub> O <sub>8</sub> .	Disposal at Envirocare of Utah, Inc. <sup>a</sup>	Disposal at NTS. <sup>a</sup>

<sup>a</sup> DOE plans to decide the specific disposal location(s) for the depleted U<sub>3</sub>O<sub>8</sub> conversion product after additional appropriate NEPA review. Accordingly, DOE will continue to evaluate its disposal options and will consider any further information or comments relevant to that decision. DOE will give a minimum 45-day notice before making the specific disposal decision and will provide any supplemental NEPA analysis for public review and comment.

Before shipment, each cylinder would be inspected to determine if it met DOT requirements. This inspection would include a record review to determine if the cylinder was overfilled; a visual inspection for damage or defects; a pressure check to determine if the cylinder was overpressurized; and an ultrasonic wall thickness measurement (based on a visual inspection, if necessary). If a cylinder passed the inspection, the appropriate documentation would be prepared, and the cylinder would be loaded directly for shipment.

This EIS considers three options for shipping noncompliant cylinders from ETTP: obtaining an exemption from the DOT to ship the cylinders “as-is” or following repairs, use of cylinder overpacks, and use of a cylinder transfer facility. For an exemption to be granted, DOE would have to demonstrate that the proposed shipments would achieve a level of safety that would be at least equal to the level required by the regulations, likely requiring some type of compensatory measures. An overpack (the second option) is a container into which a cylinder is placed for shipment. The overpack would be designed, tested, and certified to meet all DOT shipping requirements. It would be suitable for containing, transporting, and storing the cylinder contents regardless of cylinder condition. The third option considers the transfer of the DUF<sub>6</sub> from substandard cylinders to new or used cylinders that would meet all DOT requirements. This option could require the construction of a new cylinder transfer facility at ETTP, for which there are no current plans. If a decision were made to construct such a facility, additional NEPA

review would be conducted. Transportation impacts are estimated for shipment by both truck and rail after cylinder preparation.

#### **S.2.2.6 Construction of a New Cylinder Storage Yard at Portsmouth**

It may be necessary to construct an additional yard at Portsmouth for storing the ETTP cylinders, depending on when and at what rate the ETTP cylinders are shipped. DOE is currently in the process of determining if a new yard is required, or if existing storage yard space could be used for the ETTP cylinders. The potential environmental impacts from the construction of a new cylinder storage yard at two possible locations have been included in this EIS to account for current uncertainties (Figure S-6).

#### **S.2.2.7 Option of Shipping ETTP Cylinders to Paducah**

As discussed above, DOE proposes to ship the DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders at ETTP to Portsmouth. However, this EIS considers shipping the ETTP cylinders to Paducah as an option. If the ETTP cylinders were shipped to Paducah, the Portsmouth conversion facility would have to operate for 14 rather than 18 years to convert the Portsmouth inventory. In Chapter 5, this EIS presents a discussion of the potential environmental impacts associated with this reduction in the operational period. Potential impacts associated with transportation of the ETTP cylinders to Paducah are evaluated in detail in the site-specific Paducah conversion facility EIS (DOE/EIS-0359).

#### **Transportation Requirements for DUF<sub>6</sub> Cylinders**

All shipments of UF<sub>6</sub> cylinders have to be made in accordance with applicable DOT regulations for the shipment of radioactive materials; specifically, the provisions of 49 CFR Part 173, Subpart I. The DOT regulations require that each UF<sub>6</sub> cylinder be designed, fabricated, inspected, tested, and marked in accordance with the various engineering standards that were in effect at the time the cylinder was manufactured. The DOT requirements are intended to maintain the safety of shipments during both routine and accident conditions. The following provisions are particularly important relative to DUF<sub>6</sub> cylinder shipments:

1. A cylinder must be filled to less than 62% of the certified volumetric capacity (the fill limit was reduced from 64% to 62% in about 1987).
2. The pressure within a cylinder must be less than 14.8 psia (subatmospheric pressure).
3. A cylinder must be free of cracks, excessive distortion, bent or broken valves or plugs, and broken or torn stiffening rings or skirts, and it must not have a shell thickness that has decreased below a specified minimum value. (Shell thicknesses are assessed visually by a code vessel inspector, and ultrasonic testing may be specified at the discretion of the inspector to verify wall thickness, when and in areas the inspector deems necessary.)
4. A cylinder must be designed so that it will withstand (1) a hydraulic test at an internal pressure of at least 1.4 megapascals (200 psi) without leakage; (2) a free drop test onto a flat, horizontal surface from a height of 1 ft (0.3 m) to 4 ft (1.2 m), depending on the cylinder's mass, without loss or dispersal; and (3) a 30-minute thermal test equivalent to being engulfed in a hydrocarbon fuel/air fire having an average temperature of at least 800°C (1,475°F) without rupture of the containment system.

### **S.2.2.8 Option of Expanding Conversion Facility Operations**

The conversion facility at Portsmouth is currently being designed to process the DOE DUF<sub>6</sub> cylinder inventory at the site over 18 years by using three process lines (see Sections S.2.2.4 and 2.2.2). There are no current plans to operate the conversion facility beyond this time period or to increase the throughput of the facility by adding a fourth process line. However, a future decision to extend conversion facility operations or increase throughput at the site could be made for several reasons. Consequently, this EIS includes an evaluation of the environmental impacts associated with expanding conversion facility operations at the site (either by increasing throughput or by extending operations beyond 18 years) in order to provide future planning flexibility (impacts are discussed in Section S.5.22 and presented in detail in Section 5.2.8). The possible reasons for expanding operations in the future are discussed below.

The DOE Office of Inspector General (OIG) issued a final audit report in March 2004 recommending that the Office of Environmental Management (EM) conduct a cost benefit analysis to determine the optimum size of the Portsmouth conversion facility and, on the basis of the results of that review, implement the most cost-effective approach. The report states that by adding an additional process line to the Portsmouth facility, the time to process the Portsmouth and ETTP inventories of DUF<sub>6</sub> could be shortened by 5 years at a substantial cost savings of 55 million dollars. As stated in the DOE EM response to the OIG report, DOE is not planning to increase the number of process lines within the Portsmouth conversion facility in response to the OIG recommendations. Instead, on the basis of experience with other projects, DOE believes that higher throughput rates can be achieved by improving the efficiency of the planned equipment. Although there are no plans to increase the throughput at the Portsmouth facility by adding an additional process line, the potential environmental impacts associated with increasing the plant throughput, by both process improvements and by the addition of a fourth process line, are evaluated in the EIS (see Section S.5.22).

A future decision to extend operations or expand throughput might also result from the fact that DOE could assume management responsibility for DUF<sub>6</sub> in addition to the current inventory. The possible reasons include future DOE management responsibility for DUF<sub>6</sub> due to regulatory changes or possible MOAs between USEC and DOE; development of an advanced enrichment technology by USEC at Portsmouth that would generate DUF<sub>6</sub> that might be transferred to DOE; and new commercial uranium enrichment facilities that may be built and operated in the United States by commercial companies other than USEC. In addition, because the Portsmouth facility would conclude operations approximately 7 years before the current Paducah inventory would be converted at the Paducah site, it is possible that some DUF<sub>6</sub> cylinders could be transferred from Paducah to Portsmouth, particularly if DOE assumes responsibility for additional DUF<sub>6</sub> at Paducah. These possibilities are discussed and evaluated in this EIS in order to provide future planning flexibility.

### **S.2.3 Alternatives Considered but Not Analyzed in Detail**

#### **S.2.3.1 Use of Commercial Conversion Capacity**

An alternative examined was using existing UF<sub>6</sub> conversion capacity at commercial nuclear fuel fabrication facilities that convert natural or enriched UF<sub>6</sub> to UO<sub>2</sub> in lieu of constructing new conversion capacity for DUF<sub>6</sub>. This alternative was not analyzed in detail because the small capacity possibly available to DOE, coupled with the low interest level expressed by facility owners, indicates that the feasibility of this suggested alternative is low, and the duration of the conversion period is long (more than 125 years).

#### **S.2.3.2 Sites Other Than Portsmouth**

The consideration of alternative sites was limited to alternative locations within the Portsmouth site in response to Congressional direction. As discussed in detail in Section 1.1, Congress has acted twice regarding the construction and operation of DUF<sub>6</sub> conversion facilities at Portsmouth and Paducah. Both P.L. 105-204 and P.L. 107-206 directed DOE to construct and operate conversion facilities at these two sites.

#### **S.2.3.3 Alternative Conversion Processes**

Potential environmental impacts associated with alternative conversion processes were considered during the procurement process, including the preparation of an environmental critique and environmental synopsis (Appendix D of this EIS), which were prepared in accordance with the requirements of 10 CFR 1021.216. The environmental synopsis concluded that, on the basis of assessment of potential environmental impacts presented in the critique, no proposal received by DOE was clearly environmentally preferable. The potential environmental impacts associated with the proposals were found to be similar to, and generally less than, those presented in the DUF<sub>6</sub> PEIS for representative conversion technologies.

#### **S.2.3.4 Long-Term Storage and Disposal Alternatives**

There are no current plans for long-term storage of conversion products; long-term storage alternatives were analyzed in the PEIS, including storage as DUF<sub>6</sub> and storage as an oxide (either U<sub>3</sub>O<sub>8</sub> or UO<sub>2</sub>). The potential environmental impacts from long-term storage were evaluated in the PEIS for representative and generic sites. Therefore, long-term storage alternatives were not evaluated in this EIS.

With respect to disposal, this EIS evaluates the impacts from packaging, handling, and transporting depleted uranium conversion products from the conversion facility to a LLW disposal facility that would be (1) selected in a manner consistent with DOE policies and orders and (2) authorized or licensed to receive the conversion products by DOE (in conformance with

DOE orders), the NRC (in conformance with NRC regulations), or an NRC Agreement State agency (in conformance with state laws and regulations determined to be equivalent to NRC regulations). Assessment of the impacts and risks from on-site handling and disposal at the LLW disposal facility is deferred to the disposal site's site-specific NEPA or licensing documents. However, this EIS covers the impacts from transporting the DUF<sub>6</sub> conversion products to both the Envirocare of Utah, Inc., facility and the NTS. DOE plans to decide the specific disposal location(s) for the depleted U<sub>3</sub>O<sub>8</sub> conversion product after additional appropriate NEPA review. Accordingly, DOE will continue to evaluate its disposal options and will consider any further information or comments relevant to that decision. DOE will give a minimum 45-day notice before making the specific disposal decision and will provide any supplemental NEPA analysis for public review and comment.

#### **S.2.3.5 Other Transportation Modes**

Transportation by air and barge were considered but not analyzed in detail. Transportation by air was deemed to not be reasonable for the types and quantities of materials that would be transported to and from the conversion site. Transportation by barge was also considered and deemed to be unreasonable. ETTP is the only site with a nearby barge facility. Portsmouth would either have to build new facilities or use existing facilities that are located 20 to 30 mi (32 to 48 km) from the Portsmouth site. Use of existing facilities would require on-land transport by truck or rail over the 20- to 30-mi (32- to 48-km) distance, and the cylinders would have to go through one extra unloading/loading step at the end of the barge transport. Currently, there are no initiatives to build new barge facilities closer to the Portsmouth site. If barge shipment was proposed in the future and considered to be reasonable, an additional NEPA review would be conducted.

#### **S.2.3.6 One Conversion Plant for Two Sites**

In the NOI published in the *Federal Register* on September 18, 2001, construction and operation of one conversion plant was identified as a preliminary alternative that would be considered in the conversion EIS. However, with the passage of P.L. 107-206, which mandates the award of a contract for the construction and operation of conversion facilities at both Paducah and Portsmouth, the one conversion plant alternative was considered but not analyzed in this EIS.

### **S.3 AFFECTED ENVIRONMENT**

This EIS considers the proposed action at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories. Chapter 3 presents a detailed description of the affected environment at and around the Portsmouth and ETTP sites. Environmental resources and values that could potentially be affected at Portsmouth and ETTP include the following:

- Cylinder yards,
- Site infrastructure,
- Air quality,
- Noise,
- Soils,
- Surface and groundwater,
- Vegetation,
- Wildlife,
- Wetlands,
- Threatened and endangered species,
- Public and occupational safety and health,
- Socioeconomics,
- Waste management,
- Land use,
- Cultural resources, and
- Environmental justice.

#### **S.4 ENVIRONMENTAL IMPACT ASSESSMENT APPROACH, ASSUMPTIONS, AND METHODOLOGY**

Potential environmental impacts were assessed by examining all of the activities required to implement each alternative, including construction of the required facility, operation of the facility, and transportation of materials between sites (Figure S-7). For continued cylinder storage under the no action alternative, potential long-term impacts from cylinder breaches occurring at Portsmouth and ETTP were also estimated. For each alternative, potential impacts to workers, members of the general public, and the environment were estimated for both normal operations and for potential accidents.

The analysis for this EIS considered all potential areas of impact and emphasized those that might have a significant impact on human health or the environment, would be different under different alternatives, or would be of special interest to the public (such as potential radiation effects). The estimates of potential environmental impacts for the action alternatives were based on characteristics of the proposed UDS conversion facility.

The process of estimating environmental impacts from the conversion of DUF<sub>6</sub> is subject to some uncertainty because final facility designs are not yet available. In addition, the methods used to estimate impacts have uncertainties associated with their results. This EIS impact assessment was designed to ensure — through selection of assumptions, models, and input parameters — that impacts would not be underestimated and that relative comparisons among the alternatives would be valid and meaningful. Although uncertainty may characterize estimates of the absolute magnitude of impacts, a uniform approach to impact assessment enhances the ability to make valid comparisons among alternatives. This uniform approach was implemented in the analyses conducted for this EIS to the extent practicable.

Table S-5 summarizes the major assumptions and parameters that formed the basis of the analyses in this EIS.

## S.5 CONSEQUENCES AND COMPARISON OF ALTERNATIVES

This EIS analyzes potential impacts at the Portsmouth and ETTP sites under both the no action alternative and the proposed action alternatives. Under the no action alternative, potential impacts associated with the continued storage of DUF<sub>6</sub> cylinders in yards are evaluated through 2039; in addition, the long-term impacts that could result from releases of DUF<sub>6</sub> and HF from future cylinder breaches are evaluated. For the proposed action, potential impacts are evaluated at three alternative locations for a construction period of 2 years and an operational period of 18 years; impacts at ETTP from the preparation of cylinders for shipment is also included.

The potential environmental impacts at Portsmouth under the proposed action alternatives and under the no action alternative are presented in Table S-6 (placed at the end of this summary). To supplement the information in Table S-6, each area of impact evaluated in this EIS is discussed below. Major similarities and differences among the alternatives are highlighted. Additional details and discussion are provided in Chapter 5 for each alternative.

### S.5.1 Human Health and Safety — Construction and Normal Facility Operations

Under the no action and action alternatives, it is estimated that potential exposures of workers and members of the general public to radiation and chemicals would be well within applicable public health standards and regulations during normal facility operations (including 10 CFR 835, 40 CFR 61 Subpart H, and DOE Order 5400.5). The estimated doses and risks from radiation and/or chemical exposures of the general public and noninvolved workers would be very low, with zero latent cancer fatalities (LCFs) expected among these groups over the time periods considered, and with minimal adverse health impacts from chemical exposures expected. (Dose and risk estimates are shown in Table S-6.) In general, the location of a conversion facility within the Portsmouth site would not significantly affect potential impacts (i.e., no significant differences in impacts from alternative Locations A, B, or C were identified) to workers or the general public during normal facility operations.

#### Key Concepts in Estimating Risks from Radiation

The health effect of concern from exposure to radiation at levels typical of environmental and occupational exposures is the inducement of cancer. Radiation-induced cancers may take years to develop following exposure and are generally indistinguishable from cancers caused by other sources. Current radiation protection standards and practices are based on the premise that any radiation dose, no matter how small, can result in detrimental health effects (cancer) and that the number of effects produced is in direct proportion to the radiation dose. Therefore, doubling the radiation dose is assumed to result in doubling the number of induced cancers. This approach is called the “linear-no-threshold hypothesis” and is generally considered to result in conservative estimates (i.e., over-estimates) of the health effects from low doses of radiation.

Involved workers (persons directly involved in the handling of radioactive or hazardous materials) could be exposed to low-level radiation emitted by uranium during the normal course

of their work activities, and this exposure could result in a slight increase in the risk for radiation-induced LCFs to individual involved workers. (The possible presence of TRU and Tc contamination in the cylinder inventory would not contribute to exposures during normal operations.) The annual number of workers exposed could range from about 33 (under the no action alternative for Portsmouth and ETTP combined) to 163 under the action alternatives. Under all alternatives, it is estimated that radiation exposure of involved workers would be unlikely to result in additional LCFs among the entire involved worker populations (risks from radiation exposure range from a 1-in-10 chance of one additional LCF among the entire conversion facility involved worker population over the life of the project to a 1-in-5 chance of one additional LCF among the involved cylinder maintenance workers at Portsmouth under the no action alternative).

Possible radiological exposures from using groundwater potentially contaminated as a result of releases from breached cylinders or facility releases were also evaluated. In general, these exposures would be within applicable public health standards and regulations. However, the uranium concentration in groundwater could exceed 20 µg/L (the drinking water guideline used for comparison in this EIS) at some time in the future under the no action alternative if cylinder corrosion was not controlled. This scenario is highly unlikely because ongoing cylinder inspections and maintenance would prevent significant releases from occurring.

## **S.5.2 Human Health and Safety — Facility Accidents**

### **S.5.2.1 Physical Hazards**

Under all alternatives, workers could be injured or killed as a result of on-the-job accidents unrelated to radiation or chemical exposure. On the basis of accident statistics for similar industries, it is estimated that under the no action alternative, zero fatalities and about 70 injuries might occur through 2039 at the Portsmouth and ETTP sites (about 1 injury per year at Portsmouth, and about 0.7 injury per year at ETTP). Under the action alternatives, the risk of physical hazards would not depend on the location of the conversion facility. No fatalities are predicted, but about 11 injuries during conversion facility construction and up to 142 injuries during operations could occur at the conversion facility (about 6 injuries per year during a 2-year construction period and about 8 injuries per year during operations). In addition, 1 injury would be expected from construction of a new cylinder yard for ETTP cylinders. Accidental injuries and deaths are not unusual in industries that use heavy equipment to manipulate heavy objects and bulk materials.

### **S.5.2.2 Facility Accidents Involving Radiation or Chemical Releases**

Under all alternatives, it is possible that accidents could release radiation or chemicals to the environment, potentially affecting both the workers and members of the general public. Of all the accidents considered, those involving DUF<sub>6</sub> cylinders and those involving chemicals at the conversion facility would have the largest potential effects.

The DUF<sub>6</sub> Management Plan (DOE 1996e) outlines required cylinder maintenance activities and procedures to be undertaken in the event of a cylinder breach and/or release of DUF<sub>6</sub> from one or more cylinders. Under all alternatives, there is a low probability that accidents involving DUF<sub>6</sub> cylinders could occur at the current storage locations. If an accident occurred, DUF<sub>6</sub> could be released to the environment. The DUF<sub>6</sub> would combine with moisture in the air, forming gaseous HF and UO<sub>2</sub>F<sub>2</sub>, a soluble solid in the form of small particles. The depleted uranium and HF could be dispersed downwind, potentially exposing workers and members of the general public to radiation and chemical effects. The amount released would depend on the severity of the accident and the number of cylinders involved. The probability of cylinder accidents would decrease under the action alternatives as the DUF<sub>6</sub> was converted and the number of cylinders in storage decreased as a result.

For releases involving DUF<sub>6</sub> and other uranium compounds, both chemical and radiological effects could occur if the material was ingested or inhaled. The chemical effect of most concern associated with internal uranium exposure is kidney damage, and the radiological effect of concern is an increase in the probability of developing cancer. With regard to uranium, chemical effects occur at lower exposure levels than do radiological effects. Exposure to HF from accidental releases could result in a range of health effects, from eye and respiratory irritation to death, depending on the exposure level. Large anhydrous NH<sub>3</sub> releases could also cause severe respiratory irritation and death (NH<sub>3</sub> is used to generate hydrogen, which is required for the conversion process).

Chemical and radiological exposures to involved workers under accident conditions would depend on how rapidly the accident developed, the exact location and response of the workers, the direction and amount of the release, the physical forces causing or caused by the accident, meteorological conditions, and the characteristics of the room or building if the accident occurred indoors. Impacts to involved workers under accident conditions would likely be dominated by physical forces from the accident itself; thus, quantitative dose/effect estimates would not be meaningful. For these reasons, the impacts to involved workers during accidents are not quantified in this EIS. However, it is recognized that injuries and fatalities among involved workers would be possible if an accident did occur.

### Health Effects from Accidental Chemical Releases

The impacts from accidental chemical releases were estimated by determining the numbers of people downwind who might experience adverse effects and irreversible adverse effects:

**Adverse Effects:** Any adverse health effects from exposure to a chemical release, ranging from mild and transient effects, such as respiratory irritation or skin rash (associated with lower chemical concentrations), to irreversible (permanent) effects, including death or impaired organ function (associated with higher chemical concentrations).

**Irreversible Adverse Effects:** A subset of adverse effects, irreversible adverse effects are those that generally occur at higher concentrations and are permanent in nature. Irreversible effects may include death, impaired organ function (such as central nervous system or lung damage), and other effects that may impair everyday functions.

Under the no action alternative, for accidents involving cylinders that might happen at least once in 100 years (i.e., likely accidents), it is estimated that the off-site concentrations of HF and uranium would be considerably below levels that would cause adverse chemical effects among members of the general public from exposure to these chemicals (see text box). However, up to 70 noninvolved workers might experience potential adverse effects from exposure to HF and uranium (mild and temporary effects, such as respiratory irritation or temporary decrease in kidney function). It is estimated that up to 3 noninvolved workers would experience potential irreversible adverse effects that are permanent in nature (such as lung damage or kidney damage); no fatalities are expected. Radiation exposures would be unlikely to result in additional LCFs among noninvolved workers or members of the general public for these types of accidents.

Cylinder accidents that are less likely to occur could be more severe, having greater consequences that could potentially affect off-site members of the general public. These types of accidents are considered extremely unlikely, expected to occur with a frequency of between once in 10,000 years and once in 1 million years of operations. Based on the expected frequency, through 2039, the probability of this type of accident was estimated to be about 1 chance in 2,500. Among all the cylinder accidents analyzed, the postulated accident that would result in the largest number of people with adverse effects (including mild and temporary as well as permanent effects) would be an accident that involves rupture of cylinders in a fire. If this type of accident occurred at the Portsmouth site, it is estimated that up to 680 members of the general public and up to 1,000 noninvolved workers might experience adverse chemical effects from HF and uranium exposure (mild and temporary effects, such as respiratory irritation or temporary decrease in kidney function).

The postulated cylinder accident that would result in the largest number of persons with irreversible adverse health effects is a corroded cylinder spill under wet conditions, with an estimated frequency of between once in 10,000 years and once in 1 million years of operations. If this accident occurred, it is estimated that 1 member of the general public and up to 140 noninvolved workers might experience irreversible adverse effects (such as lung damage or kidney damage). No fatalities are expected among members of the general public; there would be a potential for 1 fatality among noninvolved workers from chemical effects. Radiation exposures would be unlikely to result in additional LCFs among noninvolved workers (1 chance in 100) or the general public (1 chance in 30).

#### **Accident Categories and Frequency Ranges**

***Likely:*** Accidents estimated to occur one or more times in 100 years of facility operations (frequency  $\geq 1 \times 10^{-2}/\text{yr}$ ).

***Unlikely:*** Accidents estimated to occur between once in 100 years and once in 10,000 years of facility operations (frequency = from  $1 \times 10^{-2}/\text{yr}$  to  $1 \times 10^{-4}/\text{yr}$ ).

***Extremely Unlikely:*** Accidents estimated to occur between once in 10,000 years and once in 1 million years of facility operations (frequency = from  $1 \times 10^{-4}/\text{yr}$  to  $1 \times 10^{-6}/\text{yr}$ ).

***Incredible:*** Accidents estimated to occur less than one time in 1 million years of facility operations (frequency  $< 1 \times 10^{-6}/\text{yr}$ ).

In addition to the cylinder accidents discussed above is a certain class of accidents that the DOE investigated; however, because of security concerns, information about such accidents is not available for public review but is presented in a classified appendix to the EIS. All classified information will be presented to state and local officials, as appropriate.

The number of persons actually experiencing adverse or irreversible adverse effects from cylinder accidents would likely be considerably fewer than those estimated for this analysis and would depend on the actual circumstances of the accident and the individual chemical sensitivities of the affected persons. For example, although exposures to releases from cylinder accidents could be life-threatening (especially with respect to immediate effects from inhalation of HF at high concentrations), the guideline exposure level of 20 parts per million (ppm) of HF used to estimate the potential for irreversible adverse effects from HF exposure is likely to result in overestimates. This is because no animal or human deaths have been known to occur as a result of acute exposures (i.e., 1 hour or less) at concentrations of less than 50 ppm; generally, if death does not occur quickly after HF exposure, recovery is complete.

Similarly, the guideline intake level of 30 mg used to estimate the potential for irreversible adverse effects from the intake of uranium in this EIS is the level suggested in NRC guidance. This level is somewhat conservative; that is, it is intended to overestimate rather than underestimate the potential number of irreversible adverse effects in the exposed population following uranium exposure. In more than 40 years of cylinder handling activities, no accidents involving releases from cylinders containing *solid* UF<sub>6</sub> have occurred that have caused diagnosable irreversible adverse effects among workers. In previous accidental exposure incidents involving *liquid* UF<sub>6</sub> in gaseous diffusion plants, some worker fatalities occurred immediately after the accident as a result of inhalation of HF generated from the UF<sub>6</sub>. However, no fatalities occurred as a result of the toxicity of the uranium exposure. A few workers were exposed to amounts of uranium estimated to be about three times the guideline level (30 mg) used for assessing irreversible adverse effects; none of these workers, however, actually experienced such effects.

Under the action alternatives, low-probability accidents involving chemicals at the conversion facility could have large potential consequences for noninvolved workers and members of the general public. At a conversion site, accidents involving chemical releases, such as NH<sub>3</sub> and HF, could occur. NH<sub>3</sub> is used to generate hydrogen for conversion, and HF can be produced as a co-product of converting DUF<sub>6</sub>. Although the UDS proposal uses NH<sub>3</sub> to generate hydrogen, hydrogen can also be produced using natural gas. In that case, the accident impacts would be less than those discussed in this section for NH<sub>3</sub> accidents. (Details about potential NH<sub>3</sub> and other accidents are in Section 5.2.3.2 [conversion facility] and Section 5.2.5 [transportation].)

The conversion accident estimated to have the largest potential consequences is an accident involving the rupture of tanks containing either 70% HF or anhydrous NH<sub>3</sub>. Such an accident could be caused by a large earthquake and is expected to occur with a frequency of less than once in 1 million years of operations. The probability of this type of accident occurring during the operation of a conversion facility is a function of the period of operation; over 18 years of operations, the accident probability would be less than 1 chance in 56,000.

If an aqueous HF or anhydrous NH<sub>3</sub> tank ruptured at the conversion facility, a maximum of up to about 2,300 members of the general public might experience adverse effects (mild and temporary effects, such as respiratory irritation or temporary decrease in kidney function) as a result of chemical exposure. A maximum of about 210 people might experience irreversible adverse effects (such as lung damage or kidney damage), with the potential for about 4 fatalities. With regard to noninvolved workers, up to about 1,400 workers might experience adverse effects (mild and temporary) as a result of chemical exposures. A maximum of about 1,400 noninvolved workers might experience irreversible adverse effects, with the potential for about 30 fatalities.

The location of the conversion facility within the Portsmouth site would affect the number of noninvolved workers and the general public who might experience adverse or irreversible adverse effects from an HF or anhydrous NH<sub>3</sub> tank rupture accident. However, the differences among the locations within each site would generally be small and within the uncertainties associated with the exact accident sequence and weather conditions at the time of the accident. An exception would be that the number of noninvolved workers impacted would be higher for Location B for both potential adverse and irreversible adverse effects.

Although such high-consequence accidents at a conversion facility are possible, they are expected to be extremely rare. The risk (defined as consequence × probability) for these accidents would be less than 1 fatality and less than 1 irreversible adverse health effect for noninvolved workers and members of the public combined. NH<sub>3</sub> and HF are commonly used for industrial applications in the United States, and there are well-established accident prevention and mitigative measures for HF and NH<sub>3</sub> storage tanks. These include storage tank siting principles, design recommendations, spill detection measures, and containment measures. These measures would be implemented, as appropriate.

Under the action alternatives, the highest consequence radiological accident is estimated to be an earthquake damaging the depleted U<sub>3</sub>O<sub>8</sub> product storage building. If this accident occurred, it is estimated that about 135 lb (61 kg) of depleted U<sub>3</sub>O<sub>8</sub> would be released to the atmosphere outside of the building. The maximum collective doses received by the general public and noninvolved workers would be about 30 person-rem and 530 person-rem, respectively. There would be about a 1-in-50 chance of an LCF among the general public and a 1-in-5 chance of an LCF among the noninvolved workers. Because the accident has a probability of occurrence that is about 1 chance in 6,000, the risk posed by the accident would be essentially zero LCFs among both the public and the workers.

### **S.5.3 Human Health and Safety — Transportation**

Under the no action alternative, only small amounts of the LLW and low-level radioactive mixed waste (LLMW) that would be generated during routine cylinder maintenance activities would require transportation (about one shipment per year). Only negligible impacts are expected from such shipments. No DUF<sub>6</sub> or non-DUF<sub>6</sub> cylinders would be transported between sites.

Under the action alternatives, the total number of shipments would include the following:

1. If U<sub>3</sub>O<sub>8</sub> was disposed of in emptied cylinders, there would be approximately 4,200 railcar shipments of depleted U<sub>3</sub>O<sub>8</sub> from the conversion facility to Envirocare (proposed) or NTS (option), or up to 21,000 truck shipments (alternative) to either Envirocare or NTS. The numbers of shipments would be about 8,800 for trucks or 2,200 for railcars if bulk bags were used as disposal containers.
2. About 8,200 truck or 1,640 railcar shipments of aqueous (70% and 49%) HF could occur; alternatively, the aqueous HF could be neutralized to CaF<sub>2</sub>, requiring a total of about 13,600 truck or 3,400 railcar shipments. Currently, the destination for these shipments is not known.
3. About 700 truck or 350 railcar shipments of anhydrous NH<sub>3</sub> from a supplier to the site. Currently, the origin of these shipments is not known.
4. Emptied heel cylinders to Envirocare or NTS, if bulk bags were used to dispose of the depleted U<sub>3</sub>O<sub>8</sub>.
5. Approximately 5,400 truck or 1,400 railcar shipments of cylinders from ETTP to Portsmouth.

During normal transportation operations, radioactive material and chemicals would be contained within their transport packages. Health impacts to crew members (i.e., workers) and members of the general public along the routes could occur if they were exposed to low-level external radiation in the vicinity of uranium material shipments. In addition, exposure to vehicle emissions (engine exhaust and fugitive dust) could potentially cause latent fatalities from inhalation.

The risk estimates for emissions are based on epidemiological data that associate mortality rates with particulate concentrations in ambient air. (Increased latent mortality rates resulting from cardiovascular and pulmonary diseases have been linked to incremental increases in particulate concentrations.) Thus, the increase in ambient air particulate concentrations caused by a transport vehicle, with its associated fugitive dust and diesel exhaust emissions, is related to such premature latent fatalities in the form of risk factors. Because of the conservatism of the assumptions made to reconcile results among independent epidemiological studies and associated uncertainties, the latent fatality risks estimated for normal vehicle emissions should be considered to be an upper bound.<sup>3</sup> For the transport of conversion products and co-products (depleted U<sub>3</sub>O<sub>8</sub>, aqueous HF, and emptied cylinders, if not used as disposal containers), it is conservatively estimated that a total of about 10 fatalities from vehicle emissions could occur if

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<sup>3</sup> For perspective, in a recently published EIS for a geologic repository at Yucca Mountain, Nevada, the same risk factors were used for vehicle emissions; however, they were adjusted to reduce the amount of conservatism in the estimated health impacts. As reported in the Yucca Mountain EIS, the adjustments resulted in a reduction in the emission risks by a factor of about 30.

shipments were only by truck and if aqueous HF product was sold and transported 620 mi (1,000 km) from the site (about 20 fatalities are estimated if HF was neutralized to CaF<sub>2</sub> and transported 620 mi [1,000 km] from the site). The number of fatalities occurring from exhaust emissions if shipment were only by rail would be less than 1 if the HF was sold and about 1 if the HF was neutralized to CaF<sub>2</sub>.

Exposure to external radiation during normal transportation operations is estimated to cause less than 1 LCF under both truck and rail options. Members of the general public living along truck and rail transportation routes would receive extremely small doses of radiation from shipments, less than 0.1 mrem over the duration of the program. This would be true even if a single person was exposed to every shipment of radioactive material during the program.

Traffic accidents could occur during the transportation of radioactive materials and chemicals. These accidents could potentially affect the health of workers (i.e., crew members) and members of the general public, either from the accident itself or from accidental releases of radioactive materials or chemicals.

The total number of traffic fatalities (unrelated to the type of cargo) was estimated on the basis of national traffic statistics on shipments by both truck and rail. If the aqueous HF was sold, about 1 traffic fatality would be estimated under both transportation modes. If HF was neutralized to CaF<sub>2</sub>, about 2 fatalities would be estimated for the truck option and 1 fatality for the rail option.

Severe transportation accidents could also result in a release of radioactive material or chemicals from a shipment. The consequences of such a release would depend on the material released, location of the accident, and atmospheric conditions at the time. Potential consequences would be greatest in urban areas because more people could be exposed. Accidents that occurred when the atmospheric conditions were very stable (typical of nighttime) would have higher potential consequences than accidents that occurred when the conditions were unstable (i.e., turbulent, typical of daytime) because the stability would determine how quickly the released material dispersed and diluted to lower concentrations as it moved downwind.

For the action alternatives, the highest potential accident consequences during transportation activities would be caused by a rail accident involving anhydrous NH<sub>3</sub>. Although anhydrous NH<sub>3</sub> is a hazardous gas, it has many industrial applications and is commonly safely transported by industry as a pressurized liquid in trucks and rail tank cars.

The occurrence of a severe anhydrous NH<sub>3</sub> railcar accident in a highly populated urban area under stable atmospheric conditions is extremely rare. The probability of such an accident occurring if all the anhydrous NH<sub>3</sub> needed was transported 620 mi (1,000 km) is estimated to be less than 1 chance in 400,000. Nonetheless, if such an accident (i.e., release of anhydrous NH<sub>3</sub> from a railcar in a densely populated urban area under stable atmospheric conditions) occurred, up to 5,000 persons might experience irreversible adverse effects (such as lung damage), with the potential for about 100 fatalities. If the same type of NH<sub>3</sub> rail accident occurred in a typical rural area, which would have a smaller population density than an urban area, potential impacts would be considerably less. It is estimated that in a rural area, approximately 20 persons might

experience irreversible adverse effects, with no expected fatalities. The atmospheric conditions at the time of an accident would also significantly affect the consequences of a severe NH<sub>3</sub> accident. The consequences of an NH<sub>3</sub> accident would be less severe under unstable conditions, the most likely conditions in the daytime. Unstable conditions would result in more rapid dispersion of the airborne NH<sub>3</sub> plume and lower downwind concentrations. Under unstable conditions in an urban area, approximately 400 persons could experience irreversible adverse effects, with the potential for about 8 fatalities. If the accident occurred in a rural area under unstable conditions, 1 person would be expected to experience an irreversible adverse effect, with zero fatalities expected. When the probability of an NH<sub>3</sub> accident occurring is taken into account, it is expected that no irreversible adverse effects and no fatalities would occur over the shipment period.

For perspective, anhydrous NH<sub>3</sub> is routinely shipped commercially in the United States for industrial and agricultural applications. On the basis of information provided in the DOT *Hazardous Material Incident System (HMIS) Database* for 1990 through 2002, 2 fatalities and 19 major injuries to the public or to transportation or emergency response personnel have occurred as a result of anhydrous NH<sub>3</sub> releases during nationwide commercial truck and rail operations. These fatalities and injuries occurred during transportation or loading and unloading operations. Over that period, truck and rail NH<sub>3</sub> spills resulted in more than 1,000 and 6,000 evacuations, respectively. Five very large spills, more than 10,000 gal (38,000 L), have occurred; however, these spills were all en route derailments from large rail tank cars. The two largest spills, both around 20,000 gal (76,000 L), occurred in rural or lightly populated areas and resulted in 1 major injury. Over the past 30 years, the safety record for transporting anhydrous NH<sub>3</sub> has significantly improved. Safety measures contributing to this improved safety record include the installation of protective devices on railcars, fewer derailments, closer manufacturer supervision of container inspections, and participation of shippers in the Chemical Transportation Emergency Center.

After anhydrous NH<sub>3</sub>, the types of accidents that are estimated to result in the second highest consequences are those involving shipment of 70% aqueous HF produced during the conversion process. The estimated numbers of irreversible adverse effects for 70% HF rail accidents are about one-third of those from the anhydrous NH<sub>3</sub> accidents. However, the number of estimated fatalities is about one-sixth of those from NH<sub>3</sub> accidents, because the percent of fatalities among the individuals experiencing irreversible adverse effects is 1% as opposed to 2% for NH<sub>3</sub> exposures. For perspective, since 1971, the period covered by DOT records, no fatal or serious injuries to the public or to transportation or emergency response personnel have occurred as a result of anhydrous HF releases during transportation. (Most of the HF transported in the United States is anhydrous HF, which is more hazardous than aqueous HF.) Over that period, 11 releases from railcars were reported to have no evacuations or injuries associated with them. The only major release (estimated at 6,400 lb [29,000 kg] of HF) occurred in 1985 and resulted in approximately 100 minor injuries. Another minor HF release during transportation occurred in 1990. The safety record for transporting HF has improved in the past 10 years for the same reasons as those discussed above for NH<sub>3</sub>. Transportation accidents involving the shipment of DUF<sub>6</sub> cylinders were also evaluated, with the estimated consequences being less than those discussed above for NH<sub>3</sub> and HF (see Section 5.2.5.3).

### S.5.4 Air Quality and Noise

Under the no action alternative, air quality from construction and operations would be within national and state ambient air quality standards. If continued cylinder maintenance and painting are effective in controlling corrosion, as expected, concentrations of HF would be kept within air quality standards at the Portsmouth and ETTP sites. If cylinder corrosion was not controlled, the maximum 24-hour HF concentration at the ETTP site boundary could be about equal to the Tennessee primary standard of 2.9  $\mu\text{g}/\text{m}^3$  around the year 2020 (standards would not be exceeded at Portsmouth). However, because of the on-going cylinder maintenance program, it is not expected that this high breach rate would occur at the ETTP site.

Under the action alternatives, air quality impacts during construction were found to be similar for all three alternative locations. The total (modeled plus the measured background value representative of the site) concentrations due to emissions of most criteria pollutants — such as sulfur dioxide ( $\text{SO}_2$ ), nitrogen oxides ( $\text{NO}_x$ ), and carbon monoxide (CO) — would be well within applicable air quality standards. As is often the case for construction, the primary concern would be particulate matter (PM) released from near-ground-level sources. Total concentrations of  $\text{PM}_{10}$  and  $\text{PM}_{2.5}$  (PM with an aerodynamic diameter of 10  $\mu\text{m}$  or less and 2.5  $\mu\text{m}$  or less, respectively) at the construction site boundaries would be close to or above the standards because of the high background concentrations and the proximity of the new cylinder yard and the proposed conversion facility to potentially publicly accessible areas. The background data used are the maximum values from the last 5 years of monitoring at the nearest monitoring location (operated by the Ohio Environmental Protection Agency [OEPA]) to the site, located about 20 mi (32 km) away in the town of Portsmouth. On the basis of these values, exceedance of the annual  $\text{PM}_{2.5}$  standard would be unavoidable, because the background concentration already exceeds the standard (background is 24.1  $\mu\text{g}/\text{m}^3$ , in comparison with the standard of 15  $\mu\text{g}/\text{m}^3$ ). Accordingly, construction activities should be conducted so as to minimize further impacts on ambient air quality. To mitigate impacts, water could be sprayed on disturbed areas more often, and dust suppressant or pavement could be applied to roads with frequent traffic.

During operations, it is estimated that total concentrations for all annual average criteria pollutants except  $\text{PM}_{2.5}$  would be well within standards. The background level of  $\text{PM}_{2.5}$  in the area of the Portsmouth site approaches or already exceeds the standard. Again, impacts during operations were found to be similar for all three alternative locations.

Noise impacts are expected to be negligible under the no action alternative. Under the action alternatives, estimated noise levels at the nearest residence (located 0.9 km [0.6 mi] from the alternative locations) would be below the U.S. Environmental Protection Agency (EPA) guideline of 55 dB(A)<sup>4</sup> as day-night average sound level (DNL)<sup>5</sup> for residential zones during construction and operations.

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<sup>4</sup> dB(A) is a unit of weighted sound-pressure level, measured by the use of the metering characteristics and the A-weighting specified in the *American National Standard Specification for Sound Level Meters*, ANSI S1.4-1983, and in Amendment S1.4A-1985.

<sup>5</sup> DNL is the 24-hour average sound level, expressed in dB(A), with a 10-dB penalty artificially added to the nighttime (10 p.m.–7 a.m.) sound level to account for noise-sensitive activities (e.g., sleep) during these hours.

### S.5.5 Water and Soil

Under the no action alternative, uranium concentrations in surface water, groundwater, and soil would remain below guidelines throughout the project duration. However, if cylinder maintenance and painting were not effective in reducing cylinder corrosion rates, the uranium concentration in groundwater could be greater than the guideline at both the Portsmouth and ETTP sites at some time in the future (no earlier than about 2100). If continued cylinder maintenance and painting were effective in controlling corrosion, as expected, groundwater uranium concentrations would remain less than the guideline.

During construction of the conversion facility, construction material spills could contaminate surface water, groundwater, or soil. However, by implementing storm water management, sediment and erosion controls (e.g., temporary and permanent seeding; mulching and matting; sediment barriers, traps, and basins; silt fences; runoff and earth diversion dikes), and good construction practices (e.g., covering chemicals with tarps to prevent interaction with rain, promptly cleaning up any spills), concentrations in soil and wastewater (and therefore surface water and groundwater) could be kept well within applicable standards or guidelines.

During operations, no appreciable impacts on surface water, groundwater, or soils would result from the conversion facility because no contaminated liquid effluents are anticipated, and because airborne emission would be at very low levels (e.g., <0.25 g/yr of uranium). Impacts among the three alternative locations would be similar.

### S.5.6 Socioeconomics

The socioeconomic analysis evaluates the effects of construction and operation of a new cylinder yard and conversion facility on population, employment, income, regional growth, housing, and community resources in the region of influence (ROI) around the site. In general, socioeconomic impacts tend to be positive, creating jobs and income, with only minor impacts on housing, public finances, and employment in local public services.

The no action alternative would result in a small socioeconomic impact at both the Portsmouth and ETTP sites combined, creating a total of 130 jobs during operations (direct and indirect jobs) and generating a total of \$5.3 million in personal income per operational year. No significant impacts on regional growth and housing, local finances, and public service employment in the ROI are expected.

Under the action alternatives, jobs and income would be generated during both construction and operation. Construction of the conversion facility would create 280 jobs (direct and indirect) and generate \$9 million in personal income in the peak construction year (construction occurs over a 2-year period). Operation of the conversion facility would create 320 jobs and generate \$13 million in personal income each year. No significant impacts on regional growth and housing, local finances, and public service employment in the ROI are expected. The socioeconomic impacts are not dependent on the location of the conversion facility; therefore, the impacts would be the same for alternative Locations A, B, and C.

### S.5.7 Ecology

Under the no action alternative, continued cylinder maintenance and surveillance activities would have negligible impacts on ecological resources (i.e., vegetation, wildlife, threatened and endangered species). No yard reconstruction is planned for either the Portsmouth or ETTP sites. It is estimated that potential concentrations of contaminants in the environment from future cylinder breaches would be below levels harmful to biota. However, there is a potential for impacts to aquatic biota from cylinder yard runoff during painting activities.

For the action alternatives, the total area disturbed during conversion facility construction would be 65 acres (26 ha). Vegetation communities would be impacted in this area with a loss of habitat. However, for all three alternative locations, impacts could be minimized depending on exactly where the facility was placed within each location. These habitat losses would constitute less than 1% of available land at the site. It was found that concentrations of contaminants in the environment during operations would be below harmful levels. Negligible impacts to vegetation and wildlife are expected at all locations.

Wetlands at or near Locations A, B, and C could be adversely affected at the Portsmouth site. Impacts to wetlands could be minimized depending on where exactly the facility was placed within each location. Unavoidable impacts to wetlands that are within the jurisdiction of the U.S. Army Corps of Engineers may require a Clean Water Act (CWA) Section 404 Permit, which would trigger the requirement for a CWA 401 water quality certification from Ohio. Impacts at Location A may potentially be avoided by an alternative routing of the entrance road, or mitigation may be developed in coordination with the appropriate regulatory agencies. A mitigation plan might be required prior to the initiation of construction.

Construction of the conversion facility should not directly affect federal- or state-listed species. However, impacts on deciduous forest might occur. Impacts to forested areas could be avoided if temporary construction areas were placed in previously disturbed locations. Trees with exfoliating bark, such as shagbark hickory or dead trees with loose bark, can be used by the Indiana bat (federal- and state-listed as endangered) as roosting trees during the summer. There is a potential that such trees could be disturbed during construction at Locations A or C at Portsmouth. If either live or dead trees with exfoliating bark are encountered on construction areas, they should be saved if possible. If necessary, the trees should be cut before April 15 or after September 15.

### S.5.8 Waste Management

Under the no action alternative, LLW, LLMW, and PCB-containing waste could be generated from cylinder scraping and painting activities. The amount of wastes generated would represent an increase of less than 1% in the sites' loads of these wastes, representing negligible impacts on site waste management operations.

Under the action alternatives, waste management impacts would not depend on the location of the facility within the site and would be the same for alternative Locations A, B,

and C. Waste generated during construction and operations would have negligible impacts on the Portsmouth site waste management operations, with the exception of possible impacts from disposal of CaF<sub>2</sub>. Industrial experience indicates that HF, if produced, would contain only trace amounts of depleted uranium (less than 1 ppm). It is expected that HF would be sold for use. If sold for use, the sale would be subject to review and approval by DOE in coordination with the NRC, depending on the specific use (as discussed in Appendix E of this EIS).

The U<sub>3</sub>O<sub>8</sub> produced during conversion would generate about 4,700 yd<sup>3</sup> (3,570 m<sup>3</sup>) per year of LLW. This is 5% of Portsmouth's annual projected volume and would have a low impact on site LLW management.

If the HF was not sold but instead neutralized to CaF<sub>2</sub>, it is currently unknown whether (1) the CaF<sub>2</sub> could be sold, (2) the low uranium content would allow the CaF<sub>2</sub> to be disposed of as nonhazardous solid waste, or (3) disposal as LLW would be required. The low level of uranium contamination expected (i.e., less than 1 ppm) suggests that sale or disposal as nonhazardous solid waste would be most likely. If sold for use, the sale would be subject to review and approval by DOE in coordination with the NRC, depending on the specific use. Waste management for disposal as nonhazardous waste could be handled through appropriate planning and design of the facilities. If the CaF<sub>2</sub> had to be disposed of as LLW, it could represent a potentially large impact on waste management operations.

A small quantity of TRU could be entrained in the gaseous DUF<sub>6</sub> during the cylinder emptying operations. These contaminants would be captured in the filters between the cylinders and the conversion equipment. The filters would be monitored and replaced routinely to maintain concentrations below regulatory limits for TRU waste. The spent filters would be disposed of as LLW, generating up to 25 drums of LLW waste over the life of the project.

Current UDS plans are to leave the heels in the emptied cylinders, add a stabilizer, and use the cylinders as disposal containers for the U<sub>3</sub>O<sub>8</sub> product, to the extent practicable. An alternative is to process the emptied cylinders and dispose of them directly as LLW. Either one of these approaches is expected to meet the waste acceptance criteria of the disposal facilities and minimize the potential for generating TRU waste through washing of the cylinders to remove the heels. Although cylinder washing is not considered a foreseeable option at this time, for completeness, an analysis of the maximum potential quantities of TRU waste that could be generated from cylinder washing is included in Appendix B of this EIS, as is a discussion of PCBs contained in some cylinder coatings.

### **S.5.9 Resource Requirements**

Resource requirements include construction materials, fuel, electricity, process chemicals, and containers. In general, all alternatives would have a negligible effect on the local or national availability of these resources.

### **S.5.10 Land Use**

Under the no action alternative, all activities would occur in areas previously used for conducting similar activities; therefore, no land use impacts are expected. Under the action alternatives, a total of 65 acres (26 ha) could be disturbed for the conversion facility, with some areas cleared for railroad or utility access and not adjacent to the construction site. Up to 6.3 additional acres (2.5 ha) could also be disturbed for construction of a new cylinder yard. All three alternative locations are within an already-industrialized facility, and impacts to land use would be similar for the three locations. The permanently altered areas represent less than 1% of available land already developed for industrial purposes. Negligible impacts on land use are thus expected.

### **S.5.11 Cultural Resources**

Under the no action alternative, impacts on cultural resources at the current storage locations would be unlikely because all activities would occur in areas already dedicated to cylinder storage. Under the action alternatives, impacts on cultural resources could be possible for all three alternative locations. Archaeological and architectural surveys have not been finalized for the candidate locations and must be completed prior to initiation of the action alternatives. However, if archaeological resources were encountered, or historical or traditional cultural properties were identified, a mitigation plan would be required.

### **S.5.12 Environmental Justice**

No disproportionately high and adverse human health or environmental impacts are expected to minority or low-income populations during normal facility operations under the action alternatives. Although the consequences of facility accidents could be high if severe accidents occurred, the risk of irreversible adverse effects (including fatalities) among members of the general public from these accidents (taking into account the consequences and probability of the accidents) would be less than 1. Furthermore, transportation accidents with high and adverse impacts are unlikely; their locations cannot be projected, and the types of persons who would be involved cannot be reliably predicted. Thus, there is no reason to expect that minority and low-income populations would be affected disproportionately by high and adverse impacts.

### **S.5.13 Impacts from Cylinder Preparation at ETTP**

The cylinders at ETTP would have to be prepared to be shipped by either truck or rail. Approximately 5,900 cylinders (4,800 DUF<sub>6</sub> cylinders for conversion and about 1,100 non-DUF<sub>6</sub> cylinders) would require preparation for shipment at ETTP. Three cylinder preparation options are considered for the shipment of noncompliant cylinders.

In general, the use of cylinder overpacks would result in small potential impacts. Overpacking operations would be similar to current cylinder handling operations, and impacts

would be limited to involved workers. No LCFs among involved workers from radiation exposure are expected. Impacts would be similar if noncompliant cylinders were shipped “as-is” under a DOT exemption, assuming appropriate compensatory measures.

The use of a cylinder transfer facility would likely require the construction of a new facility at ETTP; there are no current plans to build such a facility. Operational impacts would generally be small and limited primarily to external radiation exposure of involved workers, with no LCFs expected. Transfer facility operations would generate a large number of emptied cylinders requiring disposition. If a decision were made to construct and operate a transfer facility at ETTP, additional NEPA review would be conducted.

If ETTP cylinders were transported to Paducah for conversion, the operational period at Portsmouth would be reduced by 4 years. Annual impacts would be the same as discussed for each technical discipline. No significant decrease in overall impacts would be expected.

#### **S.5.14 Impacts Associated with Conversion Product Sale and Use**

The conversion of the DUF<sub>6</sub> inventory produces products having some potential for reuse (no large-scale market exists for depleted U<sub>3</sub>O<sub>8</sub>). These products include HF and CaF<sub>2</sub>, which are commonly used as commercial materials. An investigation of the potential reuse of HF and CaF<sub>2</sub> has been included as part of this EIS. Areas examined include the characteristics of these materials as produced within the conversion process, the current markets for these products, and the potential socioeconomic impacts should these products be provided to the commercial sector. Because there would be some residual radioactivity associated with these materials, the DOE process for authorizing release of materials for unrestricted use (referred to as “free release”) and an estimate of the potential human health effects of such free release have also been included in this investigation. The results of the analysis of HF and CaF<sub>2</sub> use are included in Table S-6.

If the products were to be released for restricted use (e.g., in the nuclear industry for the manufacture of nuclear fuel), the impacts would be less than those for unrestricted release.

Conservative estimates of the amount of uranium and technetium that might transfer into the HF and CaF<sub>2</sub> were used to evaluate the maximum expected dose to workers using the material if it was released for commercial use or the general public. On the basis of very conservative assumptions concerning use, the maximum dose to workers was estimated to be less than 1 mrem/yr, much less than the regulatory limit of 100 mrem/yr specified for members of the general public. Doses to the general public would be even lower.

Socioeconomic impact analyses were conducted to evaluate the impacts of the introduction of the conversion-produced HF or CaF<sub>2</sub> into the commercial marketplace. A potential market for the aqueous HF has been identified as the current aqueous HF acid producers. The impact of HF sales on the local economy in which the existing producers are located and on the U.S. economy as a whole is likely to be minimal. No market for the CaF<sub>2</sub> that might be produced in the conversion facility has been identified. Should such a market be found, the impact of CaF<sub>2</sub> sales on the U.S. economy is also predicted to be minimal.

### S.5.15 Impacts from D&D Activities

D&D would involve the disassembly and removal of all radioactive and hazardous components, equipment, and structures. For the purposes of analysis in this EIS, it was also assumed that the various buildings would be dismantled and “greenfield” (unrestricted use) conditions would be achieved. The “clean” waste will be sent to a landfill that accepts construction debris. Low-level waste will be sent to a licensed or DOE disposal facility, where it will likely be buried in accordance with the waste acceptance criteria and other requirements in effect at that time. Hazardous and mixed waste will be disposed of in a licensed facility in accordance with applicable regulatory requirements. D&D impacts to involved workers would be primarily from external radiation; expected exposures would be a small fraction of operational doses; no LCFs would be expected. It is estimated that no fatalities and up to five injuries would result from occupational accidents. Impacts from waste management would include total generation of about 275 yd<sup>3</sup> (210 m<sup>3</sup>) of LLW, 157 yd<sup>3</sup> (120 m<sup>3</sup>) of LLMW, and 157 yd<sup>3</sup> (120 m<sup>3</sup>) of hazardous waste; these volumes would result in low impacts in comparison with projected site annual generation volumes.

### S.5.16 Cumulative Impacts

The Council on Environmental Quality (CEQ) guidelines for implementing NEPA define cumulative effects as the impacts on the environment resulting from the incremental impact of an action under consideration when added to other past, present, and reasonably foreseeable future actions (40 CFR 1508.7) Activities considered for cumulative analysis include those in the vicinity of the Portsmouth site that might affect environmental conditions at or near that locality under both the no action alternative and the proposed action alternatives. Activities considered also include those at the ETTP site associated with transporting cylinders to Portsmouth (under the proposed action) and continued long-term storage of DUF<sub>6</sub> (under the no action alternative).

One action considered reasonably foreseeable under cumulative impacts is the development of a uranium enrichment facility at either the Paducah or Portsmouth site. An agreement between USEC and DOE on June 17, 2002, established the possibility of constructing an enrichment plant at either site. In January 2004, USEC announced that it planned to site its American Centrifuge Facility at the Portsmouth site. This EIS assumes that such an enrichment facility would employ the existing gas centrifuge technology and would generate impacts similar to those outlined in a 1977 analysis of environmental consequences that considered such an action. (The facility proposed in 1977 was never completed or operated.)

Other actions planned at the Portsmouth site include continued waste management activities, waste disposal activities, environmental restoration activities, industrial reuse of sections of the site, and the DUF<sub>6</sub> management activities considered in this EIS. Activities involving gaseous diffusion uranium enrichment at Portsmouth were discontinued early in 2002. Cumulative impacts at the Portsmouth site and vicinity would be as follows for the no action alternative and the proposed action alternatives:

- The cumulative radiological exposure to the off-site population would be considerably below the maximum DOE dose limit of 100 mrem per year to the off-site maximally exposed individual (MEI) and below the limit of 25 mrem/yr specified in 40 CFR 190 for uranium fuel cycle facilities. Annual individual doses to involved workers would be monitored to maintain exposure below the regulatory limit of 5 rem per year.
- Under the no action alternative cumulative impacts assessment, although less than 1 shipment per year of radioactive wastes is expected from cylinder management activities, up to 3,500 rail shipments and 4,500 truck shipments could be associated with existing and planned actions. Under the action alternatives, up to 6,800 rail shipments and 12,300 truck shipments of radioactive material could occur. The cumulative maximum dose to the MEI along the transportation route near the site entrance would be less than 1 mrem/yr under all alternatives for all transportation options considered.
- The Portsmouth site is located in an attainment region. However, the background annual-average PM<sub>2.5</sub> concentration exceeds the standard. Cumulative impacts would not affect the attainment status.
- Data from the 2000 annual groundwater monitoring showed that five pollutants exceeded primary drinking water regulation levels in groundwater at the Portsmouth site. Alpha and beta activity were also detected. Good engineering and construction practices should ensure that indirect impacts associated with the conversion facility would be minimal.
- Cumulative ecological impacts should be negligible, with little change to intact ecosystems contributed by any alternative considered in this EIS in conjunction with the effects of other activities.
- Impacts on land use similarly would be minimal, with DUF<sub>6</sub> conversion activities confined to the Portsmouth site, which is already heavily developed for such activities.
- It is unlikely that any noteworthy cumulative impacts on cultural resources would occur under any alternative, and any such impacts would be adequately mitigated before activities for the chosen action would continue.
- Given the absence of high and adverse cumulative impacts for any impact area considered in this EIS, no environmental justice cumulative impacts are anticipated for the Portsmouth site, despite the presence of disproportionately high percentages of low-income populations in the vicinity.
- Socioeconomic impacts under all the alternatives considered are anticipated to be generally positive, often temporary, and relatively small.

Actions planned at the ETTP site include continued waste management activities, reindustrialization of the ETTP site, environmental restoration activities, possibly other DOE programs involving the disposition of enriched uranium, and the DUF<sub>6</sub> management activities considered in this EIS. Cumulative impacts at the ETTP site and vicinity would not be large under either the no action or the action alternatives.

### **S.5.17 Mitigation**

On the basis of the analyses conducted for this EIS, the following recommendations can be made to reduce the impacts of the proposed action:

- Current cylinder management activities, including inspecting cylinders, carrying out cylinder maintenance activities (such as painting), and promptly cleaning up releases from any breached DUF<sub>6</sub> cylinders, should be continued to avoid future impacts on site air and groundwater. In addition, runoff from cylinder yards should be collected and sampled so that contaminants can be detected and their release to surface water or groundwater can be avoided. If future cylinder painting results in permit violations, treating cylinder yard runoff prior to release may be required.
- Temporary impacts on air quality from fugitive dust emissions during construction of any new facility should be controlled by the best available practices to avoid temporary exceedances of the PM<sub>10</sub> and PM<sub>2.5</sub> standard. Technologies that will be used to mitigate air quality impacts during construction include using water sprays on dirt roadways and on bare soils in work areas for dust control; covering open-bodied trucks transporting materials likely to become airborne when full and at all times when in motion; water spraying and covering bunkered or staged excavated and replacement soils; maintaining paved roadways in good repair and in a clean condition; using barriers and windbreaks around construction areas such as soil banks, temporary screening, and/or vegetative cover; mulching or covering exposed bare soil areas until vegetation has time to recover or paving has been installed; and prohibiting any open burning.
- During construction, impacts to water quality and soil can be minimized through implementing storm water management, sediment and erosion controls (e.g., temporary and permanent seeding; mulching and matting; sediment barriers, traps, and basins; silt fences; runoff and earth diversion dikes), and good construction practices (e.g., covering chemicals with tarps to prevent interaction with rain, promptly cleaning up any spills).
- Potential impacts to wetlands at the Portsmouth site could be minimized or eliminated by maintaining a buffer near adjacent wetlands during construction. Impacts at Location A may potentially be avoided by an

alternative routing of the entrance road, or mitigation may be developed in coordination with the appropriate regulatory agencies.

- If trees (either live or dead) with exfoliating bark were encountered on construction areas, they should be saved if possible to avoid destroying potential habitat for the Indiana bat. If necessary, the trees should be cut before April 15 or after September 15.
- The quantity of radioactive and hazardous materials stored on site, including the products of the conversion process, should be minimized.
- The construction of a DUF<sub>6</sub> conversion facility at Portsmouth would have the potential to impact cultural resources. Neither an archaeological nor an architectural survey has been completed for the Portsmouth site as a whole or for any of the alternative locations, although an archaeological sensitivity study has been conducted. In accordance with Section 106 of the National Historic Preservation Act, the adverse effects of this undertaking must be evaluated once a location is chosen.
- Testing should be conducted either prior to or during the conversion facility startup operations to determine if the air vented from the autoclaves should be monitored or if any alternative measures would need to be taken to ensure that worker exposures to PCBs above allowable Occupational Safety and Health Administration limits do not occur.
- The nuclear properties of DUF<sub>6</sub> are such that the occurrence of a nuclear criticality is not a concern, regardless of the amount of DUF<sub>6</sub> present. However, criticality is a concern for the handling, packaging, and shipping of enriched UF<sub>6</sub>. For enriched UF<sub>6</sub>, criticality control is accomplished by employing, individually or collectively, specific limits on uranium-235 enrichment, mass, volume, geometry, moderation, and spacing for each type of cylinder. The amount of enriched UF<sub>6</sub> that may be contained in an individual cylinder and the total number of cylinders that may be transported together are determined by the nuclear properties of enriched UF<sub>6</sub>. Spacing of enriched UF<sub>6</sub> cylinders in transit during routine and accident conditions is ensured by use of regulatory approval packages that provide protection against impact and fire.
- Because of the relatively high consequences estimated for some accidents, special attention will be given to the design and operational procedures for components that may be involved in such accidents. For example, the tanks holding hazardous chemicals on site such as anhydrous NH<sub>3</sub> and aqueous HF would be designed to all applicable codes and standards, and special procedures would be in place for gaining access to the tanks and for filling of the tanks. In addition, although the probabilities of occurrence for a high-consequence accident are extremely low, emergency response plans and

procedures would be in place to respond to any emergencies should an accident occur.

### **S.5.18 Unavoidable Adverse Impacts**

Unavoidable adverse impacts are those impacts that cannot be mitigated by choices associated with siting and facility design options. Such impacts would be unavoidable, no matter which options were selected, and would include the following:

- Exposure of workers to radiation in the storage yards and the conversion facility that would be below applicable standards;
- Generation of vehicle exhaust and particulate air emissions during construction (emissions that would exceed air quality standards would be mitigated);
- Disturbance of up to 65 acres (26 ha) of land during construction, with approximately 10 acres (4 ha) required for the facility footprint;
- Loss of terrestrial and aquatic habitats from construction and disturbance of wildlife during operations; and
- Generation of vehicle exhaust and particulate air emissions during transportation.

### **S.5.19 Irreversible and Irrecoverable Commitment of Resources**

A commitment of a resource is considered *irreversible* when the primary or secondary impacts from its use limit the future options for its use. An *irrecoverable* commitment refers to the use or consumption of a resource that is neither renewable nor recoverable for later use by future generations. The major irreversible and irrecoverable commitment of natural and man-made resources related to the alternatives analyzed in this EIS include the land used to dispose of any conversion products, energy usage, and materials used for construction of the facility that could not be recovered or recycled.

### **S.5.20 Relationship between Short-Term Use of the Environment and Long-Term Productivity**

Disposal of solid nonhazardous waste resulting from new facility construction, operations, and D&D would require additional land at a sanitary landfill site, which would be unavailable for other uses in the long term. Any radioactive or hazardous waste generated by the various alternatives would involve the commitment of associated land, transportation, and disposal resources, and resources associated with the processing facilities for waste management.

For the construction and operation of the conversion facility, the associated construction activities would result in both short-term and long-term losses of terrestrial and aquatic habitats from natural productivity. After closure of the new facility, it would be decommissioned and could be reused, recycled, or remediated.

#### **S.5.21 Pollution Prevention and Waste Minimization**

Implementation of the EIS alternatives would be conducted in accordance with all applicable pollution prevention and waste minimization guidelines. A consideration of opportunities for reducing waste generation at the source, as well as for recycling and reusing material, will be incorporated to the extent possible into the engineering and design process for the conversion facility. Pollution prevention and waste minimization will be major factors in determining the final design of any facility to be constructed. Specific pollution prevention and waste minimization measures will be considered in designing and operating the final conversion facility.

#### **S.5.22 Potential Impacts Associated with the Option of Expanding Conversion Facility Operations**

As discussed in Sections S.2.2.8 and 2.2.7, several reasonably foreseeable activities could result in a future decision to increase the conversion facility throughput or extend the operational period at one or both of the conversion facility sites. Although there are no current plans to do so, to account for these future possibilities and provide future planning flexibility, Section 5.2.8 includes an evaluation of the environmental impacts associated with expanding conversion facility operations at Portsmouth, either by increasing throughput (such as by adding a fourth process line) or by extending operations.

The throughput of the Portsmouth facility could be increased either by making process efficiency improvements or by adding an additional (fourth) process line. As described in Section 5.2.8, a throughput increase through process improvements would not be expected to significantly change the overall environmental impacts when compared with the current plant design (three process lines). Efficiency improvements are generally on the order of 10%, which is within the uncertainty that is inherent in the impact estimate calculations. Slight variations in plant throughput are not unusual from year to year because of operational factors (e.g., equipment maintenance or replacement) and are generally accounted for by the conservative nature of the impact calculations.

In contrast to process efficiency improvements, the addition of a fourth process line at the Portsmouth facility would require the installation of additional plant equipment and would result in a nominal 33% increase in throughput compared with the current base design. The plant capacity would be similar to the capacity planned for the Paducah site (evaluated in DOE/EIS-0359). This throughput increase would reduce the time necessary to convert the Portsmouth and ETTP DUF<sub>6</sub> inventories by about 5 years. The construction impacts presented

above and summarized in Table S-6 for three process lines would be the same if a fourth line was added, because a fourth line would fit within the current process building design.

In general, a 33% increase in throughput (e.g., by the addition of a fourth line) would not result in significantly greater environmental impacts during operations than those discussed above and summarized in Table S-6 for three process lines. Although annual impacts in certain areas might increase up to 33% (proportional to the throughput increase), the estimated annual impacts during operations would remain well within applicable guidelines and regulations, with collective and cumulative impacts being quite low.

One exception is the PM<sub>2.5</sub> concentration during construction, which could exceed standards because of the regionally high background level under both the three- and four-process-line cases. The background data used are the maximum values from the last 5 years of monitoring at the nearest monitoring location (operated by the OEPA) to the site, located about 20 mi (32 km) away in the town of Portsmouth. On the basis of these values, exceedance of the annual PM<sub>2.5</sub> standard would be unavoidable, because the background concentration already exceeds the standard (background is 24.1 µg/m<sup>3</sup>, in comparison with the standard of 15 µg/m<sup>3</sup>).

Because a 33% increase in throughput would reduce the operational period of the facility by approximately 5 years, positive socioeconomic impacts associated with employment of the conversion facility workforce would last approximately 13 years, compared with 18 years under the base design.

The conversion facility operations could also be expanded by operating the facility longer than the currently anticipated 18 years. There are no current plans to operate the conversion facilities beyond this period. However, with routine facility and equipment maintenance and periodic equipment replacements or upgrades, it is believed that the conversion facility could be operated safely beyond this time period to process any additional DUF<sub>6</sub> for which DOE might assume responsibility. As discussed in Section 5.2.8, if operations were extended beyond 18 years and if the operational characteristics (e.g., estimated releases of contaminants to air and water) of the facility remained unchanged, it is expected that the annual impacts would be essentially the same as those presented above and summarized in Table S-6 for three process lines. Impacts associated with expanded operations are shown in brackets in Table S-6 where they would differ from those presented for the proposed design. The overall cumulative impacts from the operation of the facility would increase proportionately with the increased life of the facility.

## **S.6 ENVIRONMENTAL AND OCCUPATIONAL SAFETY AND HEALTH PERMITS AND COMPLIANCE REQUIREMENTS**

DUF<sub>6</sub> cylinder management as well as construction and operation of the proposed DUF<sub>6</sub> conversion facility would be subject to many federal, state, local, and other legal requirements. In accordance with such legal requirements, a variety of permits, licenses, and other consents must be obtained. Chapter 6 of this EIS contains a detailed listing of applicable requirements.

## **S.7 PREFERRED ALTERNATIVE**

The preferred alternative is to construct and operate the proposed DUF<sub>6</sub> conversion facility at alternative Location A, which is in the west-central portion of the Portsmouth site.

## 1 INTRODUCTION

Over the last five decades, the U.S. Department of Energy (DOE) has enriched large quantities of uranium for nuclear applications by means of gaseous diffusion. This enrichment has taken place at three DOE sites located at Paducah, Kentucky; Portsmouth, Ohio; and the East Tennessee Technology Park (ETTP, formerly known as the K-25 site) in Oak Ridge, Tennessee (Figure 1-1). “Depleted” uranium hexafluoride (commonly referred to as DUF<sub>6</sub>) is a product of this process. It is being stored at the three sites. The total DUF<sub>6</sub> inventory at the three sites weighs approximately 700,000 metric tons (t) (770,000 short tons [tons])<sup>1</sup> and is stored in about 60,000 steel cylinders.

This document is a site-specific environmental impact statement (EIS) for construction and operation of a proposed DUF<sub>6</sub> conversion facility at the Portsmouth site. The proposed facility would convert the DUF<sub>6</sub> stored at Portsmouth and ETTP to a more stable chemical form suitable for use or disposal. A separate EIS (DOE 2004a) evaluates potential impacts for a proposed conversion facility to be constructed at the Paducah site. The EISs have been prepared in accordance with the National Environmental Policy Act of 1969 (NEPA) (*United States Code*, Title 42, Section 4321 et seq. [42 USC 4321 et seq.]), Council on Environmental Quality (CEQ) NEPA regulations (*Code of Federal Regulations*, Title 40, Parts 1500–1508 [40 CFR Parts 1500–1508]), and DOE’s NEPA implementing procedures (10 CFR Part 1021).

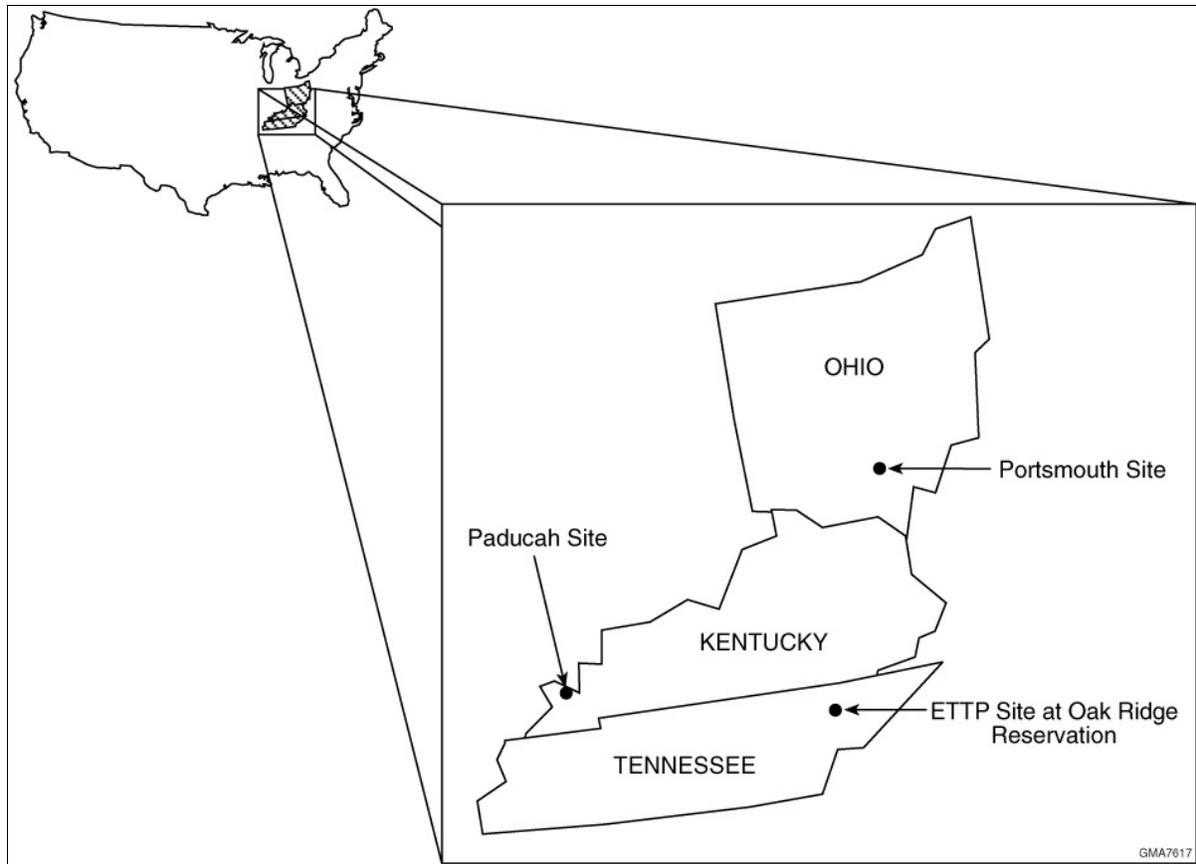
This EIS addresses the potential environmental impacts at the Portsmouth site from the construction, operation, maintenance, and decontamination and decommissioning (D&D) of the proposed conversion facility; from the transportation of the ETTP cylinders to Portsmouth; from the transportation of depleted uranium conversion products to a disposal facility; and from the transportation, sale, use, or disposal of the fluoride-containing conversion products (hydrogen fluoride [HF] or calcium fluoride [CaF<sub>2</sub>]). Three alternative locations within the Portsmouth site are evaluated for the

### National Environmental Policy Act (NEPA) Regulations

For major federal actions with the potential for significant environmental impacts, NEPA regulations require federal agencies to discuss a proposed action and all reasonable alternatives in an environmental impact statement (EIS). The information in the EIS must be sufficient for reviewers to evaluate the relative merits of each alternative.

The agency must briefly discuss any alternatives that were eliminated from further analysis. The agency should identify its preferred alternatives, if one or more exist, in the draft EIS and must identify its preferred alternative in the final EIS unless another law prohibits naming a preference. After completing the final EIS and in order to implement an alternative, the federal agency must issue a Record of Decision that announces the decision that was made and identifies the alternatives that were considered.

<sup>1</sup> In general, in this EIS, values in English units are presented first, followed by metric units in parentheses. However, when values are routinely reported in metric units, the metric units are presented first, followed by English units in parentheses.



**FIGURE 1-1 DUF<sub>6</sub> Storage Locations**

conversion facility. An option of shipping the ETTP cylinders to Paducah is also considered, as is an option of expanding facility operations. This EIS also evaluates a no action alternative, which assumes continued storage of DUF<sub>6</sub> in cylinders at the Portsmouth and ETTP sites.

## 1.1 BACKGROUND INFORMATION

The current DUF<sub>6</sub> conversion facility project is the culmination of a long history of DUF<sub>6</sub> management activities and events. To put the current project into context and provide perspective, this section provides a brief summary of this history. Additional background information on the storage and characteristics of DUF<sub>6</sub> and the DUF<sub>6</sub> cylinder inventory is provided in Section 1.2.

Uranium enrichment in the United States began as part of the atomic bomb development by the Manhattan Project during World War II. Enrichment for both civilian and military uses continued after the war under the auspices of the U.S. Atomic Energy Commission (AEC) and its successor agencies, including DOE. Three large gaseous diffusion plants (GDPs) were constructed to produce enriched uranium, first at the K-25 site (now called ETTP) and subsequently at Paducah and Portsmouth. The K-25 plant ceased operations in 1985, and the

Portsmouth plant ceased operations in 2001. The Paducah GDP continues to operate (see Section 1.1.1).

The DUF<sub>6</sub> produced during enrichment has been stored in large steel cylinders at all three gaseous diffusion plant sites since the 1950s. The cylinders are typically stacked two high and are stored outdoors on concrete or gravel yards. Figure 1.1-1 shows typical arrangements for storing cylinders.

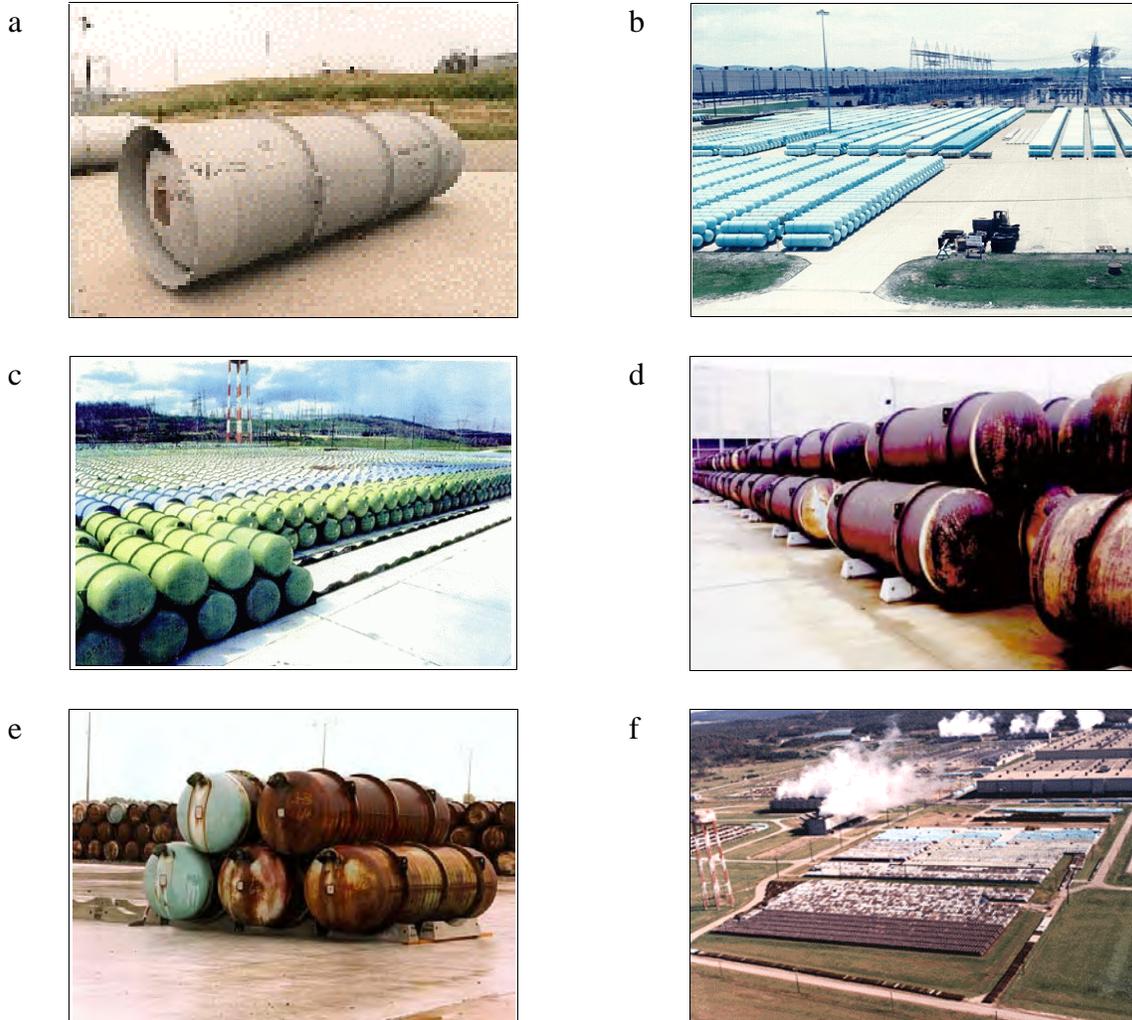
### 1.1.1 Creation of USEC

In 1993, the U.S. government began the process of privatizing uranium enrichment services by creating the United States Enrichment Corporation (USEC), a wholly owned government corporation, pursuant to the *Energy Policy Act of 1992* (Public Law [P.L.] 102-186). The Paducah and Portsmouth GDPs were leased to USEC, but DOE retained responsibility for storage, maintenance, and disposition of about 46,422 DUF<sub>6</sub> cylinders produced before 1993 and located at the three gaseous diffusion plant sites (28,351 at Paducah, 13,388 at Portsmouth, and 4,683 at K-25). In 1996, the *USEC Privatization Act* (P.L. 104-134) transferred ownership of USEC from the government to private investors. This act provided for the allocation of USEC's liabilities between the U.S. government (including DOE) and the new private corporation, including liabilities for DUF<sub>6</sub> cylinders generated by USEC before privatization.

In May and June of 1998, USEC and DOE signed two memoranda of agreement (MOAs) regarding the allocation of responsibilities for depleted uranium generated by USEC after 1993 (DOE and USEC 1998a,b). The two MOAs transferred ownership of a total of 11,400 DUF<sub>6</sub> cylinders from USEC to DOE.

### DUF<sub>6</sub> Management Time Line

1950–1993	DOE generates DUF <sub>6</sub> stored in cylinders at the ETTP, Portsmouth, and Paducah sites.
1985	K-25 (ETTP) GDP ceases operations.
1992	Ohio EPA issues Notice of Violation (NOV) to Portsmouth.
1993	USEC is created by P.L. 102-186.
1994	DOE initiates DUF <sub>6</sub> PEIS.
1995	DNFSB issues Recommendation 95-1, Safety of Cylinders Containing Depleted Uranium. DOE initiates UF <sub>6</sub> Cylinder Project Management Plan.
1996	USEC Privatization Act (P.L. 104-134) is enacted.
1997	DOE issues Draft DUF <sub>6</sub> PEIS.
1998	DOE and Ohio EPA reach agreement on NOV. Two DOE-USEC MOAs transfer 11,400 DUF <sub>6</sub> cylinders to DOE. P.L. 105-204 is enacted.
1999	DOE and TDEC enter consent order. DOE issues Final DUF <sub>6</sub> PEIS. DOE issues conversion plan in response to P.L. 105-204. DNFSB closes Recommendation 95-1. DOE issues Draft RFP for conversion services.
2000	DOE issues Final RFP for conversion services.
2001	DOE receives five proposals in response to RFP. DOE identifies three proposals in competitive range. DOE publishes NOI for site-specific DUF <sub>6</sub> Conversion EIS. DOE prepares environmental critique to support conversion services procurement process. Portsmouth GDP ceases operations. DOE holds public scoping meetings for the site-specific DUF <sub>6</sub> Conversion EIS.
2002	DOE-USEC agreement transfers 23,000 t (25,684 tons) of DUF <sub>6</sub> to DOE. P.L. 107-206 is enacted. DOE awards conversion services contract to UDS. DOE prepares environmental synopsis to support conversion services procurement process.
2003	DOE announces Notice of Change in NEPA Compliance Approach and issues the draft EIS. DOE issues draft site-specific conversion facility EISs.
2004	Final site-specific conversion facility EISs issued.



**FIGURE 1.1-1 Storage of DUF<sub>6</sub> Cylinders: (a) Typical 14-ton (12-t) skirted cylinder. (b) New cylinder storage yard at the Paducah site. (c, d, e) Cylinders stacked two high on concrete chocks. (f) Cylinder yards at the Portsmouth site.**

On June 17, 2002, DOE and USEC signed a third agreement (DOE and USEC 2002) to transfer up to 23,300 t (25,684 tons) of DUF<sub>6</sub> from USEC to DOE between 2002 and 2006. The exact number of cylinders was not specified. Transfer of ownership of all the material will take place at Paducah. While title to the DUF<sub>6</sub> is transferred to DOE under this agreement, custody and cylinder management responsibility remains with USEC until DOE requests that USEC deliver the cylinders for processing in the conversion facility.

### 1.1.2 Growing Concern over the DUF<sub>6</sub> Inventory

In May 1995, the Defense Nuclear Facilities Safety Board (DNFSB), an independent DOE oversight organization within the Executive Branch, issued Recommendation 95-1 regarding storage of the DUF<sub>6</sub> cylinders. This document advised that DOE should take three

actions: (1) start an early program to renew the protective coating on cylinders containing DUF<sub>6</sub> from the historical production of enriched uranium, (2) explore the possibility of additional measures to protect the cylinders from the damaging effects of exposure to the elements as well as any additional handling that might be called for, and (3) institute a study to determine whether a more suitable chemical form should be selected for long-term storage of depleted uranium.

In response to Recommendation 95-1, DOE began an aggressive effort to better manage its DUF<sub>6</sub> cylinders, known as the *UF<sub>6</sub> Cylinder Project Management Plan* (Lockheed Martin Energy Systems, Inc. [LMES] 1997a). This plan incorporated more rigorous and more frequent inspections, a multiyear schedule for painting and refurbishing cylinders, and construction of concrete-pad cylinder yards. In December 1999, the DNFSB determined that DOE's implementation of the *UF<sub>6</sub> Cylinder Project Management Plan* was successful, and, as a result, on December 16, 1999, it closed Recommendation 95-1.

Several affected states also expressed concern over the DOE DUF<sub>6</sub> inventory. In October 1992, the Ohio Environmental Protection Agency (OEPA) issued a Notice of Violation (NOV) alleging that DUF<sub>6</sub> stored at the Portsmouth facility is subject to regulation under state hazardous waste laws. The NOV stated that the OEPA had determined DUF<sub>6</sub> to be a solid waste and that DOE had violated Ohio laws and regulations by not evaluating whether such waste was hazardous. DOE disagreed with this assessment and entered into discussions with the OEPA that continued through February 1998, when an agreement was reached. Ultimately, in February 1998, DOE and the OEPA agreed to set aside the issue of whether the DUF<sub>6</sub> is subject to state hazardous waste regulation and instituted a negotiated management plan governing the storage of the Portsmouth DUF<sub>6</sub>. The agreement also requires DOE to continue its efforts to evaluate the potential use or reuse of the material. The agreement expires in 2008.

Similarly, in February 1999, DOE and the Tennessee Department of Environment and Conservation (TDEC) entered into a consent order that included a requirement for the performance of two environmentally beneficial projects: the implementation of a negotiated management plan governing the storage of the small inventory (relative to other sites) of all UF<sub>6</sub> (depleted, enriched, and natural) cylinders stored at the ETTP site and the removal of the DUF<sub>6</sub> from the ETTP site or the conversion of the material by December 31, 2009. The consent order further requires DOE to submit a plan, within 60 days of completing NEPA review of its long-term DUF<sub>6</sub> management strategy, that contains schedules for activities related to removal of cylinders from the ETTP site.

In Kentucky, a final Agreed Order between DOE and the Kentucky Natural Resources and Environmental Protection Cabinet concerning DUF<sub>6</sub> cylinder management was entered in October 2003. This Agreed Order requires that DOE provide the Kentucky Department of Environmental Protection with an inventory of all DUF<sub>6</sub> cylinders for which DOE has management responsibility at the Paducah site and, with regard to that inventory, that DOE implement the DUF<sub>6</sub> Cylinder Management Plan, which is Attachment 1 to the Agreed Order.

### 1.1.3 Programmatic NEPA Review and Congressional Interest

In 1994, DOE began work on a *Programmatic Environmental Impact Statement for Alternative Strategies for the Long-Term Management and Use of Depleted Uranium Hexafluoride* (DUF<sub>6</sub> PEIS) (DOE 1999a) (DOE/EIS-0269) to evaluate potential broad management options for DOE's DUF<sub>6</sub> inventory. Alternatives considered included continued storage of DUF<sub>6</sub> in cylinders at the gaseous diffusion plant sites or at a consolidated site, and the use of technologies for converting the DUF<sub>6</sub> to a more stable chemical form for long-term storage, use, or disposal. DOE issued the draft DUF<sub>6</sub> PEIS for public review and comment in December 1997 and held hearings near each of the three sites where DUF<sub>6</sub> is currently stored (Paducah, Kentucky; Oak Ridge, Tennessee; and Portsmouth, Ohio) and in Washington, D.C. In response to its efforts, DOE received some 600 comments.

In July 1998, while the PEIS was being prepared, the President signed into law P.L. 105-204. The text of P.L. 105-204 pertinent to the management of DUF<sub>6</sub> is as follows:

- (a) *PLAN.* – *The Secretary of Energy shall prepare, and the President shall include in the budget request for fiscal year 2000, a Plan and proposed legislation to ensure that all amounts accrued on the books of the United States Enrichment Corporation for the disposition of depleted uranium hexafluoride will be used to commence construction of, not later than January 31, 2004, and to operate, an onsite facility at each of the gaseous diffusion plants at Paducah, Kentucky, and Portsmouth, Ohio, to treat and recycle depleted uranium hexafluoride consistent with the National Environmental Policy Act.*

DOE began, therefore, to prepare a responsive plan while it proceeded with the PEIS.

On March 12, 1999, DOE submitted the plan to Congress; no legislation was proposed. In April 1999, DOE issued the final DUF<sub>6</sub> PEIS. The PEIS identified conversion of DUF<sub>6</sub> to another chemical form for use or long-term storage as part of the preferred management alternative. In the Record of Decision (ROD; *Federal Register*, Volume 64, page 43358 [64 FR 43358]), DOE decided to promptly convert the DUF<sub>6</sub> inventory to a more stable uranium oxide form (DOE 1999b). DOE also stated that it would use the depleted uranium oxide as much as possible and store the remaining depleted uranium oxide for potential future uses or disposal, as necessary. In addition, DUF<sub>6</sub> would be converted to depleted uranium metal only if uses for metal were available. DOE did not select a specific site or sites for the conversion facilities but reserved that decision for subsequent NEPA review. (This EIS is that site-specific review.)

Then, in July 1999, DOE issued the *Final Plan for the Conversion of Depleted Uranium Hexafluoride as Required by Public Law 105-204* (DOE 1999c). The Conversion Plan describes the steps that would allow DOE to convert the DUF<sub>6</sub> inventory to a more stable chemical form. It incorporates information received from the private sector in response to a DOE request for expressions of interest; ideas from members of the affected communities, Congress, and other interested stakeholders; and the results of the analyses for the final DUF<sub>6</sub> PEIS. The Conversion

Plan describes DOE's intent to chemically process the DUF<sub>6</sub> to create products that would present a lower long-term storage hazard and provide a material suitable for use or disposal.

#### 1.1.4 DOE Request for Contractor Proposals and Site-Specific NEPA Review

DOE initiated the final Conversion Plan on July 30, 1999, and announced the availability of a draft Request for Proposals (RFP) for a contractor to design, construct, and operate DUF<sub>6</sub> conversion facilities at the Paducah and Portsmouth sites.

In early 2000, the RFP was modified to allow for a wider range of potential conversion product forms and process technologies than had been previously reviewed in the DUF<sub>6</sub> PEIS (the PEIS considered conversion to triuranium octaoxide [U<sub>3</sub>O<sub>8</sub>] and uranium dioxide [UO<sub>2</sub>] for disposal and conversion to uranium metal for use). DOE stated that, if the selected conversion technology would generate a previously unconsidered product (e.g., depleted uranium tetrafluoride [UF<sub>4</sub>]), DOE would review the potential environmental impacts as part of the site-specific NEPA review.

On October 31, 2000, DOE issued a final RFP to procure a contractor to design, construct, and operate DUF<sub>6</sub> conversion facilities at the Paducah and Portsmouth sites. The RFP stated that any conversion facilities that would be built would have to convert the DUF<sub>6</sub> within a 25-year period to a more stable chemical form that would be suitable for either beneficial use or disposal. The selected contractor would use its proposed technology to design, construct, and operate the conversion facilities for an initial 5-year period. Operation would include (1) maintaining the DUF<sub>6</sub> inventories and conversion product inventories; (2) transporting all UF<sub>6</sub> storage cylinders currently located at ETTP to a conversion facility at the Portsmouth site, as appropriate; and (3) transporting to an appropriate disposal site any conversion product for which no use was found. The selected contractor would also be responsible for preparing such excess material for disposal.

In March 2001, DOE announced the receipt of five proposals in response to the RFP, three of which proposed conversion to U<sub>3</sub>O<sub>8</sub> and two of which proposed conversion to UF<sub>4</sub>. In August 2001, DOE deemed three of these proposals to be within the competitive range; two conversion to U<sub>3</sub>O<sub>8</sub> proposals and one conversion to UF<sub>4</sub> proposal.

On September 18, 2001, DOE published a Notice of Intent (NOI) in the *Federal Register* (66 FR 48123) announcing its intention to prepare an EIS for the proposed action to construct, operate, maintain, and decontaminate and decommission two DUF<sub>6</sub> conversion facilities at Portsmouth, Ohio, and Paducah, Kentucky. DOE held three scoping meetings to provide the public with an opportunity to present comments on the scope of the EIS and to ask questions and discuss concerns with DOE officials regarding the EIS. The scoping meetings were held in Piketon, Ohio, on November 28, 2001; in Oak Ridge, Tennessee, on December 4, 2001; and in Paducah, Kentucky, on December 6, 2001.

The alternatives identified in the NOI included a two-plant alternative (one at the Paducah site and another at the Portsmouth site), a one-plant alternative (only one plant would be

built, at either the Paducah or the Portsmouth site), an alternative using existing UF<sub>6</sub> conversion capacity at commercial nuclear fuel fabrication facilities, and a no action alternative. For alternatives that involved constructing one or two new plants, DOE planned to consider alternative conversion technologies, local siting alternatives within the Paducah and Portsmouth site boundaries, and the shipment of DUF<sub>6</sub> cylinders stored at ETTP to either the Portsmouth site or to the Paducah site. The technologies to be considered in the EIS were those submitted in response to the October 2000 RFP, plus any other technologies that DOE believed must be considered.

### 1.1.5 Public Law 107-206 Passed by Congress

During the site-specific NEPA review process, Congress acted again regarding DUF<sub>6</sub> management, and on August 2, 2002, the President signed the *2002 Supplemental Appropriations Act for Further Recovery from and Response to Terrorist Attacks on the United States* (P.L. 107-206). The pertinent part of P.L. 107-206 had several requirements: that no later than 30 days after enactment, DOE must select for award of a contract for the scope of work described in the October 2000 RFP, including design, construction, and operation of a DUF<sub>6</sub> conversion facility at each of the Department's Paducah, Kentucky, and Portsmouth, Ohio, gaseous diffusion sites; that the contract require groundbreaking for construction to occur no later than July 31, 2004; that the contract require construction to proceed expeditiously thereafter; that the contract include as an item of performance the transportation, conversion, and disposition of DU contained in cylinders located at ETTP, consistent with environmental agreements between the state of Tennessee and the Secretary of Energy; and that no later than 5 days after the date of groundbreaking for each facility, the Secretary of Energy shall submit to Congress a certification that groundbreaking has occurred. The relevant portions of the Appropriations Act are set forth in Appendix A.

In response to P.L. 107-206, on August 29, 2002, DOE awarded a contract to Uranium Disposition Services, LLC (hereafter referred to as UDS) for construction and operation of two conversion facilities. DOE also reevaluated the appropriate scope of its site-specific NEPA review and decided to prepare two separate EISs, one for the plant proposed for the Paducah site and a second for the Portsmouth site. This change was announced in the *Federal Register* Notice of Change in NEPA Compliance Approach published on April 28, 2003 (68 FR 22368).

The two draft site-specific conversion facility EISs were mailed to stakeholders in late November 2003, and a notice of availability was published by the EPA in the *Federal Register* on November 28, 2003 (68 FR 66824). Comments on the draft EISs were accepted during a 67-day review period, from November 28, 2003, until February 2, 2004. Public hearings on the draft EISs were held near Portsmouth, Ohio, on January 7, 2004; Paducah, Kentucky, on January 13, 2004; and Oak Ridge, Tennessee, on January 15, 2004. (Section 1.6.3 provides additional information on the public review of the draft EISs).

## 1.2 CHARACTERISTICS OF DUF<sub>6</sub>

DUF<sub>6</sub> results from the process of making uranium suitable for use as fuel in nuclear reactors or for military applications. The use of uranium in these applications requires that the proportion of the uranium-235 isotope found in natural uranium, which is approximately 0.7% by weight (wt%), be increased through an isotopic separation process. To achieve this increase, a uranium-235 enrichment process called gaseous diffusion is used in the United States. The gaseous diffusion process uses uranium in the form of UF<sub>6</sub>, primarily because UF<sub>6</sub> can conveniently be used in gaseous form for processing, in liquid form for filling or emptying containers, and in solid form for storage. Solid UF<sub>6</sub> is a white, dense, crystalline material that resembles rock salt.

Depleted uranium is uranium that, through the enrichment process, has been stripped of a portion of the uranium-235 that it once contained so that its proportion is lower than the 0.7 wt% found in nature. The uranium in most of DOE's DUF<sub>6</sub> has between 0.2 wt% and 0.4 wt% uranium-235.

The chemical and physical characteristics of DUF<sub>6</sub> pose potential health risks, and the material is handled accordingly. Uranium and its decay products in DUF<sub>6</sub> emit low levels of alpha, beta, gamma, and neutron radiation. The radiation levels measured on the outside surface of filled DUF<sub>6</sub> storage cylinders are typically about 2 to 3 millirem per hour (mrem/h), decreasing to about 1 mrem/h at a distance of 1 ft (0.3 m). If DUF<sub>6</sub> is released to the atmosphere, it reacts with water vapor in air to form HF and a uranium oxyfluoride compound called uranyl fluoride (UO<sub>2</sub>F<sub>2</sub>), which can be harmful to human health if inhaled or ingested in sufficient quantities. Uranium is a heavy metal that, in addition to being radioactive, can have harmful chemical effects (primarily on the kidneys) if it enters the bloodstream by means of ingestion or inhalation. HF is an extremely corrosive gas that can

### Cylinder-Related Terms Used in This EIS

#### Types of UF<sub>6</sub>

UF <sub>6</sub>	A chemical composed of one atom of uranium combined with six atoms of fluorine. UF <sub>6</sub> is a volatile white crystalline solid at ambient conditions.
Normal UF <sub>6</sub>	UF <sub>6</sub> made with uranium that contains the isotope uranium-235 at a concentration equal to that found in nature, that is, 0.7% uranium-235.
DUF <sub>6</sub>	UF <sub>6</sub> made with uranium that contains the isotope uranium-235 in concentrations less than the 0.7% found in nature. In general, the DOE DUF <sub>6</sub> contains between 0.2% and 0.4% uranium-235.
Enriched UF <sub>6</sub>	UF <sub>6</sub> made with uranium containing more than 0.7% uranium-235. In general, DOE enriched UF <sub>6</sub> considered in this EIS contains less than 5% uranium-235.
Reprocessed UF <sub>6</sub>	UF <sub>6</sub> made with uranium that was previously irradiated in a nuclear reactor and chemically separated during reprocessing.

#### Types of Cylinders

Full DUF <sub>6</sub>	Cylinders filled to 62% of their volume with DUF <sub>6</sub> (some cylinders are slightly overfilled).
Partially full	Cylinders that contain more than 50 lb (23 kg) of DUF <sub>6</sub> but less than 62% of their volume.
Heel	Cylinders that contain less than 50 lb (23 kg) of residual nonvolatile material left after the DUF <sub>6</sub> has been removed.
Empty	Cylinders that have had the DUF <sub>6</sub> and heel material removed and contain essentially no residual material.
Feed	Cylinders used to supply UF <sub>6</sub> into the enrichment process. Most feed cylinders contain natural UF <sub>6</sub> , although some historically contained reprocessed UF <sub>6</sub> .
Non-DUF <sub>6</sub>	A term used in this EIS to refer to cylinders that contain enriched UF <sub>6</sub> or normal UF <sub>6</sub> .

damage the lungs and cause death if inhaled at high enough concentrations. In light of such characteristics, DOE stores DUF<sub>6</sub> in a manner designed to minimize the risk to workers, the public, and the environment.

DUF<sub>6</sub> has been stored at all three storage sites since the 1950s in large steel cylinders. Several different cylinder types are in use, although the vast majority of cylinders have a 14-ton (12-t) capacity. (Typical cylinders in storage are shown in Figure 1.1-1.) The cylinders with a 14-ton (12-t) capacity are 12 ft (3.7 m) long by 4 ft (1.2 m) in diameter; most have a steel wall that is 5/16 in. (0.79 cm) thick. The cylinders have external stiffening rings that provide support. Lifting lugs for handling are attached to the stiffening rings. A small percentage of the cylinders have skirted ends (extensions of the cylinder walls past the rounded ends of the cylinder), as shown in Figure 1.1-1. Each cylinder has a single valve for filling and emptying located on one end at the 12 o'clock position. Similar but slightly smaller cylinders with a capacity of 10 tons (9 t) are also in use. Most of the cylinders were manufactured in accordance with an American National Standards Institute standard (ANSI N14.1, *American National Standard for Nuclear Materials — Uranium Hexafluoride — Packaging for Transport*) as specified in 49 CFR 173.420, the federal regulations governing transport of DUF<sub>6</sub>.

### 1.2.1 Cylinder Inventory

This EIS considers conversion of the DUF<sub>6</sub> inventory stored at the Portsmouth site for which DOE has management responsibility, as well as conversion of the DUF<sub>6</sub> stored at ETTP after it has been shipped to Portsmouth. Statistics on the cylinders managed by DOE at the Portsmouth and ETTP sites as of January 26, 2004, are summarized in Table 1.1-1. The EIS considers the conversion of about 21,000 cylinders containing 250,000 t (275,000 tons) of DUF<sub>6</sub>. In addition, this EIS considers the transportation to Portsmouth of about 1,100 cylinders from ETTP that contain enriched UF<sub>6</sub> or normal UF<sub>6</sub> (collectively called “non-DUF<sub>6</sub>” cylinders in this EIS) or are empty. The management of these non-DUF<sub>6</sub> cylinders, along with the non-DUF<sub>6</sub> cylinders currently at Portsmouth, is also included; however, they would not be processed in the conversion facility.

The conversion facility proposed for Portsmouth is designed to convert 13,500 t (14,881 tons) of DUF<sub>6</sub> per year (approximately 1,000 cylinders per year). At that rate of throughput, it will take approximately 18 years to convert the Portsmouth and ETTP cylinder inventories.

In addition to the Portsmouth and ETTP inventories, approximately 36,200 cylinders are managed at the Paducah site. Construction and operation of a conversion facility at the Paducah site for conversion of the Paducah inventory is the subject of a separate EIS (DOE 2004a).

As shown in Table 1.1-1, the total number of non-DUF<sub>6</sub> cylinders is 2,693 at Portsmouth and 1,102 at ETTP. The non-DUF<sub>6</sub> cylinders contain a total of approximately 13,545 t (14,900 tons) of UF<sub>6</sub> (26 t [29 tons] of enriched UF<sub>6</sub> plus 13,519 t [14,871 tons] of normal UF<sub>6</sub>) (Hightower 2004). Nearly 100% of the Portsmouth enriched UF<sub>6</sub> and over 98% of the ETTP

**TABLE 1.1-1 Inventory of DOE UF<sub>6</sub> Cylinders Considered in This EIS<sup>a</sup>**

Location	No. of Cylinders	Weight of UF <sub>6</sub> (t)
Portsmouth – DUF <sub>6</sub>	16,109	195,800
Non-DUF <sub>6</sub>		
Enriched UF <sub>6</sub>	1,444	19
Normal UF <sub>6</sub>	1,249	13,500
Empty	485	0
ETTP <sup>b</sup> – DUF <sub>6</sub>	4,822	54,300
Non-DUF <sub>6</sub>		
Enriched UF <sub>6</sub>	881	7
Normal UF <sub>6</sub>	221	19
Empty	20	0
Total		
DUF <sub>6</sub>	20,931	250,100
Non-DUF <sub>6</sub>	3,795	13,544
Empty	505	0

<sup>a</sup> As of January 26, 2004 (Hightower 2004).

<sup>b</sup> The proposed action calls for shipment of the ETTP cylinders to Portsmouth.

enriched UF<sub>6</sub> contains less than 5% uranium-235. This EIS considers the shipment of the ETTP non-DUF<sub>6</sub> cylinders to Portsmouth. It is assumed that the normal UF<sub>6</sub> and enriched UF<sub>6</sub> from both sites would be put to beneficial uses; therefore, conversion of the contents of the non-DUF<sub>6</sub> cylinders is not considered.

Although the current proposal is to ship all the cylinders at ETTP to Portsmouth, this EIS does consider an option of shipping the ETTP cylinders to Paducah. If the ETTP cylinders were shipped to Paducah, the Portsmouth conversion facility would operate for approximately 14 years rather than 18 to convert the DUF<sub>6</sub> cylinders.

The evaluation of the no action alternative in this EIS is based on the assessment conducted for the PEIS, which was revised to reflect updated information. To account for uncertainties related to the amount of USEC-generated DUF<sub>6</sub> to be managed in the future, the PEIS analysis used for this EIS assumed that a total of approximately 16,400 DUF<sub>6</sub> cylinders at the Portsmouth site would need to be managed.

Several reasonably foreseeable activities could potentially result in a future increase in the number of DUF<sub>6</sub> cylinders for which DOE has management responsibility. These include potential transfers of DUF<sub>6</sub> to DOE from continued USEC gaseous diffusion plant operations at Paducah; from a future USEC advanced enrichment technology plant at Portsmouth, Paducah, or elsewhere; and from some unspecified future commercial uranium enrichment facility licensed and operated in the United States. Such an inventory increase could result in a future decision to

extend conversion facility operations or expand throughput at one or both of the conversion facility sites. An option of expanding operations at the conversion facility is considered in the EIS, as discussed in detail in Section 2.2.7 and in the assessment of impacts presented in Chapter 5.

### 1.2.2 Cylinder Condition and Potential Contamination

As the inventory of DUF<sub>6</sub> cylinders ages, some cylinders have begun to show evidence of external corrosion. As of August 2002, at all three storage sites combined, 11 cylinders had developed holes (breaches) (see text box). The majority of these breaches were the result of handling damage during stacking or handling damage followed by corrosion. Only 2 of 11 breaches are believed to have resulted from corrosion alone. At Portsmouth, a total of three cylinder breaches have occurred. Five breaches have occurred at ETTP. (The remaining three breaches have occurred at Paducah.) However, since DUF<sub>6</sub> is solid at ambient temperatures and pressures, it is not readily released after a cylinder leak or breach. When a cylinder is breached, moist air reacts with the exposed solid DUF<sub>6</sub> and iron, forming a dense plug of solid uranium and iron compounds and a small amount of HF gas. The plug limits the amount of material released from a breached cylinder. When a cylinder breach is identified, the cylinder is typically repaired or its contents are transferred to a new cylinder.

Because reprocessed uranium was enriched in the early years of gaseous diffusion, some of the DUF<sub>6</sub> inventory is contaminated with small amounts of technetium (Tc) and the transuranic (TRU)

#### Summary Data for Breached Cylinders at the Storage Sites through 2003

##### **Portsmouth Site, three breached cylinders:**

Two identified in 1990 were initiated by mechanical damage during stacking; the damage was not noticed immediately, and subsequent corrosion occurred at the point of damage. The largest breach size was about 9 in. × 18 in. (23 cm × 46 cm); the estimated mass of DUF<sub>6</sub> lost was between 17 and 109 lb (7.7 and 49 kg). The next largest cylinder breach had an area of about 2 in. (5.1 cm) in diameter; the estimated DUF<sub>6</sub> lost was less than 4 lb (1.8 kg). The third breached cylinder occurred in 1996 and was the result of handling equipment knocking off a cylinder plug.

##### **ETTP Site, five breached cylinders:**

Four were identified in 1991 and 1992. Two of these were initiated by mechanical damage during stacking, and two were caused by external corrosion due to prolonged ground contact. The breach areas for these four cylinders were about 2 in. (5.1 cm), 6 in. (15 cm), and 10 in. (25 cm) in diameter for three circular breaches, and 17 in. × 12 in. for a rectangular-shaped breach. The mass of material loss from the cylinders could not be estimated because equipment to weigh the cylinders was not available at the ETTP site. The fifth breach occurred in 1998 and was caused by steel grit blasting, which resulted in a breach at the location of an as-fabricated weld defect (immediately repaired without loss of DUF<sub>6</sub>).

##### **Paducah Site, three breached cylinders:**

One identified in 1992 was initiated by mechanical damage during stacking. The breached area was about 0.06 in. × 2 in. (0.16 cm × 5.1 cm). Estimated material loss was 0. The other two cylinder breaches were identified as breached because of missing cylinder plugs; they were identified between 1998 and 2002. Material loss from these cylinders was not estimated.

elements plutonium (Pu), neptunium (Np), and americium (Am). In 2000, DOE, on the basis of existing process knowledge and results from additional sampling of cylinders, characterized the TRU and Tc contamination in the DUF<sub>6</sub> cylinders. As indicated in a report by Oak Ridge National Laboratory (ORNL) (Hightower et al. 2000), nondetectable or very low levels of TRU elements were found to be dispersed in the DUF<sub>6</sub> stored in the cylinders. However, higher levels of TRU elements, associated with the “heels” remaining in a small number of cylinders formerly used to store reprocessed uranium, are expected to occur. (The term “heel” refers to the residual amount of nonvolatile material left in a cylinder following removal of the DUF<sub>6</sub>, typically less than 50 lb [23 kg].) The final RFP for providing conversion services concluded that any DUF<sub>6</sub> contaminated with TRU elements and Tc at the concentrations expected to be encountered could be safely handled in a conversion facility. The data and assumptions used in this EIS to evaluate potential impacts from the DUF<sub>6</sub> contaminated with Tc and TRU elements are described in Appendix B.

Some of the cylinders manufactured before 1978 were painted with coatings containing polychlorinated biphenyls (PCBs). (Although PCBs are no longer in production in the United States, from the 1950s to the late 1970s, PCBs were added to some paints as fungicides and to increase durability and flexibility.) The long persistence of PCBs in the environment and the tendency for bioaccumulation in the foodchain has resulted in regulations to prevent their release and distribution in the environment. As a result, the cylinders with PCB-containing coatings may require special measures during transport, such as bagging, to ensure that PCB-containing paint chips are not released. Additionally, environmental monitoring and maintenance of cylinder storage and process areas may be required to ensure that PCBs are not released during storage or processing. Potential issues associated with PCB-containing cylinder coatings are discussed in Appendix B. As discussed in Appendix B, the presence of PCBs in the coatings of some cylinders is not expected to result in health and safety risks to workers or the public.

### 1.3 PURPOSE AND NEED

DOE needs to convert its inventory of DUF<sub>6</sub> to a more stable chemical form for use or disposal. This need follows directly from (1) the decision presented in the August 1999 ROD for the PEIS, namely, to begin conversion of the DUF<sub>6</sub> inventory as soon as possible, and (2) P.L. 107-206, which directs DOE to award a contract for construction and operation of conversion facilities at both the Paducah site and the Portsmouth site.

### 1.4 PROPOSED ACTION

The proposed action evaluated in this EIS is to construct and operate a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products. The proposed action includes the shipment of DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders from the ETTP site to Portsmouth and the construction of a new cylinder storage pad at Portsmouth for the ETTP cylinders, if required. The time period considered is a construction period of approximately 2 years, an operational period of 18 years, and a 3-year period for D&D of the facility.

This EIS assesses the potential environmental impacts from the following proposed activities:

- Construction, operation, maintenance, and D&D of the proposed DUF<sub>6</sub> conversion facility at the Portsmouth site;
- Transportation of DUF<sub>6</sub> cylinders from ETTP to Portsmouth for conversion, as well as transportation of the non-DUF<sub>6</sub> cylinders from ETTP to Portsmouth;
- Construction of a new cylinder storage yard (if required) for ETTP cylinders;
- Transportation of uranium conversion products and waste materials to a disposal facility;
- Transportation and sale of the HF produced as a co-product of conversion; and
- Neutralization of HF to CaF<sub>2</sub> and its sale or disposal in the event that the HF product is not sold.

Three alternative locations for the conversion facility within the Portsmouth site are considered. In addition, this EIS includes an evaluation of the impacts that would result from a no action alternative (i.e., continued DUF<sub>6</sub> cylinder storage at the Portsmouth and ETTP sites).

## 1.5 DOE DUF<sub>6</sub> MANAGEMENT PROGRAM

In fiscal year (FY) 2001, the responsibility for all uranium program activities was transferred from DOE's Office of Nuclear Energy, Science, and Technology (NE) to its Office of Environmental Management (EM). All activities related to this program are managed by DOE's Lexington Office. The uranium program supports important government activities associated with the federal enrichment program that were not transferred to USEC under the provisions of the National Energy Policy Act of 1992 (P.L. 102-486), including management of highly enriched uranium; management of the facilities at the Paducah and Portsmouth sites; responsibility for preexisting liabilities; management of DOE's inventories of DUF<sub>6</sub> and other surplus uranium; and oversight of the construction of DUF<sub>6</sub> conversion facilities.

Within the uranium program is DOE's DUF<sub>6</sub> management program, whose mission is to safely and efficiently manage DOE's inventory of DUF<sub>6</sub> in a way that protects the health and safety of workers and the public and protects the environment until the DUF<sub>6</sub> is either used or disposed of. In addition to the conversion activities that are the subject of this EIS, the DUF<sub>6</sub> management program involves two other primary activities: (1) surveillance and maintenance of cylinders and (2) development of beneficial uses for depleted uranium.

Since it may take 25 years to convert the DUF<sub>6</sub> in the inventory to a more stable chemical form, DOE intends to ensure the continued surveillance and maintenance of the DUF<sub>6</sub> cylinders

currently in storage. Day-to-day management includes actions designed to cost-effectively improve cylinder storage conditions, such as:

- Performing regular inspections and general maintenance of cylinders and storage yards, including:
  - Restacking and respacing the cylinders to improve drainage and allow for more thorough inspections,
  - Repainting cylinder bodies and the ends of skirted cylinders as needed to arrest corrosion, and
  - Constructing new concrete cylinder storage yards and reconditioning existing yards from gravel to concrete to improve storage conditions.
- Performing routine cylinder valve surveys and maintenance.

DOE is committed to exploring the safe, beneficial use of depleted uranium and other materials that result from the conversion of DUF<sub>6</sub> (e.g., HF and empty carbon steel cylinders) in order to conserve more resources and increase savings over levels achieved through disposal. Accordingly, a DOE research and development (R&D) program on uses for depleted uranium has been initiated. This program is exploring the risks and benefits associated with several uses for depleted uranium, such as a radiation shielding material, a catalyst, and a semiconductor material in electronic devices. More information about DOE's R&D on depleted uranium uses is available on the *Depleted UF<sub>6</sub> Management Program Information Network* Web site (<http://web.ead.anl.gov/uranium>). In addition, in the RFP for conversion services, DOE requested that the bidders investigate and propose viable uses for the conversion products.

## 1.6 SCOPE

The scope of an EIS refers to the range of actions, alternatives, and impacts it considers. An agency generally determines the scope of an EIS through a two-part process: internal scoping and public scoping. Internal scoping refers to the agency's efforts to identify potential alternatives and important issues and to determine which analyses to include in an EIS. Public scoping refers to the agency's request for public comments on the proposed action and on the results from its internal scoping. It involves consultations with federal, state, and local agencies as well as requests for comments from stakeholder organizations and members of the general public. The EIS scoping process provides a means for the public to provide input into the decision-making process. DOE is committed to ensuring that the public has ample opportunity to participate in the review. This section summarizes the public scoping conducted for this EIS (Section 1.6.1), discusses the range of issues and alternatives that resulted from the internal and public scoping process (Section 1.6.2), and summarizes the public review of the draft EIS (Section 1.6.3).

### 1.6.1 Public Scoping Process for This Environmental Impact Statement

On September 18, 2001, DOE published a NOI in the *Federal Register* (66 FR 48123) announcing its intention to prepare an EIS for a proposal to construct, operate, maintain, and decontaminate and decommission DUF<sub>6</sub> conversion facilities at Portsmouth, Ohio, and/or Paducah, Kentucky. The purpose of the NOI was to encourage early public involvement in the EIS process and to solicit public comments on the proposed scope of the EIS, including the issues and alternatives it would analyze. To facilitate public comments, the NOI included a detailed discussion of the project background, a list of the preliminary alternatives and environmental impacts that DOE proposed to evaluate in the EIS, and a project schedule. The NOI announced that the scoping period for the EIS would be open until November 26, 2001. The scoping period was later extended to January 11, 2002.

During the scoping process, the public was given six ways to submit comments on the DUF<sub>6</sub> proposal to DOE:

1. Attendance at public scoping meetings held in Piketon, Ohio; Oak Ridge, Tennessee; and Paducah, Kentucky;
2. Traditional mail delivery;
3. Toll-free facsimile transmission;
4. Toll-free voice message;
5. Electronic mail; and
6. Directly through the *Depleted UF<sub>6</sub> Management Information Network Web* site on the Internet (<http://web.ead.anl.gov/uranium>).

Numerous ways to communicate about issues and submit comments were provided to encourage maximum participation. All comments, regardless of how they were submitted, received equal consideration.

A total of approximately 100 individuals attended the three scoping meetings, and 20 of these individuals provided oral comments. Individuals in attendance included federal officials, state regulators, local officials, site oversight committee members, representatives of interested companies, members of local media, and private individuals. In addition, about 20 individuals and organizations provided comments through the other means available (fax, telephone, mail, e-mail, and Web site). Some of the comments received through these other means were duplicates of comments made at the scoping meetings. During the scoping period (September 18, 2001, through January 11, 2002), the *Depleted UF<sub>6</sub> Management Information Network Web* site was used a great deal; a total of 64,366 pages were viewed (averaging 554 per day) during 9,983 user sessions (averaging 85 per day) by 4,784 unique visitors.

Approximately 140 comments were received from about 30 individuals and organizations during the scoping period. Appendix C of this EIS provides a summary of these comments. These comments were examined to finalize the proposed scope of this EIS. Comments were related primarily to five major issues: (1) DOE policy; (2) alternatives; (3) cylinder inventory, maintenance, and surveillance; (4) transportation; and (5) general environmental concerns.

Most of the comments made during the public scoping period were related to issues that DOE was already planning to discuss in this EIS. Such comments helped to clarify the need for addressing those issues. However, a few issues were raised that DOE was not able to address in this EIS. These issues and the reasons why they are not addressed are summarized below.

- A request was made to clean up the Portsmouth site before building another facility there. Activities related to remediation of the site are considered in the cumulative impacts section of this EIS. However, waiting until all remediation activities have been completed to start construction of the conversion facility would not be consistent with the requirements of P.L. 107-206.
- One commentator stated that DOE should not consider any alternatives other than the two conversion plants alternative because Congress had mandated that two plants be built: one at Paducah and one at Portsmouth. NEPA requires that the no action alternative be one of the alternatives considered. Therefore, the no action alternative has been included in this EIS.
- A request was made to designate specific routes and perform route-specific risk analyses for transporting the ETTP cylinders to Portsmouth. Specific routes will not be known until the selected contractor is ready to ship the cylinders from ETTP. The exact routes will be determined on the basis of the shipment mode selected (truck or rail), applicable regulations, and other factors, as appropriate. Before the shipments occur, a transportation plan will be coordinated with the appropriate regulatory agencies. However, this EIS does present an evaluation of transportation risks for representative routes that were identified by using route prediction models for truck and rail modes.
- Requests were made to analyze the impacts associated with the use of conversion products. As described further below, no large-scale uses of the depleted uranium conversion product have been identified, and current plans assume disposal of the material. The DUF<sub>6</sub> PEIS (DOE 1999a) analyzed the generic impacts associated with the manufacture of waste containers using depleted uranium and depleted UO<sub>2</sub>. Impacts associated with actual use of any depleted uranium products will be analyzed if specific uses are identified and any necessary licenses, permits, or exemptions are obtained. This EIS does evaluate impacts associated with the potential sale and use of fluoride-containing conversion products (i.e., HF and CaF<sub>2</sub>).

## 1.6.2 Scope of This Environmental Impact Statement

In response to the congressional mandate to build conversion plants at the Portsmouth and Paducah sites (P.L. 107-206), DOE reevaluated the appropriate scope of its NEPA review and decided to prepare two separate site-specific EISs in parallel; one EIS for the facility proposed for the Paducah site and a second EIS for the Portsmouth site. This change in approach was announced in a *Federal Register* Notice published on April 28, 2003 (DOE 2003b).

This EIS addresses the potential environmental impacts at Portsmouth from the construction, operation, maintenance, and D&D of the proposed conversion facility; from the transportation of the ETTP cylinders to Portsmouth; from the transportation of depleted uranium conversion products to a disposal facility; and from the transportation, sale, use, or disposal of the fluoride-containing conversion products (HF or CaF<sub>2</sub>). Three alternative locations within the Portsmouth site are evaluated for the conversion facility. An option of shipping the ETTP cylinders to Paducah for conversion is also considered. In addition, this EIS evaluates a no action alternative, which assumes continued storage of DUF<sub>6</sub> in cylinders at the Portsmouth and ETTP sites. Additional details are provided in the sections below.

### 1.6.2.1 Alternatives

The alternatives that are evaluated and compared in this EIS include a no action alternative and three action alternatives that focus on where to site the conversion facility within the Portsmouth site:

1. *No Action Alternative.* Under the no action alternative, conversion would not occur. Current cylinder management activities (handling, inspection, monitoring, and maintenance) would continue, so the status quo would be maintained at Portsmouth and ETTP indefinitely, consistent with the *UF<sub>6</sub> Cylinder Project Management Plan* (LMES 1997a) and the Ohio and Tennessee consent orders, which cover actions needed to meet safety and environmental requirements.
2. *Action Alternatives.* The proposed action considers the construction and operation of a conversion facility at the Portsmouth site. Three alternative locations within the site are evaluated (Locations A [preferred], B, and C, which are defined in Chapter 2). The proposed action includes the transportation of the cylinders currently stored at the ETTP site to Portsmouth. In addition, an option of transporting the ETTP cylinders to Paducah is considered, as well as an option of expanding conversion facility operations.

These alternatives and options, as well as the alternatives that were considered but not evaluated in detail, are described more fully in Chapter 2.

### 1.6.2.2 Depleted Uranium Conversion Technologies and Products

As noted in Section 1.1.5, DOE awarded a conversion services contract to UDS on August 29, 2002. The proposed UDS facility would convert DUF<sub>6</sub> to a mixture of depleted uranium oxides (primarily U<sub>3</sub>O<sub>8</sub>), a form suitable for disposal if uses are not identified. In addition to depleted U<sub>3</sub>O<sub>8</sub>, the UDS conversion facility would produce aqueous HF, which is a product that has commercial value and could potentially be sold for industrial use. The evaluation of the proposed action in this EIS is based on the proposed UDS conversion technology and facility design, which is described in Section 2.2.

The conversion project RFP did not specify the conversion product technology or form. Three proposals submitted in response to the RFP were deemed to be in the competitive range; two of these proposals involved conversion of DUF<sub>6</sub> to U<sub>3</sub>O<sub>8</sub> and the third involved conversion to depleted UF<sub>4</sub>. Potential environmental impacts associated with these proposals were considered during the procurement process, which involved the preparation of an environmental critique and environmental synopsis that were prepared in accordance with the requirements of 10 CFR 1021.216.

The environmental critique, which contains proprietary information, focuses on environmental issues pertinent to a decision among the proposals within the competitive range and includes a discussion of the purpose of the procurement and each offer, a discussion of the salient characteristics of each offer, and a comparative evaluation of the environmental impacts of the offers. The environmental synopsis is a summary document based on the environmental critique; it does not include proprietary information. The synopsis documents the evaluation of potential environmental impacts associated with the proposals in the competitive range and does not contain procurement-sensitive information. The environmental synopsis is presented in Appendix D.

The environmental synopsis concludes that, on the basis of the assessment of potential environmental impacts presented in the critique, no proposal was clearly environmentally preferable. Although differences in a number of impact areas were identified, none of the differences were considered to result in one proposal being preferable over the others. In addition, the potential environmental impacts associated with the proposals were found to be similar to, and generally less than, those presented in the DUF<sub>6</sub> PEIS (DOE 1999a) for representative conversion technologies.

### 1.6.2.3 Transportation Modes

This EIS considers shipping the cylinders at ETTP to Portsmouth, including DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders. This EIS considers several transportation methods for preparing the DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders and shipping them to the conversion facility. Many of the cylinders currently stored at ETTP do not meet U.S. Department of Transportation (DOT) requirements for shipment without some type of preparation first. The DUF<sub>6</sub> PEIS (DOE 1999a) and a separate transportation impact assessment (Biwer et al. 2001) contain detailed information on cylinder conditions, regulations, and preparation methods. As described in detail in Section 2.2.4, three

options for preparing noncompliant cylinders are considered in this EIS: (1) use of overpacks, certified to meet DOT shipping requirements, into which cylinders could be placed; (2) use of a cylinder transfer facility, in which the UF<sub>6</sub> contents could be transferred from noncompliant cylinders to compliant ones; and (3) obtaining an exemption from DOT allowing the cylinders to be shipped “as-is” or following repairs. This EIS also considers the transportation of conversion products to a user or disposal facility. Transportation of DUF<sub>6</sub> cylinders and conversion products by two modes, truck and train, are analyzed in this EIS.

#### 1.6.2.4 Conversion Product Disposition

As noted, the products of the DUF<sub>6</sub> conversion process would consist of depleted U<sub>3</sub>O<sub>8</sub> and HF. DOE has been working with industrial and academic researchers for several years to identify potential uses for both products. Some potential uses for depleted uranium exist or are being developed, and DOE believes that a viable market exists for the HF generated during conversion. To take advantage of these to the extent possible, DOE requested in the RFP that the bidders for conversion services investigate and propose viable uses.

Currently, there are several uses for depleted uranium, including (1) reactor fuel in breeder reactors; (2) conventional military applications, such as tank armor and armor-piercing projectiles; (3) biological shielding, which provides protection from x-rays or gamma rays; and (4) counterweights for use in aircraft applications. One characteristic of all these applications is that the amount of depleted uranium that they require is small, and existing demand can be met by depleted uranium stocks separate from the DUF<sub>6</sub> considered in this EIS; thus, these applications do not and are not expected to have a significant effect on the inventory of depleted uranium contained in the DOE DUF<sub>6</sub> inventory.

In the RFP, DOE acknowledges that uses for much of the depleted uranium may not be found, thus requiring that it be dispositioned as low-level radioactive waste (LLW). In its proposal, UDS confirmed that widescale applications of the depleted U<sub>3</sub>O<sub>8</sub> conversion product are not currently available and that the material will likely require disposal. Studies conducted by ORNL for DOE indicate that both the Nevada Test Site (NTS) (a DOE facility) and Envirocare of Utah, Inc. (a commercial facility) are potential disposal facilities for depleted uranium (Croff et al. 2000a,b). These studies included reviews of the LLW acceptance programs and disposal capacities of both NTS and Envirocare of Utah, Inc. It was concluded that either facility would have the capacity needed to dispose of the U<sub>3</sub>O<sub>8</sub> product from the proposed DOE DUF<sub>6</sub> conversion program, and that the U<sub>3</sub>O<sub>8</sub> material to be sent to these facilities would likely meet each site’s waste acceptance criteria. In its proposal to design, construct, and operate the DUF<sub>6</sub> conversion facilities, UDS provided evidence that both sites can presently accept the U<sub>3</sub>O<sub>8</sub> and identified the Envirocare facility as the primary disposal site and NTS as the secondary disposal site.

Shipments of depleted U<sub>3</sub>O<sub>8</sub> to a disposal facility are expected to begin shortly after conversion facility operations commence, currently planned for late 2006. The conversion facilities are being designed with a short-term storage capacity of 6 months’ worth of depleted uranium conversion products. This storage capacity is being provided in order to accommodate

potential delays in disposal activities without affecting conversion operations. If a delay was to extend beyond 6 months, DOE would evaluate possible options and conduct appropriate NEPA review for those options.

This EIS evaluates the impacts from packaging, handling, and transporting depleted U<sub>3</sub>O<sub>8</sub> from the conversion facility to disposal sites that would be (1) selected in a manner consistent with DOE policies and orders and (2) authorized or licensed to receive the conversion products by DOE (in conformance with DOE orders), the U.S. Nuclear Regulatory Commission (NRC; in conformance with NRC regulations), or an NRC Agreement State agency (in conformance with state laws and regulations determined to be equivalent to NRC regulations). Assessment of the impacts and risks from on-site handling and disposal at the LLW disposal facility are deferred to the disposal site's site-specific NEPA or licensing documents. DOE plans to decide the specific disposal location(s) for the depleted U<sub>3</sub>O<sub>8</sub> conversion product after additional appropriate NEPA review. Accordingly, DOE will continue to evaluate its disposal options and will consider any further information or comments relevant to that decision. DOE will give a minimum 45-day notice before making the specific disposal decision and will provide any supplemental NEPA analysis for public review and comment.

In addition, UDS believes that aqueous HF generated during conversion is a valuable commercial commodity that could be readily sold for industrial use. Thus, this EIS evaluates impacts associated with HF sale and use. To account for the possibility that uses for HF will not be identified, this EIS also evaluates a contingency for the neutralization of HF to the unreactive solid CaF<sub>2</sub> for sale or disposal.

#### **1.6.2.5 Human Health and Environmental Issues**

This EIS evaluates and compares the potential impacts on human health and the environment at the Portsmouth site under the alternatives and options described above. In general, this EIS emphasizes those impacts that might differ under the various alternatives and those impacts that would be of special interest to the general public (such as potential radiation effects).

This EIS includes assessments of impacts on human health and safety, air, water, soil, biota, socioeconomics, cultural resources, site waste management capabilities, resource requirements, and environmental justice. Impacts judged by DOE to be of the greatest concern or public interest and to receive more detailed analysis include impacts on human health and safety, air and water, waste management capabilities, and socioeconomics. These issues are consequently treated in greater detail in this EIS.

The process of estimating environmental impacts from the conversion of DUF<sub>6</sub> is subject to some uncertainty because final facility designs are not yet available. In addition, the methods used to estimate impacts have uncertainties associated with their results. This EIS impact assessment was designed to ensure — through the selection of assumptions, models, and input parameters — that impacts would not be underestimated and that relative comparisons among the alternatives would be valid and meaningful. This approach was developed by uniformly

applying common assumptions to each alternative and by choosing assumptions intended to produce conservative estimates of impacts — that is, assumptions that would lead to overestimates of the expected impacts. Although uncertainty may characterize estimates of the absolute magnitude of impacts, a uniform approach to impact assessment enhances the ability to make valid comparisons among alternatives. This uniform approach was implemented in the analyses conducted for this EIS to the extent practicable.

### 1.6.3 Public Review of the Draft EIS

The two draft site-specific conversion facility EISs were mailed to stakeholders in late November 2003, and a notice of availability was published by the EPA in the *Federal Register* on November 28, 2003 (68 FR 66824). In addition, each EIS was also made available in its entirety on the Internet at the same time, and e-mail notification was sent to those on the project Web site mailing list. Stakeholders were encouraged to provide comments on the draft EISs during a 67-day review period, from November 28, 2003, until February 2, 2004. Comments could be submitted by calling a toll-free number, by fax, by letter, by e-mail, or through the project Web site. Comments could also be submitted at public hearings held near Portsmouth, Ohio, on January 7, 2004; Paducah, Kentucky, on January 13, 2004; and Oak Ridge, Tennessee, on January 15, 2004. The public hearings were announced on the project Web site and in local newspapers prior to the meetings.

A total of about 210 comments were received during the comment period. The comments received and DOE's responses to those comments are presented in Volume 2 of this EIS. Because of the similarities in the proposed actions and the general applicability of many of the comments to both site-specific conversion facility EISs, all comments received on the Portsmouth and Paducah EISs are included in Volume 2. In addition, all comments received were considered in the preparation of both final EISs.

Several revisions were made to the two site-specific conversion facility draft EISs on the basis of the comments received (changes are indicated by vertical lines in the right margin of the document). The vast majority of the changes were made to provide clarification and additional detail. Specific responses to each comment received on the draft EISs are presented in Volume 2 of this EIS; a summary of the most common issues raised by the reviewers and the general DOE responses to these issues are listed below.

- *Comments related to the proposed action and preferred alternative.*

Numerous reviewers expressed support for the DOE conversion project in general and agreement with the preferred alternatives identified in the draft EISs. Reviewers stressed the importance of meeting the requirements of P.L. 107-206, as well as the consent orders that DOE has signed with each of the affected states.

DOE appreciates support for the conversion project and is committed to complying with all applicable regulations, agreements, and orders.

- *Comments related to transportation of cylinders.*

Several reviewers raised concerns over the safe transportation of cylinders from the ETTP site. Common themes included a preference for the use of overpacks, opposition to transporting noncompliant cylinders “as-is” under a DOT exemption, a general desire that shipments be made in a manner protective of health and safety, and questions concerning the potential use of barge transportation.

DOE is committed to conducting all transportation activities in a manner protective of human health and safety and in compliance with all applicable regulations. A Transportation Plan will be developed for each shipping program related to the DUF<sub>6</sub> conversion facility project. Each Plan will be developed to address specific issues associated with the commodity being shipped, the origin and destination points, and concerns of jurisdictions transited by the shipments. In all cases, DOE-sponsored shipments will comply with all applicable State and Federal regulations and will be reflected in many of the operational decisions that will be made and presented in the Plan. The transportation regulations are designed to be protective of public health and safety during both accident and routine transportation conditions.

To allow flexibility in planning and future operations, the transportation analysis in each EIS evaluates a range of options for cylinder preparation and transport modes. For example, all three options for shipping noncompliant cylinders, including obtaining a DOT exemption, using overpacks, and transferring the contents from noncompliant to compliant cylinders, are evaluated in the EISs, as are both truck and rail modes. Because barge transport has not been proposed as part of the current conversion facility project and for the reasons discussed in Section 2.3.5, a detailed evaluation has not been included in the final EISs. If barge transportation was proposed in the future and considered to be a reasonable option, additional NEPA review would be conducted.

- *Comments related to removal of cylinders from the ETTP site.*

Several reviewers stressed the importance of DOE compliance with the 1999 consent order with the TDEC that requires the removal of the DUF<sub>6</sub> cylinders from the ETTP site or the conversion of the material by December 31, 2009.

DOE is committed to complying with the 1999 consent order. Toward that end, the DOE contract for accelerated cleanup of the ETTP site, including removal of the DUF<sub>6</sub> cylinders, calls for completion of this activity by the end of FY 2008.

- *Comments related to the potential for DOE to receive additional DUF<sub>6</sub> cylinders from other sources.*

Several reviewers noted that DOE may receive additional DUF<sub>6</sub> cylinders from other sources, including continued USEC operations, the proposed American Centrifuge Facility at the Portsmouth site, and other potential commercial enrichment facilities. Some reviewers requested that DOE design the conversion facilities to accommodate such an increase.

At the present time, there are no plans or proposals for DOE to accept DUF<sub>6</sub> cylinders for conversion beyond the current inventory for which it has responsibility. However, Section 2.2.7 of the Portsmouth site-specific conversion facility EIS and Section 2.2.5 of the Paducah EIS discuss a number of possible future sources of additional DUF<sub>6</sub> that could require conversion. The potential environmental impacts associated with expanding plant operations (by either extending operations or increasing the throughput) to accommodate processing of additional cylinders are discussed in Section 5.2.8 of the Portsmouth EIS and Section 5.2.6 of the Paducah EIS. Because of the uncertainty associated with possible future sources of DUF<sub>6</sub> for which DOE could assume responsibility, there is no current proposal to increase throughputs of the conversion facilities or extend the operational period.

- *Comments related to USEC's American Centrifuge Facility.*

Several reviewers noted the January 2004 announcement by USEC that the American Centrifuge Facility would be sited at Portsmouth, and stated that the EISs should be revised accordingly, including consideration of the facility under Portsmouth cumulative impacts.

The two site-specific conversion facility EISs have been revised to reflect that Portsmouth has been selected as the site for the USEC American Centrifuge Facility. Although Location B is the likely site for construction of the centrifuge facility, it has been retained in the final Portsmouth conversion EIS as a siting alternative. The cumulative impacts analysis included in both the draft and final Portsmouth conversion facility EIS assumed that a new USEC centrifuge enrichment facility would be constructed and operated at the Portsmouth site (see Sections S.5.16 and 5.3.2). As stated in Sections S.5.16 and 5.3.2, the analysis assumed that such a plant would be sited at Portsmouth, that the existing DOE gas centrifuge technology would be used, and that the environmental impacts of such a facility would be similar to those outlined in a 1977 EIS for Expansion of the Portsmouth Gaseous Diffusion Plant that considered a similar action that was never completed. It should be noted that the NRC licensing activities for the proposed centrifuge enrichment plant will include preparation of an EIS that must also evaluate cumulative impacts at the Portsmouth site. The centrifuge enrichment facility cumulative impacts analysis will be based on the anticipated USEC enrichment facility design,

which does not currently exist, and will benefit from the detailed evaluation of conversion facility impacts presented in this EIS.

- *Comments related to current cylinder management.* Several reviewers raised questions and concerns about the current management of the cylinders at the three DOE storage sites.

In response to these concerns, it has been emphasized that DOE's current cylinder management program provides for safe storage of the depleted DUF<sub>6</sub> cylinders. DOE is committed to the safe storage of the cylinders at each site through the implementation of the decision made in the ROD. DOE has an active cylinder management program designed to ensure the continued safety of cylinders until conversion is accomplished.

## 1.7 RELATIONSHIP TO OTHER NEPA REVIEWS

This site-specific DUF<sub>6</sub> Conversion EIS, along with the EIS prepared for the Paducah conversion facility (DOE 2004a), represents the second level of a tiered environmental review process being used to evaluate and implement DOE's DUF<sub>6</sub> Management Program. A "tiered" process refers to a process of first addressing higher-order decisions in a programmatic EIS (PEIS) and then conducting a more narrowly focused (project-level) environmental review. The project-level review incorporates, by reference, the programmatic analysis, as appropriate, as well as additional site-specific analyses. The DUF<sub>6</sub> PEIS (DOE 1999a), issued in April 1999, represents the first level of this tiered process.

DOE prepared, or is in the process of preparing, other NEPA reviews that are related to the management of DUF<sub>6</sub> or to the current DUF<sub>6</sub> storage sites. The DUF<sub>6</sub> PEIS includes an extensive list of reviews that were prepared before 1999; that list is not repeated here. The following related NEPA reviews were conducted after publication of the DUF<sub>6</sub> PEIS; these reviews are related to this EIS primarily because they evaluate activities occurring at Portsmouth or ETTP.

- *Supplement Analysis for Transportation of DOT Compliant Depleted Uranium Hexafluoride Cylinders from the East Tennessee Technology Park to the Portsmouth Gaseous Diffusion Plant in Fiscal Years 2003 through 2005* (DOE 2003d): The purpose of this supplement analysis is to provide a basis for determining whether the existing PEIS NEPA analysis and documentation would be sufficient to allow DOE to transport up to 1,700 full cylinders containing DUF<sub>6</sub> from its ETTP location to the Portsmouth site in FYs 2003 through 2005. All of these cylinders would be compliant with DOT regulatory requirements. Details of the proposed shipment campaign are presented in a transportation plan prepared by Bechtel Jacobs Company LLC (2003). Based on the Supplement Analysis, DOE issued an amended ROD to the PEIS concluding that the estimated impacts for the proposed shipment of up to 1,700 cylinders were less than or equal to those considered in the PEIS and

that no further NEPA documentation was required (68 FR 53603). However, this EIS considers shipment of all DUF<sub>6</sub> and non-DUF<sub>6</sub> at ETTP to Portsmouth (proposed) and Paducah (option). No shipments were made in FY 2003; it is expected that the planned shipments would occur in FY 2004 and FY 2005.

- *Draft Environmental Assessment: Reindustrialization Program at the Portsmouth Gaseous Diffusion Plant, Piketon, Ohio* (DOE 2001b): DOE proposes to transfer real property (i.e., underutilized, surplus, or excess Portsmouth GDP land and facilities) by lease and/or disposal (e.g., sale, donation, transfer to another federal agency, exchange) via a reindustrialization program. DOE prepared this environmental assessment (EA) to give the public information on the potential impacts that could result from the proposed transfer of land and facilities and to ensure that environmental impacts are considered in the decision-making process. This EA (1) describes the existing environment at Portsmouth relevant to potential impacts associated with the proposed action and alternatives; (2) analyzes potential environmental impacts, including those from development of a range of industrial and commercial uses; (3) identifies and characterizes cumulative impacts that could result from Portsmouth reindustrialization in relation to other ongoing or proposed activities within the surrounding area; and (4) provides DOE with environmental information to use in prescribing restrictions to protect, preserve, and enhance the human environment and natural ecosystems.
- *Environmental Assessment: Winterization Activities in Preparation for Cold Standby at the Portsmouth Gaseous Diffusion Plant, Piketon, Ohio* (DOE 2001c): DOE proposes to conduct winterization activities in preparation for cold standby of facilities at DOE's Portsmouth GDP in Piketon, Ohio. Winterization of Portsmouth was deemed necessary because DOE had decided to place the plant in cold standby and because facilities and systems had to be protected from freezing after USEC was to stop enriching uranium at Portsmouth in 2001. DOE prepared this EA to give the public information on the potential impacts that could result from the proposed action and reasonable alternatives and to ensure that potential environmental impacts would be considered in the decision-making process. This EA (1) describes the existing environment at Portsmouth relevant to potential impacts of the proposed action and alternatives; (2) analyzes potential environmental impacts; (3) identifies and characterizes cumulative impacts that could result from Portsmouth in relation to other ongoing or proposed activities within the surrounding area; and (4) provides DOE with environmental information to use in prescribing restrictions to protect, preserve, and enhance the human environment and natural ecosystems.

- *Draft Environmental Assessment Addendum for the Proposed Transfer of Parcel ED-1 to the Community Reuse Organization of East Tennessee* (DOE 2002a): In January 1996, DOE executed a lease for the Community Reuse Organization of East Tennessee (CROET) to develop an industrial/business park at the 957-acre (387-ha) Parcel ED-1 of Oak Ridge Reservation (ORR). The purpose of the DOE action was to transfer excess DOE real property in order to continue and further support economic development in the region. This proposed action is being evaluated in response to a proposal from CROET to transfer fee title for the presently leased Parcel ED-1. DOE's action is needed to help offset economic losses resulting from DOE downsizing, facility closures, and workforce restructuring. DOE also recognizes that transferring excess land for economic development purposes can benefit the federal government by reducing or eliminating landlord costs. The purpose of this EA addendum is to analyze the DOE proposal to transfer title of Parcel ED-1 to CROET.
- *Final Programmatic Environmental Assessment for the U.S. Department of Energy, Oak Ridge Operations Implementation of a Comprehensive Management Program for the Storage, Transportation, and Disposition of Potentially Re-Usable Uranium Materials* (DOE 2003c): DOE proposes to implement a comprehensive management program to safely, efficiently, and effectively manage its potentially reusable low-enriched uranium, normal uranium, and depleted uranium. Uranium materials presently located at multiple sites are to be consolidated by transporting the materials to one or several locations to facilitate disposition. Management would include the storage, transport, and ultimate disposition of these materials. This programmatic EA (PEA) addresses the proposed action to implement a long-term (more than 20 years) management plan for DOE's inventory of potentially reusable low-enriched, normal, and depleted uranium. A Finding of No Significant Impact (FONSI) was approved on October 16, 2002.
- *Environmental Assessment for Transportation of Low-Level Radioactive Waste from the Oak Ridge Reservation to Off-Site Treatment or Disposal Facilities* (DOE 2001a): DOE proposes to transport LLW from ORR for treatment or disposal at various locations in the United States. This EA for the transport of LLW was prepared in accordance with CEQ and DOE regulations and DOE orders and guidance. On the basis of the findings presented in this EA, DOE has determined that the proposed transportation of legacy and operational LLW from ORR for treatment or disposal at representative DOE sites and licensed commercial facilities located in the continental United States would not constitute a major federal action that would significantly affect the quality of the human environment within the context of NEPA. DOE concluded that preparation of an EIS was not required.

- *Final Environmental Impact Statement for Treating Transuranic (TRU)/Alpha Low-Level Waste at the Oak Ridge National Laboratory (DOE 2000b)*: DOE proposes to construct, operate, and decontaminate and decommission a TRU waste treatment facility in Oak Ridge, Tennessee. The four waste types that would be treated at the proposed facility would be (1) remote-handled TRU mixed waste sludge, (2) liquid LLW associated with the sludge, (3) contact-handled TRU/alpha LLW solids, and (4) remote-handled TRU/alpha LLW solids. The mixed waste sludge and some of the solid waste contain metals regulated under the Resources Conservation and Recovery Act (RCRA) and might be classified as mixed waste. This document analyzes the potential environmental impacts associated with five alternatives: no action, the low-temperature drying alternative (preferred alternative), the vitrification alternative, the cementation alternative, and the treatment and waste storage at ORNL alternative.
- *Construction and Operation of the Spallation Neutron Source Facility (DOE 1999d)*: DOE proposes to construct and operate a state-of-the-art, short-pulsed spallation neutron source composed of an ion source, a linear accelerator, a proton accumulator ring, and an experiment building containing a liquid mercury target and a suite of neutron scattering instrumentation. The proposed Spallation Neutron Source would be designed to operate at a proton beam power of 1 MW. The design would accommodate future upgrades to a peak operating power of 4 MW. This document analyzes the potential environmental impacts from the proposed action and the alternatives. The analysis assumes the facility would operate at powers of 1 and 4 MW over its lifetime. The two primary alternatives analyzed in this final EIS are the proposed action (to proceed with building the Spallation Neutron Source) and the no action alternative. The no action alternative describes the expected condition of the environment if no action was taken. Four siting alternatives for the Spallation Neutron Source are evaluated: ORNL in Oak Ridge, Tennessee (preferred alternative); Argonne National Laboratory (ANL) in Argonne, Illinois; Brookhaven National Laboratory (BNL) in Upton, New York; and Los Alamos National Laboratory (LANL) in Los Alamos, New Mexico.
- *Final Waste Management Programmatic Environmental Impact Statement for Managing Treatment, Storage, and Disposal of Radioactive and Hazardous Waste (DOE 1997a)*: This EIS (referred to herein as the WM PEIS) evaluates the impacts of different approaches to the treatment, storage, and disposal of the existing and projected DOE inventory of certain types of waste management program wastes over the next 20 years. The WM PEIS considers radioactive low-level, high-level, TRU, and mixed wastes, as well as toxic and hazardous wastes. The amounts of wastes analyzed for treatment, storage, or disposal range from thousands to millions of cubic meters and include wastes generated at the DOE sites in Paducah, Kentucky; Portsmouth, Ohio; and Oak Ridge, Tennessee. The WM PEIS does not evaluate management of DUF<sub>6</sub>

because that material is considered a source material, not a waste. The draft WM PEIS was issued in September 1995, and the final was issued in May 1997.

The WM PEIS considers the impacts of waste management at Paducah, Portsmouth, and ORR on the basis of the existing and projected inventories of waste generated during site operations. The three sites are also considered candidate sites for regionalized waste management sites, and waste management impacts are evaluated for these scenarios as well. Cumulative impacts of current operations, waste management, and proposed future operations are also assessed for the three sites in the WM PEIS.

## **1.8 OTHER DOCUMENTS AND STUDIES RELATED TO DUF<sub>6</sub> MANAGEMENT AND CONVERSION ACTIVITIES**

In addition to the related NEPA reviews described in Section 1.7, other reports that relate to managing the DUF<sub>6</sub> inventory (covering conversion, transportation, characterization, and disposal activities) that were completed after the DUF<sub>6</sub> PEIS was published were also reviewed in preparing this EIS. A list of the reports reviewed and used as a part of the preparation for this EIS is provided here.

- *Final Plan for the Conversion of Depleted Uranium Hexafluoride as Required by Public Law 105-204* (DOE 1999b): This report is the final plan for converting DOE's DUF<sub>6</sub> inventory, as required by P.L. 105-204. This Conversion Plan describes the steps that would allow DOE to convert the DUF<sub>6</sub> inventory to a more stable chemical form. It incorporates information received from the private sector in response to DOE's request for expressions of interest; ideas from members of the affected communities, Congress, and other interested stakeholders; and the results of the analyses for the final DUF<sub>6</sub> PEIS. The Conversion Plan describes DOE's intent to chemically process the DUF<sub>6</sub> to create products that would present a lower long-term storage hazard and provide a material suitable for use or disposal.
- *U.S. Department of Energy DUF<sub>6</sub> Materials Use Roadmap* (DOE 2000a): This report meets the commitment presented in the Conversion Plan by providing a comprehensive roadmap that DOE will use to guide any future R&D activities for the materials associated with its DUF<sub>6</sub> inventory. It supports the decision presented in the ROD, namely, to begin conversion of the DUF<sub>6</sub> inventory to uranium oxide, uranium metal, or a combination of both as soon as possible, while allowing for future uses for as much of this inventory as possible. This roadmap is intended to explore potential uses for the DUF<sub>6</sub> conversion products and identify areas where further development is needed. Although it focuses on potential governmental uses of DUF<sub>6</sub> conversion products, it also incorporates a limited analysis of private sector

uses. This roadmap also addresses other surplus depleted uranium, primarily in the form of depleted uranium trioxide (UO<sub>3</sub>) and depleted UF<sub>4</sub>.

- *Depleted Uranium Hexafluoride Management Program: Data Compilation for the Portsmouth Site in Support of Site-Specific NEPA Requirements for Continued Cylinder Storage, Cylinder Preparation, Conversion, and Long-Term Storage Activities* (Hartmann 1999a): This report is a compilation of data and analyses for the Portsmouth site that were obtained and conducted to prepare the DUF<sub>6</sub> PEIS. The report describes the affected environment at the Portsmouth site and summarizes potential environmental impacts that could result from conducting the following DUF<sub>6</sub> activities at the site: continued cylinder storage, preparation of cylinders for shipment, conversion, and long-term storage.
- *Depleted Uranium Hexafluoride Management Program: Data Compilation for the K-25 Site in Support of Site-Specific NEPA Requirements for Continued Cylinder Storage and Cylinder Preparation Activities* (Hartmann 1999b): This report is a compilation of data and analyses for the ETTP site (formerly called the K-25 site) that were obtained and conducted to prepare the DUF<sub>6</sub> PEIS. The report describes the affected environment at the ETTP site and summarizes the potential environmental impacts that could result from continued cylinder storage and preparation of cylinders for shipment at the site.
- *Evaluation of UF<sub>6</sub>-to-UO<sub>2</sub> Conversion Capability at Commercial Nuclear Fuel Fabrication Facilities* (Ranek and Monette 2001): This report examines the capabilities of existing commercial nuclear fuel fabrication facilities to convert DUF<sub>6</sub> to depleted UO<sub>2</sub>. For domestic facilities, the information summarized includes currently operating capacity to convert DUF<sub>6</sub> to UO<sub>2</sub>; transportation distances from DUF<sub>6</sub> storage locations near Oak Ridge, Portsmouth, and Paducah to the commercial conversion facilities; and regulatory requirements for nuclear fuel fabrication and transportation of DUF<sub>6</sub>. The report concludes that current U.S. commercial nuclear fuel fabricators could convert 5,200 t (5,700 tons) of DUF<sub>6</sub> per year to UO<sub>2</sub> (which includes 666 t (734 tons) of DUF<sub>6</sub> per year of capacity that was scheduled for shutdown by the end of 2001). However, only about 300 t (330 tons) of DUF<sub>6</sub> per year of this capacity could be confirmed as being possibly available to DOE. The report also provides some limited descriptions of the capabilities of foreign fuel fabrication plants to convert DUF<sub>6</sub> to UO<sub>2</sub>.
- *Assessment of Preferred Depleted Uranium Disposal Forms* (Croff et al. 2000a): This study assesses the acceptability of various potential depleted uranium conversion products for disposal at likely LLW disposal sites. The objective is to help DOE decide the preferred form for the depleted uranium conversion product and determine a path that will ensure reliable and efficient disposal. The study was conducted under the expectation that if worthwhile

beneficial uses could not be found for the converted depleted uranium product, it would be sent to an appropriate site for disposal. The depleted uranium products are considered to be LLW under both DOE orders and NRC regulations. A wide range of issues associated with disposal are discussed in the report. The report concludes that, on balance, the four potential forms of depleted uranium (uranium metal, UF<sub>4</sub>, UO<sub>2</sub>, and U<sub>3</sub>O<sub>8</sub>) considered in the study should be acceptable, with proper controls, for near-surface disposal at sites such as NTS and Envirocare.

- *Evaluation of the Acceptability of Potential Depleted Uranium Hexafluoride Conversion Products at the Envirocare Disposal Site* (Croff et al. 2000b): With regard to the Envirocare site, the earlier report (Croff et al. 2000a), concluded that “current waste acceptance criteria suggest that the acceptability of depleted uranium hexafluoride conversion material for disposal at Envirocare of Utah is questionable. Further investigation is required before a definitive determination can be made.” The purpose of this report is to document the more thorough investigation suggested in the earlier report. It concludes that an amendment to the Envirocare license issued on October 5, 2000, has reduced the uncertainties associated with disposal of the depleted uranium product at Envirocare to the point that they are now comparable with uncertainties associated with the disposal of the depleted uranium product at NTS that were discussed in the earlier report.
- *Transportation Impact Assessment for Shipment of Uranium Hexafluoride (UF<sub>6</sub>) Cylinders from the East Tennessee Technology Park to the Portsmouth and Paducah Gaseous Diffusion Plants* (Biber et al. 2001): This report presents a transportation impact assessment for shipping the 4,683 full cylinders of DUF<sub>6</sub> (containing a total of approximately 56,000 t [62,000 tons]) stored at ETTP to the Portsmouth and Paducah sites for conversion. It also considers the transport of 2,394 cylinders stored at ETTP that contain a total of 25 t (28 tons) of enriched and normal uranium or that are empty. Shipments by both truck and rail are considered, with and without cylinder overpacks. In addition, the report contains an analysis of the current and pending regulatory requirements applicable to packaging UF<sub>6</sub> for transport by truck or rail, and it evaluates regulatory options for meeting the packaging requirements.
- *Strategy for Characterizing Transuranics and Technetium Contamination in Depleted UF<sub>6</sub> Cylinders* (Hightower et al. 2000): This report summarizes the results of a study performed to develop a strategy for characterizing low levels of radioactive contaminants (Pu, Np, Am, and Tc) in DUF<sub>6</sub> cylinders at the ETTP, Portsmouth, and Paducah sites. The principal conclusion from this review and analysis is that even without additional sampling, the current body of knowledge is sufficient to give potential conversion vendors an adequate basis for designing facilities that can operate safely. The report also provides upper-bound estimates of Pu, Np, and Tc concentrations in DUF<sub>6</sub> cylinders.

- *A Peer Review of the Strategy for Characterizing Transuranics and Technetium Contamination in Depleted Uranium Hexafluoride Tails Cylinders* (Brumburgh et al. 2000): This document provides the findings from a peer review of the ORNL study (Hightower et al. 2000) that set forth a strategy for characterizing low levels of radioactive contaminants in DUF<sub>6</sub> cylinders at the ETTP, Portsmouth, and Paducah sites. This peer review evaluates the ORNL study in three main areas: TRU chemistry/radioactivity, statistical approach, and the uranium enrichment process. It provides both general and specific observations about the general characterization strategy and its recommendations.

## 1.9 ORGANIZATION OF THIS ENVIRONMENTAL IMPACT STATEMENT

This DUF<sub>6</sub> Conversion EIS consists of two volumes. Volume 1 contains 10 chapters and 8 appendixes. Volume 2 contains the comment response document for the review of the draft EIS. Brief summaries of the main components of the EIS follow:

Volume 1 — Main Text and Appendixes:

- Chapter 1 introduces the EIS, discussing pertinent background information, the purpose of and need for the DOE action, the scope of the assessment, related NEPA reviews, other related reports and studies, and EIS organization.
- Chapter 2 defines the alternatives and implementation options considered in the EIS, defines alternatives considered but not analyzed in detail, and presents a summary comparison of the estimated environmental impacts.
- Chapter 3 discusses the environmental setting at the Portsmouth and ETTP sites.
- Chapter 4 addresses the assumptions on which this EIS and its analyses are based, defines the approaches to and methods for environmental impact assessment used in developing this EIS, and presents background information on the human health assessment.
- Chapter 5 discusses the potential environmental impacts of the alternatives. This chapter also discusses potential cumulative impacts at the Portsmouth and ETTP sites; possible mitigation of adverse impacts that are unavoidable; irreversible commitment of resources; the relationship between short-term use of the environment and long-term productivity; pollution prevention and waste minimization; and impacts from D&D activities.

- Chapter 6 identifies the major laws, regulations, and other requirements applicable to implementing the alternatives.
- Chapter 7 is an alphabetical listing of all the references cited in the EIS. All cited references are available to the public.
- Chapter 8 lists the names, education, and experience of persons who helped prepare the EIS. Also included are the subject areas for which each preparer was responsible.
- Chapter 9 presents brief definitions of the technical terminology used in the EIS.
- Chapter 10 is a subject matter index that provides the numbers of pages where important terms and concepts are discussed.
- Appendix A presents the pertinent text of P.L. 107-206, which mandates the construction of conversion facilities at the Portsmouth and Paducah sites.
- Appendix B discusses issues associated with potential TRU and Tc contamination of a portion of the DUF<sub>6</sub> inventory as well as PCBs contained in some cylinder coatings and describes how such contamination was addressed in this EIS.
- Appendix C summarizes the comments received during public scoping.
- Appendix D contains the environmental synopsis prepared to support the DUF<sub>6</sub> conversion process.
- Appendix E discusses potential uses of HF and CaF<sub>2</sub>, the DOE-authorized release process, and impacts associated with sale and use.
- Appendix F describes the assessment methodologies used to evaluate the potential environmental impacts.
- Appendix G contains copies of consultation letters regarding the preparation of this EIS that were sent to state agencies and recognized Native American groups.
- Appendix H contains the contractor disclosure statement.

#### Volume 2 — Responses to Public Comments:

- Chapter 1 provides an overview of the public participation and comment process.

- Chapter 2 provides copies of the actual letters or other documents that contain comments on the draft EIS to DOE.
- Chapter 3 lists DOE responses to all comments received.

## 2 DESCRIPTION AND COMPARISON OF ALTERNATIVES

Alternatives for building and operating a DUF<sub>6</sub> conversion facility at the Portsmouth site were evaluated for their potential impacts on the human and natural environment. This EIS considers the proposed action of building and operating a conversion facility for conversion of the Portsmouth and ETTP DUF<sub>6</sub> cylinder inventories and a no action alternative. Under the proposed action, three action alternatives are considered that focus on where to construct the conversion facility within the Portsmouth site. The action alternatives include the shipment of DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders currently stored at ETTP to Portsmouth. In addition, the construction of a new cylinder storage yard at Portsmouth, if required for ETTP cylinders, is considered. The no action alternative assumes that a conversion facility is not built at Portsmouth and that the cylinders would continue to be stored indefinitely at Portsmouth and ETTP in a manner consistent with current management practices. This chapter defines these alternatives and options in detail and discusses the types of activities that would be required under each. A summary of the alternatives considered in this EIS is presented in Table 2.1-1.

### Alternatives Considered in This EIS

**No Action:** NEPA regulations require evaluation of a no action alternative. In this EIS, the no action alternative is storage of DUF<sub>6</sub> cylinders indefinitely in yards at the Portsmouth and ETTP sites, with continued cylinder surveillance and maintenance activities.

**Proposed Action:** Construction and operation of a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products.

**Action Alternatives:** Three action alternatives focus on where to construct the conversion facility within the Portsmouth site (Alternative Location A, B, or C). The preferred alternative is Location A.

A separate EIS prepared for construction and operation of a conversion facility at the Paducah site (DOE 2004a) also includes a no action alternative. The no action alternative defined in the Paducah EIS includes an evaluation of the potential impacts of indefinite long-term storage of cylinders at Paducah.

In addition to describing the alternatives evaluated in this EIS, this chapter includes a discussion of alternatives considered but not analyzed in detail (Section 2.3) and a summary comparison of the potential environmental impacts from the alternatives (Section 2.4). The comparison of alternatives is based on information about the environmental setting provided in Chapter 3, descriptions of the assessment methodologies provided in Chapter 4, and the detailed assessment results presented in Chapter 5.

### 2.1 NO ACTION ALTERNATIVE

Under the no action alternative, it is assumed that DUF<sub>6</sub> cylinder storage would continue indefinitely at the Portsmouth and ETTP sites. The no action alternative assumes that DOE would continue surveillance and maintenance activities to ensure the continued

**TABLE 2.1-1 Summary of Alternatives Considered**

Alternative	Description	Options Considered
No Action (Section 2.1)	Continued storage of the DUF <sub>6</sub> cylinders indefinitely at the Portsmouth and ETTP sites, with continued cylinder surveillance and maintenance.	None.
Proposed Action (Section 2.2)	<p>Construction and operation of a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products. This EIS assesses the potential environmental impacts from the following proposed activities:</p> <ul style="list-style-type: none"> <li>• Construction, operation, maintenance, and D&amp;D of the proposed DUF<sub>6</sub> conversion facility at the Portsmouth site;</li> <li>• Transportation of DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders from ETTP to Portsmouth;</li> <li>• Construction of a new cylinder storage yard (if required) for ETTP cylinders;</li> <li>• Transportation of uranium conversion products and waste materials to a disposal facility;</li> <li>• Transportation and sale of the HF conversion product; and</li> <li>• Neutralization of HF to CaF<sub>2</sub> and sale or disposal in the event that the HF product is not sold.</li> </ul>	<p><i>ETTP Cylinders:</i> This EIS considers an option of shipping cylinders at ETTP to Paducah.</p> <p><i>Transportation:</i> This EIS evaluates the shipment of cylinders and conversion products by both truck and rail.</p> <p><i>Expanded Operations:</i> This EIS discusses the impacts associated with potential expansion of plant operations by extending the operational period and by increasing throughput (by efficiency improvements or by adding a fourth process line).</p>
Alternative Location A (Preferred) (Section 2.2.1.1)	Construction of the conversion facility at Location A, an area that encompasses 26 acres (10 ha) in the west-central portion of the site.	
Alternative Location B (Section 2.2.1.2)	Construction of the conversion facility at Location B, an area that encompasses 50 acres (20 ha) in the southwest portion of the site.	
Alternative Location C (Section 2.2.1.3)	Construction of the conversion facility at Location C, an area that encompasses 78 acres (31 ha) in the southeast portion of the site.	

safe storage of cylinders. Potential environmental impacts are estimated through the year 2039. The year 2039 was selected to be consistent with the DUF<sub>6</sub> PEIS (DOE 1999a), which evaluated a 40-year cylinder storage period (1999 through 2039). In addition, long-term impacts (i.e., occurring after 2039) from potential cylinder breaches are assessed. A similarly defined no action alternative was also evaluated in the DUF<sub>6</sub> PEIS. The assessment of the no action alternative in this EIS has been updated to reflect changes that have occurred since publication of the DUF<sub>6</sub> PEIS in 1999. Details are provided below.

#### **No Action Alternative**

It is assumed that the DUF<sub>6</sub> cylinders would continue to be stored indefinitely at the Portsmouth and ETTP sites and that cylinder surveillance and maintenance would also continue. Impacts are evaluated through the year 2039; in addition, potential long-term (after 2039) impacts are evaluated.

Specifically, the activities assumed to occur include routine cylinder inspections, ultrasonic testing of the wall thickness of selected cylinders, painting of selected cylinders to prevent corrosion, cylinder yard surveillance and maintenance, and relocation of some cylinders. It is assumed that cylinders would be painted every 10 years. On the basis of these activities, an assessment of the potential impacts on workers, members of the public, and the environment was conducted.

Breached cylinders are cylinders that have a hole of any size at some location on the wall. The occurrence of cylinder breaches, caused by either corrosion or handling damage, is an important concern when the potential impacts of continued cylinder storage are evaluated. There is a general concern that the number of cylinder breaches at the sites could increase in the future as the cylinder inventory ages.

At the time the PEIS was published (1999), 8 breached cylinders had been identified at the three storage sites; 3 of those breaches were at Portsmouth and 4 were at ETTP.<sup>1</sup> Investigation of these breaches indicated that 6 of the 8 were initiated by mechanical damage during stacking; the damage was not noticed immediately, and subsequent corrosion occurred at the damaged point. It was concluded that the other 2 cylinder breaches, both at ETTP, had been caused by external corrosion due to prolonged ground contact.

For assessment purposes in this EIS, two cylinder breach cases are evaluated. In the first case, it is assumed that the planned cylinder maintenance and painting program would maintain the cylinders in a protected condition and control further corrosion. In this case, it is assumed that after initial painting, some cylinder breaches would occur from handling damage; a total of 16 breaches are estimated to occur through 2039 at the Portsmouth site and a total of 7 for the ETTP site. In the second case, it is assumed that external corrosion would not be halted by improved storage conditions, cylinder maintenance, and painting. This case is considered in order to account for uncertainties with regard to how effective painting would be in controlling

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<sup>1</sup> An additional breach that occurred at the ETTP site in 1998 was discussed in Section B.2 of the PEIS (DOE 1999a). In the period 1998 through 2002, two additional breaches were discovered at the Paducah site. A total of 11 breaches have been identified at the Portsmouth, ETTP, and Paducah sites.

cylinder corrosion and uncertainties in the future painting schedule. In this case, the numbers of future breaches estimated through 2039 are 74 for the Portsmouth site and 213 for the ETTP site. These breach estimates were determined on the basis of historical corrosion rates when cylinders were stored under poor conditions (i.e., cylinders were stacked too close together, were stacked on wooden chocks, or came in contact with the ground). Because storage conditions have improved dramatically over the last several years as a result of cylinder yard upgrades and restacking activities, it is expected that these breach estimates based on the historical corrosion rate provide a worst case for estimating the potential impacts from continued cylinder storage. The results of this assessment were used to provide an estimate of the earliest time when continued cylinder storage could begin to raise regulatory concerns under these worst-case conditions.

The impacts to human health and safety, surface water, groundwater, soil, air quality, and ecology from uranium and HF releases from breached cylinders are assessed in this EIS. For all hypothetical cylinder breaches, it is assumed that the breach would be undetected for 4 years, which is the period between planned inspections for most of the cylinders. In practice, cylinders that show evidence of damage or heavy external corrosion are inspected annually, so it is very unlikely that a breach would be undetected for a 4-year period. For each hypothetical cylinder breach, it is further assumed that 1 lb (0.45 kg) of uranium (as UO<sub>2</sub>F<sub>2</sub>) and 4.4 lb (2 kg) of HF would be released from the cylinder annually for a period of 4 years.

The estimated numbers of future breaches at the Portsmouth and ETTP sites were used to estimate potential impacts that might occur during the repair of breached cylinders and impacts from releases that might occur during continued cylinder storage. Potential radiological exposures of involved workers could result from patching breached cylinders or emptying the cylinder contents into new cylinders. The impacts on groundwater and human health and safety from uranium releases were assessed by estimating the amount of uranium that could be transported from the yards in surface runoff and the amount that could migrate through the soil to the groundwater.

For this EIS, a reassessment of the no action alternative assumptions used in the PEIS was conducted. Recent cylinder surveillance and maintenance plans — including inspections and painting — were used to update the PEIS no action alternative assessment. The results of this reevaluation, together with a consideration of the changes in the on-site worker and off-site public populations at Portsmouth and ETTP, were used to determine the impacts from the no action alternative. Additional discussion and the estimated impacts from the no action alternative are presented in Section 5.1.

## 2.2 PROPOSED ACTION

The proposed action evaluated in this EIS is to construct and operate a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products. Three locations within the Portsmouth site are evaluated as alternatives (see Section 2.2.1). The proposed action includes shipping the ETTP cylinders to Portsmouth and construction of a new cylinder storage

yard at Portsmouth for the ETTP cylinders, if required. The conversion facility would convert DUF<sub>6</sub> into a stable chemical form for beneficial use/reuse and/or disposal. The off-gas from the conversion process would yield aqueous HF, which would be processed and marketed or converted to a solid for sale or disposal. To support the conversion operations, the emptied DUF<sub>6</sub> cylinders would be stored, handled, and processed for reuse as disposal containers to the extent practicable. The time period considered is a construction period of approximately 2 years, an operational period of 18 years, and a 3-year period for the D&D of the facility. Current plans call for construction to begin in the summer of 2004. The assessment is based on the conceptual conversion facility design proposed by the selected contractor, UDS (see text box).

**Proposed Action**

The proposed action in this EIS is construction and operation of a DUF<sub>6</sub> conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide (primarily U<sub>3</sub>O<sub>8</sub>) and other conversion products. DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders would be transported from ETTP to Portsmouth; and a cylinder storage yard would be constructed at Portsmouth for ETTP cylinders, if required. Three alternative locations within the Portsmouth site are evaluated (Locations A, B, and C).

This EIS assesses the potential environmental impacts from the following proposed activities:

- Construction, operation, maintenance, and D&D of the proposed DUF<sub>6</sub> conversion facility at the Portsmouth site;
- Transportation of DUF<sub>6</sub> cylinders and non-DUF<sub>6</sub> cylinders from ETTP to Portsmouth;
- Construction of a new cylinder storage yard (if required) for ETTP cylinders;
- Transportation of uranium conversion products and waste materials to a disposal facility;
- Transportation and sale of the HF conversion product; and
- Neutralization of HF to CaF<sub>2</sub> and its sale or disposal in the event that the HF product is not sold.

**Conversion Facility Design**

The EIS is based on the conversion facility design being developed by UDS, the selected conversion contractor. At the time the draft EIS was prepared, the UDS design was in the 30% conceptual stage, with several facility design options being considered.

Following the public comment period, the draft EIS was revised on the basis of comments received and on the basis of 100% conceptual facility design. This final EIS identifies and evaluates design options to the extent possible.

In addition, an option of expanding operations by extending the conversion facility operational period or increasing throughput is discussed in this section.

### 2.2.1 Action Alternatives

The action alternatives focus on where to site the conversion facility within the Portsmouth site. The Portsmouth site was evaluated to identify alternative locations for a conversion facility (Shaw 2001). Potential locations were evaluated on the basis of the following criteria:

- *Current condition of the land and site preparation required.* This criterion looked at the condition of the land from a constructability viewpoint, considering factors that would increase the construction cost over the amount needed for a relatively level grassy topography.
- *Legacy environmental concerns.* This criterion looked at environmental factors that would affect construction at the site.
- *Availability of utilities.* This criterion looked at the relative difficulty of bringing services from existing plant utilities to the site.
- *Location.* This criterion looked at the advantages and disadvantages of location in relation to cylinder transport between the yards and the new facility.
- *Effect on current plant operations.* This criterion looked at how the conversion facility's location could affect existing plant operations.
- *Size.* This criterion looked at size to ensure that the required minimum amount of land would be available for construction of the conversion facility (assumed to be about 30 acres [12 ha]).

The three alternative locations identified at the Portsmouth site, denoted Locations A, B, and C, are shown in Figure 2.2-1.

#### 2.2.1.1 Alternative Location A (Preferred Alternative)

Location A is the preferred location for the conversion facility and is located in the west-central portion of the site, encompassing 26 acres (10 ha). This location has three existing structures that were formerly used to store containerized lithium hydroxide monohydrate. These warehouses, which were originally erected in the early 1950s to support construction of the Portsmouth GDP, have 4-in. (10-cm) concrete floors. The structures are made of steel and are what is now commonly called pre-engineered steel buildings. No utilities are functional in these buildings. The open field north and east of the buildings was rough graded several times; the last time was in the late 1970s. The site was also rough graded, and storm water ditch systems were installed. Two railroad spurs existed at one time in this area. One has had the track and ties removed, and the other has fallen into disrepair. This location was identified in the RFP for conversion services as the site for which bidders were to design their proposed facilities.

### **2.2.1.2 Alternative Location B**

Location B is in the southwest portion of the site and encompasses approximately 50 acres (20 ha). The site has two existing structures built as part of the gas centrifuge enrichment project that was begun in the early 1980s and was terminated in 1985. The first building is a two-story building (110,000 ft<sup>2</sup> [10,219 m<sup>2</sup>] of floor) constructed of steel, with metal siding to house uranium material feed and withdrawal facilities. The facility was never placed in operation, has had major equipment removed, and is currently not utilized. The other structure was constructed at the same time as an ingress and egress portal for both vehicles and pedestrians to a fenced, secure area. It is currently not utilized. The open field to the east of the buildings was developed during the same time period; it was rough graded, and storm water systems were installed.

It should be noted that USEC is currently in the process of developing and demonstrating an advanced enrichment technology based on gas centrifuges. A license for a lead test facility to be operated at the Portsmouth site was issued by the NRC in February 2004. The lead facility would be located in the existing gas centrifuge buildings within Location B. In addition, USEC has announced that it plans to site its American Centrifuge Facility at Portsmouth, although an exact location was not identified. Therefore, Location B might not be available for construction of the conversion facility.

### **2.2.1.3 Alternative Location C**

Location C is in the southeast portion of the site and has an area of about 78 acres (31 ha). This location consists of a level to very gently rolling grass field. It was graded during the construction of the Portsmouth site and has been maintained as grass fields since then.

## **2.2.2 Conversion Process Description**

This section provides a summary description of the proposed UDS conversion process and facility. The proposed UDS conversion system is based on a proven commercial process in operation at the Framatome Advanced Nuclear Power (ANP), Inc., fuel fabrication facility in Richland, Washington. The two primary sources for the information in this section are excerpts from the UDS conversion facility conceptual design report (UDS 2003a) and the UDS NEPA data package prepared for the 100% conceptual facility design (UDS 2003b).

The UDS dry conversion is a continuous process in which DUF<sub>6</sub> is vaporized and converted to a mixture of uranium oxides (primarily U<sub>3</sub>O<sub>8</sub>) by reaction with steam and hydrogen in a fluidized-bed conversion unit. The resulting depleted U<sub>3</sub>O<sub>8</sub> powder is collected and packaged for disposition. The process equipment would be arranged in parallel lines. Each line would consist of two autoclaves, two conversion units, an HF recovery system, and process off-gas scrubbers. The Portsmouth facility would have three parallel conversion lines. Equipment would also be installed to collect the HF co-product and process it into any combination of several marketable products. A backup HF acid neutralization system would be provided to

convert up to 100% of the HF acid to CaF<sub>2</sub> for storage, sale, or disposal in the future, if necessary. Figure 2.2-2 is an overall material flow diagram for the conversion facility; Figure 2.2-3 is a conceptual facility site plan. A summary of key facility characteristics is presented in Table 2.2-1.

The conversion facility will be designed to convert 13,500 t (15,000 tons) of DUF<sub>6</sub> per year, requiring 18 years to convert the Portsmouth and ETTP inventories. The total footprint of the Portsmouth processing facility would be approximately 148 ft × 271 ft (45 m × 83 m). The conversion facility would occupy a total of approximately 10 acres (4 ha), with up to 65 acres (26 ha) of land disturbed during construction (including temporary construction lay-down areas and utility access). Some of the disturbed areas would be areas cleared for railroad or utility access, not adjacent to the construction area.

DUF<sub>6</sub> cylinders would be delivered from long-term storage to the cylinder staging yard at the conversion facility by means of cylinder handling equipment already available at the site. The staging yard would accommodate short-term storage of cylinders. Cylinders in the conversion staging yard would be transferred into the conversion building airlock by using an overhead bridge crane. The cylinders would then be moved into the vaporization room to the autoclaves by an overhead monorail crane and/or rail cart. The cylinders would be loaded into autoclaves for heating and transfer of the DUF<sub>6</sub> to the conversion units.

Cylinders that could not be processed through the normal process feed system would be processed through the cylinder transfer facility. If the cylinder was overfilled, the excess DUF<sub>6</sub> would be transferred to another cylinder. This same system would be used to transfer all of the contents from unacceptable cylinders to cylinders suitable for feeding into the conversion process.

After the emptied cylinder was removed from the autoclave, a stabilizing agent would be introduced into the cylinder to neutralize residual fluoride in the heel. The cylinders would then be moved out to the staging yard for an approximate 4-month aging period so that short-lived uranium decay products in the nonvolatile heel would decay, thereby reducing potential radiation exposure during the processing of emptied cylinders. Emptied cylinders would then be reused as disposal containers or processed and disposed of as LLW.

Major conversion system components are described further in the following subsections. The plant design includes several other supporting facilities and services, including an electrical system with backup, a communications system, a deionized water system, a control system, an air supply system, a fire protection system, and a heating, ventilation, and air-conditioning system.

### **2.2.2.1 Cylinder Transfer System**

Some cylinders might be unacceptable for processing in the vaporization system autoclaves because of corrosion, damage, overfilling, or excessive size. A cylinder transfer

**TABLE 2.2-1 Summary of Portsmouth Conversion Facility Parameters**

Parameter/Characteristic	Value
Construction start	2004
Construction period	2 years
Start of operations	2006
Operational period	18 years
Facility footprint	10 acres (4 ha)
Facility throughput	13,500 t/yr (15,000 tons/yr) DUF <sub>6</sub> (≈1,000 cylinders/yr)
Conversion products	
Depleted U <sub>3</sub> O <sub>8</sub>	10,800 t/yr (11,800 tons/yr)
CaF <sub>2</sub>	18 t/yr (20 tons/yr)
70% HF acid	2,500 t/yr (2,800 tons/yr)
49% HF acid	5,800 t/yr (6,300 tons/yr)
Steel (emptied cylinders, if not used as disposal containers)	1,177 t/yr (1,300 tons/yr)
Proposed conversion product disposition (see Table 2.2-2 for details)	
Depleted U <sub>3</sub> O <sub>8</sub>	Disposal; Envirocare (primary), NTS (secondary) <sup>a</sup>
CaF <sub>2</sub>	Disposal; Envirocare (primary), NTS (secondary)
70% HF acid	Sale pending DOE approval
49% HF acid	Sale pending DOE approval
Steel (emptied cylinders, if not used as disposal containers)	Disposal; Envirocare (primary), NTS (secondary)

<sup>a</sup> DOE plans to decide the specific disposal location(s) for the depleted U<sub>3</sub>O<sub>8</sub> conversion product after additional appropriate NEPA review. Accordingly, DOE will continue to evaluate its disposal options and will consider any further information or comments relevant to that decision. DOE will give a minimum 45-day notice before making the specific disposal decision and will provide any supplemental NEPA analysis for public review and comment.

Sources: UDS (2003a,b).

system would be used to transfer the contents of up to four unacceptable cylinders per week to acceptable cylinders. Cylinder transfer system equipment would include two low-temperature autoclaves, four fill positions, a “hot box” containing controls and vacuum pumps, and an oversize cylinder heating room. Fill positions would include a water spray cooling system necessary for low-temperature DUF<sub>6</sub> transfer. The oversize cylinder heating room would contain radiant heating enclosure controls and connections.

### 2.2.2.2 Vaporization System

Cylinders that met the vaporization criteria would be brought to the vaporization room and loaded into electrically heated autoclaves. Autoclaves for each process line would be used to provide continuous feed to the DUF<sub>6</sub> conversion units. The cylinders would be heated to feed DUF<sub>6</sub> vapor to the process. The design will incorporate in-line filters to provide additional assurances that TRU isotopes would not enter the conversion system. The need for in-line filters would be evaluated during operations; they might be removed if they were not needed.

The DUF<sub>6</sub> vapor would flow through a heated enclosure called a “hot box,” which contains the equipment that would control flow to the conversion units, including vacuum pumps. The hot box has the necessary controls to achieve stable DUF<sub>6</sub> flow to the conversion units.

The autoclaves would be used to heat DUF<sub>6</sub> cylinders by internal electrical heating and to provide secondary DUF<sub>6</sub> containment. The selected autoclaves would be American Society of Mechanical Engineers standard pressure vessels, sufficiently designed to provide containment of DUF<sub>6</sub> and HF from a full, DUF<sub>6</sub> cylinder that had ruptured. Each autoclave system would include equipment and controls to connect to the cylinder, control DUF<sub>6</sub> flow, monitor DUF<sub>6</sub> weight, and control vaporization conditions.

Electrically heated autoclaves would provide a safety advantage over steam-heated units. If DUF<sub>6</sub> leaks in a steam autoclave, the DUF<sub>6</sub> reacts with the steam and generates HF gas, which pressurizes the autoclave and is extremely corrosive. If DUF<sub>6</sub> leaks in an electrically heated autoclave, however, the only moisture available is humidity in the air, which limits HF generation and subsequent pressurization and corrosion. This also makes cleanup of the autoclave much easier since the autoclave is evacuated directly to the conversion unit and does not produce wet uranium recycle and liquid wastes.

### 2.2.2.3 Conversion System

DUF<sub>6</sub> vapor would be reacted with steam and hydrogen in fluidized-bed conversion units. The hydrogen would be generated by using anhydrous ammonia (NH<sub>3</sub>). Nitrogen is also used as an inert purging gas and is released to the atmosphere through the building stack as part of the clean off-gas stream. The oxide powder would be retained in the conversion unit by passing the process off-gas through sintered metal filters. Uranium oxide powder would be continuously withdrawn from the conversion unit to match the feed rate of DUF<sub>6</sub>. Each conversion unit would be electrically heated and integrated with a heating/insulation jacket.

All equipment components (vessels, filters, etc.) in the conversion system would be fabricated of corrosion-resistant alloys suited to process conditions. In the event of a system failure or an unscheduled shutdown, the DUF<sub>6</sub> shutoff valve in the autoclave would automatically close. The DUF<sub>6</sub> piping would then be purged with nitrogen. In the event of power, instrument, air, or other failure, a fail-safe design would be used for valves and for the control system.

#### 2.2.2.4 Depleted Uranium Conversion Product Handling System

Depleted U<sub>3</sub>O<sub>8</sub> powder would be cooled as it was discharged from the conversion unit. An in-line water-cooled heat exchanger would cool the powder before it dropped into a vacuum transfer station enclosure. The vacuum transfer station would include connections, a vacuum transfer pickup device, a support vessel, a hopper, and a secondary enclosure to facilitate packaging the depleted U<sub>3</sub>O<sub>8</sub>. A package fill station would be located below each hopper. Powder fill would be controlled by weight in the fill container, and a secondary containment enclosure would be provided at the fill station. The filled packages would be lifted and conveyed by using an overhead monorail crane through an airlock and loaded into railcars for shipment to the disposal site. Each packaging station would operate on a semicontinuous basis with intermittent package removal and installation. Continuous level control would maintain the oxide hopper at 20% to 25% of capacity. Prior to package change out, the oxide discharge would be stopped.

UDS proposes to use the emptied cylinders as disposal containers to the extent practicable. An option of using bulk bags (large capacity, strong, flexible bags) as disposal containers is also being considered. After being processed (see Section 2.2.2.6), the emptied cylinders would be moved to the conversion product transfer station and refilled with depleted U<sub>3</sub>O<sub>8</sub> powder. The refilled cylinders would be sealed and loaded to railcars for shipment to the disposal site. Bulk bags would be handled similarly.

The conversion facilities are being designed with a short-term storage capacity for 6 months' worth of depleted uranium conversion products. This storage capacity is being provided in order to accommodate potential delays in disposal activities without affecting conversion operations. If a delay was to extend beyond 6 months, DOE would evaluate possible options and conduct appropriate NEPA review for those options.

#### 2.2.2.5 HF Recovery System

The fluorine component of the DUF<sub>6</sub> would leave the conversion unit as HF gas through sintered metal filters that would retain nearly all (greater than 99.9%) of the uranium in the conversion unit. The HF would be condensed, along with the unreacted excess steam, and the resulting HF acid would flow by gravity to receiver tanks. In addition, the off-gas would be passed through a series of two scrubbers to recover most of the uncondensed HF. In each scrubber, process off-gas would come into contact with 20% potassium hydroxide (KOH) solution. HF vapor would combine with KOH in the solution to form potassium fluoride (KF) and water (H<sub>2</sub>O); thus HF would be removed from the process off-gas stream.

The HF acid would be automatically transferred from the receivers to interim bulk storage tanks located outside the building. An in-line uranium analyzer in each transfer line would be used as a final verification that containment of the uranium was intact. High-integrity piping and equipment made with corrosion-resistant materials would result in zero leakage of HF, either gaseous or liquid, to the environment. The HF would be stored on site at each conversion facility for approximately 2 weeks or less under normal conditions and then shipped

to a vendor. The storage capacity for HF at each site is limited, and if the material could not be moved, it would be converted to CaF<sub>2</sub> or processing would stop.

#### **2.2.2.6 Emptied Cylinder Processing**

UDS proposes to use the emptied cylinders as disposal containers to the extent practicable. After removal of the cylinders from the autoclaves, a stabilizing agent would be introduced to the cylinders to neutralize residual fluoride in the heels. After an approximate 4-month aging period, emptied cylinders (with heel) would be transferred to the conversion product transfer stations, as described above. Alternatively, if bulk bags were used for depleted U<sub>3</sub>O<sub>8</sub> disposal containers, after an approximate 4-month aging period, emptied cylinders (with heel) would be transported into the cylinder disposition facility. A forklift would be used to move the cylinders to the feed queue outside the facility airlock. Cylinders would then be brought into the disposition facility via an overhead monorail crane and placed into a compactor feed station. The plugs would be removed from the cylinder to vent the cylinder during crushing. The cylinder would then be pushed by a ram into the compactor itself, where it would be compacted radially to a maximum thickness of 8 in. (20 cm). The compacted cylinder would then be pushed to the cutting station, where it would be cut in half to reduce the length. The two pieces of metal would be picked up with an overhead crane and placed into an intermodal shipping container. Debris from these operations would then be collected in a container by a vacuum system and loaded into the intermodal container.

Secondary containment would be provided for the intermodal container loadout. In addition, small cylinders that had not been compacted, as well as valves, plugs, and facility secondary waste, might also be loaded into the intermodal containers. Cylinders that were destined for disposal at NTS would not be introduced into the facility but would instead be loaded directly onto trucks or railcars for transport.

#### **2.2.2.7 Management of Potential Transuranic and PCB Contamination**

As discussed in Section 1.2.2, as a result of enrichment of reprocessed uranium in the early years of gaseous diffusion, some of the DUF<sub>6</sub> inventory is contaminated with small amounts of Tc and the TRU elements Pu, Np, and Am. In addition, a portion of the cylinder inventory was originally painted with coatings containing PCBs.

TRU contamination in the cylinders would exist as fluoride compounds that would be both insoluble in liquid DUF<sub>6</sub> and nonvolatile but capable of being entrained from the cylinders during the vaporization and feeding of DUF<sub>6</sub> into the conversion process. The TRU contamination would exist primarily as (1) small particulates dispersed throughout the DUF<sub>6</sub> contents and (2) small quantities in the residual heels from the original feed cylinders in a relatively small but unknown number of cylinders (see Appendix B for more details). Tc contamination would exist as fluoride and oxyfluoride compounds that would be stable and partially volatile, and the contamination would be present both uniformly dispersed throughout the DUF<sub>6</sub> and in the heel material referred to previously.

The TRU contaminants that are dispersed throughout the DUF<sub>6</sub> might be entrained in the gaseous DUF<sub>6</sub> during the cylinder emptying operations and carried out of the cylinders. These contaminants could be captured in filters between the cylinders and the conversion units. These filters would be monitored and changed out periodically to prevent buildup of TRU. They would be disposed of as LLW.

It is also expected that the nonvolatile forms of Tc that exist in the cylinders would remain in the heels or be captured in the filters. However, because of the existence of some volatile technetium fluoride compounds, and for the purposes of analyses in this EIS, it is assumed that all of the Tc dispersed in the DUF<sub>6</sub> would volatilize with DUF<sub>6</sub> and be carried into the conversion process equipment. Any Tc compounds transferred into the conversion units would be oxidized along with the DUF<sub>6</sub>. For this EIS, it is also assumed that the Tc in the form of oxides would partition into the U<sub>3</sub>O<sub>8</sub> and HF products in the same ratio as the uranium. It is assumed that Tc left in the heels from the original feedstock would remain behind after the DUF<sub>6</sub> was vaporized.

If bulk bags were used for depleted U<sub>3</sub>O<sub>8</sub> disposal, the emptied cylinders would be processed as described in Section 2.2.2.6. The emptied cylinders would be surveyed by using nondestructive assay techniques to determine the presence of a significant quantity of TRU isotopes. If TRU isotopes were detected, samples would be taken and analyzed. Cylinders that exceeded the disposal site limits at the Envirocare of Utah, Inc., facility would be treated to immobilize the heel (e.g., with grout) within the cylinder, compacted, and sectioned; then the cylinder/heel waste stream would be sent to NTS and disposed of as LLW.

As noted in Section 1.2.2, the paints applied to some cylinders prior to 1978 included PCBs, which were typically added as a fungicide and to increase durability and flexibility. Records of the PCB concentrations in the paints used were not kept, so it is currently unknown how many cylinders are coated with paint containing PCBs. However, paint chips from a representative sample of cylinders at the ETTP site have been analyzed for PCBs. The results indicate that up to 50% of the cylinders at ETTP may have coatings containing PCBs. Because the Portsmouth and Paducah inventories contain a large number of cylinders produced before 1978, it is reasonable to assume that a significant number of cylinders at those sites also are coated with paint containing PCBs.

For each of the three storage sites, the PCBs in cylinder paints constitute an extremely small proportion of the PCBs that were previously and are currently at the sites. For example, although the Paducah site has been working for several years to dispose of PCB-containing equipment, the site still had about 870 liquid PCB-containing items (mostly capacitors) in service at the end of 2001. The Portsmouth and ETTP sites also still have a large number of liquid PCB-containing items in service. The three sites are suspected to have had spills of PCB liquids during past operations, prior to the identification of the health and environmental hazards of PCBs.

Each of the three current DUF<sub>6</sub> cylinder storage sites has an existing program for managing PCB-contaminated waste under the Toxic Substances Control Act (TSCA). In addition, the environmental monitoring program at each site includes monitoring of PCB concentrations in soil, sediment, groundwater, surface water, and biota on and in the vicinity of

the sites (see Sections 3.1 and 3.2). These programs would be expected to continue throughout cylinder management activities.

Under the proposed action, storage, conversion, transportation, and disposal operations will comply with applicable TSCA regulations. Additional details are provided in Appendix B.

### 2.2.3 Conversion Product Disposition

The conversion process would generate four conversion products that have a potential use or reuse: depleted U<sub>3</sub>O<sub>8</sub>, HF, CaF<sub>2</sub>, and steel from emptied DUF<sub>6</sub> cylinders (if not used as disposal containers). DOE has been working with industrial and academic researchers for several years to identify potential uses for these products. Some potential uses for depleted uranium exist or are being developed, and DOE believes that a viable market exists for the HF generated during conversion. To take advantage of these to the extent possible, DOE requested in the RFP that the bidders for conversion services investigate and propose viable uses. The probable disposition paths identified by UDS for each of the conversion products are summarized in Table 2.2-2 (UDS 2003b).

According to UDS, of the four conversion products, only HF has a viable commercial market currently interested in the product. Therefore, UDS expects that the HF would be sold to a commercial vendor pending DOE approval of the residual contamination limits and the sale. Commercial-grade HF produced at the Framatome ANP, Inc. (a UDS partner), facility in Richland, Washington, is currently sold commercially under an NRC-approved license. UDS is currently working with DOE through a formal process to evaluate and establish authorized release limits for the HF. Details on this process and on HF sale and use are provided in Appendix E. Should the release of the HF not be allowed, it would be neutralized to CaF<sub>2</sub> for sale or disposal, creating about 2 t (2.2 tons) per 1 t (1.1 ton) of HF. UDS will seek to obtain DOE approval to sell this material as well. However, the market is not as strong as that for the HF; thus, the CaF<sub>2</sub> produced during normal operations might become waste.

Although the depleted U<sub>3</sub>O<sub>8</sub> and emptied cylinders have the potential for use or reuse, currently none of the uses have been shown to be viable because of cost, perception, feasibility, or the need for additional study. Thus, UDS expects that most, if not all, of the uranium oxide and emptied cylinders will require disposal. These materials would be processed and may be shipped to Envirocare for disposal, as summarized in Table 2.2-2.

The EIS evaluation of conversion product disposition considers:

- Transportation of the uranium oxide conversion product and emptied cylinders by truck and rail to both Envirocare (proposed) and NTS (option) for disposal. DOE plans to decide the specific disposal location(s) for the depleted U<sub>3</sub>O<sub>8</sub> conversion product after additional appropriate NEPA review. Accordingly, DOE will continue to evaluate its disposal options and will consider any further information or comments relevant to that decision.

**TABLE 2.2-2 Summary of Proposed Conversion Product Treatment and Disposition**

Conversion Product	Packaging/Storage	Proposed Disposition	Optional Disposition
Depleted U <sub>3</sub> O <sub>8</sub>	U <sub>3</sub> O <sub>8</sub> would be loaded into emptied cylinders, which would be loaded onto railcars. An option of using bulk bags as disposal containers is also considered.	Disposal at Envirocare of Utah, Inc. <sup>a</sup>	Disposal at NTS. <sup>a</sup>
CaF <sub>2</sub>	Packaged for sale or disposal.	Commercial sale pending DOE approval of authorized release limits, as appropriate.	Disposal at Envirocare of Utah, Inc. <sup>a</sup>
HF acid (49% and 70%)	HF produced by the dry conversion facility would be commercial grade. HF would be stored on site until loaded into rail tank cars.	Sale to commercial HF acid supplier pending DOE approval of authorized release limits, as appropriate.	Neutralization of HF to CaF <sub>2</sub> for use or disposal.
Steel (emptied cylinders)	Emptied cylinders would be reused as disposal containers for U <sub>3</sub> O <sub>8</sub> to the extent practicable. If bulk bags were used, the emptied cylinders would have a stabilizing agent added to neutralize residual fluorine, be stored for 4 months, crushed to reduce the size, sectioned, and packaged in intermodal containers.	Disposal at Envirocare of Utah, Inc. <sup>a</sup>	Disposal at NTS. <sup>a</sup>

<sup>a</sup> DOE plans to decide the specific disposal location(s) for the depleted U<sub>3</sub>O<sub>8</sub> conversion product after additional appropriate NEPA review. Accordingly, DOE will continue to evaluate its disposal options and will consider any further information or comments relevant to that decision. DOE will give a minimum 45-day notice before making the specific disposal decision and will provide any supplemental NEPA analysis for public review and comment.

DOE will give a minimum 45-day notice before making the specific disposal decision and will provide any supplemental NEPA analysis for public review and comment.

- Transportation and sale of the HF conversion product, and
- Neutralization of HF to CaF<sub>2</sub> and its sale or disposal in the event that the HF product is not sold.

Because specific destinations are unknown at this time, impacts from the shipment of HF and CaF<sub>2</sub> for use are based on a range of representative route distances. Additional details concerning the transportation assessment are provided in Appendix F, Section F.3.

### Transportation Requirements for DUF<sub>6</sub> Cylinders

All shipments of UF<sub>6</sub> cylinders have to be made in accordance with applicable DOT regulations for the shipment of radioactive materials; specifically, the provisions of 49 CFR Part 173, Subpart I. The DOT regulations require that each UF<sub>6</sub> cylinder be designed, fabricated, inspected, tested, and marked in accordance with the various engineering standards that were in effect at the time the cylinder was manufactured. The DOT requirements are intended to maintain the safety of shipments during both routine and accident conditions. The following provisions are particularly important relative to DUF<sub>6</sub> cylinder shipments:

1. A cylinder must be filled to less than 62% of the certified volumetric capacity (the fill limit was reduced to from 64% to 62% in about 1987).
2. The pressure within a cylinder must be less than 14.8 psia (subatmospheric pressure).
3. A cylinder must be free of cracks, excessive distortion, bent or broken valves or plugs, and broken or torn stiffening rings or skirts, and it must not have a shell thickness that has decreased below a specified minimum value. (Shell thicknesses are assessed visually by a code vessel inspector, and ultrasonic testing may be specified at the discretion of the inspector to verify wall thickness, when and in areas the inspector deems necessary.)
4. A cylinder must be designed so that it will withstand (1) a hydraulic test at an internal pressure of at least 1.4 megapascals (200 psi) without leakage; (2) a free drop test onto a flat, horizontal surface from a height of 1 ft (0.3 m) to 4 ft (1.2 m), depending on the cylinder's mass, without loss or dispersal; and (3) a 30-minute thermal test equivalent to being engulfed in a hydrocarbon fuel/air fire having an average temperature of at least 800°C (1,475°F) without rupture of the containment system.

#### 2.2.4 Preparation and Transportation of ETTP Cylinders

DOE proposes to ship cylinders stored at ETTP to Portsmouth for conversion. This EIS evaluates the preparation of DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders at ETTP and the transportation of those cylinders to Portsmouth by several different methods, as described below.

All shipments of ETTP cylinders would have to be made consistent with DOT regulations for the shipment of radioactive materials as specified in Title 49 of the CFR (see text box and Chapter 6). The cylinders could be shipped by truck or rail.

The majority of DUF<sub>6</sub> cylinders were designed, built, tested, and certified to meet the DOT requirements. The DOT requirements are intended to maintain the safety of shipments during both routine and accident conditions. A summary of the applicable transportation regulations for shipment of UF<sub>6</sub> is provided in Chapter 6 of this EIS; a detailed discussion of pertinent transportation regulations is presented in Biwer et al. (2001). Cylinders meeting the DOT requirements could be loaded directly onto specially designed truck trailers or railcars for shipment. However, after several decades in storage, some cylinders have physically deteriorated such that they no longer meet the DOT requirements.

It is unknown exactly how many DUF<sub>6</sub> cylinders do not meet DOT transportation requirements. As discussed in Section 1.7, it is estimated that up to 1,700 cylinders are DOT compliant, with the remainder not meeting the DOT requirements. Problems are related to the following DOT requirements that must be satisfied before shipment: (1) documentation must be available showing that each cylinder was properly designed, fabricated, inspected, and tested prior to being filled; (2) cylinders must be filled to less than 62% of the maximum capacity; (3) the pressure within cylinders must be less than atmospheric pressure; (4) cylinders must not leak or be damaged so they are unsafe; and (5) cylinders must have a specified minimum wall thickness. Cylinders not meeting these requirements are referred to as “noncompliant.” Some cylinders might fail to meet more than one requirement.

Three options exist for shipping noncompliant cylinders (Biber et al. 2001):

1. The DUF<sub>6</sub> contents could be transferred from noncompliant cylinders into new or compliant cylinders.
2. An exemption could be obtained from DOT that would allow the DUF<sub>6</sub> cylinder to be transported either “as is” or following repairs. The primary finding that DOT would have to make to justify granting an exemption is this: the proposed alternative would have to achieve a safety level that would be at least equal to the level required by the otherwise applicable regulation or, if the otherwise applicable regulation did not establish a required safety level, would be consistent with the public interest and adequately protect against the risks to life and property that are inherent when transporting hazardous materials in commerce.
3. Noncompliant cylinders could be shipped in a protective overpack. In this case, the shipper would have to obtain an exemption from DOT that would allow the existing cylinder, regardless of its condition, to be transported if it was placed in an overpack. The overpack would have to be specially designed. Furthermore, DOT would have to determine that, if the overpack was fabricated, inspected, and marked according to its design, the resulting packaging (including the cylinder and the overpack) would have a safety level at least equal to the level required for a new UF<sub>6</sub> cylinder.

Before shipment, each cylinder would be inspected to determine if it met DOT requirements. This inspection would include a record review to determine if the cylinder was overfilled; a visual inspection for damage or defects; a pressure check to determine if the cylinder was overpressurized; and an ultrasonic wall thickness measurement (based on a visual inspection, if necessary). If a cylinder passed the inspection, the appropriate documentation would be prepared, and the cylinder would be loaded directly for shipment. The preparation of compliant cylinders (cylinders that meet DOT requirements) would include inspection activities, unstacking, on-site transfer, and loading onto a truck trailer or railcar. The cylinders would be secured by using the appropriate tiedowns, and the shipment would be labeled in accordance with DOT requirements. Handling and support equipment and the procedures for on-site

movement and for loading the cylinders would be of the same type currently used for cylinder management activities at the storage sites.

This EIS considers the three options for shipping noncompliant cylinders from ETTP. The information on these activities is based on preconceptual design data provided in the Engineering Analysis Report (Dubrin et al. 1997) prepared for the DUF<sub>6</sub> PEIS and the analysis of potential environmental impacts presented in Appendix E of the DUF<sub>6</sub> PEIS (DOE 1999a).

An overpack is a container into which a cylinder is placed for shipment. The overpack would be designed, tested, and certified to meet all DOT shipping requirements. It would be suitable for containing, transporting, and storing the cylinder contents regardless of cylinder condition. For transportation, a noncompliant cylinder would be placed into an overpack that was already on a truck trailer or railcar. The overpack would be closed and secured, and the shipment would be labeled in accordance with DOT requirements. The overpacks could be reused following shipment.

The second cylinder preparation option for transporting noncompliant cylinders considered in this EIS is the transfer of the DUF<sub>6</sub> from substandard cylinders to new or used cylinders that would meet all DOT requirements. This option could require the construction of a new cylinder transfer facility, for which there are no current plans. Following transfer of the DUF<sub>6</sub>, the compliant cylinders could be shipped by placing them directly onto appropriate trucks or railcars. If a decision were made to construct a transfer facility at ETTP, additional NEPA review would be conducted.

The third option is to ship the cylinders “as-is” under a DOT exemption. As discussed above, for this to occur, it must be demonstrated that the cylinders would be shipped in a manner achieving a level of safety that would be at least equal to the level required by the regulations, which would likely require some compensatory measures.

In this EIS, transportation impacts are estimated for shipment by either truck or rail after cylinder preparation. The impacts are assessed by determining truck and rail routes between ETTP and the Portsmouth site.

### **2.2.5 Construction of a New Cylinder Storage Yard at Portsmouth**

It might be necessary to construct an additional yard at Portsmouth for storing the ETTP cylinders, depending on when and at what rate the ETTP cylinders were shipped. DOE is currently in the process of determining if a new yard is required, or if existing storage yard space could be used for the ETTP cylinders. The potential environmental impacts from the construction of a new cylinder storage yard have been included in this EIS to account for current uncertainties.

Two possible locations for new cylinder yard construction were identified at the Portsmouth site, as shown in Figure 2.2-4 (also identified in Figure 2.2-4 is an existing concrete

pad being evaluated for temporary storage of the ETTP cylinders). Both areas are adjacent to current DOE cylinder storage yards. Proposed Area 1 consists of three smaller sections with a total area of about 5.5 acres (2.2 ha). Proposed Area 2 consists of two smaller sections with a total area of about 6.3 acres (2.5 ha). New yards would be constructed of concrete and would be similar to other concrete yards constructed at the Portsmouth site. Potential environmental impacts from construction of a new yard at both locations identified are evaluated in this EIS.

### **2.2.6 Option of Shipping ETTP Cylinders to Paducah**

As discussed above, DOE proposes to ship the DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders at ETTP to Portsmouth. However, this EIS considers shipping the ETTP cylinders to Paducah as an option. If the ETTP cylinders were shipped to Paducah, the Portsmouth conversion facility would have to operate for 14 rather than 18 years to convert the Portsmouth inventory. In Chapter 5, this EIS presents a discussion of the potential environmental impacts associated with this reduction in the operational period. Potential impacts associated with transportation of the ETTP cylinders to Paducah are evaluated in detail in the site-specific Paducah conversion facility EIS (DOE 2004a).

### **2.2.7 Option of Expanding Conversion Facility Operations**

The conversion facility at Portsmouth is currently being designed to process the DOE DUF<sub>6</sub> cylinder inventory at the site over 18 years by using three process lines. There are no current plans to operate the conversion facility beyond this time period or to increase the throughput of the facility by adding a fourth process line. However, a future decision to extend conversion facility operations or increase throughput at the site could be made for several reasons. Consequently, this EIS includes an evaluation of the environmental impacts associated with expanding conversion facility operations at the site (either by increasing throughput or by extending operations beyond 18 years) in order to provide future planning flexibility (impacts are presented in Section 5.2.8). The possible reasons for expanding operations in the future are discussed below.

The DOE Office of Inspector General (OIG) issued a final audit report in March 2004 recommending that EM conduct a cost benefit analysis to determine the optimum size of the Portsmouth conversion facility and, on the basis of the results of that review, implement the most cost-effective approach (DOE 2004c). The report states that by adding an additional process line to the Portsmouth facility, the time to process the Portsmouth and ETTP inventories of DUF<sub>6</sub> could be shortened by 5 years at a substantial cost savings of 55 million dollars.

As stated in the DOE EM response to the OIG report (DOE 2004b), DOE is not planning to increase the number of process lines within the Portsmouth conversion facility in response to the OIG recommendations. Instead, on the basis of experience with other projects, DOE believes that higher throughput rates can be achieved by improving the efficiency of the planned equipment (DOE 2004b). The conversion contract provides significant incentives to the conversion contractor to improve efficiency. For example, the current facility designs are based

on an assumption that the conversion plant would have an 84% on-line availability (percent of time system is on line and operational). However, Framatome's experience at the Richland plant indicates that the on-line availability is expected to be at least 90%. Therefore, there is additional capacity expected to be realized in the current design. Although there are no plans to increase the throughput at the Portsmouth facility by adding an additional process line, as recommended by the OIG, the potential environmental impacts associated with increasing the plant throughput, by both process improvements and the addition of a fourth process line, are discussed in Section 5.2.8 of this EIS.

A future decision to extend operations or expand throughput might also result from the fact that DOE could assume management responsibility for DUF<sub>6</sub> in addition to the current inventory. Two statutory provisions make this possible. First, Sections 161v. [42 USC 2201(v)] and 1311 [42 USC 2297b-10] of the AEA of 1954 [P.L. 83-703], as amended, provide that DOE may supply services in support of USEC. In the past, these provisions were used once to transfer DUF<sub>6</sub> cylinders from USEC to DOE for disposition in accordance with DOE orders, regulations, and policies. Second, Section 3113(a) of the USEC Privatization Act [42 USC 2297h-11(a)] requires DOE to accept LLW, including depleted uranium that has been determined to be LLW, for disposal upon request and reimbursement of costs by USEC or any other person licensed by the NRC to operate a uranium enrichment facility. This provision has not been invoked, and the form in which depleted uranium would be transferred to DOE by a uranium enrichment facility invoking this provision is not specified. However, DOE believes depleted uranium transferred under this provision in the future would most likely be in the form of DUF<sub>6</sub>, thus adding to the inventory of material needing conversion at the DUF<sub>6</sub> conversion facilities and disposition.

Several possible sources of additional DUF<sub>6</sub> generated from uranium enrichment activities include the following:

1. USEC continues to operate the gaseous diffusion plant at the Paducah site, generating approximately 1,000 cylinders per year of DUF<sub>6</sub>. In the past, DOE signed MOAs with USEC transferring DUF<sub>6</sub> cylinders to DOE (DOE and USEC 1998a,b); the latest was signed in June 2002 for DUF<sub>6</sub> generated from 2002 through 2005. Future MOAs are possible. Consequently, DOE may assume responsibility for additional DUF<sub>6</sub> cylinders at the Paducah site.
2. USEC is currently in the process of developing and demonstrating an advanced enrichment technology based on gas centrifuges. A license for a lead test facility to be operated at the Portsmouth site was issued by the NRC in February 2004. In January 2004, USEC announced that its future enrichment facility using the advanced technology would be sited at the Portsmouth site. Consequently, additional DUF<sub>6</sub> could be generated at this site that ultimately could be transferred to DOE.
3. New commercial uranium enrichment facilities may be built and operated in the United States by commercial companies other than USEC. Although there are no agreements for DOE to accept DUF<sub>6</sub> from such commercial sources, it is possible in the future.

If DOE took responsibility for additional DUF<sub>6</sub> in the future, it is reasonable to assume that the conversion facilities at Portsmouth and/or Paducah could be operated longer than specified in the current plans in order to convert this material or that the throughput of the facilities could be increased. The duration of extended operations or the size of a throughput increase would depend on the quantity of material transferred and the location of the transfer.

In addition, because, under the current plans, the Portsmouth facility could conclude operations approximately 7 years before the current Paducah inventory would be converted at the Paducah site, it is possible that DUF<sub>6</sub> cylinders could be transferred from Paducah to Portsmouth to facilitate conversion of the entire inventory, particularly if DOE assumed responsibility for additional DUF<sub>6</sub> at Paducah.

The potential environmental impacts associated with extended plant operations, increased facility throughput, and Paducah-to-Portsmouth cylinder shipments are discussed in Section 5.2.8.

## **2.3 ALTERNATIVES CONSIDERED BUT NOT ANALYZED IN DETAIL**

### **2.3.1 Utilization of Commercial Conversion Capacity**

During the scoping process for the PEIS, it was suggested that DOE consider using existing UF<sub>6</sub> conversion capacity at commercial nuclear fuel fabrication facilities that convert natural or enriched UF<sub>6</sub> to UO<sub>2</sub> in lieu of constructing new conversion capacity for DUF<sub>6</sub>. Accordingly, in May 2001, DOE investigated the capabilities of existing commercial nuclear fuel fabrication facilities in the United States to determine whether this suggested approach would be a reasonable alternative. Publicly available information was reviewed, and an informal telephone survey of U.S. commercial fuel cycle facilities was conducted. The investigation report concluded that if 100% of the UF<sub>6</sub> conversion capacity of domestic commercial nuclear fuel fabrication facilities operating in May 2001 could be devoted to converting DOE's DUF<sub>6</sub> inventory, approximately 5,500 t (6,100 tons) of DUF<sub>6</sub> could be converted per year. On the basis of this conclusion, the investigation report estimated that it would take more than 125 years to convert DOE's DUF<sub>6</sub> inventory by using only existing conversion capacity. Furthermore, during the informal telephone survey, U.S. commercial fuel fabrication facilities were willing to confirm a capacity of only about 300 t (331 tons) of UF<sub>6</sub> per year as being possibly available to DOE. The investigation report indicated that there seems to be a general lack of interest on the part of the facility owners in committing existing operating or mothballed capacity to conversion of the DOE DUF<sub>6</sub> inventory (Ranek and Monette 2001).

Even though UF<sub>6</sub> conversion capacity at commercial nuclear fuel fabrication facilities might become available in the future, the small capacity identified in 2001 as being possibly available to DOE, coupled with the low interest level expressed at that time by facility owners, indicates that the feasibility of this suggested alternative is low. Therefore, this EIS does not analyze in detail the alternative of using existing capacity at commercial nuclear fuel fabrication facilities.

### 2.3.2 Other Sites

The consideration of alternative sites was limited to alternative locations within the Portsmouth site in response to Congressional direction. As discussed in detail in Section 1.1, Congress has acted twice regarding the construction and operation of DUF<sub>6</sub> conversion plants at Portsmouth and Paducah.

First, in July 1998, P.L. 105-204 directed DOE to make a plan consistent with NEPA for the construction and operation of conversion facilities at Portsmouth and Paducah. Consequently, DOE prepared a plan (DOE 1999b) and published an NOI in the *Federal Register* on September 18, 2001 (68 FR 48123) that identified the range of alternatives to be considered in a conversion facility EIS, including the alternative of constructing only one conversion plant.

Second, while the preparation of the conversion facility EIS was underway, Congress acted again regarding DUF<sub>6</sub> management by passing P.L. 107-206 in August 2002. The pertinent part of P.L. 107-206 directed DOE to award a contract for construction and operation of conversion facilities at the Portsmouth and Paducah sites and to commence construction no later than July 31, 2004. Subsequently, DOE reevaluated the appropriate approach of the NEPA review and decided to prepare two separate site-specific EISs. This change was announced in the *Federal Register* on April 28, 2003 (68 FR 22368). Consistent with the direction of P.L. 107-206, the alternatives for placing the conversion facilities were limited in each site-specific EIS to locations within the Portsmouth and Paducah sites, respectively.

### 2.3.3 Other Conversion Technologies

This EIS provides a detailed analysis of impacts associated with the proposed UDS conversion of DUF<sub>6</sub> to depleted U<sub>3</sub>O<sub>8</sub>. As discussed in Section 1.6.2.2, the conversion project RFP did not specify the conversion product technology or form. Three proposals submitted in response to the RFP were deemed to be in the competitive range; two of these proposals involved conversion of DUF<sub>6</sub> to U<sub>3</sub>O<sub>8</sub> and the third involved conversion to depleted UF<sub>4</sub>. Potential environmental impacts associated with these proposals were considered during the procurement process, including the preparation of an environmental critique and environmental synopsis, which were prepared in accordance with the requirements of 10 CFR 1021.216.

The environmental synopsis is presented in Appendix D. The environmental synopsis concluded that, on the basis of the assessment of potential environmental impacts presented in the critique, no proposal was clearly environmentally preferable. Although differences in a number of impact areas were identified, none of the differences were considered to result in one proposal being preferable over the others. In addition, the potential environmental impacts associated with the proposals were found to be similar to, and generally less than, those presented in the DUF<sub>6</sub> PEIS (DOE 1999a) for representative conversion technologies.

### 2.3.4 Long-Term Storage and Disposal Alternatives

This EIS considers the site-specific impacts from conversion operations at the Portsmouth site, impacts from the transportation of depleted uranium conversion products to NTS and Envirocare for disposal, and impacts from the potential sale of HF and CaF<sub>2</sub> produced from conversion. Environmental impacts are not explicitly evaluated for the long-term storage of conversion products or for disposal.

At this time, there are no specific proposals for the long-term storage of conversion products that would warrant more detailed analysis. Long-term storage alternatives were analyzed in the PEIS, including storage as DUF<sub>6</sub> and storage as an oxide (either U<sub>3</sub>O<sub>8</sub> or UO<sub>2</sub>). For long-term storage of DUF<sub>6</sub>, the options considered were storage in outdoor yards, buildings, and an underground mine. For long-term storage as an oxide, storage in buildings, underground vaults, and an underground mine were considered. The potential environmental impacts from long-term storage were evaluated for representative and generic sites. Preconceptual designs presented in the Engineering Analysis Report (Dubrin et al. 1997) were used as the basis for the analysis, and the evaluation of environmental impacts considered a 40-year period.

This EIS evaluates the impacts from packaging, handling, and transporting conversion products from the conversion facilities to a LLW disposal facility. The disposal facility would be (1) selected in a manner consistent with DOE policies and orders and (2) authorized or licensed to receive the conversion products by either DOE (in conformance with DOE orders), the NRC (in conformance with NRC regulations), or an NRC Agreement State agency (in conformance with state laws and regulations determined to be equivalent to NRC regulations). Assessment of the impacts and risks from on-site handling and disposal at the LLW disposal facility is deferred to the disposal site's site-specific NEPA or licensing documents. However, this EIS covers the impacts from transporting the DUF<sub>6</sub> conversion products to both Envirocare and NTS.

### 2.3.5 Other Transportation Modes

Transportation by air and barge were considered but not analyzed in detail. Transportation by air was deemed to not be reasonable for the types and quantities of materials that would be transported to and from the conversion site. Any transportation by air would involve only small quantities of specialty materials or items generally carried through mail delivery services.

Transportation by barge was also considered, but although it could be used to ship cylinders among the three current storage sites, it was not evaluated in detail. As explained more fully in Section 4.1 of the Engineering Analysis Report (Dubrin et al. 1997), ETTP is the only site with a nearby barge facility. Portsmouth would either have to build new facilities or use existing facilities that are located 20 to 30 mi (32 to 48 km) from the Portsmouth site. Use of existing facilities would require on-land transport by truck or rail over the 20- to 30-mi (32- to 48-km) distance, and the cylinders would have to go through one extra unloading/loading step at the end of the barge transport. Currently, there are no initiatives to build new barge facilities

closer to the Portsmouth site. If barge shipment was proposed in the future and considered to be a reasonable option, additional NEPA review would be conducted.

### 2.3.6 One Conversion Plant Alternative

In the NOI published in the *Federal Register* on September 18, 2001, construction and operation of one conversion plant was identified as a preliminary alternative that would be considered in the conversion EIS. However, with the passage of P.L. 107-206, which mandates the award of a contract for the construction and operation of conversion facilities at both Paducah and Portsmouth, the one conversion plant alternative was considered but not analyzed in this EIS.

## 2.4 COMPARISON OF ALTERNATIVES

### 2.4.1 General

This EIS includes analyses of a no action alternative and the proposed action of building and operating a conversion facility at three alternative locations within the Portsmouth site. Listed below is a general comparison of the activities required for each alternative and the types of environmental impacts that could be expected from each. A detailed comparison of the estimated environmental impacts associated with the alternatives is provided in Section 2.4.2.

- The no action alternative would consist of the continued surveillance and maintenance of the DUF<sub>6</sub> inventories at the Portsmouth and ETTP sites. No conversion facility would be constructed or operated. Only minor yard reconstruction would be required, and no cylinders would be shipped off site. Cylinder breaches could occur as a result of damage during handling or external corrosion.

Potential environmental impacts associated with the no action alternative would be primarily limited to (1) the exposure of involved workers to external radiation in the cylinder yards during surveillance and maintenance activities, (2) impacts associated with the possible release of depleted uranium and HF from breached cylinders and their dispersal in the environment (before the breaches were identified and repaired), and (3) potential accidents that could damage cylinders and result in a release of DUF<sub>6</sub>.

- The proposed action would involve the construction and operation of a conversion facility at Portsmouth. Three alternative locations are considered. It would take the conversion facility approximately 18 years to convert the entire DUF<sub>6</sub> inventory to U<sub>3</sub>O<sub>8</sub> at a rate of approximately 1,000 cylinders (13,500 t [15,000 tons]) per year. This includes conversion of about 4,800 DUF<sub>6</sub> cylinders to be transported from the ETTP site. Shipping of about

1,100 non-DUF<sub>6</sub> cylinders from ETTP to Portsmouth is also included; however, conversion of the contents of these cylinders is not included under the proposed action. Finally, aqueous HF could also be produced for sale during the conversion process, or the HF could be neutralized to CaF<sub>2</sub> for sale or disposal.

The proposed action also evaluates construction of a new cylinder storage yard at Portsmouth for the ETTP cylinders, if required. Two alternate areas for the storage yard are considered (see Figure 2.2-4).

The option of shipping approximately 5,900 cylinders (approximately 4,800 DUF<sub>6</sub> cylinders for conversion and about 1,100 non-DUF<sub>6</sub> cylinders) from ETTP to Paducah rather than to Portsmouth is also evaluated. This option would reduce the period of operation of the Portsmouth conversion facility from 18 to 14 years.

After conversion, the conversion products (U<sub>3</sub>O<sub>8</sub>, aqueous HF or CaF<sub>2</sub>, and emptied cylinders, if not used as disposal containers for U<sub>3</sub>O<sub>8</sub>) would be shipped by truck or rail to a user or disposal facility (either NTS or Envirocare).

Potential environmental impacts associated with the proposed action alternatives would include (1) impacts to local air, water, soil, ecological, and cultural resources during storage yard and facility construction; (2) impacts to workers from conversion facility construction and operations; (3) impacts from small amounts of depleted uranium and other hazardous compounds released to the environment through normal conversion plant air effluents; (4) impacts from the shipment of cylinders, conversion products, and waste products; and (5) impacts from potential accidents involving the release of radioactive material or hazardous chemicals.

## 2.4.2 Summary and Comparison of Potential Environmental Impacts

This EIS includes analyses of potential impacts at the Portsmouth and ETTP sites under the no action alternative and potential impacts at Portsmouth under the proposed action alternatives. Under the no action alternative, potential impacts associated with the continued storage of DUF<sub>6</sub> cylinders in yards are evaluated through 2039; in addition, the long-term impacts that could result from releases of DUF<sub>6</sub> and HF from future cylinder breaches are evaluated. For the proposed action, potential impacts are evaluated at three alternative locations for the following:

- The conversion facility construction period of approximately 2 years;
- Construction of a new cylinder storage yard over a period of about 3 months, if necessary;

- The operational period required to convert the entire DUF<sub>6</sub> inventory, which would equal 18 years (14 years if the ETTP inventory was shipped to Paducah instead); and
- A facility D&D period of 3 years.

Under each alternative, potential consequences are evaluated in many areas: human health and safety (during normal operations, accidents, and transportation), air quality, noise, water, soil, socioeconomics, ecology, waste management, resource requirements, land use, cultural resources, and environmental justice. (Methodologies are discussed in Chapter 4 and Appendix F.) The assessment considers impacts that could result from the construction of necessary facilities, normal operations of facilities, accidents, preparation of cylinders for shipment, transportation of materials, and the D&D of facilities after conversion is complete. In addition, the production and sale of aqueous HF is evaluated, as is the possibility of neutralizing HF to CaF<sub>2</sub> for sale or disposal.

The potential environmental impacts at Portsmouth under the proposed action alternatives and at Portsmouth and ETTP under the no action alternative are presented in Table 2.4-1 (placed at the end of this chapter). To supplement the information in Table 2.4-1, each area of impact evaluated in the EIS is discussed below. Major similarities and differences among the alternatives are highlighted. This section provides a summary comparison; additional details and discussion are provided in Chapter 5 for each alternative and area of impact.

#### **2.4.2.1 Human Health and Safety — Construction and Normal Facility Operations**

Under the no action alternative and the action alternatives, it is estimated that potential exposures of workers and members of the public to radiation and chemicals would be well within applicable public health standards and regulations during normal facility operations (including 10 CFR 835, 40 CFR 61 Subpart H, and DOE Order 5400.5). The estimated doses and risks from radiation and/or chemical exposures of the general public and noninvolved workers would be very low, with zero latent cancer fatalities (LCFs) expected among these groups over the time periods considered, and with no adverse health impacts from chemical exposures expected. (Dose and risk estimates are shown in Table 2.4-1.) In general, the location of a conversion facility within the Portsmouth site would not significantly affect potential impacts to workers or the public during normal facility operations (i.e., no significant differences in impacts were identified at alternative Locations A, B, or C).

Involved workers (persons directly involved in the handling of radioactive or hazardous materials) could be exposed to low-level radiation emitted by uranium during the normal course of their work activities, and this exposure could result in a slight increase in the risk for radiation-induced LCFs to individual involved workers. (The possible presence of TRU and Tc contamination in the cylinder inventory would not contribute to exposures during normal operations.) The annual number of workers exposed could range from about 33 (under the no action alternative for Portsmouth and ETTP combined) to 163 under the action alternatives. Under all alternatives, it is estimated that radiation exposure of involved workers would be

unlikely to result in additional LCFs among the entire involved worker populations (risks from radiation exposure range from a 1-in-10 chance of one additional LCF among the entire conversion facility involved worker population over the life of the project to a 1-in-5 chance of one additional LCF among the involved cylinder maintenance workers at Portsmouth under the no action alternative).

Possible radiological exposures from using groundwater potentially contaminated as a result of releases from breached cylinders or facility releases were also evaluated. In general, these exposures would be within applicable public health standards and regulations. However, the uranium concentration in groundwater could exceed 20 µg/L (the drinking water guideline used for comparison in this EIS) at some time in the future under the no action alternative if cylinder corrosion was not controlled. This scenario is highly unlikely because ongoing cylinder inspections and maintenance would prevent significant releases from occurring.

#### **2.4.2.2 Human Health and Safety — Facility Accidents**

**2.4.2.2.1 Physical Hazards.** Under all alternatives, workers could be injured or killed as a result of on-the-job accidents unrelated to radiation or chemical exposure. On the basis of accident statistics for similar industries, it is estimated that under the no action alternative, zero fatalities and about 70 injuries might occur through 2039 at the Portsmouth and ETTP sites (about 1 injury per year at Portsmouth, and about 0.7 injury per year at ETTP). Under the action alternatives, the risk of physical hazards would not depend on the location of the conversion facility. No fatalities are predicted, but about 11 injuries during conversion facility construction and up to 142 injuries during operations could occur at the conversion facility (about 6 injuries per year during construction and about 8 injuries per year during operations). In addition, 1 injury would be expected from construction of a new cylinder yard for ETTP cylinders. Accidental injuries and deaths are not unusual in industries that use heavy equipment to manipulate weighty objects and bulk materials.

**2.4.2.2.2 Facility Accidents Involving Radiation or Chemical Releases.** Under all alternatives, it is possible that accidents could release radiation or chemicals to the environment, potentially affecting both the workers and members of the public. Of all the accidents considered, those involving DUF<sub>6</sub> cylinders and those involving chemicals at the conversion facility would have the largest potential effects.

The DUF<sub>6</sub> Management Plan (DOE 1996e) outlines required cylinder maintenance activities and procedures to be undertaken in the event of a cylinder breach and/or release of DUF<sub>6</sub> from one or more cylinders. Under all alternatives, there is a low probability that accidents involving DUF<sub>6</sub> cylinders could occur at the current storage locations. If an accident occurred, DUF<sub>6</sub> could be released to the environment. The DUF<sub>6</sub> would combine with moisture in the air, forming gaseous HF and UO<sub>2</sub>F<sub>2</sub>, a soluble solid in the form of small particles. The depleted uranium and HF could be dispersed downwind, potentially exposing workers and members of the general public to radiation and chemical effects. The amount released would depend on the

severity of the accident and the number of cylinders involved. The probability of cylinder accidents would decrease under the action alternatives as the DUF<sub>6</sub> was converted and the number of cylinders in storage decreased as a result.

For releases involving DUF<sub>6</sub> and other uranium compounds, both chemical and radiological effects could occur if the material was ingested or inhaled. The chemical effect of most concern associated with internal uranium exposure is kidney damage, and the radiological effect of concern is an increase in the probability of developing cancer. With regard to uranium, chemical effects occur at lower exposure levels than do radiological effects. Exposure to HF from accidental releases could result in a range of health effects, from eye and respiratory irritation to death, depending on the exposure level. Large anhydrous NH<sub>3</sub> releases could also cause severe respiratory irritation and death. (NH<sub>3</sub> is used to generate hydrogen, which is required for the conversion process.)

Chemical and radiological exposures to involved workers (those within 100 m [329 ft] of the release) under accident conditions would depend on how rapidly the accident developed, the exact location and response of the workers, the direction and amount of the release, the physical forces causing or caused by the accident, meteorological conditions, and the characteristics of the room or building if the accident occurred indoors. Impacts to involved workers under accident conditions would likely be dominated by physical forces from the accident itself; thus quantitative dose/effect estimates would not be meaningful. For these reasons, the impacts to involved workers during accidents are not quantified in this EIS. However, it is recognized that injuries and fatalities among involved workers would be possible if an accident did occur.

Under the no action alternative, for accidents involving cylinders that might happen at least once in 100 years (i.e., likely accidents [see Section 5.1.2.1.2]), it is estimated that the off-site concentrations of HF and uranium would be considerably below levels that would cause adverse chemical effects among members of the general public from exposure to these chemicals. However, up to 70 noninvolved workers might experience potential adverse effects from exposure to HF and uranium (mild and temporary effects, such as respiratory irritation or temporary decrease in kidney function). It is estimated that up to 3 noninvolved workers would experience potential irreversible adverse effects that are permanent in nature (such as lung damage or kidney damage); no fatalities are expected. Radiation exposures would be unlikely to result in additional LCFs among noninvolved workers or members of the general public for these types of accidents.

Cylinder accidents that are less likely to occur could be more severe, having greater consequences that could potentially affect off-site members of the general public. These types of accidents are considered extremely unlikely, expected to occur with a frequency of between once in 10,000 years and once in 1 million years of operations. Based on the expected frequency, through 2039, the probability of this type of accident was estimated to be about 1 chance in 2,500. Among all the cylinder accidents analyzed, the postulated accident that would result in the largest number of people with adverse effects (including mild and temporary as well as permanent effects) would be an accident that involves rupture of cylinders in a fire. If this type of accident occurred at the Portsmouth site, it is estimated that up to 680 members of the general public and up to 1,000 noninvolved workers might experience adverse chemical effects from HF

and uranium exposure (mild and temporary effects, such as respiratory irritation or temporary decrease in kidney function).

The postulated cylinder accident that would result in the largest number of persons with irreversible adverse health effects is a corroded cylinder spill under wet conditions, with an estimated frequency of between once in 10,000 years and once in 1 million years of operations. If this accident occurred, it is estimated that 1 member of the general public and up to 140 noninvolved workers might experience irreversible adverse effects (such as lung damage or kidney damage). No fatalities are expected among members of the general public; there would be a potential for 1 fatality among noninvolved workers from chemical effects. Radiation exposures would be unlikely to result in additional LCFs among noninvolved workers (1 chance in 100) or the general public (1 chance in 30).

In addition to the cylinder accidents discussed above is a certain class of accidents that the DOE investigated; however, because of security concerns, information about such accidents is not available for public review but is presented in a classified appendix to the EIS. All classified information will be presented to state and local officials, as appropriate.

The number of persons actually experiencing adverse or irreversible adverse effects from cylinder accidents would likely be considerably fewer than those estimated for this analysis and would depend on the actual circumstances of the accident and the individual chemical sensitivities of the affected persons. For example, although exposures to releases from cylinder accidents could be life-threatening (especially with respect to immediate effects from inhalation of HF at high concentrations), the guideline exposure level of 20 parts per million (ppm) of HF used to estimate the potential for irreversible adverse effects from HF exposure is likely to result in overestimates. This is because no animal or human deaths have been known to occur as a result of acute exposures (i.e., 1 hour or less) at concentrations of less than 50 ppm; generally, if death does not occur quickly after HF exposure, recovery is complete.

Similarly, the guideline intake level of 30 mg used to estimate the potential for irreversible adverse effects from the intake of uranium in this EIS is the level suggested in NRC guidance. This level is somewhat conservative; that is, it is intended to overestimate rather than underestimate the potential number of irreversible adverse effects in the exposed population following uranium exposure. In more than 40 years of cylinder handling activities, no accidents involving releases from cylinders containing *solid* UF<sub>6</sub> have occurred that have caused diagnosable irreversible adverse effects among workers. In previous accidental exposure incidents involving *liquid* UF<sub>6</sub> in gaseous diffusion plants, some worker fatalities occurred immediately after the accident as a result of inhalation of HF generated from the UF<sub>6</sub>. However, no fatalities occurred as a result of the toxicity of the uranium exposure. A few workers were exposed to amounts of uranium estimated to be about three times the guideline level (30 mg) used for assessing irreversible adverse effects; none of these workers, however, actually experienced such effects.

Under the action alternatives, low-probability accidents involving chemicals at the conversion facility could have large potential consequences for noninvolved workers and members of the public. At a conversion site, accidents involving chemical releases, such as NH<sub>3</sub>

and HF, could occur. NH<sub>3</sub> is used to generate hydrogen for conversion, and HF can be produced as a co-product of converting DUF<sub>6</sub>. Although the UDS proposal uses NH<sub>3</sub> to produce hydrogen, hydrogen can also be produced by using natural gas. In that case, the accident impacts would be much less than those discussed in this section for NH<sub>3</sub> accidents. (Details about potential NH<sub>3</sub> and other accidents are in Section 5.2.3.2 [conversion facility] and Section 5.2.5 [transportation].)

The conversion accident estimated to have the largest potential consequences is an accident involving the rupture of tanks containing either 70% HF or anhydrous NH<sub>3</sub>. Such an accident could be caused by a large earthquake and is expected to occur with a frequency of less than once in 1 million years of operations. The probability of this type of accident occurring during the operation of a conversion facility is a function of the period of operation; over 18 years of operations, the accident probability would be less than 1 chance in 56,000.

If an aqueous HF or anhydrous NH<sub>3</sub> tank ruptured at the conversion facility, a maximum of up to about 2,300 members of the general public might experience adverse effects (mild and temporary effects, such as respiratory irritation or temporary decrease in kidney function) as a result of chemical exposure. A maximum of about 210 people might experience irreversible adverse effects (such as lung damage or kidney damage), with the potential for about 4 fatalities. With regard to noninvolved workers, up to about 1,400 workers might experience adverse effects (mild and temporary) as a result of chemical exposures. A maximum of about 1,400 noninvolved workers might experience irreversible adverse effects, with the potential for about 30 fatalities.

The location of the conversion facility within the Portsmouth site would affect the number of noninvolved workers and members of the general public who might experience adverse or irreversible adverse effects from an HF or anhydrous NH<sub>3</sub> tank rupture accident. However, the differences among the locations within each site would generally be small and within the uncertainties associated with the exact accident sequence and weather conditions at the time of the accident. An exception would be that the number of noninvolved workers impacted would be higher for Location B for both potential adverse and irreversible adverse effects.

Although such high-consequence accidents at a conversion facility are possible, they are expected to be extremely rare. The risk (defined as consequence × probability) for these accidents would be less than 1 fatality and less than 1 irreversible adverse health effect for noninvolved workers and members of the public combined. NH<sub>3</sub> and HF are commonly used for industrial applications in the United States, and there are well-established accident prevention and mitigative measures for HF and NH<sub>3</sub> storage tanks. These include storage tank siting principles, design recommendations, spill detection measures, and containment measures. These measures would be implemented, as appropriate.

Under the action alternatives, the highest consequence radiological accident is estimated to be an earthquake damaging the depleted U<sub>3</sub>O<sub>8</sub> product storage building. If this accident occurred, it is estimated that about 135 lb (61 kg) of depleted U<sub>3</sub>O<sub>8</sub> would be released to the atmosphere outside of the building. The maximum collective dose received by the general public and the noninvolved workers would be about 30 person-rem and 530 person-rem, respectively.

There would be about a 1-in-50 chance of an LCF among the public and a 1-in-5 chance of an LCF among the noninvolved workers. Because the accident has a probability of occurrence that is about 1 chance in 6,000, the risk posed by the accident would be essentially zero LCFs among both the public and the workers.

### 2.4.2.3 Human Health and Safety — Transportation

Under the no action alternative, only small amounts of the LLW and low-level radioactive mixed waste (LLMW) that would be generated during routine cylinder maintenance activities would require transportation (about one shipment per year). Only negligible impacts are expected from such shipments. No DUF<sub>6</sub> or non-DUF<sub>6</sub> cylinders would be transported between sites.

Under the action alternatives, the total number of shipments would include the following:

1. If U<sub>3</sub>O<sub>8</sub> was disposed of in emptied cylinders, there would be approximately 4,200 railcar shipments of depleted U<sub>3</sub>O<sub>8</sub> from the conversion facility to Envirocare (proposed) or NTS (option), or up to 21,000 truck shipments (alternative) to either Envirocare or NTS. The numbers of shipments would be about 8,800 for truck and 2,200 for railcar if bulk bags were used as disposal containers.
2. About 8,200 truck or 1,640 railcar shipments of aqueous (70% and 49%) HF could occur; alternatively, the aqueous HF could be neutralized to CaF<sub>2</sub>, requiring a total of about 13,600 truck or 3,400 railcar shipments. Currently, the destination for these shipments is not known.
3. About 700 truck or 350 railcar shipments of anhydrous NH<sub>3</sub> from a supplier to the site. Currently, the origin of these shipments is not known.
4. Emptied heel cylinders to Envirocare or NTS, if bulk bags were used to dispose of the depleted U<sub>3</sub>O<sub>8</sub>.
5. Approximately 5,400 truck or 1,400 railcar shipments of cylinders from ETTP to Portsmouth.

During normal transportation operations, radioactive material and chemicals would be contained within their transport packages. Health impacts to crew members (i.e., workers) and members of the general public along the routes could occur if they were exposed to low-level external radiation in the vicinity of uranium material shipments. In addition, exposure to vehicle emissions (engine exhaust and fugitive dust) could potentially cause latent fatalities from inhalation.

The risk estimates for emissions are based on epidemiological data that associate mortality rates with particulate concentrations in ambient air. (Increased latent mortality rates

resulting from cardiovascular and pulmonary diseases have been linked to incremental increases in particulate concentrations.) Thus, the increase in ambient air particulate concentrations caused by a transport vehicle, with its associated fugitive dust and diesel exhaust emissions, is related to such premature latent fatalities in the form of risk factors. Because of the conservatism of the assumptions made to reconcile results among independent epidemiological studies and associated uncertainties, the latent fatality risks estimated for normal vehicle emissions should be considered to be an upper bound (Biwer and Butler 1999).<sup>2</sup> For the transport of conversion products and co-products (depleted U<sub>3</sub>O<sub>8</sub>, aqueous HF, and emptied cylinders, if not used as disposal containers), it is conservatively estimated that a total of about 10 fatalities from vehicle emissions could occur if shipments were only by truck and if aqueous HF product was sold and transported 620 mi (1,000 km) from the site (about 20 fatalities are estimated if HF was neutralized to CaF<sub>2</sub> and transported 620 mi [1,000 km] from the site). The number of fatalities occurring from exhaust emissions if shipment was only by rail would be less than 1 if the HF was sold and about 1 if the HF was neutralized to CaF<sub>2</sub>.

Exposure to external radiation during normal transportation operations is estimated to cause less than 1 LCF under both truck and rail options. Members of the general public living along truck and rail transportation routes would receive extremely small doses of radiation from shipments, less than 0.1 mrem over the duration of the program. This would be true even if a single person was exposed to every shipment of radioactive material during the program.

Traffic accidents could occur during the transportation of radioactive materials and chemicals. These accidents could potentially affect the health of workers (i.e., crew members) and members of the general public, either from the accident itself or from accidental releases of radioactive materials or chemicals.

The total number of traffic fatalities (unrelated to the type of cargo) was estimated on the basis of national traffic statistics on shipments by both truck and rail. If the aqueous HF was sold, about 1 traffic fatality would be estimated under both transportation modes. If HF was neutralized to CaF<sub>2</sub>, about 2 fatalities would be estimated for the truck option and 1 fatality for the rail option.

Severe transportation accidents could also result in a release of radioactive material or chemicals from a shipment. The consequences of such a release would depend on the material released, location of the accident, and atmospheric conditions at the time. Potential consequences would be greatest in urban areas because more people could be exposed. Accidents that occurred when the atmospheric conditions were very stable (typical of nighttime) would have higher potential consequences than accidents that occurred when the conditions were unstable (i.e., turbulent, typical of daytime) because the stability would determine how quickly the released material dispersed and diluted to lower concentrations as it moved downwind.

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<sup>2</sup> For perspective, in a recently published EIS for a geologic repository at Yucca Mountain, Nevada (DOE 2002h), the same risk factors were used for vehicle emissions; however, they were adjusted to reduce the amount of conservatism in the estimated health impacts. As reported in the Yucca Mountain EIS, the adjustments resulted in a reduction in the emission risks by a factor of about 30.

A detailed discussion of the accident scenarios modeled for the action alternatives is provided in Section 5.2.5.3. For the action alternatives, the highest potential accident consequences during transportation activities would be caused by a rail accident involving anhydrous NH<sub>3</sub>. Although anhydrous NH<sub>3</sub> is a hazardous gas, it has many industrial applications and is commonly safely transported by industry as a pressurized liquid in trucks and rail tank cars.

The probability of a severe anhydrous NH<sub>3</sub> railcar accident occurring in a highly populated urban area under stable atmospheric conditions is extremely rare. The probability of such an accident occurring if all the anhydrous NH<sub>3</sub> needed was transported 620 mi (1,000 km) is estimated to be less than 1 chance in 400,000. Nonetheless, if such an accident (i.e., release of anhydrous NH<sub>3</sub> from a railcar in a densely populated urban area under stable atmospheric conditions) occurred, up to 5,000 persons might experience irreversible adverse effects (such as lung damage), with the potential for about 100 fatalities. If the same type of NH<sub>3</sub> rail accident occurred in a typical rural area, which would have a smaller population density than an urban area, potential impacts would be considerably less. It is estimated that in a rural area, approximately 20 persons might experience irreversible adverse effects, with no expected fatalities. The atmospheric conditions at the time of an accident would also significantly affect the consequences of a severe NH<sub>3</sub> accident. The consequences of an NH<sub>3</sub> accident would be less severe under unstable conditions, the most likely conditions in the daytime. Unstable conditions would result in more rapid dispersion of the airborne NH<sub>3</sub> plume and lower downwind concentrations. Under unstable conditions in an urban area, approximately 400 persons could experience irreversible adverse effects, with the potential for about 8 fatalities. If the accident occurred in a rural area under unstable conditions, 1 person would be expected to experience an irreversible adverse effect, with zero fatalities expected. When the probability of an NH<sub>3</sub> accident occurring is taken into account, it is expected that no irreversible adverse effects and no fatalities would occur over the shipment period.

For perspective, anhydrous NH<sub>3</sub> is routinely shipped commercially in the United States for industrial and agricultural applications. On the basis of information provided in the DOT *Hazardous Material Incident System (HMIS) Database* (DOT 2003b) for 1990 through 2002, 2 fatalities and 19 major injuries to the public or to transportation or emergency response personnel have occurred as a result of anhydrous NH<sub>3</sub> releases during nationwide commercial truck and rail operations. These fatalities and injuries occurred during transportation or loading and unloading operations. Over that period, truck and rail NH<sub>3</sub> spills resulted in more than 1,000 and 6,000 evacuations, respectively. Five very large spills, more than 10,000 gal (38,000 L), have occurred; however, these spills were all en route derailments from large rail tank cars. The two largest spills, both around 20,000 gal (76,000 L), occurred in rural or lightly populated areas and resulted in 1 major injury. Over the past 30 years, the safety record for transporting anhydrous NH<sub>3</sub> has significantly improved. Safety measures contributing to this improved safety record include the installation of protective devices on railcars, fewer derailments, closer manufacturer supervision of container inspections, and participation of shippers in the Chemical Transportation Emergency Center.

After anhydrous NH<sub>3</sub>, the types of accidents that are estimated to result in the second highest consequences are those involving shipment of 70% aqueous HF produced during the

conversion process. The estimated numbers of irreversible adverse effects for 70% HF rail accidents are about one-third of those from the anhydrous NH<sub>3</sub> accidents. However, the number of estimated fatalities is about one-sixth of those from NH<sub>3</sub> accidents, because the percent of fatalities among the individuals experiencing irreversible adverse effects is 1% as opposed to 2% for NH<sub>3</sub> exposures (Policastro et al. 1997). For perspective, since 1971, the period covered by DOT records, no fatal or serious injuries to the public or to transportation or emergency response personnel have occurred as a result of anhydrous HF releases during transportation. (Most of the HF transported in the United States is anhydrous HF, which is more hazardous than aqueous HF.) Over that period, 11 releases from railcars were reported to have no evacuations or injuries associated with them. The only major release (estimated at 6,400 lb [29,000 kg] of HF) occurred in 1985 and resulted in approximately 100 minor injuries. Another minor HF release during transportation occurred in 1990. The safety record for transporting HF has improved in the past 10 years for the same reasons as those discussed above for NH<sub>3</sub>. Transportation accidents involving the shipment of DUF<sub>6</sub> cylinders were also evaluated, with the estimated consequences being less than those discussed above for NH<sub>3</sub> and HF (see Section 5.2.5.3).

#### 2.4.2.4 Air Quality and Noise

Under the no action alternative, air quality from construction and operations would be within national and state ambient air quality standards. If continued cylinder maintenance and painting are effective in controlling corrosion, as expected, concentrations of HF would be kept within air quality standards at the Portsmouth and ETTP sites. If cylinder corrosion is not controlled, the maximum 24-hour HF concentration at the ETTP site boundary could be about equal to the Tennessee primary standard of 2.9 µg/m<sup>3</sup> around the year 2020 (standards would not be exceeded at Portsmouth). However, because of the on-going cylinder maintenance program, it is not expected that this high breach rate would occur at the ETTP site.

Under the action alternatives, it was found that air quality impacts during construction would be similar for all three alternative locations. The total (modeled plus the measured background value representative of the site) concentrations due to emissions of most criteria pollutants — such as sulfur dioxide (SO<sub>2</sub>), nitrogen oxides (NO<sub>x</sub>), and carbon monoxide (CO) — would be well within applicable air quality standards. As is often the case for construction, the primary concern would be particulate matter (PM) released from near-ground-level sources. Total concentrations of PM<sub>10</sub> and PM<sub>2.5</sub> (PM with a mean aerodynamic diameter of 10 µm or less and 2.5 µm or less, respectively) at the construction site boundaries would be close to or above the standards because of the high background concentrations and the proximity of the new cylinder yard and the proposed conversion facility to potentially publicly accessible areas. The background data used are the maximum values from the last 5 years of monitoring at the nearest monitoring location (operated by the OEPA) to the site, located about 20 mi (32 km) away in the town of Portsmouth. On the basis of these values, exceedance of the annual PM<sub>2.5</sub> standard would be unavoidable, because the background concentration already exceeds the standard (background is 24.1 µg/m<sup>3</sup>, in comparison with the standard of 15 µg/m<sup>3</sup>). Accordingly, construction activities should be conducted so as to minimize further impacts on ambient air quality. To mitigate impacts, water could be sprayed on disturbed areas more often, and dust suppressant or pavement could be applied to roads with frequent traffic.

During operations, it is estimated that total concentrations for all criteria pollutants except PM<sub>2.5</sub> would be well within standards. The background level of PM<sub>2.5</sub> in the area of the Portsmouth site approaches or already exceeds the standard. Again, impacts during operations were found to be similar for all three alternative locations.

Noise impacts are expected to be negligible under the no action alternative. Under the action alternatives, estimated noise levels at the nearest residence (located 0.9 km [0.6 mi] from the alternative location) would be below the U.S. Environmental Protection Agency (EPA) guideline of 55 dB(A)<sup>3</sup> as day-night average sound level (DNL)<sup>4</sup> for residential zones during construction and operations.

#### 2.4.2.5 Water and Soil

Under the no action alternative, uranium concentrations in surface water, groundwater, and soil would remain below guidelines throughout the project duration. However, if cylinder maintenance and painting were not effective in reducing cylinder corrosion rates, the uranium concentration in groundwater could be greater than the guideline at both the Portsmouth and ETTP sites at some time in the future (no earlier than about 2100). If continued cylinder maintenance and painting were effective in controlling corrosion, as expected, groundwater uranium concentrations would remain less than the guideline.

During construction of the conversion facility, construction material spills could contaminate surface water, groundwater, or soil. However, by implementing storm water management, sediment and erosion controls (e.g., temporary and permanent seeding; mulching and matting; sediment barriers, traps, and basins; silt fences; runoff and earth diversion dikes), and good construction practices (e.g., covering chemicals with tarps to prevent interaction with rain, promptly cleaning up any spills), concentrations in soil and wastewater (and therefore surface water and groundwater) could be kept well within applicable standards or guidelines.

During operations, no appreciable impacts on surface water, groundwater, or soils would result from the conversion facility because no contaminated liquid effluents are anticipated, and because airborne emission would be at very low levels (e.g., <0.25 g/yr of uranium). Impacts would be similar for all three alternative locations.

#### 2.4.2.6 Socioeconomics

The socioeconomic analysis evaluates the effects of construction and operation of a new cylinder yard and conversion facility on population, employment, income, regional growth,

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<sup>3</sup> dB(A) is a unit of weighted sound-pressure level, measured by the use of the metering characteristics and the A-weighting specified in the *American National Standard Specification for Sound Level Meters*, ANSI S1.4-1983, and in Amendment S1.4A-1985 (Acoustical Society of America 1983, 1985).

<sup>4</sup> DNL is the 24-hour average sound level, expressed in dB(A), with a 10-dB penalty artificially added to the nighttime (10 p.m.–7 a.m.) sound level to account for noise-sensitive activities (e.g., sleep) during these hours.

housing, and community resources in the region of influence (ROI) around the site. In general, socioeconomic impacts tend to be positive, creating jobs and income, with only minor impacts on housing, public finances, and employment in local public services.

The no action alternative would result in a small socioeconomic impact at both the Portsmouth and ETTP sites combined, creating a total of 130 jobs during operations (direct and indirect jobs) and generating a total of \$5.3 million in personal income per operational year. No significant impacts on regional growth and housing, local finances, and public service employment in the ROI are expected.

Under the action alternatives, jobs and income would be generated during both construction and operation. Construction of the conversion facility would create 280 jobs and generate \$9 million in personal income in the peak construction year (construction occurs over a 2-year period). Operation of the conversion facility would create 320 jobs and generate \$13 million in income each year. Only minor impacts on regional growth and housing, local finances, and public service employment in the ROI are expected. The socioeconomic impacts would not depend on the location of the conversion facility; therefore, the impacts would be the same for alternative Locations A, B, and C.

#### **2.4.2.7 Ecology**

Under the no action alternative, continued cylinder maintenance and surveillance activities would have negligible impacts on ecological resources (i.e., vegetation, wildlife, wetlands, and threatened and endangered species). No yard reconstruction is planned for either the Portsmouth or ETTP sites. It is estimated that potential concentrations of contaminants in the environment from future cylinder breaches would be below levels harmful to biota. However, there is a potential for impacts to aquatic biota from cylinder yard runoff during painting activities.

Under the action alternatives, the total area disturbed during conversion facility construction would be 65 acres (26 ha). Vegetation communities would be impacted in this area from a loss of habitat. However, for all three alternative locations, impacts could be minimized, depending on exactly where the facility was placed within each location. These habitat losses would constitute less than 1% of available land at the site. It was found that concentrations of contaminants in the environment during operations would be below harmful levels. Impacts to vegetation and wildlife would be negligible at all three locations.

Wetlands at or near Locations A, B, and C could be adversely affected at the Portsmouth site. Impacts to wetlands could be minimized depending on where exactly the facility was placed within each location. Unavoidable impacts to wetlands that are within the jurisdiction of the U.S. Army Corps of Engineers (USACE) may require a Clean Water Act (CWA) Section 404 Permit, which would trigger the requirement for a CWA 401 water quality certification from Ohio. Impacts at Location A may potentially be avoided by an alternative routing of the entrance road, or mitigation may be developed in coordination with the appropriate regulatory agency. A mitigation plan might be required prior to the initiation of construction.

Construction of the conversion facility should not directly affect federal- or state-listed species. However, impacts on deciduous forest might occur. Impacts to forested areas could be avoided if temporary construction areas were placed in previously disturbed locations. Trees with exfoliating bark, such as shagbark hickory, or dead trees with loose bark can be used by the Indiana bat (federal- and state-listed as endangered) as roosting trees during the summer. There is a potential that such trees could be disturbed during construction at Locations A or C at Portsmouth. If either live or dead trees with exfoliating bark are encountered on construction areas, they should be saved if possible. If cutting of such trees is necessary, it should be performed before April 15 or after September 15.

#### **2.4.2.8 Waste Management**

Under the no action alternative, LLW, LLMW, and PCB-containing waste could be generated from cylinder scraping and painting activities. The amount of wastes generated would represent an increase of less than 1% in the loads of these wastes at the Portsmouth and ETTP sites, representing negligible impacts on waste management operations at both sites.

Under the action alternatives, waste management impacts would not be dependent on the location of the facility within the site and would be the same for alternative Locations A, B, and C. Waste generated during construction and operations would have negligible impacts on the Portsmouth site waste management operations, with the exception of possible impacts from disposal of CaF<sub>2</sub>. Industrial experience indicates that HF, if produced, would contain only trace amounts of depleted uranium (less than 1 ppm). It is expected that HF would be sold for use. If sold for use, the sale would be subject to review and approval by DOE in coordination with the NRC, depending on the specific use (as discussed in Appendix E).

The U<sub>3</sub>O<sub>8</sub> produced from conversion would generate about 4,700 yd<sup>3</sup> (3,570 m<sup>3</sup>)/yr of LLW. This is 5% of Portsmouth's annual projected volume and would have a low impact on site LLW management.

If the HF was not sold but instead neutralized to CaF<sub>2</sub>, it is currently unknown whether (1) the CaF<sub>2</sub> could be sold, (2) the low uranium content would allow the CaF<sub>2</sub> to be disposed of as nonhazardous solid waste, or (3) disposal as LLW would be required. The low level of uranium contamination expected (i.e., less than 1 ppm) suggests that sale or disposal as nonhazardous solid waste would be most likely. If sold for use, the sale would be subject to review and approval by DOE in coordination with the NRC, depending on the specific use. Waste management for disposal as nonhazardous waste could be handled through appropriate planning and design of the facilities. If the CaF<sub>2</sub> had to be disposed of as LLW, it could represent a potentially large impact on waste management operations.

A small quantity of TRU could be entrained in the gaseous DUF<sub>6</sub> during the cylinder emptying operations. These contaminants would be captured in the filters between the cylinders and the conversion equipment. The filters would be monitored and replaced routinely to maintain concentrations below regulatory limits for TRU waste. The spent filters would be disposed of as LLW, generating up to 25 drums of LLW over the life of the project.

Current UDS plans are to leave the heels in the emptied cylinders, add a stabilizer, and use the cylinders as disposal containers for the U<sub>3</sub>O<sub>8</sub> product to the extent practicable. An alternative is to process the empty cylinders and dispose of them directly as LLW. Either one of these approaches is expected to meet the waste acceptance criteria of the disposal facilities and minimize the potential for generating TRU waste through washing of the cylinders to remove the heels. Although cylinder washing is not considered a foreseeable option at this time, for completeness, an analysis of the maximum potential quantities of TRU waste that could be generated from cylinder washing is included in Appendix B, as is a discussion of PCBs contained in some cylinder coatings.

#### **2.4.2.9 Resource Requirements**

Resource requirements include construction materials, fuel, electricity, process chemicals, and containers. In general, all alternatives would have a negligible effect on the local or national availability of these resources.

#### **2.4.2.10 Land Use**

Under the no action alternative, all activities would occur in areas previously used for conducting similar activities; therefore, no land use impacts are expected. Under the action alternatives, a total of 65 acres (26 ha) could be disturbed for the conversion facility, with some areas cleared for railroad or utility access and not adjacent to the construction site. Up to 6.3 additional acres (2.5 ha) could also be disturbed for construction of a new cylinder yard. All three alternative locations are within an already industrialized facility, and impacts to land use would be similar for the three locations. The permanently altered areas would represent less than 1% of available land already developed for industrial purposes. Negligible impacts on land use are thus expected.

#### **2.4.2.11 Cultural Resources**

Under the no action alternative, impacts on cultural resources at the current storage locations would be unlikely because all activities would occur in areas already dedicated to cylinder storage. Under the action alternatives, impacts on cultural resources could be possible at all three alternative locations. Archaeological and architectural surveys have not been finalized for the candidate locations and must be completed prior to initiation of the action alternatives. If archaeological resources were encountered, or historical or traditional cultural properties were identified, a mitigation plan would be required.

#### **2.4.2.12 Environmental Justice**

No disproportionately high and adverse human health or environmental impacts are expected to minority or low-income populations during normal facility operations under the

action alternatives. Although the consequences of facility accidents could be high if severe accidents occurred, the risk of irreversible adverse effects (including fatalities) among members of the general public from these accidents (taking into account the consequences and probability of the accidents) would be less than 1. Furthermore, transportation accidents with high and adverse impacts are unlikely; their locations cannot be projected, and the types of persons who would be involved cannot be reliably predicted. Thus, there is no reason to expect that minority and low-income populations would be affected disproportionately by high and adverse impacts.

#### **2.4.2.13 Impacts from Cylinder Preparation at ETTP**

The cylinders at ETTP would have to be prepared to be shipped by either truck or rail. Approximately 5,900 cylinders (4,800 DUF<sub>6</sub> cylinders for conversion and about 1,100 non-DUF<sub>6</sub> cylinders) would require preparation for shipment at ETTP. As discussed in Chapter 5, three cylinder preparation options are considered for the shipment of noncompliant cylinders.

In general, the use of cylinder overpacks would result in small potential impacts. Overpacking operations would be similar to current cylinder handling operations, and impacts would be limited to involved workers. No LCFs among involved workers from radiation exposure are expected. Impacts would be similar if noncompliant cylinders were shipped “as-is” under a DOT exemption, with appropriate compensatory measures.

The use of a cylinder transfer facility would likely require the construction of a new facility at ETTP; there are no current plans to build such a facility. Operational impacts would generally be small and limited primarily to external radiation exposure of involved workers, with no LCFs expected. Transfer facility operations would generate a large number of emptied cylinders requiring disposition. If a decision were made to construct and operate a transfer facility at ETTP, additional NEPA review would be conducted.

If ETTP cylinders were transported to Paducah for conversion, the operational period at Portsmouth would be reduced by 4 years. Annual impacts would be the same as discussed for each technical discipline. No significant decrease in overall impacts would be expected.

#### **2.4.2.14 Impacts Associated with Conversion Product Sale and Use**

The conversion of the DUF<sub>6</sub> inventory produces products having some potential for reuse (no large-scale market exists for depleted U<sub>3</sub>O<sub>8</sub>). These products include HF and CaF<sub>2</sub>, which are commonly used as commercial materials. An investigation of the potential reuse of HF and CaF<sub>2</sub> is included as part of this EIS (Chapter 5 and Appendix E). Areas examined include the characteristics of these materials as produced within the conversion process, the current markets for these products, and the potential socioeconomic impacts should these products be provided to the commercial sector. Because there would be some residual radioactivity associated with these materials, the DOE process for authorizing release of materials for unrestricted use (referred to as “free release”) and an estimate of the potential human health effects of such free release are

also considered in this investigation. The results of the analysis of HF and CaF<sub>2</sub> use are included in Table 2.4-1.

If the products were to be released for restricted use (e.g., in the nuclear industry for the manufacture of nuclear fuel), the impacts would be less than those for unrestricted release.

Conservative estimates of the amount of uranium and technetium that might transfer into the HF and CaF<sub>2</sub> were used to evaluate the maximum expected dose to workers using the material if it was released for commercial use or the general public. On the basis of very conservative assumptions concerning use, the maximum dose to workers was estimated to be less than 1 mrem/yr, much less than the regulatory limit of 100 mrem/yr specified for members of the general public. Doses to the general public would be even lower.

Socioeconomic impact analyses were conducted to evaluate the impacts of the introduction of the conversion-produced HF or CaF<sub>2</sub> into the commercial marketplace. A potential market for the aqueous HF has been identified as the current aqueous HF acid producers. The impact of HF sales on the local economy in which the existing producers are located and on the U.S. economy as a whole is likely to be minimal. No market for the CaF<sub>2</sub> that might be produced in the conversion facility has been identified. Should such a market be found, the impact of CaF<sub>2</sub> sales on the U.S. economy is also predicted to be minimal.

#### **2.4.2.15 Impacts from D&D Activities**

D&D would involve the disassembly and removal of all radioactive and hazardous components, equipment, and structures. For the purposes of analysis in this EIS, it was also assumed that the various buildings would be dismantled and “greenfield” (unrestricted use) conditions would be achieved. The “clean” waste will be sent to a landfill that accepts construction debris. Low-level waste will be sent to a licensed or DOE disposal facility, where it will likely be buried in accordance with the waste acceptance criteria and other requirements in effect at that time. Hazardous and mixed waste will be disposed of in a licensed facility in accordance with applicable regulatory requirements. D&D impacts to involved workers would be primarily from external radiation; expected exposures would be a small fraction of operational doses; no LCFs would be expected. It is estimated that no fatalities and up to 5 injuries would result from occupational accidents. Impacts from waste management would include total generation of about 275 yd<sup>3</sup> (210 m<sup>3</sup>) of LLW, 157 yd<sup>3</sup> (120 m<sup>3</sup>) of LLMW, and 157 yd<sup>3</sup> (120 m<sup>3</sup>) of hazardous waste; these volumes would result in low impacts in comparison with projected site annual generation volumes.

#### **2.4.2.16 Cumulative Impacts**

The CEQ guidelines for implementing NEPA define cumulative effects as the impacts on the environment resulting from the incremental impact of an action under consideration when added to other past, present, and reasonably foreseeable future actions (40 CFR 1508.7) Activities considered for cumulative analysis include those in the vicinity of the Portsmouth site

that might affect environmental conditions at or near that locality under both the no action alternative and the action alternatives. Activities considered also include those at the ETTP site associated with transporting cylinders to Portsmouth (under the proposed action) and continued long-term storage of DUF<sub>6</sub> (under the no action alternative).

One action considered reasonably foreseeable under cumulative impacts is the development of a uranium enrichment facility at the Portsmouth site. An agreement between USEC and DOE on June 17, 2002, established the possibility of constructing an enrichment plant at either site. In January 2004, USEC announced that it planned to site its American Centrifuge Facility at the Portsmouth site. This EIS assumes that such an enrichment facility would employ the existing gas centrifuge technology and would generate impacts similar to those outlined in a 1977 analysis of environmental consequences that considered such an action. (The facility proposed in 1977 was never completed or operated.)

Other actions planned at the Portsmouth site include continued waste management activities, waste disposal activities, environmental restoration activities, industrial reuse of sections of the site, and the DUF<sub>6</sub> management activities considered in this EIS. Activities involving gaseous diffusion uranium enrichment at Portsmouth were discontinued early in 2002. Cumulative impacts at the Portsmouth site and vicinity would be as follows for the no action alternative and the proposed action alternatives:

- The cumulative radiological exposure to the off-site population would be considerably below the maximum DOE dose limit of 100 mrem per year to the off-site maximally exposed individual (MEI) and below the limit of 25 mrem/yr specified in 40 CFR 190 for uranium fuel cycle facilities. Annual individual doses to involved workers would be monitored to maintain exposure below the regulatory limit of 5 rem per year.
- Under the no action alternative cumulative impacts assessment, although less than one shipment per year of radioactive wastes is expected from cylinder management activities; up to 3,500 rail shipments and 4,500 truck shipments would be associated with existing and planned actions. Under the action alternatives, up to 6,800 rail shipments and 12,300 truck shipments of radioactive material could occur. The cumulative maximum dose to the MEI along the transportation route near the site entrance would be less than 1 mrem/yr for all transportation options considered.
- The Portsmouth site is located in an attainment region. However, the background annual average PM<sub>2.5</sub> concentration exceeds the standard. Cumulative impacts would not affect the attainment status.
- Data from the 2000 annual groundwater monitoring showed that five pollutants exceeded primary drinking water regulation levels in groundwater at the Portsmouth site. Alpha and beta activity were also detected. Good engineering and construction practices should ensure that indirect impacts associated with the conversion facility would be minimal.

- Cumulative ecological impacts should be negligible, with little change to intact ecosystems contributed by any alternative considered in this EIS in conjunction with the effects of other activities.
- Impacts on land use similarly would be minimal, with DUF<sub>6</sub> conversion activities confined to the Portsmouth site, which is already heavily developed for such activities.
- It is unlikely that any noteworthy cumulative impacts on cultural resources would occur under any alternative, and any such impacts would be adequately mitigated before activities for the chosen action would start.
- Given the absence of high and adverse cumulative impacts for any impact area considered in this EIS, no environmental justice cumulative impacts are anticipated for the Portsmouth site, despite the presence of disproportionately high percentages of low-income populations in the vicinity.
- Socioeconomic impacts under all the alternatives considered are anticipated to be generally positive, often temporary, and relatively small.

Actions planned at the ETTP site include continued waste management activities, reindustrialization of the ETTP site, environmental restoration activities, possibly other DOE programs involving the disposition of enriched uranium, and the DUF<sub>6</sub> management activities considered in this EIS. Cumulative impacts at the ETTP site and vicinity would not be large under either the no action or the action alternatives.

#### **2.4.2.17 Potential Impacts Associated with the Option of Expanding Conversion Facility Operations**

As discussed in Section 2.2.7, several reasonably foreseeable activities could result in a future decision to increase the conversion facility throughput (such as by adding a fourth process line) or to extend the operational period at one or both of the conversion facility sites, although there are no current plans to do so. To account for these future possibilities and provide future planning flexibility, Section 5.2.8 includes an evaluation of the environmental impacts associated with expanding conversion facility operations at Portsmouth, either by increasing throughput or by extending operations.

The throughput of the Portsmouth facility could be increased either by making process efficiency improvements or by adding an additional (fourth) process line. As described in Section 5.2.8, a throughput increase through process improvements would not be expected to significantly change the overall environmental impacts when compared with the current plant design (three process lines). Efficiency improvements are generally on the order of 10%, which is within the uncertainty that is inherent in the impact estimate calculations. Slight variations in plant throughput are not unusual from year to year because of operational factors

(e.g., equipment maintenance or replacement) and are generally accounted for by the conservative nature of the impact calculations.

In contrast to process efficiency improvements, the addition of a fourth process line at the Portsmouth facility would require the installation of additional plant equipment and would result in a nominal 33% increase in throughput compared with the current base design. The plant capacity would be similar to the capacity planned for the Paducah site (evaluated in DOE/EIS-0359). This throughput increase would reduce the time necessary to convert the Portsmouth and ETTP DUF<sub>6</sub> inventories by about 5 years. The construction impacts presented above and summarized in Table 2.4-1 for three process lines would be the same if a fourth line was added, because a fourth line would fit within the process building.

In general, a 33% increase in throughput (e.g., by the addition of a fourth line) would not result in significantly greater environmental impacts during operations than those discussed above and summarized in Table 2.4-1 for three process lines (impacts associated with expanded operations are shown in brackets in Table 2.4-1 where they would differ from those presented for the proposed design). Although annual impacts in certain areas might increase up to 33% (proportional to the throughput increase), the estimated annual impacts during operations would remain well within applicable guidelines and regulations, with collective and cumulative impacts being quite low.

One exception is the PM<sub>2.5</sub> concentration during construction, which could exceed standards because of the regionally high background level under both three- and four-process-line cases. The background data used are the maximum values from the last 5 years of monitoring at the monitoring location nearest to the site (operated by the OEPA), located about 20 mi (32 km) away in the town of Portsmouth. On the basis of these values, exceedance of the annual PM<sub>2.5</sub> standard would be unavoidable, because the background concentration already exceeds the standard (background is 24.1 µg/m<sup>3</sup>, in comparison with the standard of 15 µg/m<sup>3</sup>).

Because a 33% increase in throughput would reduce the operational period of the facility by approximately 5 years, positive socioeconomic impacts associated with employment of the conversion facility workforce would last approximately 13 years, compared with 18 years under the base design.

The conversion facility operations could also be expanded by operating the facility longer than the currently anticipated 18 years. There are no current plans to operate the conversion facilities beyond this period. However, with routine facility and equipment maintenance and periodic equipment replacements or upgrades, it is believed the conversion facility could be operated safely beyond this time period to process any additional DUF<sub>6</sub> for which DOE might assume responsibility. As discussed in Section 5.2.8, if operations were extended beyond 18 years and if the operational characteristics (e.g., estimated releases of contaminants to air and water) of the facility remained unchanged, it is expected that the annual impacts would be essentially the same as those presented above and summarized in Table 2.4-1. The estimated annual impacts during operations are generally within applicable guidelines and regulations, with collective and cumulative impacts being quite low. This would also be expected during extended

operations. The overall cumulative impacts from the operation of the facility would increase proportionately with the increased life of the facility.

## **2.5 PREFERRED ALTERNATIVE**

DOE's preferred alternative is to construct and operate the proposed DUF<sub>6</sub> conversion facility at alternative Location A, which is located in the west-central portion of the Portsmouth site.

### 3 AFFECTED ENVIRONMENT

This EIS considers the proposed action of building and operating a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> cylinder inventories. Section 3.1 presents a detailed description of the affected environment for the Portsmouth site. Because the option of shipping cylinders from the ETTP site in Oak Ridge, Tennessee, to the Portsmouth site for conversion is part of the proposed action, a detailed description of the affected environment for the ETTP site is provided in Section 3.2.

#### 3.1 PORTSMOUTH SITE

The Portsmouth site is located in Pike County, Ohio, approximately 22 mi (35 km) north of the Ohio River and 3 mi (5 km) southeast of the town of Piketon (Figure 3.1-1). The two largest cities in the vicinity are Chillicothe, located 26 mi (42 km) north of the site, and Portsmouth, 22 mi (35 km) south.

The Portsmouth site includes the Portsmouth Gaseous Diffusion Plant (PORTS), a gaseous diffusion plant previously operated first by DOE and then by USEC. Uranium enrichment operations at PORTS were discontinued in May 2001, and the plant has been placed in cold standby, a nonoperational condition in which the plant retains the ability to resume operations within 18 to 24 months (DOE 2001c).

The Portsmouth site occupies 3,714 acres (1,500 ha) of land, with an 800-acre (320-ha) fenced core area that contains the former production facilities. The 2,914 acres (1,180 ha) outside the core area includes restricted buffers, waste management areas, plant management and administrative facilities, gaseous diffusion plant support facilities, and vacant land (Martin Marietta Energy Systems, Inc. [MMES] 1992b). Wayne National Forest borders the plant site on the east and southeast, and Brush Creek State Forest is located to the southwest, slightly more than 1 mi (1.6 km) from the site boundaries.

The Portsmouth site is not listed on the Comprehensive Environmental Response, Compensation, and Liability Act (CERCLA) National Priorities List. Investigation and cleanup of hazardous substances (as defined in CERCLA) and hazardous wastes (as defined in the RCRA) that have been released to air, surface water, groundwater, soils, and solid waste management units as a result of past operational activities at the Portsmouth site are being conducted under the provisions of the following administrative edicts, which have been issued pursuant to RCRA, CERCLA, and/or Ohio state law:

- State of Ohio v. U.S. Department of Energy, Divested Atomic Corporation, et al., Consent Decree. Civil Action C2-89-732. August 31, 1989 (referred to as the 1989 Ohio Consent Decree). The 1989 Ohio Consent Decree addresses certain hazardous waste compliance issues at the Portsmouth site and requires the performance of corrective actions in addition to other requirements.

- In the Matter of United States Department of Energy: Portsmouth Gaseous Diffusion Plant, Administrative Consent Order. U.S. Environmental Protection Agency (EPA) Administrative Docket No. OH7 890 008 983. August 12, 1997 (agreement between DOE, U.S. EPA, and Ohio EPA) (referred to as the 1997 Three-Party Administrative Consent Order). The 1997 Three-Party Administrative Consent Order replaced a prior U.S. EPA Administrative Consent Order, which was issued during 1989 and amended in 1994, and defines oversight roles at the Portsmouth site for the Ohio EPA and U.S. EPA with respect to corrective action/response action activities. It also defines certain cleanup performance obligations for DOE.
- In the Matter of United States Department of Energy and Bechtel Jacobs Company LLC, Director’s Final Findings and Orders. March 17, 1999 (referred to as the 1999 Ohio Integration Order). The 1999 Ohio Integration Order integrates the closure requirements for specified units at the Portsmouth site as established under the 1989 Ohio Consent Decree, the Ohio Administrative Code, and the 1997 Three-Party Administrative Consent Order. The purpose of this integration is to avoid duplication of effort, and efficiently perform site-wide groundwater monitoring and surveillance and maintenance activities at the Portsmouth site.

**3.1.1 Cylinder Yards**

The Portsmouth site has a total of 16,109 DOE-managed cylinders containing DUF<sub>6</sub> (Table 3.1-1). The cylinders are located in two storage yards that have concrete bases (Figure 3.1-2). The cylinders are stacked two high to comply with DNFSB requirements. All 10- and 14-ton (9- and 12-t) cylinders stored in these yards have been or are being inspected and repositioned. They have been placed on new concrete saddles with sufficient room between cylinders and cylinder rows to permit adequate visual inspection of cylinders.

**TABLE 3.1-1 DOE-Managed DUF<sub>6</sub> Cylinders at the Portsmouth Site**

Cylinder Type	No. of Cylinders
Full	16,018
Partially full	42
Heel	49
Total	16,109

**3.1.2 Site Infrastructure**

The Portsmouth site has direct access to major highway and rail systems, a nearby regional airport, and barge terminals on the Ohio River. Use of the Ohio River barge terminals requires transportation by public road from the Portsmouth site.

Source: Hightower (2004).

The Portsmouth site obtains its water supply from an on-site water treatment plant that draws water from off-site supply wells on the Scioto River. In 2001, total groundwater production from this system averaged 6.6 million gal/d (25 million L/d) for the site, including USEC activities (DOE 2002d).

The Ohio Valley Electric Corporation supplies the site with electrical power. The current electrical consumption is about 20 to 40 MW; the maximum electrical design capacity is 2,260 MW.

### **3.1.3 Climate, Air Quality, and Noise**

#### **3.1.3.1 Climate**

The Portsmouth site is located in the humid continental climatic zone and has weather conditions that vary greatly throughout the year (DOE 2001c). For the 1961 through 1990 period in Waverly, about 10 mi (16 km) north of the site, the annual average temperature was 52.9°F (11.6°C), with the highest monthly average temperature of 74.1°F (23.4°C) in July and the lowest of 28.8°F (−1.8°C) in January (National Oceanic and Atmospheric Administration [NOAA] 2000). Record extreme maximum and minimum temperatures are 102°F (39°C) and −24°F (−31°C). Annual precipitation averages about 39.7 in. (100.7 cm). Precipitation is relatively evenly distributed throughout the year but is somewhat higher in spring and summer than in winter and fall. Snowfall in Portsmouth averages 17.3 in. (43.9 cm) per year, occurring from November to April. Annual average relative humidity in Columbus, Dayton, and Cincinnati was more than 70% (Wood 1996).

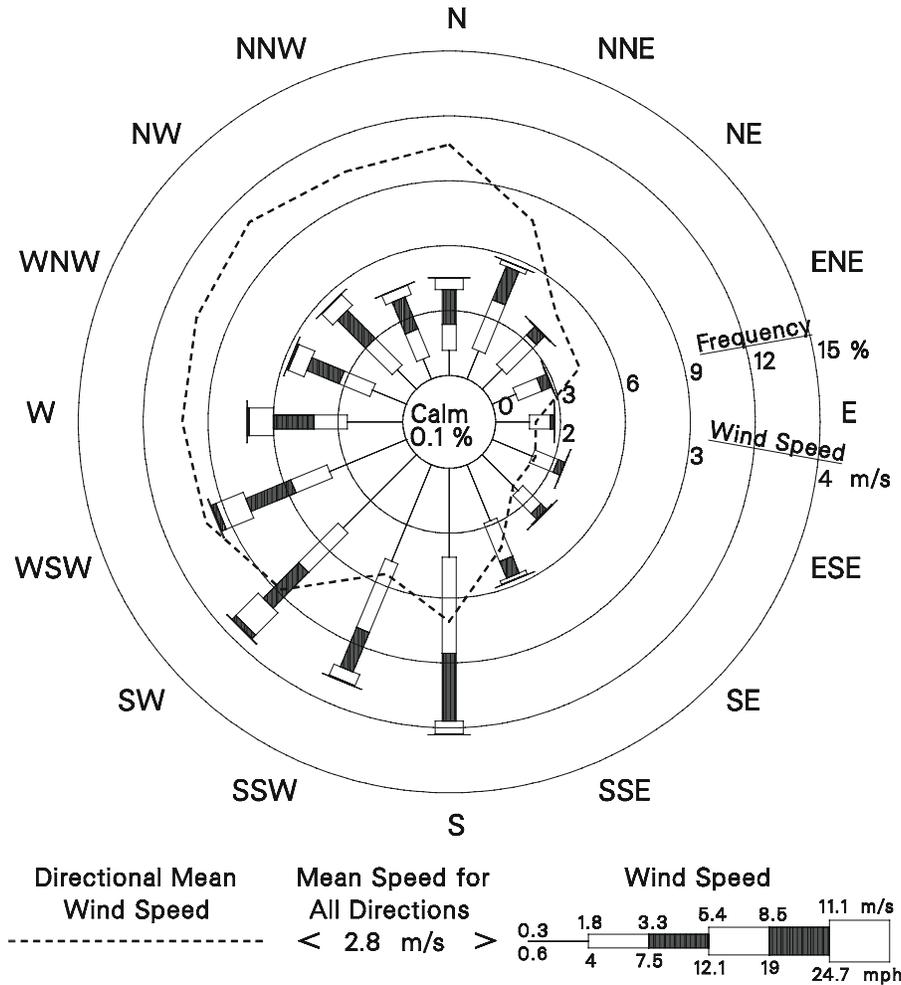
Surface meteorological data, including wind data, have been collected at the on-site meteorological tower at the 10-, 30-, and 60-m (33-, 98-, and 197-ft) levels. The tower is in the southern part of the site. A comparison of annual wind roses for the period 1995 through 2001 indicates that wind patterns at the 10-m (33-ft) level are different from those at the 30-m and 60-m (98- and 197-ft) levels. Winds at the 10-m (33-ft) level appear to be influenced by local topographical and/or vegetative features. Accordingly, wind data at the 30-m (98-ft) level, believed to be representative of the site, are presented in Figure 3.1-3, which was prepared on the basis of hourly surface data from the on-site tower (Takacs 2002). More than 40% of the time, wind blew from the southwest quadrant, with the prevailing wind being from the south. Average wind speed was about 6.2 mph (2.8 m/s). Directional wind speed was highest, at 7.4 mph (3.3 m/s), from the northwest, and it was lowest, at 4.0 mph (1.8 m/s), from the east.

Tornadoes are rare in the area surrounding the Portsmouth site, and those that do occur are less destructive in this region than those occurring in other parts of the Midwest. For the 1950 through 1995 period, 656 tornadoes were reported in Ohio, with an average of 14 tornadoes per year (Storm Prediction Center 2002). For the same period, 3 tornadoes were reported in Pike County, but most of those were relatively weak — at most, F2 of the Fujita tornado scale.

#### **3.1.3.2 Existing Air Emissions**

Nonradiological air emissions from USEC are predominant sources in Pike County (EPA 2003b). Currently, USEC has three OEPA operating permits. The Title V permit for USEC

Site : PORTS, OH (30-m Level)  
 Period : 1995-2001



**FIGURE 3.1-3 Wind Rose for the Portsmouth Site (30-m level), 1995-2001 (Source: Takacs 2002)**

operations has been issued and was effective August 21, 2003, which is a sitewide, federally enforceable operating permit to cover emissions of all regulated air pollutants at the facility. In submissions to the OEPA, USEC reported the following criteria pollutant emissions for the year 2001 (see Table 3.1-2): 59.86 tons (54.30 t) of particulate matter with a mean diameter of 10  $\mu\text{m}$  or less ( $\text{PM}_{10}$ ), 1.42 tons (1.29 t) of volatile organic compounds (VOCs), 2,627.64 tons (2,473.57 t) of  $\text{SO}_2$ , and 362.05 tons (328.45 t) of  $\text{NO}_x$ . These emissions are associated with the boilers at the X-600 steam plant (which provides steam for the Portsmouth reservation), a boiler at the X-611 water treatment plant, an emergency generator, and a trash pump (DOE 2002d). DOE operates numerous small sources that release criteria pollutants and VOCs. At the end of 2001, DOE had eight permitted and seven registered air emission sources (Richmond 2003). In November 2001, DOE began operation of the X-6002 recirculating hot water plant to provide heat for the DOE facilities that were formerly heated by hot water from the gaseous diffusion

**TABLE 3.1-2 Annual Criteria Pollutant and Volatile Organic Compound Emissions from USEC and DOE Sources at the Portsmouth Site in 2001**

Major Emission Source	Emission Rate (tons/yr)					
	SO <sub>2</sub>	NO <sub>x</sub>	CO	VOCs	PM <sub>10</sub>	PM <sub>2.5</sub>
USEC facilities <sup>a</sup>	2,627.64	362.05	NA <sup>b</sup>	1.42	59.86	NA
DOE facilities <sup>c</sup>	21.5	93.6	58.5	5.7	5.3	NA

<sup>a</sup> Source: DOE (2002d).

<sup>b</sup> NA = not available.

<sup>c</sup> Proposed maximum annual emissions based on the assumption that two boilers would operate full time.

Source: Richmond (2003).

process. Proposed maximum annual emissions from plant operations account for most of the DOE emissions (Richmond 2003) (see Table 3.1-2). Other emission sources at DOE, which include two landfill venting systems, two glove boxes (not used in 2001), two aboveground storage tanks in the X-6002A fuel oil storage facility, and two groundwater treatment facilities, emit less than 1 ton per year of conventional air pollutants (on an individual basis).

Airborne discharges of radionuclides from the Portsmouth site are regulated under the CAA, 40 CFR 61, Subpart H, National Emission Standards for Hazardous Air Pollutants (NESHAPs). Currently, USEC is responsible for most of the sources that emit radionuclides because DOE leased the production facilities to USEC. In 2001, USEC and DOE reported emissions of 0.2 and 0.00063 Ci from their radionuclide emission sources, respectively. These values were used to estimate doses to members of the general public (DOE 2002d).

### 3.1.3.3 Air Quality

The Ohio State Ambient Air Quality Standards (SAAQS) for six criteria pollutants — SO<sub>2</sub>, nitrogen dioxide (NO<sub>2</sub>), CO, ozone (O<sub>3</sub>), PM (PM<sub>10</sub> and PM<sub>2.5</sub>), and lead (Pb) — are the same as the National Ambient Air Quality Standards (NAAQS)<sup>1</sup> (OEPA 2002), as shown in Table 3.1-3.

The Portsmouth site is located in the Wilmington-Chillicothe-Logan Intrastate Air Quality Control Region (AQCR), which covers the south-central part of Ohio. Currently, Pike county is designated as being in attainment for all criteria pollutants (40 CFR 81.336). Ambient concentration data for criteria pollutants around the site are not available. On the basis of

<sup>1</sup> The EPA promulgated new O<sub>3</sub> 8-hour and PM<sub>2.5</sub> standards in July 1997.

1997 through 2002 monitoring data, the highest concentration levels for SO<sub>2</sub>, NO<sub>2</sub>, CO, PM<sub>10</sub>, and Pb representative of the Portsmouth site are less than 64% of their respective NAAQS, as listed in Table 3.1-3 (EPA 2003b). However, the highest O<sub>3</sub> and PM<sub>2.5</sub> concentrations are approaching or somewhat higher than the applicable NAAQS. These high ozone concentrations of regional concern are associated with high precursor emissions from the Ohio Valley region and long-range transport from southern states.

Ambient air monitoring stations in and around the site consist of a network of 15 air samplers that primarily collect data on radionuclides released from the site. These data are used to assess whether air emissions from the Portsmouth site would affect air quality in the surrounding area. If a person lived close to a monitoring station, the net dose calculated was 0.00019 mrem/yr, which is well below the 10-mrem/yr NESHAPs limit applicable to Portsmouth (see Section 3.1.7.1). In addition to the radionuclides, samples for fluoride were collected weekly from 15 ambient monitoring stations in and around PORTS. In 2001, the average ambient concentrations were similar to or less than those collected at the background station, except for a station that is within the process area immediately east of the X-326 building.

Prevention of significant deterioration (PSD) regulations (40 CFR 52.21) limit the maximum allowable incremental increases in ambient concentrations of SO<sub>2</sub>, NO<sub>2</sub>, and PM<sub>10</sub> above established baseline levels, as shown in Table 3.1-3. The PSD regulations, which are designed to protect ambient air quality in Class I and Class II attainment areas, apply to major new sources and major modifications to existing sources. The nearest Class I PSD areas are Otter Creek Wilderness Area in West Virginia, about 177 mi (285 km) east of the Portsmouth site; Dolly Sods Wilderness Area in West Virginia, about 193 mi (311 km) east of the site; and Mammoth Cave National Park in Kentucky, about 200 mi (322 km) southwest of the site. These Class I areas are not located downwind of prevailing winds at the Portsmouth site (see Figure 3.1-3).

#### **3.1.3.4 Existing Noise Environment**

The Noise Control Act of 1972, along with its subsequent amendments (Quiet Communities Act of 1978; 42 USC 4901–4918), delegates authority to the states to regulate environmental noise and directs government agencies to comply with local community noise statutes and regulations. The State of Ohio and Pike County, where the Portsmouth site is located, have no quantitative noise-limit regulations.

The EPA has recommended a maximum noise level of 55 dB(A) as the DNL to protect against outdoor activity interference and annoyance (EPA 1974a). This level is not a regulatory goal but is “intentionally conservative to protect the most sensitive portion of the American population” with “an additional margin of safety.” For protection against hearing loss in the general population from nonimpulsive noise, the EPA guideline recommends an L<sub>eq</sub>(24 h) of 70 dB(A) or less.<sup>2</sup>

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<sup>2</sup> L<sub>eq</sub> is the equivalent steady sound level that, if continuous during a specific time period, would contain the same total energy as the actual time-varying sound. For example, L<sub>eq</sub>(24 h) is the 24-hour equivalent sound level.

The noise-producing activities within the Portsmouth site are associated with processing and construction activities and local traffic, similar to those at any other typical industrial site. During site operations, noise levels near the cooling towers are relatively high, but most noise sources are enclosed in the buildings. Currently, the site is in cold standby mode, so no major noise-producing activities exist on site. Another noise source is associated with rail traffic in and out of the Portsmouth site. In particular, train whistle noise, at a typical noise level of 95 to 115 dB(A), is high at public grade crossings. Currently, rail traffic noise is not a factor in the local noise environment because of infrequent traffic (one train per week).

The Portsmouth site is in a rural setting, and no residences or other sensitive receptor locations (e.g., schools, hospitals) exist in the immediate vicinity of any noisy on-site operations. (The nearest sensitive receptor is located about 1 mi (2 km) from Location A for the proposed conversion facility.) Ambient sound level measurements around the site are not currently available; the ambient noise level around the site is relatively low, however, except for infrequent vehicular noise. In general, the background environment is typical of rural areas; day-night average sound level (DNL) from the population density in Pike County is estimated to be about 40 dB(A) (EPA 1974b).

### **3.1.4 Geology and Soil**

#### **3.1.4.1 Topography, Structure, and Seismic Risk**

The topography of the Portsmouth site area consists of steep hills and narrow valleys, except where major rivers have formed broad floodplains. The site is underlain by bedrock composed of shale and sandstone.

The Portsmouth site is situated within the Appalachian Plateau Physiographic Province of the Appalachian Highland region near its northwestern terminus at the Central Lowlands Province. The Appalachian Plateau is characterized by deeply dissected valleys and nearly accordant ridge tops. The summits of the main ridges just east of the Scioto River rise to an altitude of more than 1,100 ft (355 m) above mean sea level, with relief of up to 500 ft (150 m) from the bottom of the valleys.

Portsmouth is located within the Portsmouth paleoriver valley. Surface and near-surface geology at the site have been heavily influenced by glaciation and the resultant ice damming and drainage reversals. The site is located in an abandoned river valley that was filled with lacustrine (lake) sediments deposited during the existence of prehistoric Lake Tight (Rogers et al. 1988). The sedimentary units of interest at the site are, in ascending order, Ohio Shale, Bedford Shale, Berea Sandstone, Sunbury Shale, Cuyahoga Shale, Gallia Sand, and Minford Clay.

The Ohio Shale is 300 to 400 ft (90 to 120 m) thick at the site. It is black and thinly bedded and may contain oil. The Bedford Shale consists of interbedded thin sandstone and shale. The Berea Sandstone has a larger sand content than the Bedford Shale but is otherwise similar. At the site, the Berea Sandstone forms an aquifer that has an average thickness of about 30 ft (9 m). The Sunbury Shale is a black carbonaceous shale. This unit thins from east to west and

may be completely absent in western portions of the site (ANL 1991b). The Teays Formation overlies the Sunbury Shale and is made up of Gallia Sand (unconsolidated Quaternary deposit) and Minford Clay (unconsolidated Quaternary deposit), in ascending order. These unconsolidated deposits have a fluvial origin and occupy paleochannels of the Teays River System. The Gallia Sand member is a silty to clayey, coarse to fine-grained sand with a pebble base. The Minford Clay member contains interbedded silts and clays and is divided into two zones: an upper zone of clay and a lower zone of silty clay.

The Portsmouth site is within 60 mi (96 km) of the Bryand Station-Hickman Creek Fault (ANL 1991b). No correlation has been made between this fault and historical seismicity. Seismic Source Zone 60 is a north-northeast-trending zone in central and eastern Ohio and includes the Portsmouth site.

The largest recorded seismic event in this zone was the Sharpsburg, Kentucky, earthquake of July 1980. That earthquake registered a magnitude of 5.3 and a Modified Mercalli intensity of VII. For this site, the evaluation-basis earthquake (EBE) was designated by DOE to have a return period of 250 years. A detailed analysis indicated that the peak ground motion for the EBE was approximately 0.06 times the acceleration of gravity (LMES 1997c). The estimated mean value of peak ground acceleration for a 1,000-year return period is 0.11 times the acceleration of gravity (ANL 1991b). Ground motion from such an earthquake would be equivalent to a Class VI or VII earthquake.

#### **3.1.4.2 Soils**

A majority of the soils at Portsmouth are formed on alluvial and lacustrine deposits. Other important soil-forming materials are parent material, colluvium, and loess (windblown material) (ANL 1991b). Approximately 1,500 acres (600 ha) of the site consists of moderately drained soils of the Urban Land-Omulga silt loam complex. The Omulga soil at the site is a dark grayish brown silt loam about 10-in. (25-cm) thick. Beneath this layer is about 54 in. (137 cm) of yellowish-brown subsoil. This material is characterized by a friable silt loam, a silty clay fragipan (low-permeability layer), and, near the bottom, a friable silt loam. Within the fragipan, the subsoil has slow permeability. Other soils of Portsmouth include the Clifty and Wilbur silt loams, which occur in stream valleys. The uplands areas contain a mixture of Coolville, Blairton, Latham, Princeton, Shelocta, and Wyatt soils. A description of these soils is provided in Hendershot et al. (1990).

The substances in soil that might be associated with cylinder management activities at the Portsmouth site are uranium and fluoride compounds, which could be released if breached cylinders or faulty valves were present. In 2001, soil was sampled for radioactive parameters, including uranium, at 24 on-site, 18 off-site, and 4 background locations (DOE 2002c). Analytical results for all off-site and most on-site sampling locations were similar to background values. Concentrations of uranium ranged from 2.1 to 23.3 µg/g, with the maximum at sampling location RIS-19, adjacent to the X-705 decontamination building (DOE 2002c). This area is known to be contaminated from historical small spills; the source of uranium was not considered

to be the cylinder storage yards. Fluoride has not been analyzed in soil samples, but it occurs naturally in soils and is low in toxicity.

After a March 1978 cylinder handling accident, soil samples were collected to determine whether the X-745-C and X-745-B yards were contaminated (Geraghty & Miller, Inc. 1994a). Total uranium concentrations in the X-745-C yard did not appear to be elevated; they ranged from 2.2 to 4.4 µg/g. VOCs, semivolatile organic compounds (SVOCs), and PCBs were detected in shallow soil samples at maximum concentrations up to about 3 µg/g (for polycyclic aromatic hydrocarbons [PAHs]). Although a few VOCs were detected at low concentrations in groundwater from one well, the source is unlikely to be the X-745-C yard (Geraghty & Miller, Inc. 1994a).

Contaminant concentrations in the X-745-B yard were elevated in some soil samples, ranging from 2.7 to 352 µg/g (for the PAH phenanthrene). However, no uranium, VOCs, SVOCs, or PCBs were detected in groundwater associated with the X-745-B yard. The contamination was confined to shallow soils and limited to the immediate proximity of the unit (Geraghty & Miller, Inc. 1994b).

An investigation of Location A soils was conducted in 2000 (Tetra Tech, Inc. 2000). Six surface soil samples (collected from depths of 0 to 1 ft [0 to 35 cm]) were obtained, and 23 subsurface soil samples were collected from soil borings at the same locations as those where the surface soil samples were collected. Samples were analyzed for VOCs, SVOCs, PCBs, and radionuclides. No organic compounds or PCBs were detected in surface or subsurface soil samples. In one soil boring location, alpha activity was detected at a concentration slightly greater than background in both the surface and subsurface samples (i.e., 5.2 pCi/g in a surface and subsurface soil sample versus 4.8 pCi/g background). Overall, the characterization data did not indicate soil contamination at Location A.

No characterization of soils in Locations B and C has been conducted. There is no known past or current source of contamination at either of these locations.

### **3.1.5 Water Resources**

The affected environment for water resources consists of surface water within and in the vicinity of the site boundary and groundwater beneath the site. Analyses of surface water, stream sediment, and groundwater samples indicated the presence of some contamination resulting from previous gaseous diffusion plant operations.

#### **3.1.5.1 Surface Water**

The Portsmouth site is within the Scioto River drainage basin. Both surface water and groundwater drain from the plant via a network of tributaries to the Scioto River (Rogers et al. 1988). The average flow in the Scioto River measured at Higby by the U.S. Geological Survey

(USGS) between 1930 and 1973 was  $2.1 \times 10^6$  gal/min (133 m<sup>3</sup>/s). The 10-year low-flow discharge at Higby is  $1.4 \times 10^5$  gal/min (8.58 m<sup>3</sup>/s).

The Portsmouth site is drained by several small tributaries of the Scioto River (Figure 3.1-4). The largest stream on the plant property is Little Beaver Creek, which drains the northern and northeastern portions of the site before discharging into Big Beaver Creek. Upstream of the plant, Little Beaver Creek flows intermittently during the year. On site, it receives treated process wastewater from a holding pond (via the east drainage ditch) and storm water runoff from the northwestern and northern sections of the plant via several storm sewers, water courses, and the north holding pond. The average release to Little Beaver Creek for 1993 was 940 gal/min (0.06 m<sup>3</sup>/s).

Storm sewers H, F, and G on the southern end of the plant site discharge to the south holding pond. This pond overflows to Big Run Creek, another intermittent stream that discharges into the Scioto River. A small unnamed intermittent watercourse drains the southwest corner of the site via the southwest holding pond. Farther north on the property, there is another intermittent watercourse that receives runoff from the central and western portions of the site via the west drainage ditch. All of these streams flow directly to the Scioto River and carry only storm water runoff.

At the Portsmouth site, DOE is responsible for 6 National Pollutant Discharge Elimination System (NPDES) outfalls, and USEC is responsible for 11 NPDES outfalls (DOE 2002d). Total uranium discharge in 2001 from DOE outfalls was estimated as 1.2 kg (2.7 lb); total uranium discharge in 2001 from USEC outfalls was estimated as 16.2 kg (35.8 lb).

In addition to NPDES outfall monitoring, surface waters are monitored for radioactive contamination at 14 locations, including locations upstream and downstream from the Portsmouth site. The surface water monitoring results for 2001 indicated that the measured radioactive contamination was consistently less than the applicable drinking water standards (DOE 2002c,d). Uranium concentrations were detected at levels similar to those that occurred naturally in the Scioto River surface water sampling locations in 2000. Tc-99 was detected at 43 pCi/L in a sample collected downstream of Little Beaver Creek; this level is well below the DOE derived concentration guide of 100,000 pCi/L (DOE 2002d). In addition, in 2001, surface water samples were collected monthly from five locations at the DOE cylinder storage yards and analyzed for total uranium, uranium isotopes, TRU, and Tc-99. The maximum detected concentration of uranium in these samples was 14 µg/L; the maximum Tc-99 concentration was 10 pCi/L.

Sediment samples are also collected at the same locations where USEC surface water samples are collected, and at the NPDES outfalls on the east and west sides of the Portsmouth site (DOE 2002d). In 2001, the maximum uranium concentration in sediment was 5.6 µg/g, at background sampling location RM-10W. The maximum Tc-99 concentration was 16 pCi/g, at location RM-7 downstream on Little Beaver Creek. Several inorganic substances and PCBs were also monitored; results of the monitoring indicate no major difference between upstream and downstream concentrations. PCBs were not detected in sediments.

### 3.1.5.2 Groundwater

Five hydrogeological units are important for groundwater flow and contaminant migration beneath Portsmouth. These units are, in descending order, Minford Clay, Gallia Sand, Sunbury Shale, Berea Sandstone, and Bedford Shale. The upper two units form an aquifer in unconsolidated Quaternary deposits; the lower three units form a Mississippian bedrock aquifer. At the site, the hydraulic conductivities of all of the units are very low (Geraghty & Miller, Inc. 1989a). The most conductive unit is Gallia Sand. It has a mean hydraulic conductivity of 3.4 ft/d (1 m/d) and a range of 0.11 to 150 ft/d (0.03 to 46 m/d). It acts as the principal conduit for contaminant transport. The next most permeable unit is Berea Sandstone. It has a mean hydraulic conductivity of 0.16 ft/d (0.05 m/d) and a range of 0.0045 to 15 ft/d (0.0013 to 4.6 m/d). The average conductivity of Minford Clay, the shallowest unit, is estimated to be 0.00023 ft/d ( $7.0 \times 10^{-5}$ ) in the upper zone, while the conductivity of the lower zone is about 0.0042 ft/d (0.0013 m/d).

Within the upper portion of the bedrock aquifer, permeability is primarily produced by fractures. As depth increases, the presence of fractures decreases, and permeability depends more on porosity, grain size and shape, and packing arrangement (MMES 1993). At greater depth, the Berea Sandstone is probably more permeable than the shale units, which act as confining layers. The direction of groundwater flow beneath the site is controlled by a complex interaction between the Gallia and Berea units (Geraghty & Miller, Inc. 1989a). The flow patterns are also affected by the presence of storm sewer drains and by the reduction in recharge caused by the presence of buildings and paved areas. Groundwater flow patterns in both the Gallia and Berea units are characterized by an east-west-trending groundwater divide. The direction of groundwater flow is generally to the south in the southern sections of the Portsmouth site and to the north in the northern sections.

In the vertical direction, almost all wells exhibit a downward gradient from the Gallia to the Berea unit. The extent of the gradient is influenced by the thickness of the Sunbury Shale. Where the Sunbury Shale is thick, the gradient is large. In places where the Sunbury Shale is absent, upward vertical gradients are observed. Three main discharge areas exist for the groundwater system beneath Portsmouth: Little Beaver Creek to the north and east, Big Run Creek to the south, and two unnamed drainages to the west (Geraghty & Miller, Inc. 1989a).

Although Portsmouth has the ability to use Scioto River water, all water is currently supplied by three off-site water supply well fields completed in the Scioto River alluvium located just east of the Scioto River. Recharge of the aquifers is from river and stream flow as well as precipitation (annual average rainfall is 40.7 in. [103 cm]). In 2001, total groundwater production from this system averaged 6.6 million gal/d (2.5 million L/d) for the site, including USEC activities (DOE 2002d).

On-site groundwater at and around the Portsmouth site is monitored for radioactive and nonradioactive constituents at more than 400 wells. On site, five areas of groundwater contamination have been identified that contain contaminants. The main contaminants are VOCs (mostly trichloroethylene [TCE]) and radionuclides (e.g., uranium, Tc-99) (DOE 2002d).

Data from the 2000 annual groundwater monitoring showed that five contaminants exceeded their primary drinking water standards at the Portsmouth site: beryllium, chloroethane, americium, TCE, and uranium. Alpha and beta activity also exceeded the standards (DOE 2001d,e). The concentration of contaminants and the lateral extent of the plume did not significantly increase in 2001 (DOE 2002d).

Two phytoremediation projects to clean up TCE-contaminated groundwater are currently underway at the Portsmouth site. The phytoremediation projects involve the planting of hybrid poplar trees about 5 ft (2 m) apart in areas of contamination. The tree roots take up 50 to 350 gal (190 to 1,325 L) of water per day per tree and also provide nutrients to the soil, which accelerates bacterial breakdown of contaminants in the soil. One phytoremediation project, which started in 1999, is located on a small area of about 3 acres (1 ha) that is just northeast of Location A and borders part of the proposed new cylinder storage yard Area 2. The other project, started in 2001, is located on about 28 acres (11 ha) at the southern end of the Portsmouth site, to the south and southeast of Location B.

### **3.1.6 Biotic Resources**

#### **3.1.6.1 Vegetation**

The most common type of vegetation on the Portsmouth site is managed grassland, which makes up 30% of the site (about 1,100 acres [445 ha]) (DOE 2001c). Grasses are the dominant species in these communities, and they are maintained by periodic mowing. Oak-hickory forest (covering 17% of the site) occurs on well-drained upland areas, and old-field communities (11%) occur in disturbed areas. Upland mixed hardwood forest also covers 11% of the site (400 acres [162 ha]). Black walnut, black locust, honey locust, black cherry, and persimmon are the dominant species in these mesic to dry upland communities. Riparian forest occurs in low, periodically flooded areas near streams; it makes up 4% of the site (153 acres [62 ha]). The dominant species in riparian forest communities are cottonwood, sycamore, willows, silver maple, and black walnut. Within the area surrounded by Perimeter Road, the Portsmouth site consists primarily of open grassland (including areas maintained as lawns) and developed areas consisting of buildings, paved areas, and storage yards.

Location A is approximately 26 acres (11 ha) in size and includes previously disturbed as well as undisturbed areas. Except for the northern portion, Location A is relatively level and has been graded. The northeastern portion of Location A and the area directly north of Building X-744-T support an old-field habitat, composed primarily of grasses such as fescue and broom-sedge, with crown vetch, wild carrot, and small scattered trees and shrubs. A drainage ditch bordering an old railroad bed in the east area supports sapling sycamore and black locust trees as well as mature black locust. Vegetation near the buildings is a managed grassland community and includes fescue, ox-eye daisy, and hop clover. Bulrush occurs in shallow drainage ditches. The area immediately adjacent to the buildings is infrequently mowed. At the northern boundary of Location A, the land surface slopes down to a small stream that runs along the northern margin of the location, approximately 100 ft (30 m) from the location boundary. This stream is bordered by a riparian woodland community of willow, mature sycamore, black

locust, and maple. This woodland community is classified as riparian forest; however, the tree canopy is fairly open and narrow (less than 100 ft [30 m]) in width. Small woodland areas lie north of Building X-744-U and northwest of Building X-744-T; they are continuous with the riparian woodland community bordering the stream to the north. These wooded areas are composed primarily of mature black locust trees, along with honeysuckle, sumac, and sweet clover.

Location B is approximately 50 acres (20 ha) in size. It has been disturbed by grading and construction activities and has a level ground surface. The vegetation at this location is composed entirely of a managed grassland community and generally remains unmowed. The dominant species are fescue, broom-sedge, hop clover, and birdfoot trefoil.

Location C is approximately 78 acres (32 ha) in size and has been disturbed by grading activities. This location is relatively level to gently sloping throughout and supports an open, managed grassland vegetation community that generally remains unmowed. The dominant species is fescue, with yarrow and ox-eye daisy. Two drainages in the southwest portion of this location are bordered by narrow deciduous woodland communities (approximately 60 ft [18 m] in width) with open tree canopies. These woodland communities are classified as upland mixed hardwood forest community.

### 3.1.6.2 Wildlife

Habitats on the Portsmouth site support a relatively high diversity of terrestrial and aquatic wildlife species. Species observed on the site include 27 mammal species, 114 bird species, 11 reptile species, and 6 amphibian species. Ground-nesting species include bobwhite and eastern box turtle. Various species of reptiles and amphibians are associated with streams and other surface water on the site. Migrating waterfowl use site retention ponds (ANL 1991b). Additional information on wildlife resources is available in DOE (2001c), MMES (1993), and ANL (1991b).

Fish communities in Little Beaver Creek range from good to exceptional downstream of the Portsmouth outfall, and are fair upstream (OEPA 1998). Aquatic habitat quality in Little Beaver Creek is lower upstream of the Portsmouth outfall, where stream flow is intermittent. Upstream macroinvertebrate communities are poor, while downstream communities range from poor to exceptional. The fish community in West Ditch, which is downstream of Location A is marginally good, while the macroinvertebrate community is fair (OEPA 1993).

The habitats within Locations A, B, and C support wildlife species typical of similar habitats in the vicinity. Species occurring in open grassland areas like those that are common in the three locations include eastern cottontail, meadow vole, and eastern meadowlark. Small wooded areas, such as those at Locations A and B, support numerous woodland and forest edge species such as raccoon, gray squirrel, red-headed woodpecker, cardinal, white-breasted nuthatch, and yellow-rumped warbler.

### 3.1.6.3 Wetlands

A wetland survey of the Portsmouth site was conducted in 1995. Approximately 34 acres (14 ha) of wetlands occur on the site, excluding retention ponds. Forty-one wetlands meet the criteria for jurisdictional wetlands, while four wetlands are nonjurisdictional (Chandler 1996). Wetlands on the site primarily support emergent vegetation that includes cattail, great bulrush, and rush. Palustrine forested wetlands occur on the site along Little Beaver Creek (ANL 1991b). The Ohio State Division of Natural Areas and Preserves has listed two wetland areas near the site as significant wetland communities: (1) a palustrine forested wetland, about 5 mi (8 km) east of the site, and (2) Givens Marsh, a palustrine wetland with persistent emergent vegetation, about 2.5 mi (4 km) northeast of the site. The 100-year floodplains in the vicinity of the Portsmouth site include Big Beaver Creek and Little Beaver Creek. Both of these floodplains lie outside the area surrounded by Perimeter Road.

The drainage channel in the east portion of Location A supports a palustrine emergent wetland community of fox sedge, green bulrush, drooping bulrush, narrow-leaf cattail, and rush that is 0.08 acre (0.03 ha) in size; however, only 0.05 acre (0.02 ha) of this wetland lies within the boundary of Location A (Figure 3.1-5). The steep slopes of the channel are vegetated with upland species. The drainage channel conveys surface water runoff to an intermittent stream that borders the north margin of Location A and likely also receives groundwater discharge. The stream, which lies in a low floodplain, supports a riparian woodland community of willow, maple, sycamore, and black locust. The stream and adjacent riparian area lie outside the boundary of Location A. Another small stream originates near the southwest corner of this location and enters a small holding pond west of Perimeter Road, a short distance above the confluence with the northern stream.

Wetlands do not occur at Location B. However, a number of wetlands occur in the vicinity of Location B in areas previously disturbed by industrial development. These wetlands receive surface runoff from the surrounding landscape; also, as a result of previous grading activities, soils are poorly drained. A large palustrine emergent wetland (3.2 acres [1.3 ha]), composed primarily of cattails, lies immediately to the south of the east portion of the area; it receives runoff from portions of Location B. Another small wetland (0.3 acre [0.12 ha]) lies just outside the southeast corner boundary of Location B. Several additional wetland areas are located within the open area to the south of Location B. Streams receiving drainage from Location B lie to the south and southwest and support riparian forest communities. Drainage flows into a holding pond southwest of Perimeter Road.

Although no wetlands are identified at Location C, two small drainages in the southwest portion of the area direct surface water flows from Location C to Big Run Creek. The upper segment of the X-230K holding pond is located downstream, immediately west of this location. Also, a drainage ditch along the south margin of the parking area in the northwest portion of Location C directs surface flows into a small wetland area to the west, beyond the location boundary. Finally, a drainage ditch exiting this wetland joins the upper segment of the holding pond.

### 3.1.6.4 Threatened and Endangered Species

Federal- and state-listed species in the vicinity of the Portsmouth site are listed in Table 3.1-4. No occurrence of federal-listed plant or animal species on the Portsmouth site has been documented. The Indiana bat, both federal- and state-listed as endangered, has been reported in the vicinity of the Portsmouth site and may occur on the site during spring or summer; however, no Indiana bats were collected during surveys in 1994 and 1996 (DOE 1997c). Roosting and nursery sites may include forested areas with loose barked trees (such as shagbark hickory) and standing dead trees. Potential summer habitat for the Indiana bat was identified within the corridors along Little Beaver Creek, the Northwest Tributary stream, and a wooded area east of the X-100 facility. However, most of the Portsmouth site was found to have poor summer habitat because of the small size, isolation, and insufficient maturity of the few woodlands on the site.

The sharp-shinned hawk, listed by the State of Ohio as endangered, and the rough green snake, a species of special interest in Ohio, have been observed on the Portsmouth site (DOE 2001c). Both of these species inhabit moist woods. The timber rattlesnake, listed by the State of Ohio as endangered, occurs in the vicinity of the Portsmouth site but has not been found on the site. Habitat for the timber rattlesnake is found on and near high, dry ridges. Two state-protected plant species that occur on the Portsmouth site are Carolina yellow-eyed grass, listed as endangered, and Virginia meadow-beauty, listed as potentially threatened (DOE 2001c).

**TABLE 3.1-4 Federal- and State-Listed Endangered, Potentially Threatened, and Special Concern Species near the Portsmouth Site**

Category and Scientific Name	Common Name	Status <sup>a</sup>	
		Federal	State
<b>Mammals</b>			
<i>Myotis sodalis</i>	Indiana bat	E	E
<b>Birds</b>			
<i>Accipiter striatus</i>	Sharp-shinned hawk		E
<b>Reptiles</b>			
<i>Crotalus horridus</i>	Timber rattlesnake		E
<i>Opheodrys aestivus</i>	Rough green snake		S
<b>Plants</b>			
<i>Rhexia virginica</i>	Virginia meadow-beauty		P
<i>Xyris difformis</i>	Carolina yellow-eyed grass		E

<sup>a</sup> E = endangered; P = potentially threatened; S = special concern.

Source: DOE (2001c).

These species occur in Quadrant IV, northeast of the area bounded by Perimeter Road. A population of long-beaked arrowhead, a wetland plant listed by the state as threatened, occurs just north of the site.

No federal- or state-listed species have been found to occur at Location A, B, or C. These locations do not support suitable habitat for the Indiana bat. Although Locations A and C contain small wooded areas, the proximity to paved roads and the small size and insufficient maturity of these areas would probably provide poor habitat for Indiana bats. These characteristics also limit the habitat suitability of these small wooded areas for the sharp-shinned hawk and rough green snake. Habitat for the timber rattlesnake does not occur on or near any of the three locations. The nearest populations of Carolina yellow-eyed grass and Virginia meadow-beauty are approximately 1.5 mi (2.4 km) north of Location A. The highly disturbed conditions at the three locations do not provide suitable habitat for these species.

### **3.1.7 Public and Occupational Safety and Health**

#### **3.1.7.1 Radiation Environment**

Operations at the Portsmouth site result in radiation exposures of on-site workers and members of the off-site general public (Table 3.1-5). The maximum radiation dose to an off-site member of the public as a result of on-site facility operations is estimated to be 2.0 mrem/yr, which is less than 3% of the average dose of 78 mrem/yr from natural background radiation around the Portsmouth site (DOE 2002d). The DOE dose limit for the general public is 100 mrem/yr (DOE 1990). The maximum dose was estimated by using the largest environmental media concentrations monitored at different off-site locations, emission data, and conservative exposure parameters. In reality, the actual dose received by the general public would be much lower than the maximum value estimated.

Radiation exposures of the cylinder yard workers include exposures from activities performed outside the cylinder yards. The average dose in 2001 was 64 mrem/yr, obtained from monitoring data (DOE 2002d). That dose is considerably below the maximum dose limit of 5,000 mrem/yr set for radiation workers (10 CFR Part 835). The average dose in 2001 for all monitored DOE/Portsmouth employees and subcontractors was 1.85 mrem/yr.

#### **3.1.7.2 Chemical Environment**

Estimated hazard quotients for members of the general public under existing environmental conditions near the Portsmouth site are presented in Table 3.1-6. The hazard quotient represents a comparison of estimated maximum potential human intake levels with intake levels below which adverse effects are very unlikely to occur (see Appendix F for further details). The estimated hazard quotients indicate that exposures to uranium and fluoride for members of the general public near the Portsmouth site are much lower than those that might be associated with adverse health effects.

The Occupational Safety and Health Administration (OSHA) has proposed permissible exposure limits (PELs) for uranium compounds and HF in the workplace (29 CFR Part 1910, Subpart Z, as of February 2003) as follows: 0.05 mg/m<sup>3</sup> for soluble uranium compounds, 0.25 mg/m<sup>3</sup> for insoluble uranium compounds, and 2.5 mg/m<sup>3</sup> for HF. Portsmouth worker exposures are kept below those limits.

### **3.1.8 Socioeconomics**

Socioeconomic data for the Portsmouth site focus on an ROI of four counties in Ohio: Jackson, Pike, Ross, and Scioto. The counties included in the ROI were selected on the basis of the current residential locations of government workers directly connected to Portsmouth activities. It encompasses the area in which these workers spend most of their salaries. More than 90% of Portsmouth workers currently reside in these counties (Takacs 2002). In the following sections, data are presented for each of the counties in the ROI. However, because the majority of Portsmouth workers live in Scioto and Pike Counties and in the City of Portsmouth, it is expected that the majority of impacts from Portsmouth activities would occur in these locations. Therefore, more emphasis is placed on these areas.

#### **3.1.8.1 Population**

The population of the ROI in 2000 was 212,876 people (U.S. Bureau of the Census 2002a) and was projected to reach 215,700 by 2003 (Table 3.1-7). In 2000, 79,195 people (37% of the ROI total) resided in Scioto County, with 20,909 of them residing in the City of Portsmouth itself (U.S. Bureau of the Census 2002a). During the 1990s, with the exception of Scioto County, each of the counties in the ROI experienced a small increase in population, with an ROI average increase of 0.4%, while Portsmouth itself experienced a decline of -0.8%. Over the same period, the population of Ohio grew at a rate of 0.5%.

#### **3.1.8.2 Employment**

Total employment in Scioto County was 18,691 in 2000 and was projected to reach 19,200 by 2003. The economy of the county is dominated by the trade and service sectors; employment in these sectors currently contributes more than 73% of all employment in the county (see Table 3.1-8). Employment growth in the highest growth sector, services, was 5.7% during the 1990s, compared with 1.0% in the county for all sectors as a whole (U.S. Bureau of the Census 1992, 2002b).

In 2000, total employment in Pike County was 10,739, and it was expected to reach 12,400 by 2003. The economy of the county is dominated by the manufacturing and service industries; employment in these activities currently contributes more than 78% of all employment in the county (see Table 3.1-9). Employment growth in the highest growth sector (services) was 9.5% during the 1990s, compared with 4.8% in the county for all sectors as a whole (U.S. Bureau of the Census 1992, 2002b).

**TABLE 3.1-7 Population in the Portsmouth Region of Influence and Ohio in 1990, 2000, and 2003**

Location	1990	2000	Growth Rate (%), 1990-2000 <sup>a</sup>	2003 <sup>b</sup> (Projected)
City of Portsmouth	22,676	20,909	-0.8	20,400
Scioto County	80,327	79,195	-0.1	78,900
Pike County	24,249	27,695	1.3	28,800
Jackson County	30,230	32,641	0.8	33,400
Ross County	69,330	73,345	0.6	74,600
ROI total	204,136	212,876	0.4	215,700
Ohio	10,847,115	11,353,140	0.5	11,510,000

<sup>a</sup> Average annual rate.

<sup>b</sup> ANL projections, as detailed in Appendix F.

Source: U.S. Bureau of the Census (2002a), except as noted.

**TABLE 3.1-8 Employment in Scioto County by Industry in 1990 and 2000**

Sector	No. of People Employed in 1990 <sup>a</sup>	Percentage of County Total	No. of People Employed in 2000 <sup>b</sup>	Percentage of County Total	Growth Rate (%), 1990-2000
Agriculture	921 <sup>c</sup>	5.4	567 <sup>d</sup>	3.0	-4.7 <sup>e</sup>
Mining	50	0.3	10	0.1	-14.9
Construction	795	4.7	1,159	6.2	3.8
Manufacturing	2,237	13.2	2,257	12.1	0.1
Transportation and public utilities	664	3.9	316	1.7	-7.2
Trade	6,039	35.5	4,168	22.3	-3.6
Finance, insurance, and real estate	772	4.5	825	4.4	0.7
Services	5,455	32.1	9,498	50.8	5.7
Total	16,991		18,691		1.0

<sup>a</sup> U.S. Bureau of the Census (1992).

<sup>b</sup> U.S. Bureau of the Census (2002b).

<sup>c</sup> These agricultural data are from 1992 and are taken from U.S. Department of Agriculture (USDA) (1994).

<sup>d</sup> These agricultural data are from 1999 and are taken from USDA (1999).

<sup>e</sup> Agricultural data are for 1992 and 1997.

**TABLE 3.1-9 Employment in Pike County by Industry in 1990 and 2000**

Sector	No. of People Employed in 1990 <sup>a</sup>	Percentage of County Total	No. of People Employed in 2000 <sup>b</sup>	Percentage of County Total	Growth Rate (%), 1990–2000
Agriculture	206 <sup>c</sup>	3.1	167 <sup>d</sup>	1.6	-2.1 <sup>e</sup>
Mining	60	0.9	76	0.7	2.4
Construction	183	2.7	342	3.2	6.5
Manufacturing	3,601	53.4	5,874	54.7	5.0
Transportation and public utilities	182	2.7	164	1.5	-1.0
Trade	1,269	18.8	1,361	12.7	0.7
Finance, insurance, and real estate	187	2.8	265	2.5	3.6
Services	1,018	15.1	2,517	23.4	9.5
Total	6,738		10,739		4.8

<sup>a</sup> U.S. Bureau of the Census (1992).

<sup>b</sup> U.S. Bureau of the Census (2002b).

<sup>c</sup> These agricultural data are from 1992 and are taken from USDA (1994).

<sup>d</sup> These agricultural data are from 1999 and are taken from USDA (1999).

<sup>e</sup> Agricultural data are for 1992 and 1997.

In 2000, total employment in the ROI was 63,044, and it was projected to reach 67,900 by 2003. The economy of the ROI is dominated by the manufacturing and service industries; employment in these activities currently contributes more than 66% of all employment in the ROI (see Table 3.1-10). Employment growth in the highest growth sector (services) was almost 6.6% during the 1990s, compared with 2.5% in the ROI for all sectors as a whole (U.S. Bureau of the Census 1992, 2002b). Employment at the Portsmouth site currently stands at 1,727 (Takacs 2002).

Unemployment in the ROI has remained persistently high despite falling rates during the 1990s. In Scioto County, the rate steadily declined during the 1990s from a peak rate of 11.5% in 1992 to the December 2002 rate of 7.3% (Table 3.1-11) (Bureau of Labor Statistics [BLS] 2002). In Pike County, rates also fell, from a peak of 11.7% in 1992 to the current rate of 8.9%. The December 2002 unemployment in the ROI was 7.2% compared with 5.0% for the state.

### 3.1.8.3 Personal Income

Personal income in Scioto County was about \$1.6 billion in 2000 (in 2002 dollars), and it was projected to reach almost \$1.9 billion by 2003, with an annual average rate of growth of 1.5% over the period 1990 through 2000 (Table 3.1-12). County per capita income also rose in the 1990s, and it was projected to reach \$23,600 in 2003, compared with \$17,631 at the beginning of the period.

**TABLE 3.1-10 Employment in the Portsmouth Region of Influence by Industry in 1990 and 2000**

Sector	No. of People Employed in 1990 <sup>a</sup>	Percentage of ROI Total	No. of People Employed in 2000 <sup>b</sup>	Percentage of ROI Total	Growth Rate (%), 1990-2000
Agriculture	2,568 <sup>c</sup>	5.2	2,121 <sup>d</sup>	3.4	-1.9 <sup>e</sup>
Mining	274	0.6	299	0.5	0.9
Construction	1,922	3.9	2,671	4.2	3.4
Manufacturing	12,955	26.3	16,515	26.2	2.5
Transportation and public utilities	1,818	3.7	1,293	2.1	-3.6
Trade	14,388	29.2	11,689	18.5	-2.1
Finance, insurance, and real estate	1,813	3.7	3,308	5.2	6.2
Services	13,388	27.2	25,334	40.2	6.6
Total	49,254		63,044		2.5

<sup>a</sup> U.S. Bureau of the Census (1992).

<sup>b</sup> U.S. Bureau of the Census (2002b).

<sup>c</sup> These agricultural data are from 1992 and are taken from USDA (1994).

<sup>d</sup> These agricultural data are from 1999 and are taken from USDA (1999).

<sup>e</sup> Agricultural data are for 1992 and 1997.

In Pike County, personal income totaled almost \$0.6 billion in 2000 (in 2002 dollars), and it was projected to reach almost \$0.7 billion in 2003, with an annual average rate of growth of 3.4% over the period 1990 through 2000 (Table 3.1-12). County per capita income also rose in the 1990s, and it was projected to reach \$23,700 in 2003, compared with \$16,944 at the beginning of the period.

Growth rates in total personal income were higher in the ROI as a whole than for Scioto County, but lower than those for Pike County. Total personal income grew at a rate of 2.2% in the ROI over the period 1990 through 2000, and it was projected to reach \$5.3 billion by 2003. ROI per capita income was projected to grow from \$18,109 in 1990 to \$24,500 in 2003, an average annual growth rate of 1.8%.

**TABLE 3.1-11 Unemployment Rates in Scioto and Pike Counties, the Portsmouth Region of Influence, and Ohio**

Location and Period	Rate (%)
<b>Scioto County</b>	
1992–2002 average	9.4
Dec. 2002 (current rate)	7.3
<b>Pike County</b>	
1992–2002 average	9.5
Dec. 2002 (current rate)	8.9
<b>ROI</b>	
1992–2002 average	8.0
Dec. 2002 (current rate)	7.2
<b>Ohio</b>	
1992–2002 average	5.1
Dec. 2002 (current rate)	5.0

Source: BLS (2002).

**TABLE 3.1-12 Personal Income in Scioto and Pike Counties and the Portsmouth Region of Influence in 1990, 2000, and 2003**

Location and Type of Income	1990	2000	Growth Rate (%), 1990–2000	2003 (Projected) <sup>a</sup>
<b>Scioto County</b>				
Total personal income (millions of 2002 \$)	1,416	1,624	1.5	1,900
Personal per capita income (2002 \$)	17,631	20,501	1.7	23,600
<b>Pike County</b>				
Total personal income (millions of 2002 \$)	411	556	3.4	690
Personal per capita income (2002 \$)	16,944	20,061	1.9	23,700
<b>Total ROI</b>				
Total personal income (millions of 2002 \$)	3,697	4,509	2.2	5,300
Personal per capita income (2002 \$)	18,109	21,180	1.8	24,500

<sup>a</sup> ANL projections, as detailed in Appendix F.

Source: U.S. Department of Commerce (2002).

### 3.1.8.4 Housing

Housing stock in Scioto County grew at an annual rate of 0.5% over the period 1990 through 2000 (Table 3.1-13) (U.S. Bureau of the Census 2002a), with total housing units projected to remain at 34,600 by 2003, reflecting the declining growth in county population. Housing in the City of Portsmouth declined during this period by -0.5%, with total housing units expected to fall to 10,100 in 2003. About 1,600 new units were added to the existing housing stock in the county during the 1990s, but there were 500 fewer units in the City of Portsmouth in 2000. Vacancy rates in 2000 stood at 11.0% in the city and 9.3% in the county as a whole for all types of housing. On the basis of annual population growth rates, 3,400 vacant housing units were expected in the county in 2003, of which about 1,000 were expected to be rental units available to incoming construction workers at the proposed facility.

Housing stock in Pike County grew at an annual rate of 1.8% over the period 1990 through 2000 (Table 3.1-13) (U.S. Bureau of the Census 2002b), with total housing units expected to reach 12,200 in 2003, reflecting moderate growth in county population. Almost 1,900 new units were added to the existing housing stock in the county during the 1990s. Vacancy rates in 2000 stood at 10% in the county as a whole for all types of housing. On the basis of annual population growth rates, 1,200 vacant housing units were projected in the county in 2003. About 360 of these were expected to be rental units available to incoming construction workers.

In the ROI as a whole, housing grew at a faster rate than in Scioto County or the City of Portsmouth during the 1990s, with an overall growth rate of 1.0%. Total housing units were expected to reach 91,700 by 2003, with more than 8,300 housing units added in the 1990s. On the basis of vacancy rates in 2000, which stood at 8.9%, more than 2,300 rental units were expected to be available to incoming construction workers.

**TABLE 3.1-13 Housing Characteristics in the City of Portsmouth, Scioto and Pike Counties, and the Region of Influence in 1990 and 2000**

Location and Type of Unit	No. of Units	
	1990	2000
<b><i>City of Portsmouth</i></b>		
Owner-occupied	5,478	4,853
Rental	4,189	4,267
Total unoccupied	1,091	1,128
Total	10,758	10,248
<b><i>Scioto County</i></b>		
Owner-occupied	20,774	21,646
Rental	9,012	9,225
Total unoccupied	2,622	3,183
Total	32,408	34,054
<b><i>Pike County</i></b>		
Owner-occupied	6,113	7,314
Rental	2,692	3,130
Total unoccupied	917	1,158
Total	9,722	11,602
<b><i>ROI Total</i></b>		
Owner-occupied	52,302	58,246
Rental	21,874	22,824
Total unoccupied	6,579	7,956
Total	80,755	89,026

Source: U.S. Bureau of the Census (2002a).

### 3.1.8.5 Community Resources

**3.1.8.5.1 Community Fiscal Conditions.** Revenues and expenditures for local government jurisdictions, including counties, cities, and school districts, constitute community fiscal conditions. Revenues would come primarily from state and local sales tax revenues associated with employee spending during construction and operation and would be used to support additional local community services currently provided by each jurisdiction. Tables 1 and 2 in Allison (2002) present information on revenues and expenditures by the various local government jurisdictions in the ROI.

**3.1.8.5.2 Community Public Services.** Construction and operation of the proposed facility would increase demand for community services in the counties, cities, and school districts likely to host relocating construction workers and operations employees. Additional demands would also be placed on local medical facilities and physician services. Tables 3.1-14 and 3.1-15 present data on employment and levels of service (number of employees per 1,000 population) for public safety, general local government services, and physicians. Tables 3.1.8-16 and 3.1.8-17 provide staffing data for school districts and hospitals.

### 3.1.9 Waste Management

The Portsmouth site generates several categories of waste, including wastewater; solid LLW; solid and liquid mixed hazardous and radiological waste; nonradioactive hazardous waste;

**TABLE 3.1-14 Public Service Employment in the City of Portsmouth, Scioto and Pike Counties, and Ohio in 2002**

Employment Category	City of Portsmouth		Scioto County		Pike County		Ohio <sup>b</sup>
	No. of Workers	Level of Service <sup>a</sup>	No. of Workers	Level of Service <sup>a</sup>	No. of Workers	Level of Service <sup>a</sup>	Level of Service <sup>a</sup>
Police	44	2.1	90	1.5	10	0.4	2.3
Fire <sup>c</sup>	44	2.1	0	0	0	0	1.4
General	212	10.1	730	12.5	294	12.6	34.6
Total	300	14.3	820	14.1	304	13.1	52.4

<sup>a</sup> Level of service represents the number of employees per 1,000 persons in each jurisdiction (U.S. Bureau of the Census 2002a).

<sup>b</sup> 2000 data.

<sup>c</sup> Does not include volunteers.

Sources: City of Portsmouth: Doyle (2002); Scioto County: Massey (2002); Pike County: Jones (2002); Ohio: U.S. Bureau of the Census (2002c).

**TABLE 3.1-15 Number of Physicians in Scioto and Pike Counties and Ohio in 1997**

Employment Category	Scioto County		Pike County		Ohio
	Number	Level of Service <sup>a</sup>	Number	Level of Service <sup>a</sup>	Level of Service <sup>a</sup>
Physicians	106	1.3	25	0.9	2.4

<sup>a</sup> Level of service represents the number of physicians per 1,000 persons in each jurisdiction.

Source: American Medical Association (1999).

**TABLE 3.1-16 School District Data for Scioto and Pike Counties and Ohio in 2001**

Employment Category	Scioto County		Pike County		Ohio
	No.	Student-to-Teacher Ratio <sup>a</sup>	No.	Student-to-Teacher Ratio <sup>a</sup>	Student-to-Teacher Ratio <sup>a</sup>
Teachers	732	17.9	287	19.0	10.8

<sup>a</sup> The number of students per teacher in each school district.

Source: Ohio Department of Education (2002).

**TABLE 3.1-17 Medical Facility Data for Scioto and Pike Counties in 1998**

Hospital	No. of Staffed Beds	Occupancy Rate (%) <sup>a</sup>
<b>Scioto County</b>		
Southern Ohio Medical Center	281	56
<b>Pike County</b>		
Pike Community Hospital	40	NA <sup>b</sup>

<sup>a</sup> Percentage of staffed beds occupied.

<sup>b</sup> NA = not available.

Source: Healthcare InfoSource, Inc. (1998).

and nonradioactive, nonhazardous solid waste. Disposal of waste generated from ongoing management of the DOE-generated DUF<sub>6</sub> cylinders currently in storage is managed by DOE. USEC is responsible for wastes generated from ongoing operations that are leased from DOE, except for “legacy wastes,” which contain constituents such as asbestos and PCBs. The cylinder storage yards at Portsmouth currently generate only a very small amount of waste compared with the volume of waste generated from ongoing plant operations. Cylinder yard waste consists of small amounts of metal, scrapings from cylinder maintenance operations, potentially contaminated soil, and miscellaneous items.

The site has an active program to minimize the generation of solid LLW, hazardous waste, and LLMW. Radioactive waste minimization efforts include segregating radioactive waste from nonradioactive waste; reducing radiologically controlled areas, thereby reducing the volume of personal protective equipment; and improving the segregation and handling of laboratory waste. Hazardous and mixed waste minimization actions include sorting burnable waste from radioactively contaminated materials, reducing the use of absorbent cloths to clean up PCB spills, reducing floor sweeping waste, and substituting materials containing nonhazardous components. Solid waste minimization actions include recycling corrugated cardboard, office paper, fluorescent light bulbs, batteries, and aluminum.

Table 3.1-18 lists the Portsmouth site waste loads assumed for the analysis of impacts of projected activities.

**TABLE 3.1-18 Projected Waste Generation Volumes for the Portsmouth Site<sup>a</sup>**

**3.1.9.1 Wastewater**

Wastewater at Portsmouth consists of nonradioactive sanitary and process-related wastewater streams, cooling water blowdown, radioactive process-related liquid effluent, discharges from groundwater treatment systems, and storm water runoff from plant areas, including runoff from the coal pile. Wastewater is processed at several on-site treatment facilities and then discharged to either the Scioto River or its immediate tributaries, including Little Beaver Creek, through several permitted outfalls. Treatment facilities include an activated sludge sewage treatment plant; several facilities that employ waste-specific pretreatment technologies (e.g., pH adjustment, activated carbon adsorption, metals removal, denitrification, and ion absorption); and numerous settling basins designed to facilitate solids settling, oil collection, and chlorine dissipation. The site wastewater facilities have a capacity of approximately 5.3 million gal/d (20 million L/d) (DOE 1996a).

Waste Category	Waste Treatment Volume (m <sup>3</sup> /yr)
LLW	73,000
LLMW	5,600
TRU	0
Hazardous waste	110
Nonhazardous waste <sup>b</sup>	
Solids	3,200
Wastewater	145,000

<sup>a</sup> Volumes include operational and environmental restoration wastes projected from FY 2002 to FY 2025.

<sup>b</sup> Volumes include sanitary and industrial wastes.

Source: Cain (2002c).

### **3.1.9.2 Solid Nonhazardous, Nonradioactive Waste**

Solid waste — including sanitary refuse, cafeteria waste, industrial waste, disinfected medical waste (excluding drugs), and construction and demolition waste — is collected and disposed of off site at a state-permitted sanitary landfill. Disposal is in shallow trenches covered with earthen fill.

### **3.1.9.3 Nonradioactive Hazardous and Toxic Waste**

Nonradioactive waste that is considered hazardous waste according to RCRA, or that contains PCBs defined under the Toxic Substances Control Act (TSCA), requires special handling, storage, and disposal. The Portsmouth site generates waste, including spent solvents, heavy-metal-contaminated waste, and PCB-contaminated toxic waste. Portsmouth provides long-term on-site storage for hazardous waste at the X-7725 and X-326 RCRA storage areas. Several additional 90-day satellite storage areas are available for temporary storage of hazardous waste. Hazardous waste is sent to permitted off-site contractors for final treatment and/or disposal.

### **3.1.9.4 Low-Level Radioactive Waste**

LLW generated at the Portsmouth site is stored on site pending shipment to off-site treatment/disposal facilities. Solid LLW generated at the site includes refuse, sludge, and debris contaminated with radionuclides, primarily uranium and Tc-99.

### **3.1.9.5 Low-Level Radioactive Mixed Waste**

LLW that contains PCBs or RCRA hazardous components is considered to be LLMW. All of the LLMW inventory at Portsmouth is subject to RCRA land disposal restrictions. LLMW is currently stored on site pending shipment to off-site disposal facilities.

## **3.1.10 Land Use**

The Portsmouth site is located in south-central Ohio, in the southern portion of rural Pike County about 22 mi (35 km) north of the Ohio River and about 1 mi (1.6 km) east of the Scioto River. On the basis of an analysis of Landsat satellite imagery from 1992, dominant land cover categories in Pike County include deciduous forest (64.6%), pasture/hay (21.6%), and row crops (10.3%) (Figure 3.1-6). The 1997 agricultural census recorded 435 farms in Pike County in 1997, covering more than 78,300 acres (31,687 ha) (USDA 1999). Human settlement is sparse throughout most of Pike County; the largest communities (Piketon and Waverly) are located near the Scioto River north of the Portsmouth site. Apart from the two communities just mentioned and the villages of Jasper northwest of the site and Wakefield south of the site, the portion of Pike County containing the Portsmouth site is dominated by forest, pasture, and row crops.

The Portsmouth site covers 3,714 acres (1,500 ha); the uranium enrichment facilities are located on an 800-acre (320-ha) fenced core area within the larger site. The site is heavily developed and includes about 150 buildings, trailers, and sheds. The areas between structures consist primarily of mowed grassy areas and pasture, while the area immediately surrounding the Portsmouth site generally features a combination of deciduous forest and pasture.

### 3.1.11 Cultural Resources

Southern Ohio contains evidence from most of the major prehistoric periods for Eastern North America. The earliest period, Paleoindian, is very poorly represented in southern Ohio; however, numerous sites dating to the Archaic Period (9,000 B.C.–900 B.C.) have been found in close proximity to Portsmouth. The Woodland Period (900 B.C.–A.D. 900) is also well-represented, as evidenced by the mound complexes that appear in southern Ohio. The final prehistoric period represented in southern Ohio is the Fort Ancient culture (A.D. 900–A.D. 1600). During the early historic period, the Shawnee inhabited southern Ohio, including the Scioto Valley where Portsmouth is located. No federally recognized tribe has land claims in Pike County; however, the county is in the traditional range of the Shawnee Indians. Consultations with the Shawnee and the Ohio State Historic Preservation Officer (SHPO) have been initiated (see Appendix E for consultation letters). However, no religious or sacred sites, burial sites, or resources significant to Native Americans have been identified at the Portsmouth site to date.

The first permanent non-native settlement in the region was in 1801. The economy was almost entirely based on agriculture. The populations in the Portsmouth region grew slowly. The primary impetus for growth in the Scioto Valley was the expansion of transportation routes. During the 19th and early 20th centuries, several canals, roads, and, finally, railroads were constructed in the Scioto Valley region.

In 1951, the Scioto Valley was chosen by the AEC as the location for the third gaseous uranium diffusion facility within the nation's Cold War nuclear complex, to complement the facilities at Oak Ridge, Tennessee, and Paducah, Kentucky. Construction of the Portsmouth GDP began in 1952. The plant first became operational in 1954 and was completed in 1956. The facility provided enriched uranium-235 to fuel power reactors and nuclear-powered submarines and ships. The Portsmouth facility scaled back production for many years, suspending the production of highly enriched uranium in 1991, after the end of the Cold War.

Portsmouth and its surrounding area have the potential to yield both prehistoric and historic cultural resources. Archaeological and architectural surveys were undertaken at Portsmouth in 1996; however, neither report has been finalized. Discussions between Portsmouth and the Ohio SHPO are ongoing. The proposed construction sites at Portsmouth have been previously disturbed, and preservation of archaeological sites is unlikely. Cold War era structures do exist at Locations A and B, but their significance has yet to be determined.

### **3.1.12 Environmental Justice**

#### **3.1.12.1 Minority Populations**

This EIS uses data from the most recent decennial census in 2000 to evaluate environmental justice implications of the proposed action and all alternatives with respect to minority populations. The CEQ guidelines on environmental justice recommend that “minority” be defined as members of American Indian or Alaska Native, Asian or Pacific Islander, Black non-Hispanic, and Hispanic populations (CEQ 1997). The earliest release of 2000 census data that included information necessary to identify minority populations identified individuals both according to race and Hispanic origin (U.S. Bureau of the Census 2001). It also identified individuals claiming multiple racial identities (up to six races). To remain consistent with the CEQ guidelines, the phrase “minority population” in this document refers to persons who identified themselves as partially or totally Black (including Black or Negro, African American, Afro-American, Black Puerto Rican, Jamaican, Nigerian, West Indian, or Haitian), American Indian or Alaska Native, Asian, Native Hawaiian or other Pacific Islander, or “Other Race.” The minority category also includes White individuals of Hispanic origin, although the latter is technically an ethnic category. To avoid double counting, tabulations included only White Hispanics; the above racial groups already account for non-White Hispanics. In sum, then, the minority population considered under environmental justice consisted of all non-White persons (including those of multiple racial affiliations) plus White persons of Hispanic origin.

To identify census tracts with disproportionately high minority populations, this EIS uses the percentage of minorities in each state containing a given tract as a reference point. Using the individual states to identify disproportionality acknowledges that minority distributions in the state can differ from those found in the nation as a whole. In 2000, of the 206 census tracts within 50 mi (80 km) of the proposed conversion facility at Portsmouth, 12 had minority populations in excess of state-specified thresholds — a total of 7,735 minority persons in all (Figure 3.1-7). In Pike County, 3.7% of the 2000 population was minority (U.S. Bureau of the Census 2002d).

#### **3.1.12.2 Low-Income Populations**

As recommended by the CEQ guidelines, the environmental justice analysis identifies low-income populations as those falling below the statistical poverty level identified annually by the U.S. Bureau of the Census in its Series P-60 reports on income and poverty. The Census Bureau defines poverty levels on the basis of a statistical threshold that considers for each family both overall family size and the number of related children younger than 18 years old. For example, in 1999, the poverty threshold annual income for a family of three with one related child younger than 18 was \$13,410, while the poverty threshold for a family of five with one related child younger than 18 was \$21,024 (see U.S. Bureau of the Census 2000). The 2000 census used 1999 thresholds because 1999 was the most recent year for which annual income data were available when the census was conducted. If a family fell below the poverty line for its

particular composition, the census considered all individuals in that family to be below the poverty line.

To identify census tracts with disproportionately high low-income populations, this EIS uses the percentage of low-income persons in each state containing a given tract as a reference point. In 1999, of the 206 census tracts within 50 mi (80 km) of the proposed conversion facility at Portsmouth, 142 had low-income populations in excess of state-specified thresholds — a total of 133,303 low-income persons in all (Figure 3.1-8). In Pike County, 18.6% of the individuals for whom poverty status was known in 1999 were low-income (U.S. Bureau of the Census 2002d).

### 3.2 EAST TENNESSEE TECHNOLOGY PARK

ETTP is located in eastern Roane County about 25 mi (40 km) west of Knoxville, Tennessee (Figure 3.2-1). ETTP is part of the ORR in the City of Oak Ridge, Tennessee. The site was established in 1940 with initiation of construction of the Oak Ridge Gaseous Diffusion Plant. Uranium enrichment was the site’s mission until the mid-1980s, when gaseous diffusion operations ceased. In 1990, the site was renamed as the K-25 Site, and it was renamed again in 1997 as the ETTP. Previous missions were waste management and restoration; the current mission is to “reindustrialize and reuse site assets through leasing of vacated facilities and incorporation of commercial industrial organizations as partners in the ongoing environmental restoration, D&D, waste treatment and disposal, and diffusion technology development activities” (DOE 2001f).

#### 3.2.1 Cylinder Yards

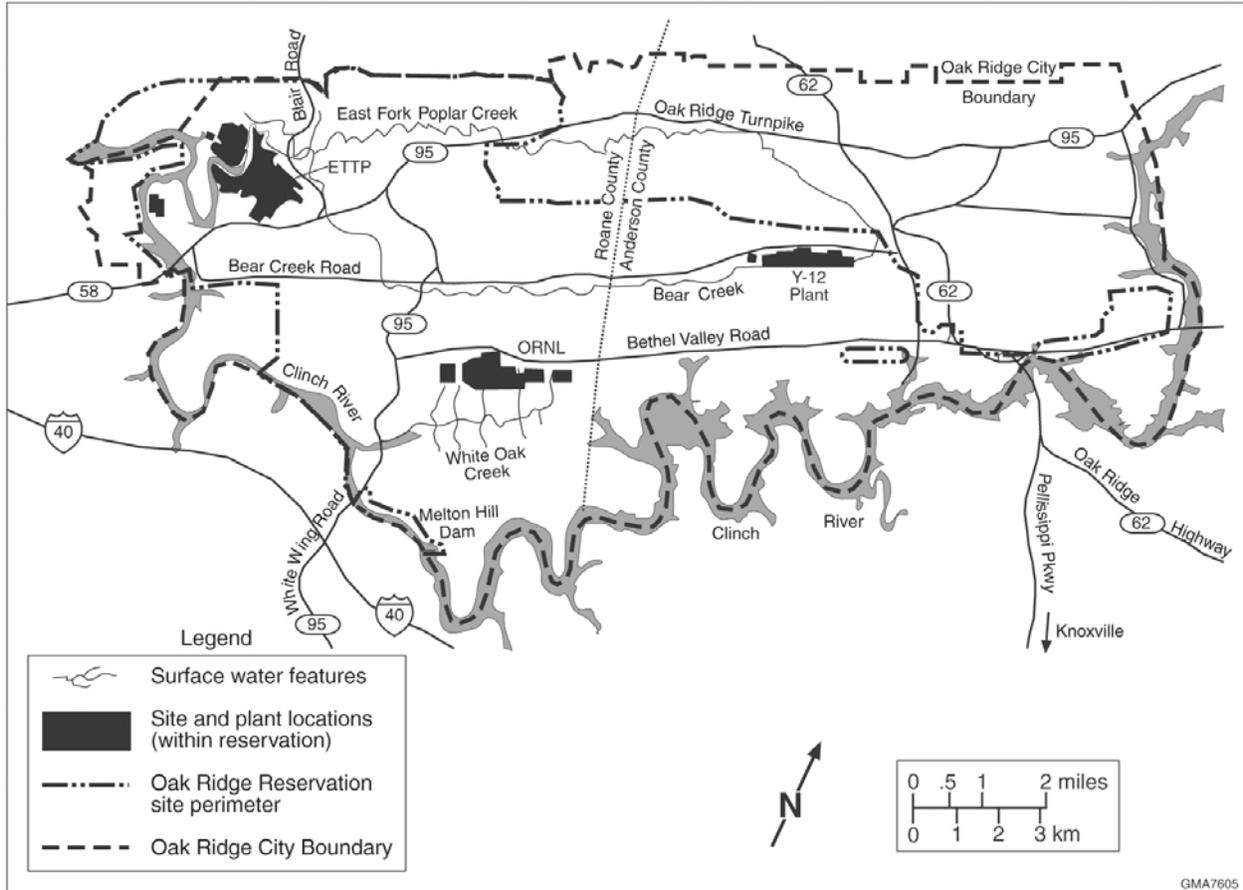
There are 4,822 DUF<sub>6</sub> storage cylinders located in ETTP site cylinder yards (Table 3.2-1; Figure 3.2-2). Cylinders are stacked two high to conserve space. About 30% of the cylinders are stored in yard K-1066-E (constructed with a concrete base), and 30% are stored in yard K-1066-K (constructed with a gravel base). The other cylinders are stored in four smaller yards.

In storage at ETTP, in addition to the cylinders that contain DUF<sub>6</sub>, are a number of cylinders in various sizes that contain enriched UF<sub>6</sub> or normal UF<sub>6</sub> or are empty. The non-DUF<sub>6</sub> cylinders total 1,102 and contain a total of about 26 t (29 tons) of UF<sub>6</sub> (7 t [8 tons] of enriched UF<sub>6</sub> plus 19 t [21 tons] of normal UF<sub>6</sub>) (Hightower 2004). About 20 cylinders are empty. Of the 881 non-DUF<sub>6</sub> cylinders that contain enriched uranium, fewer than 30 contain uranium enriched to greater than 5% uranium-235, and all of these are small, sample cylinders containing less than 3 lb (1.4 kg) of UF<sub>6</sub> each.

**TABLE 3.2-1 DOE-Managed DUF<sub>6</sub> Cylinders at the ETTP Site**

Cylinder Type	No. of Cylinders
Full	4,719
Partially full	83
Heel	20
Total	4,822

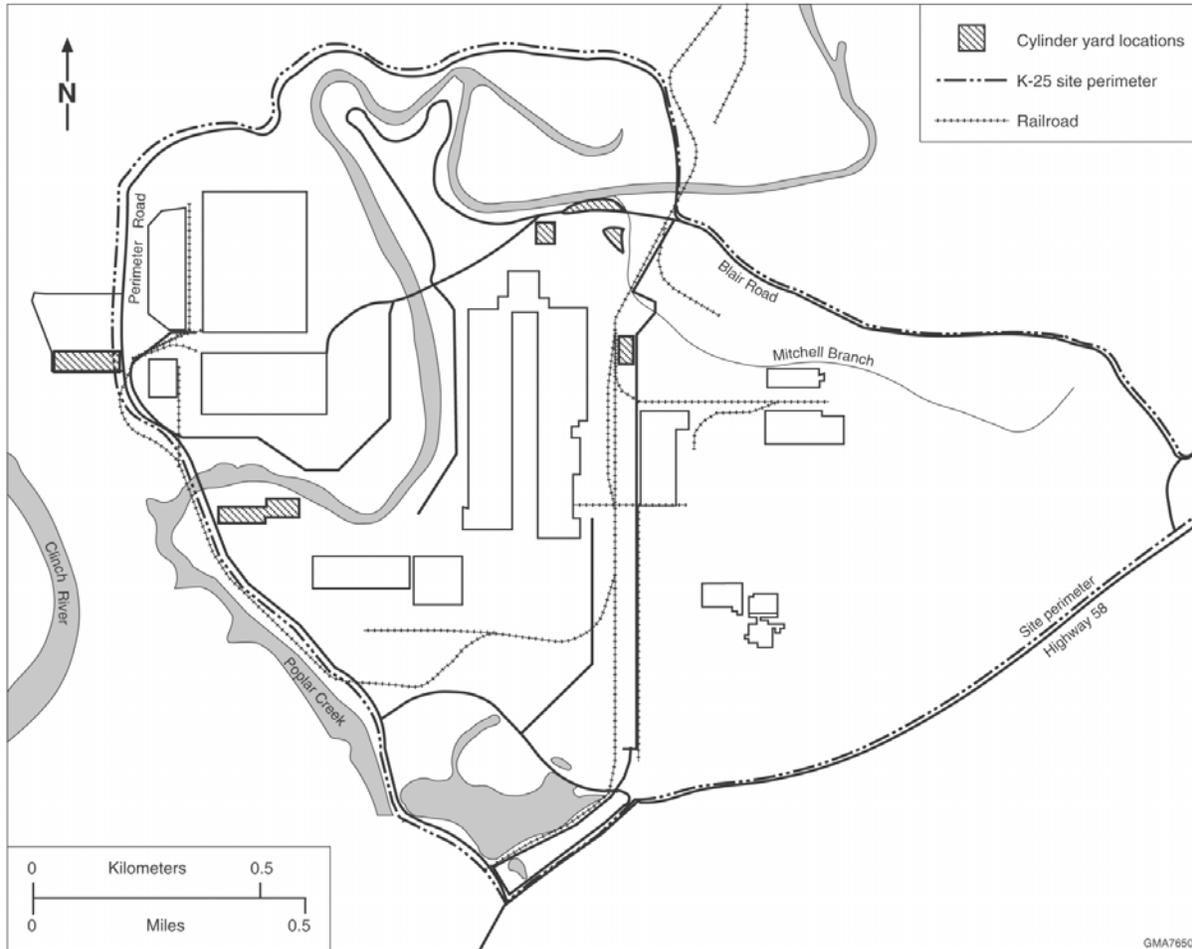
Source: Hightower (2004).



**FIGURE 3.2-1 Regional Map of the ETTP Vicinity**

Over 98% of the enriched UF<sub>6</sub> in cylinders at ETTP contains less than 5% uranium-235. It is assumed that the natural and enriched UF<sub>6</sub> would be put to beneficial uses; therefore, conversion of the contents of the non-DUF<sub>6</sub> cylinders is not considered in this EIS. This EIS does, however, include these cylinders in its evaluation of an alternative that considers the transportation of cylinders from ETTP to Portsmouth for conversion.

It is expected that many of the full DUF<sub>6</sub> cylinders at the ETTP site would not meet DOT transportation requirements because of damage and corrosion from poor historical storage conditions. It was estimated in the PEIS that a range of one-half to all of the full DUF<sub>6</sub> cylinders would not meet DOT transportation requirements (DOE 1999a). More recent estimates indicate that 1,700 cylinders are DOT compliant, with the remainder not meeting DOT requirements (see Section 1.7). No similar estimate of the condition of the non-DUF<sub>6</sub> cylinders at ETTP is available.



**FIGURE 3.2-2 Locations of Storage Yards at ETTP That Are Used to Store DOE-Managed Cylinders**

### 3.2.2 Site Infrastructure

The ETTP site is located in an area with a well-established transportation network. The site is near two interstate highways, several U.S. and state highways, two major rail lines, and a regional airport (Figure 3.2-1).

The ETTP water supply is pumped from Clinch River. The water is treated and stored in two storage tanks. This system, with a capacity of 4 million gal/d (15 million L/d), provides water to the Transportation Safeguards Facility and the ETTP site.

Electric power is supplied by the Tennessee Valley Authority (TVA). The distribution of power is managed through the ETTP Power Operations Department. The average demand for electricity by all of the DOE facilities at Oak Ridge, including the ETTP site, is approximately 100 MVA. The maximum capacity of the system is 920 MVA (DOE 1995). Natural gas is supplied by the East Tennessee Natural Gas Company; the daily capacity of 7,600 decatherms

can be increased, if necessary. The average daily usage in 1994 was 3,600 decatherms (DOE 1995).

### **3.2.3 Climate, Air Quality, and Noise**

#### **3.2.3.1 Climate**

The climate of the region, including the ETTP site, may be broadly classified as humid continental. The region is located in a broad valley between the Cumberland Mountains to the northwest and the Great Smoky Mountains to the southeast, which influence meteorological patterns over the region (Wood 1996). During the summer, tropical air masses from the south provide warm and humid conditions that often produce thunderstorms. In winter, the Cumberland Mountains have a moderating influence on local climate by shielding the region from cold air masses from the north and west.

For the 1961 through 1990 period, the annual average temperature was 13.7°C (56.6°F), with the highest monthly average temperature of 24.3°C (75.8°F) occurring in July and the lowest of 1.7°C (35.0°F) occurring in January (Wood 1996). Annual precipitation averages about 137 cm (53.8 in.), including about 25 cm (9.8 in.) of snowfall. Precipitation is evenly distributed throughout the season, with the highest occurring in spring.

Winds in the region are controlled in large part by the valley-and-ridge topography. Prevailing wind directions are from the northeast and southwest, reflecting the channeling of winds parallel to the ridges and valleys in the area. The average wind speed at Oak Ridge is about 2.0 m/s (4.4 mph); the dominant wind direction is from the southwest (Wood 1996). For 2001, the average wind speed at the 10-m (33-ft) level of the ETTP K1209 meteorological tower was 1.5 m/s (3.4 mph), as shown in Figure 3.2-3 (ORNL 2002). The dominant wind direction at the tower was southwest, with secondary peaks from the south-southwest and the east. These lower wind speeds at the ETTP tower and in the region reflect the air stagnation relatively common in eastern Tennessee.

Tornadoes rarely occur in the valley surrounding the ETTP site between the Cumberlands and the Great Smokies, and they historically have been less destructive than those in the Midwest. For the period 1950 through 1995, 541 tornadoes were reported in Tennessee, with an average of 12 tornadoes per year (Storm Prediction Center 2002). For the same period, 3 tornadoes were reported in Anderson and Roane Counties each, but these tornadoes were relatively weak, being F3 of the Fujita tornado scale, at most.

#### **3.2.3.2 Existing Air Emissions**

At the end of calendar year 2001, there were 88 active air emission sources under DOE control at ETTP (DOE 2002e). Of these 88 sources, ETTP operated 30; these were covered

under eight major air emission sources subject to rules in the Tennessee Title V Major Source Operating Permit Program under an application shield granted by the TDEC Division of Air Pollution Control. All remaining active air emission sources are exempt from permitting requirements.

Major sources for criteria pollutants and VOCs in Anderson and Roane Counties in Tennessee include TVA steam plants and DOE operations, including the Y-12, ORNL, and ETTP sites. Annual emissions from major sources and total county emissions are presented in Table 3.2-2. The SO<sub>2</sub> and NO<sub>x</sub> emissions from ETTP operations are negligible compared with those from the two TVA steam plants in Anderson and Roane Counties. However, VOC emissions account for about 39% of the Roane County emission total, and PM (PM<sub>10</sub> and PM<sub>2.5</sub>) emissions account for about 8% of the Roane County emission total. The amount of actual emissions from the ETTP site is much less than the amount of allowable emissions presented in Table 3.2-2 (DOE 2002e).

The State of Tennessee and the EPA regulate airborne emissions of radionuclides from DOE facilities under 40 CFR 61, Subpart H, NESHAPs regulations (DOE 2002e). The three ETTP major sources that operated during 2000 were the TSCA incinerator and two stacks in the K-33 building operated by British Nuclear Fuels, Ltd. Emissions from these exhaust stacks are controlled by a particulate filtration system, and continuous sampling for radionuclides emissions is conducted at these stacks to assess the dose to the public.

**TABLE 3.2-2 Annual Criteria Pollutant and Volatile Organic Compound Emissions from Selected Major Point Sources around the ETTP Site in 1999**

Major Emission Source	Emission Rate (tons/yr)					
	SO <sub>2</sub>	NO <sub>x</sub>	CO	VOC	PM <sub>10</sub>	PM <sub>2.5</sub>
TVA Bull Run Steam Plant, Clinton	38,179	13,528	420	50	529	267
Y-12 Plant (DOE)	13,375	1,672	38	19	61	21
Anderson County, Tenn., total	51,555	15,237	460	405	731	365
TVA Kingston Steam Plant, Kingston	109,194	26,055	995	122	95	98
ORNL (DOE)	361	25	53	14	363	267
ETTP (formerly K-25) (DOE)	222	60	29	86	41	34
	(0.20%, 0.14%) <sup>a</sup>	(0.23%, 0.14%)	(2.5%, 1.8%)	(39%, 14%)	(8.2%, 3.2%)	(8.5%, 4.5%)
Roane County, Tenn., total	109,777	26,149	1,157	222	498	399

<sup>a</sup> First and second values in parentheses are ETTP emissions as percentages of Roane County emissions total and combined Anderson and Roane Counties emissions total, respectively.

Source: EPA (2003b).

### 3.2.3.3 Air Quality

The Tennessee SAAQS for six criteria pollutants — SO<sub>2</sub>, NO<sub>2</sub>, CO, O<sub>3</sub>, PM (PM<sub>10</sub> and PM<sub>2.5</sub>), and Pb — are almost the same as the NAAQS (Waynick 2002), as shown in Table 3.2-3. In addition, the state has adopted standards for gaseous fluorides (expressed as HF), as presented in Table 3.2-4.

The ETTP site in Roane County is located in the Eastern Tennessee-Southwestern Virginia Interstate AQCR. Currently, the county is designated as being in attainment for all criteria pollutants (40 CFR 81.343).

Although uranium enrichment activities at ETTP were discontinued in 1985, ambient air monitoring for radionuclides, criteria pollutants (PM<sub>10</sub> and Pb),<sup>3</sup> and several metals has continued at on-site and off-site locations (DOE 2002e). Monitoring indicates that no standards were exceeded, and there was no statistically significant elevation of pollutant concentrations associated with site operations. On the basis of modeling radionuclide emissions from all major and minor point sources, the effective dose equivalent to the most exposed member of the public was 0.8 mrem/yr in 2001, well below the NESHAPs dose limit of 10 mrem/yr (DOE 2002e). Also, the airborne dose from all ETTP radionuclide emissions was still less than the ORR maximum. The highest concentration levels for SO<sub>2</sub>, NO<sub>2</sub>, CO, PM<sub>10</sub>, 24-hour PM<sub>2.5</sub>, and Pb around and within the ETTP site are less than or equal to 78% of their respective NAAQS in Table 3.2-3 (EPA 2003b; DOE 2002e). However, the highest O<sub>3</sub> and annual PM<sub>2.5</sub> concentrations that are of regional concern are approaching or somewhat higher than the applicable NAAQS.

PSD regulations (40 CFR 52.21) limit the maximum allowable incremental increases in ambient concentrations of SO<sub>2</sub>, NO<sub>2</sub>, and PM<sub>10</sub> above established baseline levels, as shown in Table 3.2-3. The PSD regulations, which are designed to protect ambient air quality in Class I and Class II attainment areas, apply to major new sources and major modifications to existing sources. The nearest Class I PSD is the Great Smoky Mountains National Park, about 55 km (34 mi) southeast of ETTP. The Joyce Kilmer-Slickrock Wilderness Area just south of the western end of Great Smoky Mountains National Park is also a Class I area. These Class I areas are not located downwind of prevailing winds at ETTP (see Figure 3.2-3).

### 3.2.3.4 Existing Noise Environment

The Noise Control Act of 1972, along with its subsequent amendments (Quiet Communities Act of 1978, 42 USC Parts 4901–4918), delegates to the states the authority to regulate environmental noise and directs government agencies to comply with local community noise statutes and regulations. Anderson County has quantitative noise-limit regulations, as shown in Table 3.2-5 (Anderson County 2002), although the State of Tennessee and Roane County do not.

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<sup>3</sup> At the end of 2001, all PM<sub>10</sub> sampling was discontinued after a review of PM<sub>10</sub> data over a 10-year period (1991 through 2000) in which all concentrations were below the ambient air quality standards.

**TABLE 3.2-4 Additional Tennessee Ambient Air Quality Standards<sup>a</sup>**

Pollutant	Averaging Time	Primary Standard	Secondary Standard
Gaseous fluorides (as HF)	12 hours	– <sup>b</sup>	3.7 µg/m <sup>3</sup> (4.5 ppb) <sup>c</sup>
	24 hours	–	2.9 µg/m <sup>3</sup> (3.5 ppb) <sup>c</sup>
	7 days	–	1.6 µg/m <sup>3</sup> (2.0 ppb) <sup>c</sup>
	30 days	–	1.2 µg/m <sup>3</sup> (1.5 ppb) <sup>c</sup>
Gaseous fluorides (as HF) <sup>d</sup>	30 days	–	0.5 µg/m <sup>3</sup> (0.6 ppb) <sup>c</sup>

<sup>a</sup> These standards are in addition to the Tennessee's SAAQS listed in Table 3.2-3.

<sup>b</sup> A dash indicates that no standard exists.

<sup>c</sup> This average is not to be exceeded more than once per year.

<sup>d</sup> Applied in the vicinity of primary aluminum reduction plants in operation on or before December 31, 1973.

Source: TDEC (1999).

**TABLE 3.2-5 Allowable Noise Level by Zoning District in Anderson County, Tennessee**

Zoning		Allowable Noise Level (dBA)	
District	Abbreviation	7 a.m.–10 p.m.	10 p.m.–7 a.m.
Suburban-residential	R-1	60	55
Rural-residential	A-2	65	60
Agriculture-forest	A-1	65	60
General commercial	C-1	70	65
Light industrial	I-1	70	70
Heavy industrial	I-2	80	80
Floodway	F-1	80	80

Source: Anderson County (2002).

The EPA has recommended a maximum noise level of 55 dB(A) as DNL to protect against outdoor activity interference and annoyance (EPA 1974a). This level is not a regulatory goal but is “intentionally conservative to protect the most sensitive portion of the American population” with “an additional margin of safety.” For protection against hearing loss in the general population from nonimpulsive noise, the EPA guideline recommends an  $L_{eq}(24\text{ h})$  of 70 dB(A) or less over a 40-year period.

The noise-producing activities within the ETTP site are associated with the DUF<sub>6</sub> cylinder project and local traffic similar to that at any other industrial site. Major noise sources within the ETTP site consist of heavy equipment, forklift, and crane operations associated with cylinder handling, steel grit blasting operations, welding/burning/hotwork activities during breach repairs, etc. (Cain 2002a).

ETTP is in a rural setting, and no residences and sensitive receptors (e.g., schools, hospitals) are located in the immediate vicinity. As part of hearing protection for workers, industrial hygiene measurements of noise associated with the DUF<sub>6</sub> cylinder project have been made since 1998. Ambient noise levels around the site are relatively low. Measurements taken at the nearby residence along Popular Creek Road (off Blair Road) to the north of the site on June 1991 at 8:30 a.m. indicated about 39 dB(A), typical of a rural environment (ANL 1991b). At three residences on Blair Road nearest the site, noises from the K-25 activities were not distinguishable from background noise. To date, there have been no complaints about noise from neighboring communities.

### **3.2.4 Geology and Soil**

#### **3.2.4.1 Topography, Structure, and Seismic Risk**

The topography of the Oak Ridge site is varied; the maximum change in elevation across the site is about 420 ft (130 m). The site is underlain by sedimentary rocks composed of limestone and dolomite. Sinkholes, large springs, and other karst features can occur in the limestone formations adjacent to the site (DOE 1995).

The ETTP site is situated in the Valley and Ridge Subregion of the Appalachian Highlands Province near the boundary with the Cumberland Plateau (DOE 1995). This subregion consists of a series of northeast-southwest trending ridges bounded by the Cumberland Escarpment on the west and by the Blue Ridge Front on the east.

The major stratigraphic units underlying the site and its confining ridges are the Rome Formation (silty shale and shale), the Conasauga Group (calcareous shale interbedded with limestone and siltstone), the Knox Group (silty dolomite), and the Chickamauga Limestone (interbedded with layers of bentonite). These units range in age from Lower Cambrian (Rome Formation) to Middle Ordovician (Chickamauga Limestone). Contacts between the members are gradational and discontinuous. Sinkholes, large springs, and other karst features are common in

the Knox Group, and areas underlain with limestone or dolomites are, for the most part, classified as karst terrains (DOE 1995).

The most important structural feature near the site is a fault system consisting of the Whiteoak Mountain Fault, which runs through the southeastern corner of the Oak Ridge facility; the Kingston Fault, a parallel fault that occurs north of Poplar Creek; and the Copper Creek Fault, located in Melton Valley. A branch of the Whiteoak Mountain Fault originates just south of the facility and runs due north through its center. None of these faults appear to have any topographic expression, and it is assumed that displacement took place prior to the development of the present surface of erosion (DOE 1979). These faults can probably be considered inactive; no seismic events have been associated with these faults near the site, and no surface movement has been reported along the faults.

### 3.2.4.2 Soils

The typical soil types of the Valley and Ridge Province at ETTP are red-yellow podsols, reddish-brown laterites, or lithosols (DOE 1979). They are usually strongly leached and acidic and have a low organic content. The thickness of alluvium beneath the site ranges from nearly 0 to 60 ft (0 to 18 m). Soils developed on the Chickamauga Formation, which underlies most of the site, are typically yellow to yellow-brown montmorillonites. The Conasauga Shale, which underlies the southeastern corner of the site, develops a silty brown, tan, greenish, and maroon clay that is micaceous and contains fragments of unweathered parent rock. In upland areas around the site, the Fullerton Soil Series is dominant. This soil has moderate infiltration rates and is moderately drained to well drained. The Nolichucky and Talbott Series soils are the most abundant valley and terrace soils within the site proper. The Nolichucky and Talbott Series soils are similar to the Fullerton Series soils (Geraghty & Miller, Inc. 1989b).

Soil and groundwater data have been collected to determine whether contamination is associated with the Oak Ridge cylinder yards (DOE 1994a). Substances in soil possibly associated with cylinder management activities are uranium and fluoride compounds, which could be released to soil if breached cylinders or faulty valves were present. In 1991, 122 systematic soil samples were collected at the K-yard; these samples had maximum concentrations of 0.14 mg/kg of uranium-235 and 13 mg/kg of uranium-238. Soil samples collected in March 1992 at the K-yard had a maximum uranium concentration of  $36 \pm 2$  mg/kg.

In 1994, 200 systematic and 28 biased soil samples were collected in areas surrounding the cylinder yards; the maximum concentrations detected in these samples were 0.83 mg/kg of uranium-235 at the K-1066-F yard (F-yard) and 75 mg/kg of uranium-238 at the E-yard. Groundwater concentrations of total uranium (measured as gross alpha and gross beta) for upgradient and downgradient wells indicate that although some elevated levels of uranium have been detected in cylinder yard soil, no migration to groundwater has occurred (DOE 1994a).

Soil samples collected as part of general site monitoring in the immediate surrounding area in 1994 had the following maximum concentrations: uranium, 6.7 mg/kg; Aroclor<sup>®</sup> 1254 (a PCB), 0.16 mg/kg; cadmium, 0.34 mg/kg; mercury, 0.15 mg/kg; and nickel,

33 mg/kg (LMES 1996c). Fluoride was not analyzed in the soil samples but is naturally occurring and of low toxicity. Concentrations of uranium in 1995 and 1996 soil monitoring were lower than the previous results (LMES 1996b, 1997b).

As part of ongoing Comprehensive Environmental Response, Compensation, and Liability Act of 1980 (CERCLA)/RCRA investigations, several areas of soil at the ETTP site have been identified as contaminated with radionuclides and/or chemicals. Remediation of this contamination is being implemented as a part of ongoing CERCLA/RCRA activities at the site.

### 3.2.5 Water Resources

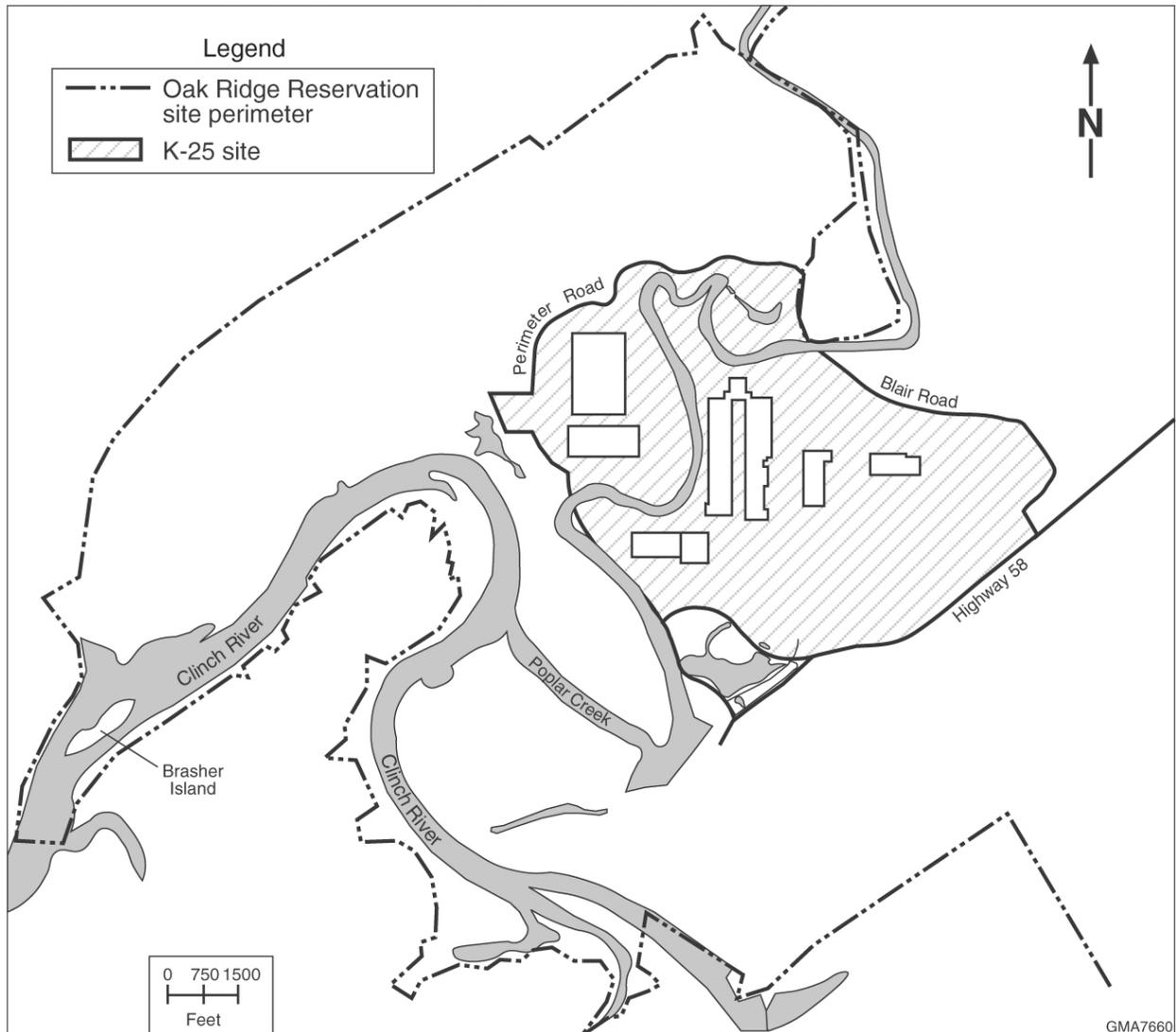
The affected environment for water resources consists of surface water within and in the vicinity of the site boundary and groundwater beneath the site. Analyses of surface water, stream sediment, and groundwater samples have indicated the presence of some contamination resulting from previous gaseous diffusion plant operations. Although several contaminants are present in the water, only small amounts of uranium and fluoride compounds are related to releases from the cylinders.

#### 3.2.5.1 Surface Water

The ETTP site is located near the confluence of the Clinch River (a tributary of the Tennessee River) and Poplar Creek (Figure 3.2-4). Effluent discharge points are located on both Poplar Creek and the Clinch River, and two water withdrawal points are on the Clinch River (DOE 1979).

All waters that drain the ETTP site eventually reach the Tennessee-Ohio-Mississippi water system. The Clinch River provides the most immediate destination for waters discharged from the site and flows southwest into the Tennessee River near Kingston, Tennessee (Geraghty & Miller, Inc. 1989b). A dam constructed in 1963 at River Mile 23.1 created the Melton Hill Reservoir, which establishes the eastern and southeastern boundaries of the Oak Ridge facility. Before this dam was constructed, flows were regulated by Watts Bar Dam, which is located about 38 mi [61 km] downstream from the mouth of the Clinch River. Because of the presence of Melton Hill and Watts Bar dams, the hydrology of the Clinch River-Poplar Creek system is very complex. Average flows in Melton Branch, Whiteoak Creek, and the East Fork of Poplar Creek were 1,120, 4,320, and 21,680 gal/min (4,240, 16,350, and 82,060 L/min), respectively, for a period of record circa 1960. The average daily discharge below Melton Hill Dam was 2 million gal/min (129 m<sup>3</sup>/s) for a 39-year period of record (Geraghty & Miller, Inc. 1989b).

The ETTP site contains a series of limited drainage basins through which small streams traverse and ultimately join with the Clinch River (DOE 1979). Poplar Creek (Figure 3.2-4) is one such stream; it receives drainage from an area of 136 mi<sup>2</sup> (352 km<sup>2</sup>), including the northwestern sector of the site. The headwaters of the East Fork are collected in the vicinity of Y-12, where they receive treated wastewater in the form of cooling tower blowdown, waste stream condensate, and process cooling water. In the uplands around the site, surface runoff is



**FIGURE 3.2-4 Surface Water Features in the Vicinity of ETTP**

largely controlled by soil cover. Within the site, runoff is largely controlled by subsurface drains and diversion ditches. Annual precipitation is 54.8 in. (139 cm). In the vicinity of ETTP, most of the facilities are free from flood hazards for both the 100-year and 500-year maximum probable floods in Poplar Creek (Rothschild et al. 1984).

The ORR site takes water from the Clinch River for makeup cooling water for its reactors at a rate of approximately 20 million gal/d (76 million L/d). An additional 4 million gal/d (15 million L/d) is withdrawn for other process water. These withdrawals occur at Clinch River Miles 11.5 and 14.4. About 25% of this water is returned to the river as treated effluent or blowdown water. Average water consumption for ETTP in 1994 was 1,324 gal/min (5,011 L/min), equaling about 700 million gal (2.6 billion L) per year.

As of 2000, surface water was being monitored at seven locations at ETTP (DOE 2002e). In the last quarter of 1999, sampling at most monitoring stations was scaled back to a semiannual frequency. Uranium levels were well within permitted levels based on radiological standards. In most instances, results for nonradiological parameters were well within their applicable Tennessee water quality standards. Heavy metals were detected, but they were always well within applicable standards. In general, analytical results for samples collected upstream of ETTP were chemically similar to those collected downstream of the site, indicating that the site has little effect on chemical concentrations in surface water.

Sediment samples have also been collected at points that coincided with the ORR water sampling locations. The sediment samples were analyzed for uranium and other parameters. For 1994, the following maximum concentrations were measured: uranium, 43 mg/kg; mercury, 6 mg/kg; nickel, 89 mg/kg; and Aroclor 1254, 10 mg/kg (LMES 1996c).

### 3.2.5.2 Groundwater

Groundwater occurs in a surficial aquifer and in bedrock aquifers in the vicinity of ETTP. The surficial aquifer consists of man-made fill, alluvium, and the residuum of weathered bedrock (Geraghty & Miller, Inc. 1989b). The depth to unweathered bedrock varies from less than 10 to more than 50 ft (<3 to >15 m), depending on the characteristics of the underlying rocks.

Bedrock aquifers in the area are composed of Cambrian to Ordovician sandstones, siltstones, shales, dolostones, and limestones. The uppermost bedrock aquifer occurs in the Chickamauga Group. This formation disconformably overlies the Knox Dolostone and is the most extensive bedrock unit underlying the site. Shale beds restrict groundwater flow in the aquifer, resulting in concentrated flow along the limestone-shale contact, with resultant solution cavities.

The next-lower aquifer occurs in the Knox Group. It is composed of dolostone with interbeds of limestone. Solution features such as sinkholes and caverns are common and are an important route for groundwater flow. This unit is the principal aquifer on the site (Rothschild et al. 1984); the mean yield of wells and springs is about 268 gal/min (1,014 L/min).

As in the Knox Group, solution cavities in the Conasauga Group are an important controlling influence for groundwater flow. Because shale beds within the group are generally less transmissive, groundwater flow is concentrated in the limestone strata. In addition to solution features, folds and faults can also control flow in this unit (Rothschild et al. 1984). The oldest units in the area are the Shady Dolomite and Rome Formation. Groundwater in these units is largely controlled by fractures and vugs (Geraghty & Miller, Inc. 1989b).

During the late spring and summer of 1981, a series of tests to determine properties of the bedrock aquifers directly across the Clinch River from site K-770 were conducted (Geraghty & Miller, Inc. 1989b). Transmissivity values for the bedrock aquifers (Upper Rome Formation, Chickamauga and Knox Groups) ranged from 22 to 15,000 gal/d per foot (270 to 185,000 L/d per meter), with most values ranging from 22 to 6,000 gal/d per foot

(270 to 73,600 L/d per meter). Slug tests performed in the unconsolidated surficial aquifer indicated that the hydraulic conductivity ranged from  $1 \times 10^{-7}$  to 0.01 cm/s. Bedrock values ranged from  $1 \times 10^{-6}$  to  $1 \times 10^{-3}$  cm/s.

On May 29 and 30, 1991, water-level measurements were collected from 185 of 191 monitoring wells at the ETTP site (Geraghty & Miller, Inc. 1991). Inferred directions of groundwater flow are to the south and southwest toward Poplar Creek. Recharge to the groundwater system occurs from surface water bodies and precipitation.

Groundwater contamination is a significant problem on the site (Rothschild et al. 1984). The problem is compounded by use of land underlain by shallow groundwater (found in most of the valleys on the reservation) and by the presence of direct conduits to groundwater (e.g., solution features and fractures), which are common. Contamination is associated with waste disposal activities, buried pipelines, and accidental spills.

In 1994 and 1995, groundwater samples were collected from a network of between 200 and 225 monitoring wells at the site (LMES 1996b,c). The number of wells monitored was greatly decreased in 1996 as a result of the reorganization of the site into six watersheds and reduced monitoring requirements (LMES 1997b). In the 1994 and 1995 sampling conducted for the larger network of monitoring wells, the following substances were detected at levels exceeding their associated primary drinking water standards: antimony, arsenic, barium, cadmium, chromium (up to 0.741 mg/L), fluoride (only at two wells), lead, nickel (up to 0.626 mg/L), thallium (up to 0.021 mg/L), benzene (up to 6 µg/L), carbon tetrachloride, 1,1-dichloroethene (greater than 1,000 µg/L), chloroform, 1,2 dichloroethene (greater than 1,000 µg/L), methylene chloride, toluene (greater than 1,000 µg/L), 1,1,2-trichloro-1,2,2-trifluoroethane (greater than 1,000 µg/L), TCE (up to 11,000 µg/L), 1,1,1-trichloroethane (up to 140,000 µg/L), 1,1,2-trichloroethane, tetrachloroethene (up to 17 µg/L), vinyl chloride, gross alpha activity (up to 43 pCi/L), and gross beta activity (up to 6,770 pCi/L) (LMES 1996b,c). Aluminum, iron, and manganese also consistently exceeded secondary, non-health-based standards because of the natural geochemical nature of the groundwater underlying the site (LMES 1996b).

Data from the 2000 annual groundwater monitoring program showed that aluminum and lead exceeded maximum contaminant levels for groundwater at ETTP (DOE 2001f). Copper, iron, and zinc were also found at elevated concentrations, but maximum concentration limits (MCLs) are not available for these analytes.

Exit-pathway groundwater surveillance monitoring was conducted in 1994 and 1995 at convergence points where shallow groundwater flows from relatively large areas of the site and converges before discharging to surface water locations (LMES 1996b,c). The exit-pathway monitoring data are representative of maximum groundwater contamination levels at locations where the general public might possibly have access in the future. For 1994, monitoring indicated that thallium, bis(2-ethylhexyl)phthalate, and TCE were present in at least one exit-pathway well sample at concentrations exceeding primary drinking water standards (LMES 1996c). The following average concentrations of these constituents were measured: thallium, 0.007 mg/L; bis(2-ethylhexyl)phthalate, 0.169 mg/L; and TCE, 0.008 mg/L. Alpha activity and

fluoride levels were also measured but did not exceed reference levels (average concentration was 4.4 pCi/L for alpha activity and 0.4 mg/L for fluoride). For 1995, monitoring indicated that no inorganic or organic substances exceeded primary drinking water standards; however, alpha activity exceeded the reference level in one well during the spring sampling event (level of 17 pCi/L) (LMES 1996b).

### **3.2.6 Biotic Resources**

#### **3.2.6.1 Vegetation**

About 65% of the land within a 5-mi (8-km) radius of the ETTP site is forested, although most of the ETTP site consists of mowed grasses. Oak-hickory forest is the predominant community on ridges and dry slopes. Mixed pine forests or pine plantations, many of which are managed, have replaced former agricultural fields. Selective logging occurred over much of the site before 1986. Cedar barrens are small communities, primarily on shallow limestone soils, that support drought-tolerant species such as little bluestem, dropseed, eastern red cedar, and stunted oak. A cedar barrens across the Clinch River from the ETTP site may be the best example of this habitat in the state and has been designated as a State Natural Area.

#### **3.2.6.2 Wildlife**

The high diversity of habitats in the area supports many wildlife species. Ground-nesting species commonly occurring on the ETTP site include red fox, ruffed grouse, and eastern box turtle. Canada geese are also common in the ETTP area, and most are probably residents (ANL 1991a). Waterfowl, wading birds, and shorebirds are numerous along the Clinch River, in its backwaters, and in ponds. Two great blue heron rookeries are located north of the ETTP site on Poplar Creek (ANL 1991a). Species commonly associated with streams and ponds include muskrat, beaver, and several species of turtles and frogs.

The aquatic communities within the Clinch River and Poplar Creek support a high diversity of fish species and other aquatic fauna. Mitchell Branch supports fewer fish species, although the diversity of fish species has increased downstream of most ETTP discharges since 1990 (DOE 2002e; LMES 1996b).

#### **3.2.6.3 Wetlands**

Numerous wetlands occur in the vicinity of ETTP, including three small wetlands along Mitchell Branch (ANL 1991a). Extensive forested wetlands occur along Poplar Creek, East Fork Poplar Creek, Bear Creek, and their tributaries. Shallow water embayments of Melton Hill Reservoir and Watts Bar Reservoir support large areas of palustrine emergent wetlands with persistent vegetation. Forested wetlands occur along these marshy areas and extend into tributaries (DOE 1995).

### 3.2.6.4 Threatened and Endangered Species

No occurrence of state- or federal-listed threatened or endangered species on the ETPP site has been documented. State- and federal-listed species that occur on the ORR are presented in Table 3.2-6. Gray bats, which are federal and state listed as endangered, have been observed on ORR as transient individuals (DOE 2002e). The bald eagle, federal listed as threatened, is a winter visitor on the reservation (DOE 2001f). Bachman's sparrow, state listed as endangered, may be present on ORR, although it has not been observed recently (DOE 2002e). Suitable nesting habitat on the reservation includes open pine woods with shrubs and dense ground cover (ANL 1991a).

## 3.2.7 Public and Occupational Safety and Health

### 3.2.7.1 Radiation Environment

Radiation doses to the ETPP cylinder yard workers and to off-site members of the general public are summarized in Table 3.2-7. Exposure to airborne emissions from ETPP operations is approximately 13% of that from operations of the entire ORR. Radiation exposure of the general public MEI is estimated to be 6.7 mrem/yr. This dose is about 7% of the maximum dose limit of 100 mrem/yr set for the general public (DOE 1990) and much smaller than the average dose from natural background radiation in the State of Tennessee. The estimated dose of 6.7 mrem/yr for the MEI was based on the assumption that the off-site public would stay far away from the cylinder yards, which is the case under normal conditions. However, potential external exposure could occur and reach 100 mrem/yr if an off-site individual would spend more than 90 hours in a year immediately at the cylinder yard fence line.

Between 1991 and 1995, the average annual dose to cylinder yard workers ranged from 32 to 92 mrem/yr, which is less than 2% of the maximum radiation dose limit of 5,000 mrem/yr set for radiation workers (10 CFR Part 835). In 1998, 400 cylinders were repainted; the maximum worker exposure was 107 mrem/yr (Cain 2002b).

### 3.2.7.2 Chemical Environment

Table 3.2-8 gives the estimated hazard quotients for members of the general public under existing environmental conditions near the ETPP site. The hazard quotient represents a comparison of the estimated human intake level of a contaminant with an intake level below which adverse effects are very unlikely to occur. The estimated hazard quotients indicate that exposures to DUF<sub>6</sub>-related contaminants in environmental media near the ETPP site are generally a small fraction of those that might be associated with adverse health effects. An exception is groundwater, for which the hazard quotient for fluoride could exceed the threshold of 1. However, it is highly unlikely that this groundwater would be used as a drinking water source.

OSHA has proposed PELs for uranium compounds and HF in the workplace (29 CFR Part 1910, Subpart Z, as of February 2003) as follows: 0.05 mg/m<sup>3</sup> for soluble uranium compounds, 0.25 mg/m<sup>3</sup> for insoluble uranium compounds, and 2.5 mg/m<sup>3</sup> for HF. ETTP worker exposures are kept below these limits.

### 3.2.8 Socioeconomics

Socioeconomic data for the ETTP site focus on an ROI comprising four Tennessee counties surrounding the site: Anderson, Knox, Loudon, and Roane. The counties included in the ROI were selected on the basis of the current residential locations of government workers directly involved in ETTP activities. The ROI is defined on the basis of the current residential locations of government workers directly connected to ETTP site activities and includes the area in which these workers spend much of their salaries. More than 90% of ETTP workers currently reside in these counties (Cain 2002b). Because the majority of ETTP workers live in Anderson and Knox Counties and in the City of Knoxville, the majority of impacts from ETTP would be expected to occur in these locations; therefore, the following discussions emphasize those areas.

#### 3.2.8.1 Population

The population of the ROI in 2000 was 544,358 people (U.S. Bureau of the Census 2002a) and was expected to reach 565,000 by 2003 (Table 3.2-9). In 2000, 382,032 people (70% of the ROI total) resided in Knox County, 71,330 people resided in Anderson County, and 173,890 people resided in the city of Knoxville itself (U.S. Bureau of the Census 2002a). During

**TABLE 3.2-9 Population in the ETTP Region of Influence and Tennessee in 1990, 2000, and 2003**

Location	1990	2000	Growth Rate (%), 1990–2000 <sup>a</sup>	2003 <sup>b</sup> (Projected)
City of Knoxville	165,121	173,890	0.5	176,600
Knox County	335,749	382,032	1.3	397,100
Anderson County	68,250	71,330	0.4	72,300
Loudon County	31,255	39,086	2.3	41,800
Roane County	47,227	51,910	1.0	53,400
ROI total	482,481	544,358	1.2	564,600
Tennessee	4,877,185	5,689,283	1.6	5,958,000

<sup>a</sup> Average annual rate.

<sup>b</sup> ANL projections, as detailed in Appendix F.

Source: U.S. Bureau of the Census (2002a), except as noted.

the 1990s, each of the counties in the ROI and the city of Knoxville experienced moderate increases in population, with an ROI average growth of 1.2%. A slightly higher growth rate was experienced in Loudon County (2.3%), which had the smallest population in the ROI. Over the same period, the population in Tennessee grew at a rate of 1.6%.

### 3.2.8.2 Employment

Total employment in Knox County was 188,114 in 2000; it was projected to reach 199,400 by 2003. The economy of the county is dominated by the trade and service sectors; employment in those sectors currently contributes more than 75% of all employment in the county (Table 3.2-10). Employment growth in the highest growth sector, the service sector, was 7.1% during the 1990s, compared with 2.0% in the county for all sectors as a whole (U.S. Bureau of the Census 1992, 2002b).

Total employment in Anderson County was 39,797 in 2000; it was projected to reach 42,000 by 2003. The economy of the county is dominated by the manufacturing and service sectors, with employment in those sectors currently contributing more than 82% of all employment in the county (Table 3.2-11). Employment growth in the highest growth sector,

**TABLE 3.2-10 Employment in Knox County by Industry in 1990 and 2000**

Sector	No. of People Employed in 1990 <sup>a</sup>	Percentage of County Total	No. of People Employed in 2000 <sup>b</sup>	Percentage of County Total	Growth Rate (%), 1990–2000
Agriculture	2,010 <sup>c</sup>	1.3	951 <sup>d</sup>	0.5	-7.2 <sup>e</sup>
Mining	775	0.5	315	0.2	-8.6
Construction	9,817	6.3	12,225	6.5	2.2
Manufacturing	22,720	14.7	16,912	9.0	-2.9
Transportation and public utilities	9,823	6.3	5,272	2.8	-6.0
Trade	52,258	33.7	41,951	22.3	-2.2
Finance, insurance, and real estate	7,228	4.7	10,668	5.7	4.0
Services	50,032	32.3	99,707	53.0	7.1
Total	154,968		188,114		2.0

<sup>a</sup> U.S. Bureau of the Census (1992).

<sup>b</sup> U.S. Bureau of the Census (2002b).

<sup>c</sup> These agricultural data are for 1992 and are taken from USDA (1994).

<sup>d</sup> These agricultural data are for 1997 and are taken from USDA (1999).

<sup>e</sup> Agricultural data are for 1992 and 1997.

**TABLE 3.2-11 Employment in Anderson County by Industry in 1990 and 2000**

Sector	No. of People Employed in 1990 <sup>a</sup>	Percentage of County Total	No. of People Employed in 2000 <sup>b</sup>	Percentage of County Total	Growth Rate (%), 1990–2000
Agriculture	577 <sup>c</sup>	1.7	243 <sup>d</sup>	0.6	-8.3 <sup>e</sup>
Mining	293	0.9	60	0.2	-14.7
Construction	857	2.6	1,175	3.0	3.2
Manufacturing	11,634	34.9	10,523	26.4	-1.0
Transportation and public utilities	801	2.4	218	0.5	-12.2
Trade	5,236	15.7	4,200	10.6	-2.2
Finance, insurance, and real estate	829	2.5	1,058	2.7	2.5
Services	13,016	39.1	22,273	56.0	5.5
Total	33,299		39,797		1.8

<sup>a</sup> U.S. Bureau of the Census (1992).

<sup>b</sup> U.S. Bureau of the Census (2002b).

<sup>c</sup> These agricultural data are for 1992 and are taken from USDA (1994).

<sup>d</sup> These agricultural data are for 1997 and are taken from USDA (1999).

<sup>e</sup> Agricultural data are for 1992 and 1997.

services, was 5.5% during the 1990s, compared with 1.8% in the county for all sectors as a whole (U.S. Bureau of the Census 1992, 2002b).

Total employment in the ROI was 248,003 in 2000; it was projected to reach 262,600 by 2003. The economy of the ROI is dominated by the trade and service sectors; combined, they contribute 72% of all employment in the ROI (see Table 3.2-12). Employment growth in the highest growth sector, services, was almost 6.8% during the 1990s, compared with 1.9% in the ROI for all sectors as a whole (U.S. Bureau of the Census 1992, 2002b). Employment at the ETTP site currently stands at 1,740 (Cain 2002b).

Unemployment in the Knoxville Metropolitan Statistical Area was 2.8% in December 2002, slightly lower than the average rate during the 1990s (Table 3.2-13). Unemployment for the state was 4.1% in December 2002, which is also slightly lower than the average rates for the last 10 years.

**TABLE 3.2-12 Employment in the ETTP Region of Influence by Industry in 1990 and 2000**

Sector	No. of People Employed in 1990 <sup>a</sup>	Percentage of ROI Total	No. of People Employed in 2000 <sup>b</sup>	Percentage of ROI Total	Growth Rate (%), 1990–2000
Agriculture	4,528 <sup>c</sup>	2.2	2,545 <sup>d</sup>	1.0	-5.6 <sup>e</sup>
Mining	1,138	0.6	407	0.2	-9.8
Construction	11,185	5.5	14,416	5.8	2.6
Manufacturing	39,633	19.3	32,706	13.2	-1.9
Transportation and public utilities	11,322	5.5	6,682	2.7	-5.1
Trade	61,583	30.1	50,387	20.3	-2.0
Finance, insurance, and real estate	8,851	4.3	12,357	5.0	3.4
Services	66,279	32.3	128,299	51.7	6.8
Total	204,922		248,003		1.9

<sup>a</sup> U.S. Bureau of the Census (1992).

<sup>b</sup> U.S. Bureau of the Census (2002b).

<sup>c</sup> These agricultural data are for 1992 and are taken from USDA (1994).

<sup>d</sup> These agricultural data are for 1997 and are taken from USDA (1999).

<sup>e</sup> Agricultural data are for 1992 and 1997.

### 3.2.8.3 Personal Income

Personal income in Knox County totaled about \$11.3 billion in 2000 (in 2002 dollars) and was projected to reach \$13.5 billion by 2003. The annual average rate of growth was 2.8% over the period 1990 through 2000 (Table 3.2-14). County per capita income also rose in the 1990s and was expected to reach \$34,400 in 2003, compared with about \$29,600 at the beginning of the period.

Personal income in Anderson County was almost \$2 billion in 2000 (in 2002 dollars) and was expected to reach \$2.2 billion by 2003. The annual average rate of growth was 1.9% over the period 1990 through 2000 (Table 3.2-14). County per capita income also rose in the 1990s and was expected to reach \$31,100 in 2003, compared with about \$27,200 at the beginning of the period.

**TABLE 3.2-13 Unemployment Rate in the Knoxville Metropolitan Statistical Area and Tennessee**

Location and Period	Rate (%)
<b><i>Knoxville MSA<sup>a</sup></i></b>	
1992–2002 average	3.7
Dec. 2002 (current rate)	2.8
<b><i>Tennessee</i></b>	
1992–2002 average	4.6
Dec. 2002 (current rate)	4.1

<sup>a</sup> Knoxville Metropolitan Statistical Area (MSA) consists of Anderson, Blount, Knox, Loudon, Sevier, and Union Counties.

Source: BLS (2002).

**TABLE 3.2-14 Personal Income in Knox and Anderson Counties and ETPP Region of Influence in 1990, 2000, and 2003**

Location and Type of Income	1990	2000	Growth Rate (%), 1990–2000	2003 (Projected) <sup>a</sup>
<b><i>Knox County</i></b>				
Total personal income (millions of 2002 \$)	8,790	11,308	2.8	13,500
Personal per capita income (2002 \$)	26,180	29,599	1.4	34,400
<b><i>Anderson County</i></b>				
Total personal income (millions of 2002 \$)	1,643	1,938	1.9	2,200
Personal per capita income (2002 \$)	24,074	27,173	1.4	31,100
<b><i>Total ROI</i></b>				
Total personal income (millions of 2002 \$)	12,118	15,516	2.8	18,500
Personal per capita income (2002 \$)	25,115	28,503	1.4	33,000

<sup>a</sup> ANL projections, as detailed in Appendix F.

Source: U.S. Department of Commerce (2002).

Growth rates in total personal income in the ROI as a whole were the same as those for Knox County and slightly higher than those for Anderson County. Total personal income in the ROI grew at a rate of 2.8% over the period 1990 through 2000 and was expected to reach almost \$18.5 billion by 2003. ROI per capita income was expected to grow from about \$28,500 in 1990 to \$33,000 by 2003, an average annual growth rate of 1.4%.

### 3.2.8.4 Housing

Housing stock in Knox County grew at an annual rate of 1.8% over the period 1990 through 2000 (Table 3.2-15) (U.S. Bureau of the Census 2002a), with 178,000 housing units expected by 2002, reflecting the growth in county population. Growth in the City of Knoxville during this period was 1.1%, with total housing units expected to reach 86,300 by 2003. During the 1990s, 27,900 new units were added to the existing housing stock in the county, with 8,528 of these units in the city of Knoxville in 2000. Vacancy rates in 2000 stood at 9.8% in the city and 7.9% in the county as a whole for all types of housing. On the basis of annual population growth rates, 14,900 housing units were expected to be vacant in the county in 2003, of which 4,800 were expected to be rental units.

Housing stock in Anderson County grew at an annual rate of 1.0% over the period 1990 to 2000 (Table 3.2-15) (U.S. Bureau of the Census 2002a), with total housing units expected to reach 33,500 in 2003, reflecting moderate growth in county population. Almost 3,130 new units were added to the existing housing stock in the county during the 1990s. Vacancy rates in 2000 stood at 8.2% in the county for all types of housing. On the basis of annual population growth

rates, 2,900 housing units were expected to be vacant in the county in 2003, of which 800 were expected to be rental units.

Housing stock grew at a slightly slower rate in the ROI as a whole than it did in Knox County during the 1990s, with an overall growth rate of 1.7%. Total housing units were expected to reach 257,400 by 2003, with more than 38,300 housing units added in the 1990s. On the basis of vacancy rates in 2000, which stood at 8.1%, more than 6,400 rental units were expected to be available in 2003.

**3.2.8.5 Community Resources**

**3.2.8.5.1 Community Fiscal Conditions.**

Construction and operation of the proposed facility might result in increased revenues and expenditures for local government jurisdictions, including counties, cities, and school districts. Revenues would come primarily from state and local sales tax revenues associated with employee spending during construction and operations, and they would be used to support additional local community services currently provided by each jurisdiction. Tables 1 and 2 of Allison (2002) present information on revenues and expenditures by the various local government jurisdictions in the ROI.

**3.2.8.5.2 Community Public Services.** Construction and operation of the proposed facility would result in increased demand for community services in the counties, cities, and school districts likely to host relocating construction workers and operations employees. Additional demands would also be placed on local medical facilities and physician services. Table 3.2-16 presents data on employment and levels of service (number of employees per 1,000 population) for public safety and general local government services, and Table 3.2-17 covers physicians. Tables 3.2-18 and 3.2-19 provide staffing data for school districts and hospitals.

**TABLE 3.2-15 Housing Characteristics in the City of Knoxville, Knox and Anderson Counties, and ETTP Region of Influence in 1990 and 2000**

Location and Type of Unit	No. of Units	
	1990	2000
<b><i>City of Knoxville</i></b>		
Owner-occupied	34,892	39,208
Rental	35,081	37,442
Total unoccupied	6,480	8,331
Total	76,453	84,981
<b><i>Knox County</i></b>		
Owner-occupied	85,369	105,562
Rental	48,270	52,310
Total unoccupied	9,943	13,567
Total	143,582	171,439
<b><i>Anderson County</i></b>		
Owner-occupied	19,401	21,592
Rental	7,983	8,188
Total unoccupied	1,939	2,671
Total	29,323	32,451
<b><i>ROI Total</i></b>		
Owner-occupied	128,300	156,219
Rental	63,331	68,577
Total unoccupied	14,603	19,740
Total	206,234	244,536

Source: U.S. Bureau of the Census (2002a).

**TABLE 3.2-16 Public Service Employment in the City of Knoxville, Region-of-Influence Counties, and Tennessee in 2001**

Employment Category	City of Knoxville		Knox County		Clinton			
	No. of Workers	Level of Service <sup>a</sup>	No. of Workers	Level of Service <sup>a</sup>	No. of Workers	Level of Service <sup>a</sup>		
Police	429	2.5	495	2.3	24	2.5		
Fire <sup>b</sup>	334	1.91.91	0	0.0	18	1.9		
General	907	5.2	2,505	11.8	58	6.1		
Total	1,670	9.6	3,000	14.1	100	10.6		

Employment Category	Lake City		City of Oak Ridge		Anderson County		Tennessee <sup>c</sup>
	No. of Workers	Level of Service <sup>a</sup>	No. of Workers	Level of Service <sup>a</sup>	No. of Workers	Level of Service	Level of Service
Police	7	3.8	56	2.0	93	2.8	2.4
Fire <sup>b</sup>	3	1.6	42	1.5	0	0.0	1.1
General	19	10.2	256	9.3	336	10.2	39.1
Total	29	15.6	354	12.9	429	13.0	52.6

<sup>a</sup> Level of service represents the number of employees per 1,000 persons in each jurisdiction (U.S. Bureau of the Census 2002a).

<sup>b</sup> Volunteers not included.

<sup>c</sup> 2000 data.

Sources: City of Knoxville: Hatfield (2002); Knox County: Rodgers (2002), Parolari (2002); Clinton: Shootman (2002); Lake City: Hayden (2002); City of Oak Ridge: McGinnis (2002); Anderson County: Worthington (2002); Tennessee: U.S. Bureau of the Census (2002d).

**TABLE 3.2-17 Number of Physicians in Knox and Anderson Counties and Tennessee in 1997**

Employment Category	Knox County		Anderson County		Tennessee
	No.	Level of Service <sup>a</sup>	No.	Level of Service <sup>a</sup>	Level of Service <sup>a</sup>
Physicians	1,519	4.1	209	3.0	2.6

<sup>a</sup> Level of service represents the number of physicians per 1,000 persons in each jurisdiction.

Source: American Medical Association (1999).

**TABLE 3.2-18 School District Data for Knox and Anderson Counties and Tennessee in 2001**

Employment Category	Knox County		Anderson County		Tennessee
	No.	Student-to-Teacher Ratio <sup>a</sup>	No.	Student-to-Teacher Ratio <sup>a</sup>	Student-to-Teacher Ratio <sup>a</sup>
Teachers	3,380	15.4	488	12.5	15.8

<sup>a</sup> The number of students per teacher in each school district.

Source: Tennessee Department of Education (2001).

**TABLE 3.2-19 Medical Facility Data for Knox and Anderson Counties in 1998**

Hospital	No. of Staffed Beds	Occupancy Rate (%) <sup>a</sup>
<b><i>Knox County</i></b>		
Baptist Hospital of East Tennessee	316	66
East Tennessee Children's Hospital	103	67
County total	319	NA <sup>b</sup>
<b><i>Anderson County</i></b>		
Methodist Medical Center of Oak Ridge	250	72
Ridgeview Psychiatric Hospital and Center	20	35
County total	270	NA

<sup>a</sup> Percent of staffed beds occupied.

<sup>b</sup> NA = not available.

Source: Healthcare InfoSource, Inc. (1998).

### 3.2.9 Waste Management

The ETTP site generates industrial and sanitary waste, including wastewater, solid nonhazardous waste, solid and liquid hazardous waste, radioactive waste, and radioactive hazardous mixed waste. The ETTP site is an active participant in the waste minimization and recycling program within the ORR complex. Much of the waste generated at ETTP is from the ongoing environmental remediation efforts at the site. The ETTP site has the capability to treat wastewater and certain radioactive and hazardous wastes. Some of the wastes generated at ETTP can also be processed or disposed of at facilities located at the Y-12 Plant and ORNL. The ETTP facilities also store and process waste generated at Y-12 and ORNL and wastes from other DOE

installations at Paducah, Portsmouth, and Fernald. Most radioactive waste at ETTP is contaminated with uranium and uranium decay products, with small amounts of fission products and TRU radionuclides from nuclear fuel recycling programs. Table 3.2-20 lists the ETTP site waste loads assumed for the analysis of impacts of projected activities in this report.

**3.2.9.1 Wastewater**

Treated wastewater at the ETTP site is discharged under an NPDES Permit. Sanitary wastewater is processed at an on-site sewage treatment plant with a capacity of 0.92 million gal/d (3.5 million L/d).

**3.2.9.2 Solid Nonhazardous, Nonradioactive Waste**

About 35,000 yd<sup>3</sup>/yr (27,500 m<sup>3</sup>/yr) of solid nonhazardous waste is generated at ORR, which includes waste from the ETTP site. The waste is disposed of at the Y-12 landfill; it is projected that about 50% of the landfill's capacity, or about 920,000 yd<sup>3</sup> (700,000 m<sup>3</sup>), would be available in the year 2020.

**3.2.9.3 Nonradioactive Hazardous and Toxic Waste**

The ETTP site generates both RCRA-hazardous and TSCA-hazardous waste. The site operates several RCRA hazardous waste treatment and storage facilities. The site also operates a permitted TSCA incinerator to treat hazardous and LLMW liquids contaminated with PCBs. The incinerator also processes PCB waste from other facilities at ORR and from off-site DOE installations.

**3.2.9.4 Low-Level Radioactive Waste**

Current ORR policy for newly generated LLW is to perform necessary packaging for direct shipment to appropriate on- and off-site treatment, storage, and disposal facilities. LLW that is not treated or disposed of at ORR is placed in storage, pending either treatment or disposal or both, at off-site facilities.

**TABLE 3.2-20 Projected Waste Generation Volumes for ETTP<sup>a</sup>**

Waste Category	Waste Treatment Volume (m <sup>3</sup> /yr)
LLW	41,000
LLMW	2,700
TRU	0
Hazardous waste	350
Nonhazardous waste <sup>b</sup>	
Solids	12,000
Wastewater	47,000

<sup>a</sup> Volumes include operational and environmental restoration waste projected from FY 2002 to FY 2025. However, it is projected that the majority of the waste would be generated by FY 2008.

<sup>b</sup> Volumes include sanitary and industrial wastes.

Source: Cain (2002c).

### 3.2.9.5 Low-Level Radioactive Mixed Waste

The majority of radioactive waste generated at ETTP is LLMW, which consists of two categories: (1) aqueous RCRA-hazardous radioactive waste contaminated with corrosives or metals and (2) organic liquids contaminated with PCBs.

Aqueous LLMW is treated on site, and resulting wastewaters are discharged to the NPDES-permitted discharges, which have a capacity of 450,000 yd<sup>3</sup>/yr (340,000 m<sup>3</sup>/yr). Organic LLMW liquids contaminated with PCBs are treated by the ETTP TSCA incinerator, which has a capacity of 1,800 yd<sup>3</sup>/yr (1,400 m<sup>3</sup>/yr).

ETTP has the capacity to treat approximately 6,500 yd<sup>3</sup>/yr (5,000 m<sup>3</sup>/yr) of liquid LLMW via grout stabilization. The site has the capacity to store 88,600 yd<sup>3</sup> (67,800 m<sup>3</sup>) of LLMW containers.

### 3.2.10 Land Use

ETTP is located in east-central Tennessee, in the eastern part of Roane County about 25 mi (40 km) west of the City of Knoxville. An analysis of Landsat satellite imagery from 1992 shows that the dominant land cover categories in Roane County include deciduous forest (42.0%), mixed forest (19.7%), evergreen forest (13.6%), and pasture/hay (10.3%) (Figure 3.2-5). The 1997 agricultural census recorded 99 farms in Roane County, covering more than 53,100 acres (21,489 ha) (USDA 1999). Human settlement is sparse throughout much of the county, with most of the population residing in the communities of Harriman, Kingston, Oak Ridge, and Rockwood. The eastern third of Roane County, where ETTP is located, is dominated by deciduous and mixed forest and pasture.

The 1,700-acre (690-ha) ETTP site contains more than 300 buildings with a combined floor space of 13 million ft<sup>2</sup> (1.2 million m<sup>2</sup>) (MMES 1994).

Land use at ETTP focuses on the reuse of facilities, equipment, materials, and utilities previously associated with the gaseous diffusion plant, with an emphasis on reindustrialization (Bechtel Jacobs Company LLC 2002). Activities at the site include a range of operations associated with environmental management at the DOE Oak Ridge Operations facilities, such as management of the TSCA incinerator and the treatment, storage, and disposal of hazardous and radioactive waste (including DUF<sub>6</sub>) (Operations Management International, Inc. 2002a). Currently, ETTP is home to two business centers: Heritage Center and Horizon Center. The Heritage Center encompasses 125 of the main buildings of the former gaseous diffusion facility, which are currently leased to more than 40 companies (Operations Management International, Inc. 2002b). The Horizon Center encompasses 1,000 acres (447 ha) of building sites aimed primarily at high-tech companies.

### 3.2.11 Cultural Resources

The ETTP site falls under the cultural resource management plan (CRMP) for ORR. That plan, which contains procedures for managing archaeological sites, historic structures, traditional cultural properties, and Native American sacred sites, was finalized in July 2001 (Souza et al. 2001). Under the plan, ETTP has responsibility for cultural resources at the eastern end of the reservation.

Cultural resource surveys at ORR have provided a considerable body of knowledge regarding the history and prehistory of the area. Archaeological evidence indicates that there has been a human presence at ORR for at least 12,000 years. All the major prehistoric Eastern Woodland archaeological periods are represented there: Paleo-Indian (10,000 B.C.–8,000 B.C.), Archaic (8,000 B.C.–900 B.C.), Woodland (900 B.C.–A.D. 900), and Mississippian (A.D. 900–A.D. 1600). While the ETTP area has not been completely surveyed, six prehistoric sites were identified there. Three of them were determined to be eligible for the *National Register of Historic Places* (NRHP). Five of the six sites lie outside the ETTP security fences. The area within the ETTP security fences underwent massive earthmoving operations during the construction of the gaseous diffusion plant. It is unlikely that unidentified intact archaeological sites remain within the fences (Morris 1998; Souza et al. 2001).

The Overhill Cherokee occupied part of eastern Tennessee from the 1700s until their relocation to Oklahoma in 1838. DOE Oak Ridge Operations has initiated consultations with the Eastern Band of the Cherokee Indians and the Cherokee Nation of Oklahoma regarding Native American issues related to the DUF<sub>6</sub> conversion project at ORR (see Appendix G). No religious or sacred sites, burial sites, or resources significant to the Cherokee have been identified at ETTP to date. However, there are mounds and other prehistoric sites at ORR thought likely to contain prehistoric burials. Similar resources could exist in the unsurveyed portions of the ETTP area (Souza et al. 2001).

Euro-American settlers began entering eastern Tennessee after 1798, and by 1804, settlement of the area that would become ORR in the 20th century had begun. An economy based on subsistence farming and, later, on coal mining developed. A survey of pre-World War II historic structures at ORR was conducted; 254 structures were evaluated, and 41 were recommended as being eligible for the NRHP, in addition to the 6 that were already listed (DuVall and Souza 1996). Two historic archaeological districts were proposed. Of these, the Wheat Community Historic District lies within the ETTP area. It includes 28 contributing structures; one (the George Jones Memorial Church) is already listed on the NRHP. The ETTP site also includes six historic cemeteries (Morris 1998; Souza et al. 2001).

In 1942, the U.S. Army began to acquire land in eastern Tennessee for the Manhattan Project's "Site X." Renamed the Clinton Engineer Works in 1943, the new facility included a gaseous diffusion plant at the K-25 Site. The K-25 Site played a significant role in the production of highly enriched uranium for weapons manufacture between 1944 and 1964, materially contributing to the development of nuclear weapons during World War II and the Cold War. The K-25 site forms the heart of ETTP. Buildings at the ETTP site were evaluated for their historical significance in 1994. One historic district, the Main Plant Historic District, is eligible for

the NRHP. The district consists of 157 buildings, 120 of which contribute to the district (37 do not). Eleven additional buildings not adjacent to the district are also considered eligible by virtue of their supporting roles in the uranium-235 enrichment process (DuVall and Souza 1996; Holcombe-Burdette 1998; Souza et al. 2001).

### **3.2.12 Environmental Justice**

#### **3.2.12.1 Minority Populations**

This EIS uses data from the most recent decennial census in 2000 to evaluate environmental justice implications of the proposed action and all alternatives with respect to minority populations. The CEQ guidelines on environmental justice recommend that “minority” be defined as members of American Indian or Alaska Native, Asian or Pacific Islander, Black non-Hispanic, and Hispanic populations (CEQ 1997). The earliest release of 2000 census data that included information necessary to identify minority populations identified individuals both according to race and Hispanic origin (U.S. Bureau of the Census 2001). It also identified individuals claiming multiple racial identities (up to six races). To remain consistent with the CEQ guidelines, the phrase “minority population” in this document refers to persons who identified themselves as partially or totally Black (including Black or Negro, African American, Afro-American, Black Puerto Rican, Jamaican, Nigerian, West Indian, or Haitian), American Indian or Alaska Native, Asian, Native Hawaiian or other Pacific Islander, or “Other Race.” The minority category also includes White individuals of Hispanic origin, although the latter is technically an ethnic category. To avoid double counting, tabulations included only White Hispanics; the above racial groups already account for non-White Hispanics. In sum, then, the minority population considered under environmental justice consisted of all non-White persons (including those of multiple racial affiliations) plus White persons of Hispanic origin.

To identify census tracts with disproportionately high minority populations, this EIS uses the percentage of minorities in each state containing a given tract as the reference point. Using the individual states to identify disproportionality acknowledges that minority distributions in the state can differ from those found in the nation as a whole. In 2000, of the 240 census tracts within 50 mi (80 km) of the storage facility at ETTP, 19 had minority populations in excess of state-specified thresholds — a total of 24,235 minority persons in all (Figure 3.2-6). In 2000, 5.2% of the Roane County population was minority (U.S. Bureau of the Census 2002e).

#### **3.2.12.2 Low-Income Populations**

As recommended by the CEQ guidelines, the environmental justice analysis identifies low-income populations as those falling below the statistical poverty level identified annually by the U.S. Bureau of the Census in its Series P-60 documents on income and poverty. The Census Bureau defines poverty levels on the basis of a statistical threshold that considers for each family both overall family size and the number of related children younger than 18 years old.

For example, in 1999, the poverty threshold annual income for a family of three with one related child younger than 18 was \$13,410, while the poverty threshold for a family of five with one related child younger than 18 was \$21,024 (U.S. Bureau of the Census 2000). The 2000 census used 1999 thresholds because 1999 was the most recent year for which annual income data were available when the census was conducted. If a family fell below the poverty line for its particular composition, the census considered all individuals in that family to be below the poverty line.

To identify census tracts with disproportionately high low-income populations, this EIS uses the percentage of low-income persons in each state containing a given tract as a reference point. In 1999, of the 240 census tracts within 50 mi (80 km) of the storage facility at ETTP, 128 had low-income populations in excess of state-specified thresholds — a total of 157,843 low-income persons in all (Figure 3.2-7). In 1999, in Roane County, 13.9% of those individuals for whom poverty status was known were low-income (U.S. Bureau of the Census 2002e).

## **4 ENVIRONMENTAL IMPACT ASSESSMENT APPROACH, ASSUMPTIONS, AND METHODOLOGY**

This EIS evaluates potential impacts on human health and the natural environment from building and operating a DUF<sub>6</sub> conversion facility at three alternative locations at the Portsmouth site and for a no action alternative. These impacts might be positive, in that they would improve conditions in the human or natural environment, or negative, in that they would cause a decline in those conditions. This chapter provides an overview of the methods used to estimate the potential impacts associated with the EIS alternatives, summarizes the major assumptions that formed the basis of the evaluation, and provides some background information on human health impacts. More detailed information on the assessment methods used to evaluate potential environmental impacts is provided in Appendix F.

### **4.1 GENERAL APPROACH**

Potential environmental impacts were assessed by examining all of the activities required to implement each alternative, including construction of the required facility, operation of the facility, and transportation of materials between sites. Potential long-term impacts from cylinder breaches occurring at Portsmouth and ETTP were also estimated. For each alternative, potential impacts to workers, members of the general public, and the environment were estimated for both normal operations and for potential accidents.

The analysis for this EIS considered all potential areas of impact but emphasized those that might have a significant impact on human health or the environment, would be different under different alternatives, or would be of special interest to the public (such as potential radiation effects). The environmental characteristics of the Portsmouth site, where the conversion facility would be built and operated, are described in Section 3.1. The environmental setting of the ETTP site, where cylinders would be prepared for shipment to Portsmouth, is described in Section 3.2.

The estimates of potential environmental impacts for the proposed action were based on characteristics of the proposed UDS conversion facility. The two primary sources of information were excerpts from the UDS conversion facility conceptual design report (UDS 2003a) and the updated UDS NEPA data package (UDS 2003b). As noted in Section 2.2, current facility designs are at the 100% conceptual design stage. Several design options are considered in the EIS to provide future flexibility.

The NEPA data package (UDS 2003b) was prepared by UDS to support preparation of this EIS. For the proposed Portsmouth conversion facility, the NEPA data package includes facility descriptions, process descriptions and material flows, anticipated waste generation, anticipated air emissions, anticipated liquid effluents, waste minimization and pollution prevention approaches, anticipated water usage, anticipated energy consumption, anticipated materials usage, anticipated toxic or hazardous chemical storage, floodplain and wetland

information, anticipated noise levels, estimated land use, employment needs, transportation needs, and safety analysis data.

The NEPA data and a variety of assessment tools and methods were used to evaluate the potential impacts that construction and operation of the conversion facility and shipment of the ETTP cylinders to Portsmouth would have on human health and the environment. These methods are described by technical discipline in Appendix F. The following sections summarize the major assessment assumptions and provide overview information on the estimation of human health impacts from radiation and chemical exposure.

## **4.2 MAJOR ASSUMPTIONS AND PARAMETERS**

Table 4.2-1 gives the major assumptions and parameters that formed the basis of the analyses in this EIS. The primary source for UDS conversion facility data was the updated UDS NEPA data package (UDS 2003b). Discipline-specific information and technical assumptions are provided in the methods described in Appendix F.

## **4.3 METHODOLOGY**

In general, the activities assessed in this EIS could affect workers, members of the general public, and the environment during construction of the new facility, during routine facility operations, during transportation, and during facility or transportation accidents. Activities could have adverse effects (e.g., human health impairment) or positive effects (e.g., regional socioeconomic benefits, such as the creation of jobs). Some impacts would result primarily from the unique characteristics of the uranium and other chemical compounds handled or generated under the alternatives. Other impacts would occur regardless of the types of materials involved, such as the impacts on air and water quality that can occur during any construction project and the vehicle-related impacts that can occur during transportation.

The areas of potential environmental impacts evaluated in this EIS are shown and described in Figure 4.3-1 (the order of presentation does not imply relative importance). For each area, different analytical methods were used to estimate the potential impacts from construction, operations, and accidents for each of the alternatives. The assessment methodologies are described in Appendix F.

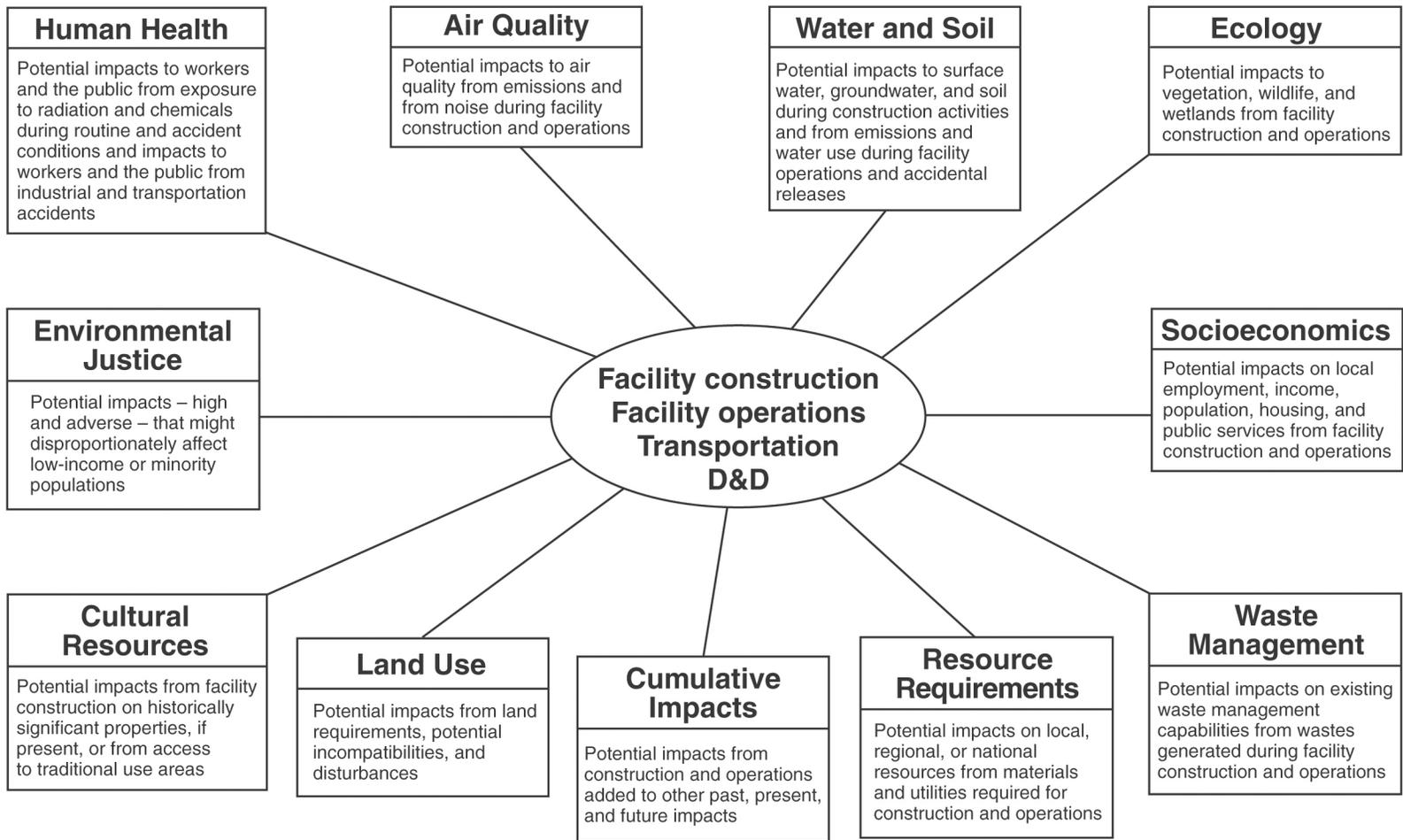
Because of the chemical and radioactive nature of the materials being processed and produced, and the fact that the conversion facility would be built on a previously disturbed industrialized site, the potential impact to the health of workers and the public is one of the areas of primary concern in this EIS. Therefore, the following sections provide background information on radiation and chemical health effects and on the approach used to evaluate accidents. The information is presented to aid in the understanding and interpretation of the potential human health impacts presented in Chapters 2 and 5.

**TABLE 4.2-1 Summary of Major EIS Data and Assumptions**

Parameter/Characteristic	Data/Assumption
<b>General</b>	
Portsmouth DUF <sub>6</sub> cylinder inventory	16,109 cylinders; 195,800 t
Portsmouth non-DUF <sub>6</sub> cylinder inventory	2,693 cylinders; 13,500 t (14,900 tons)
ETTP DUF <sub>6</sub> cylinder inventory	4,822 cylinders; 54,300 t (60,000 tons)
ETTP non-DUF <sub>6</sub> cylinder inventory	1,102 cylinders; 26 t (29 tons)
<b>No Action Alternative</b>	
	No conversion facility constructed; continued long-term storage of DUF <sub>6</sub> in cylinders at Portsmouth and ETTP.
Assessment period	Through 2039, plus long-term groundwater impacts
Construction	None
Cylinder management	Continued surveillance and maintenance activities consistent with current plans and procedures.
Assumed total number of future cylinder breaches:	
Controlled-corrosion case	16 at Portsmouth; 7 at ETTP
Uncontrolled-corrosion case	74 at Portsmouth; 213 at ETTP
<b>Action Alternatives</b>	
	Build and operate a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF <sub>6</sub> inventories; construct a new cylinder storage yard at Portsmouth for ETTP cylinders.
Construction start	2004
Construction period	≈2 years
Start of operations	2006
Operational period	18 years (14 years if ETTP cylinders are converted at Paducah)
Facility footprint	10 acres (4 ha)
Facility throughput	13,500 t/yr (15,000 tons/yr) DUF <sub>6</sub>
Conversion products	
Depleted U <sub>3</sub> O <sub>8</sub>	10,800 t/yr (11,800 tons/yr)
CaF <sub>2</sub>	18 t/yr (20 tons/yr)
70% HF acid	2,500 t/yr (2,800 tons/yr)
49% HF acid	5,800 t/yr (6,300 tons/yr)
Steel (empty cylinders, if not used as disposal containers)	1,177 t/yr (1,300 tons/yr)
Proposed conversion product disposition (see Table 2.2-2 for details):	
Depleted U <sub>3</sub> O <sub>8</sub>	Disposal; Envirocare (primary), NTS (secondary) <sup>a</sup>
CaF <sub>2</sub>	Disposal; Envirocare (primary), NTS (secondary)
70% HF acid	Sale pending DOE approval
49% HF acid	Sale pending DOE approval
Steel (empty cylinders, if not used as disposal containers)	Disposal; Envirocare (primary), NTS (secondary)

<sup>a</sup> DOE plans to decide the specific disposal location(s) for the depleted U<sub>3</sub>O<sub>8</sub> conversion product after additional appropriate NEPA review. Accordingly, DOE will continue to evaluate its disposal options and will consider any further information or comments relevant to that decision. DOE will give a minimum 45-day notice before making the specific disposal decision and will provide any supplemental NEPA analysis for public review and comment.

Sources: UDS (2003a,b).



**FIGURE 4.3-1 Areas of Potential Impact Evaluated for Each Alternative**

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### 4.3.1 Overview of the Human Health Assessment

Human health impacts were estimated for three types of potential exposures: exposure to radiation, exposure to chemicals, and exposure to physical hazards (e.g., on-the-job injuries or fatalities from falls, lifting, or equipment malfunctions). These potential human exposures could occur in and around facilities or during transportation of materials. Exposures could take place during incident-free (normal) operations or following accidents in the facilities or during transportation.

The nature of the potential impacts resulting from the three types of exposure differs. Table 4.3-1 lists and compares the key features of these types of exposures. Because of the differences in these features, it is not always appropriate to combine impacts from different exposures to get a total impact for a given human receptor.

### 4.3.2 Radiation

All of the alternatives would involve handling compounds of the element uranium, which is radioactive. Radiation, which occurs naturally, is released when one form of an element (an isotope) changes into some other atomic form. This process, called radioactive decay, occurs because unstable isotopes tend to transform into a more stable state. The radiation emitted may be in the form of particles, such as neutrons, alpha particles, or beta particles, or waves of pure energy, such as gamma rays.

The radiation released by radioactive materials (i.e., alpha, beta, neutron, and gamma radiation) can impart sufficient localized energy to living cells to cause cell damage. This damage may be repaired by the cell, the cell may die, or the cell may reproduce other altered cells, sometimes leading to the induction of cancer. An individual may be exposed to radiation from outside the body (called external exposure) or, if the radioactive material has entered the body through inhalation (breathing) or ingestion (swallowing), from inside the body (called internal exposure).

#### 4.3.2.1 Background Radiation

Everyone is exposed to radiation on a daily basis, primarily from naturally occurring cosmic rays, radioactive elements in the soil, and radioactive elements incorporated in the body. Man-made sources of radiation, such as medical x-rays or fallout from historical nuclear weapons testing, also contribute, but to a lesser extent. About 80% of background radiation originates from naturally occurring sources, with the remaining 20% resulting from man-made sources.

The amount of exposure to radiation is commonly referred to as “dose.” The estimation of radiation dose takes into account many factors, including the type of radiation exposure (neutron, alpha, gamma, or beta), the different effects each type of radiation has on living tissues,

**TABLE 4.3-1 Key Features of Potential Human Exposures to Radiological, Chemical, and Physical Hazards**

Feature	Potential Exposures		
	Radiological	Chemical	Physical Hazard
Materials of concern	Uranium and its compounds.	Uranium and its compounds, HF, and NH <sub>3</sub> .	Physical hazards associated with all facilities and transportation conditions.
Health effects	Radiation-induced cancer incidence and potential fatalities would occur a considerable time after exposure (typically 10 to 50 years). The risks were assessed in terms of LCFs above background levels.	Adverse health effects (e.g., kidney damage and respiratory irritation or injury) could be immediate or could develop over time (typically less than 1 year).	Impacts would result from occurrences in the workplace or during transportation that were unrelated to the radiological and/or chemical nature of the materials being handled. Potential impacts would include bodily injury or death due to falls, lifting heavy objects, electrical fires, and traffic accidents.
Receptor	Generally the whole body of the receptor would be affected by external radiation, with internal organs affected by ingested or inhaled radioactive materials. Internal and external doses were combined to estimate the effective dose equivalent (see Appendix F).	Generally certain internal organs (e.g., kidneys and lungs) of the receptor would be affected.	Generally any part of the body of the receptor could be affected.
Threshold	No radiological threshold exists before the onset of impacts, i.e., any radiation exposure could result in a chance of LCFs. To show the significance of radiation exposures, the estimated number of LCFs is presented, and radiation doses are compared with existing regulatory limits.	A chemical threshold exposure level exists (different for each chemical) below which exposures are considered safe (see Section 4.3.3). Where exposures were calculated at below threshold levels, “no impacts” are reported.	No threshold exists for physical hazards. Impact estimates are based on the statistical occurrence of impacts in similar industries and on the amount of labor required.

the type of exposure (i.e., internal or external), and, for internal exposure, the fact that radioactive material may be retained in the body for long periods of time. The common unit for radiation dose that accounts for these factors is the rem (1 rem equals 1,000 mrem).

In the United States, the average dose from background radiation is about 360 mrem/yr per person, of which about 300 mrem is from natural sources. For perspective, the radiation doses resulting from a number of common activities are provided in Table 4.3-2. The total dose to an individual member of the general public from DOE and other federal activities is limited by law to 100 mrem/yr (in addition to background radiation), and the dose to a member of the public from airborne emissions released from DOE facilities must be below 10 mrem/yr (40 CFR Part 61).

#### 4.3.2.2 Radiation Doses and Health Effects

Radiation exposure can cause a variety of adverse health effects in humans. Very large doses of radiation (about 450,000 mrem) delivered rapidly can cause death within days to weeks from tissue and organ damage. The potential adverse effect associated with the low doses typical of most environmental and occupational exposures is the inducement of cancers that may be fatal. This latter effect is called “latent” cancer fatality (LCF) because the cancer may take years to develop and cause death. In general, cancer caused by radiation is indistinguishable from cancer caused by other sources.

For this EIS, radiation effects were estimated by first calculating the radiation dose to workers and members of the general public from the anticipated activities required under each alternative. Doses were estimated for internal and external exposures that might occur during normal (or routine) operations and following hypothetical accidents. The analysis considered three groups of people: (1) involved workers, (2) noninvolved workers, and (3) members of the general public.

For each of these groups, doses were estimated for the group as a whole (population or collective dose). For noninvolved workers and the general public, doses were also estimated for a MEI. The MEI was defined as a hypothetical person who — because of proximity, activities, or living habits — could receive the highest possible dose. The MEI for noninvolved workers and members of the

#### **Key Concepts in Estimating Risks from Radiation**

The health effect of concern from exposure to radiation at levels typical of environmental and occupational exposures is the inducement of cancer. Radiation-induced cancers may take years to develop following exposure and are generally indistinguishable from cancers caused by other sources. Current radiation protection standards and practices are based on the premise that any radiation dose, no matter how small, can result in detrimental health effects (cancer) and that the number of effects produced is in direct proportion to the radiation dose. Therefore, doubling the radiation dose is assumed to result in doubling the number of induced cancers. This approach is called the “linear-no-threshold hypothesis” and is generally considered to result in conservative estimates (i.e., over-estimates) of the health effects from low doses of radiation.

**TABLE 4.3-2 Comparison of Radiation Doses from Various Sources**

Radiation Source	Dose to an Individual
Annual background radiation — U.S. average	
Total	360 mrem/yr
From natural sources (cosmic, terrestrial, radon)	300 mrem/yr
From man-made sources (medical, consumer products, fallout)	60 mrem/yr
Daily background radiation — U.S. average	1 mrem/d
Increase in cosmic radiation dose due to moving to a higher altitude, such as from Miami, Florida, to Denver, Colorado	25 mrem/yr
Chest x-ray	10 mrem
U.S. transcontinental flight (5 hours)	2.5 mrem
Dose from naturally occurring radioactive material in agricultural fertilizer — U.S. average	1 to 2 mrem/yr
Dose from standing 6 ft (2 m) from a full DUF <sub>6</sub> cylinder for 5 hours	1 mrem

Sources: National Council on Radiation Protection and Measurements (NCRP 1987).

general public usually was assumed to be at the location of the highest on-site or off-site air concentrations of contaminants, respectively — even if no individual actually worked or lived there. Under actual conditions, all radiation exposures and releases of radioactive material to the environment are required to be kept as low as reasonably achievable (ALARA), a practice that has as its objective the attainment of dose levels as far below applicable limits as possible.

Following estimation of the radiation dose, the number of potential LCFs was calculated by using health risk conversion factors. These factors relate the radiation dose to the potential number of expected LCFs on the basis of comprehensive studies of groups of people historically exposed to large doses of radiation, such as the Japanese atomic bomb survivors. The factors used for the analysis in this EIS were 0.0004 LCF/person-rem of exposure for workers and 0.0005 LCF/person-rem of exposure for members of the general public (International Commission on Radiological Protection [ICRP] 1991). The latter factor is slightly higher because some individuals in the public, such as infants, are more sensitive to radiation than the average worker. These factors imply that if a population of workers receives a total dose of 2,500 person-rem, on average, 1 additional LCF will occur among the workers. Similarly, if the general public receives a total dose of 2,000 person-rem, on average, 1 additional LCF will occur.

The calculation of human health effects from radiation is relatively straightforward. For example, assume the following situation:

- Each of 100,000 persons receives a radiation dose equal to background, or 360 mrem/yr (0.36 rem/yr), and
- The health risk conversion factor for the public is 0.0005 LCF/person-rem.

In this case, the number of radiation-induced LCFs caused by 1 year of exposure among the population would be  $1 \text{ yr} \times 100,000 \text{ persons} \times 0.36 \text{ rem/yr} \times 0.0005 \text{ LCF/person-rem}$ , or about 18 cancer cases, which would occur over the lifetimes of the individuals exposed. For perspective, in the same population of 100,000 persons, a total of about 23,000 (23%) would be expected to die of cancer from all causes over their lifetimes (Centers for Disease Control and Prevention 1996).

Sometimes the estimation of number of LCFs does not yield whole numbers and, especially in environmental applications, yields numbers less than 1. For example, if 100,000 persons were exposed to 1 mrem (0.001 rem) each, the estimated number of LCFs would be 0.05. The estimate of 0.05 LCF should be interpreted statistically — as the average number of deaths if the same radiation exposure was applied to many groups of 100,000 persons. In most groups, no one (zero persons) would incur an LCF from the 1-mrem exposure each person received. In some groups, 1 LCF would occur, and in exceptionally few groups, 2 or more LCFs would occur. The average number of deaths would be 0.05 (just as the average of 0, 0, 0, and 1 is 0.25). The result, 0.05 LCF, may also be interpreted as a 5% chance (1 in 20) of 1 radiation-induced LCF in the exposed population. In this EIS, fractional estimates of LCFs were rounded to the nearest whole number for purposes of comparison. Therefore, if a calculation yielded an estimate of 0.6 LCF, the outcome is presented as 1 LCF, the most likely outcome.

The same concept is assumed to apply to exposure of a single individual, such as the MEI. For example, the chance that an individual exposed to 360 mrem/yr (0.36 rem/yr) over a lifetime of 70 years would die from a radiation-induced cancer is about 0.01 ( $0.36 \text{ rem/yr} \times 0.0005 \text{ LCF/rem} \times 70 \text{ yr} = 0.01 \text{ LCF}$ ). Again, this should be interpreted statistically; the estimated effect of radiation on this individual would be a 1% (1 in 100) increase in the chance of incurring an LCF over the individual's lifetime. In the EIS, the risk to individuals is generally presented as the increased chance that the individual exposed would die from a radiation-induced cancer. As noted, the baseline chance of dying from cancer in the United States is approximately 1 in 4.

### 4.3.3 Chemicals

For this EIS, the chemicals of greatest concern are soluble and insoluble uranium compounds, HF, and anhydrous NH<sub>3</sub>. Uranium compounds can cause chemical toxicity to the kidneys; soluble compounds are more readily absorbed into the body and thus are more toxic to the kidneys. HF and NH<sub>3</sub> are corrosive gases that can cause respiratory irritation in humans, with

tissue destruction or death resulting from exposure to large concentrations. Both have a pungent and irritating odor. No deaths are known to have occurred as a result of short-term (i.e., 1 hour or less) exposures to 50 ppm or less of HF, or 1,000 ppm or less of NH<sub>3</sub>. Uranium compounds, HF, and NH<sub>3</sub> are not chemical carcinogens; thus, cancer risk calculations are not applicable for the chemical hazard assessment.

For long-term, low-level (chronic) exposures to uranium compounds and HF emitted during normal operations, potential adverse health effects for the hypothetical MEI in the noninvolved worker and general public populations were calculated by estimating the intake levels associated with anticipated activities. Intake levels were then compared with reference levels below which adverse effects are very unlikely. Risks from normal operations were quantified as hazard quotients and hazard indices (see text box).

#### 4.3.4 Accidents

The EIS considers a range of potential accidents that could occur during conversion operations and transportation. An accident is defined as a series of unexpected or undesirable events leading to a release of radioactive or hazardous material within a facility or into the natural environment. Because an accident could involve a large and uncontrolled release, such an event potentially could pose considerable health risks to workers and members of the general public. Two important elements must be considered in the assessment of risks from accidents: the consequence of the accident and the expected frequency (or probability) of the accident.

##### 4.3.4.1 Accident Consequences

The term accident consequence refers to the estimated impacts if an accident were to occur — including health effects such as fatalities. For accidents involving releases of radioactive material, the consequences are expressed in the same way as the consequences from

### Key Concepts in Estimating Risks from Low-Level Chemical Exposures

#### Reference Level

- Intake level of a chemical below which adverse effects are very unlikely.

#### Hazard Quotient

- A comparison of the estimated intake level or dose of a chemical with its reference dose.
- Expressed as a ratio of estimated intake level to reference dose.
- Example:
  - The EPA reference level (reference dose) for ingestion of soluble compounds of uranium is 0.003 mg/kg of body weight per day.
  - If a 150-lb (70-kg) person ingested 0.1 mg of soluble uranium per day, the daily rate would be  $0.1 \div 70 \approx 0.001$  mg/kg, which is below the reference dose and thus unlikely to cause adverse health effects. This would yield a hazard quotient of  $0.001 \div 0.003 = 0.33$ .

#### Hazard Index

- Sum of the hazard quotients for all chemicals to which an individual is exposed.
- A value less than 1 indicates that the exposed person is unlikely to develop adverse human health effects.

routine operations — that is, LCFs are estimated for the MEI and for populations on the basis of estimated doses from all important exposure pathways.

Assessing the consequences of accidental releases of chemicals differs from assessing routine chemical exposures, primarily because the reference doses used to generate hazard indices for long-term, low-level exposures were not intended for use in the evaluation of the short-term (e.g., duration of several hours or less), higher-level exposures often accompanying accidents. In addition, the analysis of accidental releases often requires evaluation of different chemicals, especially irritant gases, which can cause tissue damage at higher levels associated with accidental releases but are not generally associated with adverse effects from chronic, low-level exposures.

To estimate the consequences of chemical accidents, two potential health effects endpoints were evaluated: (1) adverse effects and (2) irreversible adverse effects (see text box). In addition, the number of fatalities from accidental chemical exposures was estimated. For exposures to uranium and HF, it was estimated that the number of fatalities occurring would be about 1% of the number of irreversible adverse effects (EPA 1993; Policastro et al. 1997). Similarly, for exposure to NH<sub>3</sub>, the number of fatalities was estimated to be about 2% of the number of irreversible adverse effects (Policastro et al. 1997).

Human responses to chemicals do not occur at precise exposure levels but can extend over a wide range of concentrations. However, in this EIS, the values used to estimate the number of potential chemical effects should be applicable to most individuals in the general population. In all populations, there are hypersensitive individuals who will show adverse responses at exposure concentrations far below levels at which most individuals would normally respond (American Industrial Hygiene Association [AIHA] 2002). Similarly, many individuals will show no adverse response at exposure concentrations even somewhat higher than the guideline values. For comparative purposes in this EIS analysis, use of the guideline values discussed above allowed a uniform comparison of the impacts from potential accidental chemical releases across all alternatives.

### **Health Effects from Accidental Chemical Releases**

The impacts from accidental chemical releases were estimated by determining the numbers of people downwind who might experience adverse effects and irreversible adverse effects:

**Adverse Effects:** Any adverse health effects from exposure to a chemical release, ranging from mild and transient effects, such as respiratory irritation or skin rash (associated with lower chemical concentrations), to irreversible (permanent) effects, including death or impaired organ function (associated with higher chemical concentrations).

**Irreversible Adverse Effects:** A subset of adverse effects, irreversible adverse effects are those that generally occur at higher concentrations and are permanent in nature. Irreversible effects may include death, impaired organ function (such as central nervous system or lung damage), and other effects that may impair everyday functions.

#### 4.3.4.2 Accident Frequencies

The expected frequency of an accident is the chance that the accident might occur while an operation is being conducted. If an accident is expected to happen once every 50 years, the frequency of occurrence is 0.02 per year: 1 occurrence every 50 years =  $1 \div 50 = 0.02$  occurrence per year. A frequency estimate can be converted to a probability statement. If the frequency of an accident is 0.02 per year, the probability of the accident occurring sometime during a 10-year program is 0.2 (10 years  $\times$  0.02 occurrence per year).

The accidents evaluated in this EIS were anticipated to occur over a wide range of frequencies, from once every few years to less than once in 1 million years. In general, the more unlikely it would be for an accident to occur (the lower its probability), the greater the expected consequences. Accidents were evaluated for each activity required for four frequency categories: likely, unlikely, extremely unlikely, and incredible (see text box). To interpret the importance of a predicted accident, the analysis considered the estimated frequency of occurrence of that accident. Although the predicted consequences of an incredible accident might be high, the lower consequences of a likely accident (i.e., one much more likely to occur) might be considered more important.

#### 4.3.4.3 Accident Risk

The term “accident risk” refers to a quantity that considers both the severity of an accident (consequence) and the probability that the accident will occur. Accident risk is calculated by multiplying the consequence of an accident by the accident frequency. For example, if the frequency of occurrence of a facility accident is estimated to be once in 100 years (0.01 per year) and if the estimated consequence, should the accident occur, is estimated to be 10 LCFs among the people exposed, then the risk of the accident would be reported as 0.1 LCF per year (0.01 per year  $\times$  10 LCFs). If the facility was operated for a period of 20 years, the accident risk over the operational phase of the facility would be 2 LCFs (20 years  $\times$  0.1 LCF per year).

This definition of accident risk was used to compare accidents that have different frequencies and consequences. Certain high-frequency accidents that have relatively low consequences might pose a larger overall risk than low-frequency accidents that have potentially high consequences. When calculating accident risk, the consequences are expressed in terms of

#### Accident Categories and Frequency Ranges

**Likely (L):** Accidents estimated to occur one or more times in 100 years of facility operations (frequency  $\geq 1 \times 10^{-2}/\text{yr}$ ).

**Unlikely (U):** Accidents estimated to occur between once in 100 years and once in 10,000 years of facility operations (frequency = from  $1 \times 10^{-2}/\text{yr}$  to  $1 \times 10^{-4}/\text{yr}$ ).

**Extremely Unlikely (EU):** Accidents estimated to occur between once in 10,000 years and once in 1 million years of facility operations (frequency = from  $1 \times 10^{-4}/\text{yr}$  to  $1 \times 10^{-6}/\text{yr}$ ).

**Incredible (I):** Accidents estimated to occur less than one time in 1 million years of facility operations (frequency  $< 1 \times 10^{-6}/\text{yr}$ ).

LCFs for radiological releases and in terms of adverse health effects, irreversible adverse health effects, and fatalities for chemical releases.

#### **4.3.4.4 Physical Hazard (On-the-Job) Accidents**

Physical hazards, unrelated to radiation or chemical exposures, were assessed for each alternative by estimating the number of on-the-job fatalities and injuries that could occur among workers. These impacts were calculated by using industry-specific statistics from the BLS. The injury incidence rates were for injuries involving lost workdays (excluding the day of injury). The analysis calculated the predicted number of worker fatalities and injuries as the product of the appropriate annual incidence rate, the number of years estimated for the project, and the number of full-time equivalents (FTEs) required for the project each year. Estimates for construction and operation of the facilities were computed separately because these activities have different incidence statistics. The calculation of fatalities and injuries from industrial accidents was based solely on historical industrywide statistics and therefore did not consider a threshold (i.e., any activity would result in some estimated risk of fatality and injury).

#### **4.4 UNCERTAINTY IN ESTIMATED IMPACTS**

Estimates of the environmental impacts from DUF<sub>6</sub> conversion are subject to considerable uncertainty. This uncertainty is a consequence primarily of characteristics of the methods used to estimate impacts. To account for this uncertainty, the impact assessment was designed to ensure — through uniform and careful selection of assumptions, models, and input parameters — that impacts would not be underestimated and that relative comparisons among the alternatives would be meaningful. This goal was accomplished by uniformly applying common assumptions to each alternative and by choosing assumptions that would produce conservative estimates of impacts (i.e., assumptions that would lead to overestimates of the expected impacts). Although using a uniform approach to assess impacts can still result in some uncertainty in estimates of the absolute magnitude of impacts, this approach enhances the ability to make valid comparisons among alternatives.

## 5 ENVIRONMENTAL IMPACTS OF ALTERNATIVES

This chapter discusses estimated potential impacts to the environment, including impacts to workers and members of the general public, under the no action alternative (Section 5.1) and the action alternatives (Section 5.2). The general assessment methodologies and major assumptions used to estimate the impacts are described in Chapter 4 and Appendix F of this EIS.

This EIS evaluates the proposed action, which is to construct and operate a conversion facility at the Portsmouth site for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories into depleted uranium oxide and other conversion products. Three alternative locations at the site are evaluated, one of which has been selected as the preferred location. This EIS also discusses impacts from preparation of cylinders for shipment at ETTP and shipment of these cylinders to the Portsmouth site. Shipment of ETTP cylinders to Portsmouth is part of the proposed action, as is the construction of a new cylinder storage yard for those cylinders, if required.

Under the no action alternative, potential environmental impacts from continued storage and maintenance of the cylinders in their current locations at the Portsmouth and ETTP sites are evaluated primarily through the year 2039, although potential long-term impacts from releases of DUF<sub>6</sub> and HF from future cylinder breaches are also evaluated.

This chapter also discusses the potential cumulative impacts of the alternatives (Section 5.3), potential mitigation actions (Section 5.4), unavoidable adverse impacts of the alternatives (Section 5.5), irreversible and irretrievable commitment of resources (Section 5.6), the relationship between short-term use of the environment and long-term productivity (Section 5.7), pollution prevention and waste minimization (Section 5.8), and D&D of conversion facilities (Section 5.9).

### 5.1 NO ACTION ALTERNATIVE

#### 5.1.1 Introduction

Under the no action alternative, it is assumed that storage of DUF<sub>6</sub> cylinders would continue indefinitely at the Portsmouth and ETTP sites and that DOE surveillance and maintenance activities would be ongoing to ensure the continued safe storage of cylinders. Potential environmental impacts from this alternative are estimated through 2039 in this EIS, and long-term impacts (i.e., those that would occur after 2039) from cylinder breaches are also estimated. A similarly defined no action alternative is evaluated in the DUF<sub>6</sub> PEIS (DOE 1999a). The assessment of the no

#### No Action Alternative

The no action alternative assumes that storage of the DUF<sub>6</sub> cylinders would continue for an indefinite period at the Portsmouth site, along with continued cylinder surveillance and maintenance. Impacts were evaluated through the year 2039, and potential long-term (beyond 2039) impacts were also evaluated.

action alternative in this EIS has been updated to reflect changes that have occurred since publication of the PEIS (e.g., changes in plans for new cylinder yard construction and changes in noninvolved worker and general population numbers).

A detailed discussion of the assumptions about and impacts from continued cylinder storage activities is included in Appendix D of the PEIS; changes in impacts due to the addition of USEC-generated cylinders are discussed in Section 6.3.1 of the PEIS (DOE 1999a). Updated information on ongoing and planned cylinder maintenance activities has been compiled from a database on the cylinders at the three sites and from life-cycle baseline documents for cylinder maintenance (Hightower 2002). This information was compiled prior to awarding the conversion contract to UDS and thus represents DOE's plans for long-term maintenance of cylinders without conversion, as would be the case under the no action alternative. In Section 5.1.1.1, the ongoing and planned cylinder maintenance activities assumed for the Portsmouth and ETTP sites under the no action alternative are reviewed.

Impacts associated with the following activities under the no action alternative are considered in both the PEIS and this EIS: (1) storage yard reconstruction and cylinder relocations, (2) routine and ultrasonic test inspections of cylinders and radiological monitoring and maintenance of the cylinder exteriors and valves, (3) cylinder painting, and (4) repair and removal of the contents of any cylinders that might be breached during the storage period. The frequencies for each activity assumed for the Portsmouth and ETTP sites in the PEIS are compared with planned future frequencies in Table 5.1-1. Overall, the assumptions in the PEIS result in the PEIS impacts bounding the actual impacts that could occur under current and planned future activities.

#### **5.1.1.1 Cylinder Maintenance Activities**

The PEIS assessment covered maintenance of up to 16,388 cylinders at the Portsmouth site and 4,683 cylinders at the ETTP site. The actual inventory of cylinders actively managed by DOE is changing over time as USEC transfers cylinders to DOE under three MOAs. As of January 2004, the DOE inventory at the Portsmouth site consisted of 16,109 full, partially full, and heels DUF<sub>6</sub> cylinders; the inventory at the ETTP site consisted of 4,822 full, partially full and heels DUF<sub>6</sub> cylinders (Hightower 2004). Maintenance efforts completed at the two sites include (1) reconstruction/upgrading of a yard at each site to provide stabilized concrete bases and monitored drainage for the cylinder storage areas, and (2) relocation of some cylinders that either were too close to one another to allow for adequate inspections or were located in yards that required reconstruction. Most required cylinder relocations have already been completed; few additional relocations would be required under the no action alternative.

Under the DOE-approved DUF<sub>6</sub> management plan (DOE 1996e), the stored cylinders are regularly inspected for evidence of damage or accelerated corrosion. Each cylinder must be inspected at least once every 4 years; however, annual inspections are required for cylinders that were previously stored in substandard conditions and those that show areas of heavy pitting or corrosion. In addition to these routine inspections, ultrasonic inspections are conducted on some

**TABLE 5.1-1 No Action Alternative: Comparison of Frequencies Assumed in the PEIS with Planned Frequencies for Activities at the Portsmouth and ETTP Sites**

Activity	Activity-Specific Assumption	PEIS-Assumed Average Annual Activity Frequency for Portsmouth <sup>a</sup>	Planned Average Annual Frequency for 2003–2007 for Portsmouth	PEIS-Assumed Average Annual Activity Frequency for ETTP	Planned Average Annual Frequency for 2003–2007 for ETTP
Routine cylinder inspections	30-min exposure at 1-ft (0.30-m) distance per inspection	5,900	7,000	3,400	3,900
Ultrasonic inspections	90-min exposure at about 2-ft (0.61-m) distance per inspection	165	150	70 <sup>b</sup>	120
Radiological monitoring and valve maintenance	1-h exposure at 1-ft (0.30-m) distance per inspection	5	700	2	230
Cylinder relocations	4-h exposure at about 8-ft (2.44-m) distance per relocation	0	0	0	53 <sup>c</sup>
Cylinder painting	7-h exposure at 1 to 10 ft (0.30 to 3.05 m) distance per cylinder, 2 gal (8 L) of paint used, 2 gal (8 L) of LLMW generated per cylinder	1,650	0	900	510 <sup>d</sup>

<sup>a</sup> Source: Parks (1997), with the addition of the assumption that there would be an overall increase of 22% in Portsmouth activities to address the addition of USEC cylinders.

<sup>b</sup> Average for 1999 to 2008.

<sup>c</sup> Data for 2002.

<sup>d</sup> Average for 2000 to 2004, years for which data are available.

of the cylinders. The ultrasonic testing is a nondestructive method of measuring the thickness of cylinder walls. Radiological monitoring of the cylinder surface, especially around the valves, and maintenance are also conducted for cylinders that exhibit discoloration of the valve or surrounding area during routine inspections. Leaking valves are replaced in the field. Impacts from routine inspections, ultrasonic inspections, and radiological monitoring and valve maintenance are evaluated as components of the no action alternative. In the PEIS assessment, the assumed frequencies of routine inspections were somewhat underestimated (by 20% for Portsmouth and 15% for ETTP) in comparison with rates planned for the period 2003 to 2007 (see Table 5.1-1). Radiological monitoring and valve maintenance was underestimated by a factor of more than 100; however, this activity is of short duration, with little radiological exposure.

At the time the PEIS was prepared, a painting program was undertaken in an effort to arrest corrosion of the cylinders. Because the long-term painting schedule was unknown at the time, the PEIS assessment of the no action alternative assumed that as an upper bound, each cylinder would be painted every 10 years. However, after the PEIS was prepared, it was discovered that painting the cylinders increased toxicity indicators in cylinder yard runoff, such that NPDES Permit violations were occurring. Also, the ongoing rate of cylinder breaches was found to be much less than the rate that had been predicted on the basis of theoretical estimates of cylinder corrosion rates, indicating that the other steps that had been taken to improve storage conditions (e.g., regular inspections and relocating cylinders out of ground contact and onto concrete saddles in well-drained, concrete storage yards) were also effective in controlling corrosion. Therefore, continued cylinder maintenance plans call for a greatly reduced frequency of cylinder painting in comparison with the frequency that was assumed in the PEIS (for the Portsmouth site, no cylinder painting is planned; for the ETTP site, the PEIS-assumed painting schedule overestimated that currently planned by a factor of 1.8; see Table 5.1-1). The most frequent ongoing painting activity is partial painting of the ends of skirted cylinders, which are problem areas for corrosion.

The levels of worker activity, worker exposure, and waste generation associated with cylinder painting are much higher than the levels associated with inspection, relocation, and radiological monitoring and valve maintenance activities (Table 5.1-1). Therefore, because the PEIS assumed a high frequency of cylinder painting, its estimates of impacts in several technical areas (e.g., radiological exposures of involved workers, socioeconomics, waste management) represent an upper bound on the impacts that are expected under the current and planned future cylinder maintenance programs. For this EIS, the continued storage impacts for the Portsmouth and ETTP sites estimated in the PEIS were used as the basis for the no action alternative impacts. The data have been revised as appropriate (e.g., the worker and general population numbers have been updated). Under the no action alternative in this EIS, there would not be any additional cylinder yard construction or reconstruction at either the Portsmouth or the ETTP site. Therefore, for most technical areas, the continued storage impacts for the Portsmouth and ETTP sites estimated in the DUF<sub>6</sub> PEIS are presented in this EIS as the no action alternative impacts. Impacts for cylinder yard construction at the ETTP site, included in the PEIS, have been deleted.

#### **5.1.1.2 Assumptions and Methods Used to Assess Impacts Associated with Cylinder Breaches**

To estimate the impacts from continued cylinder storage, it is necessary to predict the number of cylinder breaches that might occur in the future. A cylinder is considered breached if it has a hole of any size at some location on the cylinder wall. At the time the PEIS was published (1999), 8 breached cylinders had been identified at the three storage sites; 3 of these were at the Portsmouth site, and 4 were at the ETTP site. Investigation of these breaches indicated that 6 of the 8 were initiated by mechanical damage during stacking; the damage was not noticed immediately, and subsequent corrosion occurred at the point of damage. It was concluded that the other 2 cylinder breaches (both at the ETTP site) had been caused by external corrosion due to prolonged ground contact. The breached cylinders were patched, pending decisions on long-term management. However, patched cylinders may eventually require

emptying through cold-feeding (a lengthy process of heating a cylinder to a temperature just below the UF<sub>6</sub> liquefaction point so that the UF<sub>6</sub> changes directly from solid to gaseous form).

From 1998 through 2002, 1 additional breach was discovered at the ETTP site (Hightower 2002).<sup>1</sup> This breach was the result of handling damage. The breach rate over this time period was 0.2 per year (1 breach in 5 years). The breached cylinder was subsequently patched.

For assessment purposes in this EIS, 2 cylinder breach cases were evaluated. The first is a case in which it was assumed that the planned cylinder maintenance and painting program would maintain the cylinders in a protected condition and control further corrosion. It was assumed that after the initial painting, some cylinder breaches would result from handling damage. For this case, the number of future breaches estimated through 2039 was 16 for the Portsmouth site and 7 for the ETTP site. In the second case, it was assumed that external corrosion would not be halted by improved storage conditions, cylinder maintenance, and/or painting. This case was considered in order to account for uncertainties in both the effectiveness of painting in controlling cylinder corrosion and uncertainties in the future painting schedule. For this scenario, the number of breaches estimated through 2039 was 74 for the Portsmouth site and 213 for the ETTP site. These breach estimates are based on the historical corrosion rate determined when the cylinders were stored under poor conditions (i.e., cylinders were stacked too close together, were stacked on wooden chocks, or came in contact with the ground). Details concerning development of the breach estimates are provided in Appendix B of the PEIS (DOE 1999a).

The impacts to human health and safety, surface water, groundwater, soil, air quality, and ecology from uranium and HF releases from breached cylinders are assessed in this EIS. For all hypothetical cylinder breaches, it was assumed that the breach would go undetected for 4 years, which is the period between planned inspections for most of the cylinders. In practice, cylinders that show evidence of damage or heavy external corrosion are inspected annually, so it is very unlikely that a breach would go undetected for a 4-year period. For each hypothetical cylinder breach, it was further assumed that 1 lb (0.45 kg) of uranium (as UO<sub>2</sub>F<sub>2</sub>) and 4.4 lb (2 kg) of HF would be released from the cylinder annually for a period of 4 years. The DUF<sub>6</sub> Management Plan (DOE 1996e) outlines procedures to be taken in the event of a cylinder breach and/or release of DUF<sub>6</sub> from one or more cylinders.

Radiological exposures of involved workers could result from patching breached cylinders or emptying the contents of breached cylinders into new cylinders. The assumptions used to estimate impacts to involved workers were that (1) it would require 32 hours of exposure at a distance of 1 ft (0.30 m) to temporarily patch each cylinder, and (2) it would require an additional 961 hours of exposure at a distance of about 10 ft (3.05 m) to empty a cylinder by cold-feeding.

Groundwater impacts were assessed by first estimating the amount of uranium that could be transported from the yards in surface runoff, and then by estimating migration through the soil to groundwater. HF air concentrations were also modeled.

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<sup>1</sup> A breach that occurred at the ETTP site in 1998 was discussed in Section B.2 of the PEIS (DOE 1999a). A total of 11 breaches have been identified at the Portsmouth, ETTP, and Paducah sites (Hightower 2002).

The lower breach estimate for breaches due to cylinder handling is likely to be a reasonable upper-bound estimate of a breach rate that would occur during long-term continued storage under a no action alternative (e.g., the actual rate over the last 5 years was 0.2 breach per year; the model estimates 1 breach per year). Because storage conditions have improved dramatically as a result of cylinder yard upgrades and restacking activities over the last several years, the breach estimate based on the historical corrosion rate is likely a worst-case estimate of what could occur if DOE discontinued active management of the cylinders. In this assessment, the worst-case scenario is used to estimate the earliest time when continued cylinder storage could begin to raise regulatory concerns, such as when drinking water standards would be exceeded in groundwater or when air quality criteria would be exceeded (see Sections 5.1.2.3 and 5.1.2.4.2).

### **5.1.2 Impacts of No Action at the Portsmouth Site**

The impacts described in this section are similar to those presented in Section 3.5.2 of the data compilation report for the Portsmouth site (Hartmann 1999a); however, they have been adjusted to account for changes in the numbers of noninvolved workers and general population since the time of that earlier assessment.

#### **5.1.2.1 Human Health and Safety**

Under the no action alternative, impacts to human health and safety could result from cylinder maintenance operations during both routine conditions and accidents. In general, the impacts during normal facility operations would be limited to workers directly involved in handling cylinders. Under accident conditions, the health and safety of both workers and members of the general public around the site could be affected.

##### **5.1.2.1.1 Normal Facility Operations**

**Workers.** Cylinders containing DUF<sub>6</sub> emit low levels of gamma and neutron radiation. Involved workers would be exposed to this radiation when working near cylinders, such as during routine cylinder monitoring and maintenance activities, cylinder relocation and painting, and patching or repairing of cylinders. It is estimated that an average of about 20 cylinder yard workers would be required at the Portsmouth site. These workers would be trained to function in a radiation environment, they would use protective equipment as necessary, and their radiation exposure levels would be measured and monitored by safety personnel at the sites. Radiation exposure of workers is required by law to be maintained ALARA and not to exceed 5,000 mrem/yr (10 CFR Part 835).

The radiation exposure of involved workers (cylinder yard workers) in future years through 2039 is estimated to be well within public health standards (10 CFR Part 835). If the

same 20 workers conducted all cylinder management activities, the average annual dose to individual involved workers would be about 600 mrem/yr. Worker doses are required by health regulations to be maintained below 5,000 mrem/yr (10 CFR Part 835). The estimated doses do not account for standard ALARA practices that would be used to keep the actual doses as far below the limit as practicable. Thus, the future doses to workers are expected to be less than those estimated because of the conservatism in the assumptions and the models used to generate the estimates. In fact, in 2001, the average measured dose to cylinder yard workers at Portsmouth was about 64 mrem (DOE 2002c). The radiation exposure of the noninvolved workers was estimated to be less than 0.15 mrem/yr.

It is estimated that the total collective dose to all involved cylinder maintenance workers at the Portsmouth site from 1999 through 2039 would be about 460 person-rem. (The collective dose to noninvolved workers would be negligible [i.e., less than 0.01%], compared with the collective dose to involved workers.) This dose would be distributed among all of the workers involved with cylinder activities over the no action period. Although 20 workers would be required each year, the actual number of different individuals involved over the period would probably be much greater than 20 because workers could be rotated to different jobs and could change jobs. This level of exposure could potentially result in less than 1 LCF (i.e., 0.2 LCF) among all the workers exposed, in addition to the cancer cases that would result from all other causes not related to activities under the no action alternative.

As discussed in Chapter 1 and Appendix B of this EIS, some portion of the DUF<sub>6</sub> inventory contains TRU and Tc contamination. The contribution of these contaminants to potential external radiation exposures under normal operations was evaluated on the basis of the bounding concentrations presented in Appendix B. The dose from these contaminants was estimated and compared with the dose from the depleted uranium and uranium decay products in the DUF<sub>6</sub>. It is estimated that under normal operational conditions, the TRU and Tc contaminants would make only a very small contribution to the radiation doses, amounting to approximately 0.2% of the dose from the depleted uranium and its decay products.

No impacts to involved workers are expected from exposure to chemicals during normal cylinder maintenance operations. Exposures to chemicals during cylinder painting operations would be monitored to ensure that airborne chemical concentrations were within applicable health standards that are protective of human health and safety. If planned work activities were likely to expose involved workers to chemicals, those workers would be provided with appropriate protective equipment as necessary.

Chemical exposures to noninvolved workers could result from airborne emissions of UO<sub>2</sub>F<sub>2</sub> and HF that could be dispersed from hypothetical cylinder breaches into the atmosphere and to ground surfaces. It is estimated that the potential chemical exposures of noninvolved workers from any airborne releases during normal operations would be below levels expected to cause adverse effects. (The hazard index was estimated to be less than 0.0001 for noninvolved workers.)

**General Public.** Potential health impacts to members of the general public could occur if material released from breached cylinders entered the environment and was transported from the site through the air, surface water, or groundwater. Off-site releases of uranium and HF from breached cylinders are possible; however, the predicted future off-site concentrations of these contaminants would be much less than levels expected to cause adverse effects. Potential exposures of members of the general public would be well within public health standards. No adverse effects (LCFs or chemical effects) are expected to occur among members of the general public residing within 50 mi (80 km) of the Portsmouth site as a result of DUF<sub>6</sub> management activities.

If all the uranium and HF assumed to be released from hypothetical breached cylinders through 2039 were dispersed from the site through the air, the total radiation dose to the general public (all persons within 50 mi [80 km]) would be about 0.07 person-rem through 2039. This level of exposure would most likely result in zero cancer fatalities among members of the general public. For comparison, the average radiation dose from natural background and medical sources to the same population group in 40 years would be about  $1 \times 10^7$  person-rem. The maximum radiation dose to an individual near the site would be less than about 0.1 mrem/yr, well within health standards. Radiation doses to the general public are required by health regulations to be maintained at below 10 mrem/yr from airborne sources (40 CFR Part 61) and below a total of 100 mrem/yr from all sources combined (DOE 1990). If an individual received the maximum estimated dose every year (1999 to 2039), the total dose would be about 4 mrem, resulting in an additional chance of dying from a latent cancer of about 1 in 500,000. No noncancer health effects from exposure to airborne uranium and HF releases are expected; the estimated hazard index for an MEI is less than 0.01. This means that the total exposure would be at least 100 times less than exposure levels that might cause adverse effects.

The material released from breached cylinders could also potentially be transported from the sites in water, either in surface water runoff or by infiltrating the soil and contaminating groundwater. Members of the general public could be exposed if they used this contaminated surface water or groundwater as a source of drinking water. The results of the surface water and groundwater analyses indicate that the maximum estimated uranium concentrations in surface water accessible to the general public and in groundwater beneath the sites would be less than 20 µg/L (the proposed EPA drinking water standard has now been finalized at 30 µg/L and became effective in December 2003 [EPA 2003a]). Drinking water standards, meant to apply to water “at the tap” of the user, are set at levels protective of human health. In this assessment, 20 µg/L is used as a guideline for surface water and groundwater analyses.

If a member of the general public used contaminated water at the maximum concentrations estimated, adverse effects would be unlikely. Even if a member of the general public used contaminated surface water or groundwater as his or her primary water source, the maximum radiation dose in the future would be less than 0.4 mrem/yr. The corresponding increased risk to this individual of dying from a latent cancer would be less than 1 in 5 million per year. Noncancer health effects from exposure to possible water contamination are not expected; the estimated maximum hazard index for an individual assumed to use the groundwater is less than 0.05. This means that the total exposure would be 20 times less than the exposure level that might cause adverse effects.

If no credit was taken for the reduction in cylinder corrosion rates as a result of cylinder maintenance and painting activities, the groundwater analysis indicates that the uranium concentration in groundwater at the Portsmouth site could exceed 20 µg/L at some time after 2100 (see Hartmann 1999a, Section 3.3). This scenario is highly unlikely because ongoing cylinder inspections and maintenance prevent significant releases from occurring, especially for as many cylinders as are assumed here (i.e., 74 breaches). Nonetheless, if contamination of groundwater used as drinking water occurred in the future, treating the water or supplying an alternative source of water might be required to ensure the safety of those potentially using the water.

#### 5.1.2.1.2 Facility Accidents

**Physical Hazards (On-the-Job Injuries and Fatalities).** Accidents occur in all work environments. In 2000, about 5,200 people in the United States were killed in accidents while at work, and approximately 3.9 million disabling work-related injuries were reported (National Safety Council 2002). Although all work activities would be conducted in as safe a manner as possible, there is a chance that workers could be accidentally killed or injured under the no action alternative, unrelated to any radiation or chemical exposures.

The numbers of accidental worker injuries and fatalities that might occur through 2039 were estimated on the basis of the number of workers required and on the historical accident fatality and injury rates in similar types of industries. It is estimated that a total of less than 1 accidental fatality (i.e., about 0.03, or about 3 chances in 100 of a single fatality) might occur at the Portsmouth site over the no action period evaluated. Similarly, a total of about 40 accidental injuries (defined as injuries resulting in lost workdays) are estimated. These rates are not unique to the activities required for the no action alternative but are typical of any industrial project of similar size and scope.

**Accidents Involving Radiation or Chemical Releases.** Under the no action alternative, accidents could release radiation and chemicals from cylinders. Several types of accidents were evaluated. The accidents included those initiated by operational events, such as equipment or operator failure; external hazards; and natural phenomena, such as earthquakes. The assessment considered accidents ranging from those that would be reasonably likely to occur (expected one or more times in 100 years on average) to those that would be extremely rare (estimated to occur less than once in 1 million years on average).

The accidents of most concern at the Portsmouth site under the no action alternative would be those that could cause a release of UF<sub>6</sub> from cylinders. In a given accident, the amount potentially released would depend on the severity of the accident and the number of cylinders involved. Following a release, the UF<sub>6</sub> could combine with moisture in the air, forming gaseous HF and UO<sub>2</sub>F<sub>2</sub>, a soluble solid in the form of small particles. The depleted uranium and HF could be dispersed downwind, potentially exposing workers and members of the general public

living near the site to radiation and chemical effects. The workers considered in the accident assessment were those noninvolved workers not immediately in the vicinity of the accident; fatalities and injuries among involved workers would be possible if accidents were severe.

The estimated consequences of cylinder accidents are summarized in Table 5.1-2 for chemical effects and Table 5.1-3 for radiation effects. The impacts are the maximums estimated for the Portsmouth site. The impacts are presented separately for likely accidents and for rare, low-probability accidents estimated to result in the largest potential impacts. Although other accidents were evaluated (see Hartmann 1999a; Section 3.2.2), the estimated consequences of those other accidents would be less than those summarized in the tables. The estimated consequences are conservative in that they were based on the assumption that at the time of the accident, the wind would be blowing in the direction of the greatest number of people. In addition, the mitigating effects of protective measures, such as evacuation, were not considered.

An exception to the discussion above would be a certain class of accidents that DOE investigated; however, because of security concerns, information about such accidents is not available for public review but is presented in a classified appendix to this EIS. All classified information will be presented to state and local officials, as appropriate.

**Chemical Effects.** The potential likely accident (defined as an accident that is estimated to occur one or more times in 100 years) that would cause the largest chemical health effects is the failure of a corroded cylinder that would spill part of its contents under dry weather conditions. Such an accident could occur, for example, during cylinder handling activities. It is estimated that about 24 lb (11 kg) of UF<sub>6</sub> could be released in such an accident. The potential consequences from this type of accident would affect only on-site workers. The off-site concentrations of HF and uranium were calculated to be less than the levels that would cause adverse effects from exposure to these chemicals. Therefore, no adverse effects are expected among members of the general public. It is estimated that if this accident did occur, up to 48 noninvolved workers might experience potential adverse effects from exposure to HF and uranium (mostly mild and transient effects, such as respiratory irritation or temporary decrease in kidney function). It is also estimated that no noninvolved workers would experience potential irreversible adverse effects (such as lung or kidney damage). The number of fatalities following an HF or uranium exposure is expected to be somewhat less than 1% of the number of potential irreversible adverse effects (Policastro et al. 1997). Therefore, no fatalities are expected.

For assessment purposes, the estimated frequency of a corroded cylinder spill accident is assumed to be about once in 10 years. Therefore, over the no action period, about 4 such accidents are expected. The accident risk (defined as consequence × probability) would be about 200 workers with potential adverse effects, and no workers with potential irreversible adverse effects. The number of workers actually experiencing adverse effects would probably be considerably less, depending on the actual circumstances of the accidents and the individual chemical sensitivity of the individual workers. In previous accidental exposure incidents involving liquid UF<sub>6</sub> in gaseous diffusion plants, a few workers were exposed to amounts of uranium estimated to be approximately three times the guidelines used for assessing irreversible adverse effects in this EIS; none of those workers actually experienced irreversible adverse effects (McGuire 1991).

**TABLE 5.1-2 No Action Alternative: Estimated Consequences of Chemical Exposures for Cylinder Accidents at the Portsmouth Site<sup>a</sup>**

Receptor <sup>b</sup>	Accident Scenario	Accident Frequency Category <sup>c</sup>	Potential Effect <sup>d</sup>	Consequence <sup>e</sup> (no. of persons affected)
<b><i>Likely Accidents</i></b>				
General public	Corroded cylinder spill, dry conditions	L	Adverse effects	0
	Corroded cylinder spill, dry conditions	L	Irreversible adverse effects	0
	Corroded cylinder spill, dry conditions	L	Fatalities	0
Noninvolved workers	Corroded cylinder spill, dry conditions	L	Adverse effects	0–48
	Corroded cylinder spill, dry conditions	L	Irreversible adverse effects	0
	Corroded cylinder spill, dry conditions	L	Fatalities	0
<b><i>Low Frequency-High Consequence Accidents</i></b>				
General public	Rupture of cylinders – fire	EU	Adverse effects	4–680
	Corroded cylinder spill, wet conditions – water pool	EU	Irreversible adverse effects	0–1
	Corroded cylinder spill, wet conditions – water pool	EU	Potential fatalities	0
Noninvolved workers	Rupture of cylinders – fire	EU	Adverse effects	160–1,000
	Corroded cylinder spill, wet conditions – water pool	EU	Irreversible adverse effects	0–110
	Corroded cylinder spill, wet conditions – water pool	EU	Fatalities	0–1

**Footnotes on next page.**

**TABLE 5.1-2 (Cont.)**

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- <sup>a</sup> The accidents listed are those estimated to result in the greatest impacts among all the accidents considered (except for certain accidents with security concerns). The site-specific impacts for a range of accidents at the Portsmouth site are given in Hartmann et al. (1999a).
- <sup>b</sup> Noninvolved workers are persons who work at the site but who are not involved in handling materials. Depending on the circumstances of the accident, injuries and fatalities among involved workers are possible for all accidents.
- <sup>c</sup> Accident frequencies: L = likely, estimated to occur one or more times in 100 years of facility operations ( $> 10^{-2}/\text{yr}$ ); EU = extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years of facility operations ( $10^{-4}$  to  $10^{-6}/\text{yr}$ ).
- <sup>d</sup> Potential adverse effects include exposures that could result in mild and transient injury, such as respiratory irritation. Potential irreversible adverse effects include exposures that could result in permanent injury (e.g., impaired organ function) or death. The majority of the adverse effects would be mild and temporary in nature. It is estimated that less than 1% of the predicted potential irreversible adverse effects would result in fatalities (see text).
- <sup>e</sup> The consequence is expressed as the number of individuals with a predicted exposure level sufficient to cause the corresponding health endpoint. The range of estimated consequences reflects different atmospheric conditions at the time of an accident assumed to occur at the cylinder yard closest to the site boundary. In general, maximum risks would occur under the atmospheric conditions of F stability with a 1-m/s (2-mph) wind speed; minimum risks would occur under D stability with a 4-m/s (9-mph) wind speed. For both conditions, it was assumed that the wind would be blowing in the direction of the highest density of worker or public populations.

Accidents that are less likely to occur could have higher consequences. The potential cylinder accident at any of the sites estimated to result in the greatest total number of adverse chemical effects would be an accident involving several cylinders in a fire. It is estimated that about 24,000 lb (11,000 kg) of UF<sub>6</sub> could be released in such an accident. It is estimated that if this accident occurred, up to 680 members of the general public and 1,000 noninvolved workers might experience adverse effects from HF and uranium exposure (mostly mild and transient effects, such as respiratory irritation or temporary decrease in kidney function). This accident is considered extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years. If the frequency is assumed to be once in 100,000 years, the accident risk over the no action period would be less than one adverse effect for both workers and members of the general public.

The potential cylinder accident estimated to result in the largest total number of irreversible adverse effects is a corroded cylinder spill under wet conditions, with the UF<sub>6</sub> being released into a pool of standing water. This accident is considered extremely unlikely, expected to occur between once in 10,000 years and once in 1 million years. It is estimated that if this accident did occur, about 1 member of the general public and 110 noninvolved workers might experience irreversible adverse effects (such as lung damage) from HF and uranium exposure. The number of fatalities would be somewhat less than 1% of the estimated number of potential irreversible adverse effects (Policastro et al. 1997). Thus, no fatalities are expected among the

**TABLE 5.1-3 No Action Alternative: Estimated Consequences from Radiation Exposures for Cylinder Accidents at the Portsmouth Site<sup>a</sup>**

Receptor <sup>b</sup>	Accident Scenario	Accident Frequency Category <sup>c</sup>	MEI		Population	
			Dose (rem)	Lifetime Risk of LCF	Dose (person-rem)	Number of LCFs
<i>Likely Accidents</i>						
General public	Corroded cylinder spill, dry conditions	L	0.0022	$1 \times 10^{-6}$	0.22	0.0001
Noninvolved workers	Corroded cylinder spill, dry conditions	L	0.077	$3 \times 10^{-5}$	2.2	0.0009
<i>Low Frequency-High Consequence Accidents</i>						
General public	Rupture of cylinders – fire	EU	0.013	$6 \times 10^{-6}$	34	0.02
Noninvolved workers	Rupture of cylinders – fire	EU	0.02	$8 \times 10^{-6}$	16	0.006

<sup>a</sup> The accidents listed are those estimated to have the greatest impacts among all the accidents considered (except for certain crash accidents with security concerns). The site-specific impacts for a range of accidents at the Portsmouth site are given in Hartmann et al. (1999a). The estimated consequences were based on the assumption that at the time of an accident, the wind would be blowing in the direction of the highest density of worker or public populations and that weather conditions limited dispersion.

<sup>b</sup> Noninvolved workers are persons who work at the site but who are not involved in handling materials. Depending on the circumstances of the accident, injuries and fatalities among involved workers are possible for all accidents.

<sup>c</sup> Accident frequencies: L = likely, estimated to occur one or more times in 100 years of facility operations ( $> 10^{-2}/\text{yr}$ ); EU = extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years of facility operations ( $10^{-4}$  to  $10^{-6}/\text{yr}$ ).

general public, although 1 fatality could occur among noninvolved workers (1% of 110). If the frequency of this accident is assumed to be once in 100,000 years, the accident risk over the period 1999 through 2039 would be less than 1 (0.1) irreversible adverse health effect among workers and the general public combined.

**Radiation Effects.** Potential cylinder accidents could release uranium, which is radioactive in addition to being chemically toxic. The potential radiation exposures of members of the general public and noninvolved workers were estimated for the same cylinder accidents as those for which chemical effects were estimated (Table 5.1-3). For all cylinder accidents considered, the radiation doses from released uranium would be considerably below levels likely

to cause radiation-induced effects among noninvolved workers and the general public and below the 25-rem total effective dose equivalent established by DOE as a guideline for assessing the adequacy of protection of public health and safety from potential accidents (DOE 2000c).

For the corroded cylinder spill accident (dry conditions), the radiation dose to a maximally exposed member of the general public would be less than 3 mrem (lifetime dose), resulting in an increased risk of death from cancer of about 1 in 1 million. The total population dose to the general public within 50 mi (80 km) would be less than 1 person-rem, most likely resulting in zero LCFs. Among noninvolved workers, the dose to an MEI would be 77 mrem, resulting in an increased risk of death from cancer of about 1 in 30,000. The total dose to all noninvolved workers would be about 2.2 person-rem. This dose to workers would result in zero LCFs. The risk (consequence  $\times$  probability) of additional LCFs among members of the general public and workers combined would be much less than 1 over the period 1999 through 2039.

The cylinder accident estimated to result in the largest potential radiation doses would be the accident involving several cylinders in a fire. For this accident, it is estimated that the radiation dose to a maximally exposed member of the general public would be about 13 mrem, resulting in an increased risk of death from cancer of about 1 in 150,000. The total population dose to the general public within 50 mi (80 km) would be 34 person-rem, most likely resulting in zero LCFs. Among noninvolved workers, the dose to an MEI would be about 20 mrem, resulting in an increased risk of death from cancer of about 1 in 100,000. The total dose to all noninvolved workers would be about 16 person-rem. This dose to workers would result in zero LCFs. The risk (consequence  $\times$  probability) of additional LCFs among members of the general public and workers combined would be much less than 1 over the period 1999 through 2039.

#### **5.1.2.2 Transportation**

Continued cylinder storage under the no action alternative would potentially generate small amounts of LLW and LLMW during cylinder monitoring and maintenance activities. This material could require transportation to a treatment or disposal facility. Shipments would be made in accordance with all DOE and DOT regulations and guidelines. It is estimated that less than one waste shipment would be required each year. Because of the small number of shipments and the low concentrations of contaminants expected, the potential environmental impacts from these shipments would be negligible.

#### **5.1.2.3 Air Quality and Noise**

The assessment of potential impacts to air quality from the no action alternative at Portsmouth included a consideration of air pollutant emissions from continued cylinder storage activities, including emissions from operations (cylinder painting and vehicle emissions) and HF emissions from breached cylinders. No cylinder yard construction activities are planned at the Portsmouth site. An atmospheric dispersion model was used to estimate the concentrations of criteria pollutants at the site boundaries: SO<sub>2</sub>, NO<sub>2</sub>, CO, O<sub>3</sub>, PM (PM<sub>10</sub> and PM<sub>2.5</sub>), and Pb. The

site boundary concentrations were compared with existing air quality standards given in Chapter 3. The air concentrations of all criteria pollutants resulting from no action alternative activities would be less than 1% of the respective standards.

Painting activities could generate hydrocarbon emissions. Although no explicit air quality standard has been set for hydrocarbon emissions, these emissions are associated with the formation of O<sub>3</sub>, for which standards have been set. For the Portsmouth site, hydrocarbon emissions from painting activities would be about 0.2% of the hydrocarbon emissions from the entire surrounding county. Because O<sub>3</sub> formation is a regional issue affected by emissions for an entire area, this small additional contribution to the county total would be unlikely to substantially alter the O<sub>3</sub> levels of the county. In addition, the actual frequency of cylinder painting would likely be greatly reduced from the frequency assumed for these analyses.

Taking credit for reduced corrosion from better maintenance and painting, the estimated maximum 24-hour and annual average site boundary HF concentrations from hypothetical cylinder breaches occurring under the no action alternative are 0.12 µg/m<sup>3</sup> and 0.013 µg/m<sup>3</sup>, respectively, at the Portsmouth site. Ohio does not have ambient air quality standards for HF. However, these estimated Portsmouth concentrations are well below the Commonwealth of Kentucky standards (used for comparison) of 2.9 µg/m<sup>3</sup> (secondary standard) and 400 µg/m<sup>3</sup> (primary standard), respectively. Calculations indicate that if no credit was taken for the reduction in corrosion as a result of painting and continued maintenance and if storage continued at the Portsmouth site indefinitely, breaches occurring at the site by around 2039 could result in maximum 24-hour average HF concentrations at the site boundaries of less than 0.8 µg/m<sup>3</sup>, also considerably below the Kentucky secondary standard. Because of the ongoing maintenance program, it is not expected that this higher breach rate would occur at the Portsmouth site.

No construction activities are planned under the no action alternative at the Portsmouth site; therefore, there would be no adverse noise impacts.

Continued storage operations could result in somewhat increased noise levels at the site as a result of projected activities such as painting cylinders or repairing any infrequent cylinder breaches. However, it is estimated that the noise levels at off-site residences would not increase noticeably. Noise impacts are expected to be negligible under the no action alternative.

#### **5.1.2.4 Water and Soil**

Under the no action alternative, impacts on surface water, groundwater, and soil could occur during continued storage of the cylinders. Important elements in assessing potential impacts on surface water include changes in runoff, floodplain encroachment, and water quality. Groundwater impacts were assessed in terms of changes in recharge to the underlying aquifers, depth to groundwater, direction of groundwater flow, and groundwater quality. Potential soil impacts considered were changes in topography, permeability, erosion potential, and soil quality.

Under the no action alternative, the assessment area in which potentially important impacts might occur was determined to be quality of surface water, groundwater, and soil. The

other potential impacts include changes in water use and effluent volumes. Maximum water use during continued cylinder maintenance operations at the site would be 73,000 gal/yr (276,000 L/yr).

A contaminant of concern for evaluating surface water, groundwater, and soil quality is uranium. Surface water and groundwater concentrations of contaminants are generally evaluated through comparison with the EPA MCLs, as given in Safe Drinking Water Act regulations (40 CFR Part 141), although these limits are only directly applicable “at the tap” of the water user. The water concentration value used for comparison in this EIS is 20 µg/L (i.e., the proposed MCL for uranium has now been finalized at 30 µg/L and will become effective in December 2003 [EPA 2003a]). The 20-µg/L value is used as a guideline for evaluating surface water and groundwater concentrations of uranium in this EIS, even though it is not directly applicable as a standard. There is no standard available for limiting concentrations of uranium in soil; a health-based value of 230 µg/g (EPA 1995), applicable for residential settings, is used as a guideline for comparison.

The nearest surface water to the Portsmouth site is Little Beaver Creek, which is a tributary to the Scioto River. The Scioto is used as a drinking water source. Because of very large dilution effects, even high levels of contaminants in Little Beaver Creek would not be expected to cause levels exceeding guidelines at the drinking water intakes of the Scioto River.

**5.1.2.4.1 Surface Water.** Potential impacts on the nearest receiving water at the site (Little Beaver Creek) were estimated for uranium released from hypothetical cylinder breaches occurring through 2039. The estimated maximum concentration of uranium in Little Beaver Creek would be 0.7 µg/L, considerably below the 20-µg/L level used for comparison.

Cylinder painting activities have been associated with increased toxicity in runoff at the Paducah site. If such an impact occurred at the Portsmouth site as a result of future cylinder painting, mitigating actions, such as treating runoff, might be required.

**5.1.2.4.2 Groundwater.** Groundwater in the vicinity of the Portsmouth site is used for domestic and industrial supplies. See Chapter 3 for a discussion of existing groundwater quality at the site. At Portsmouth, sampling results indicate that residential water supplies have not been affected by site operations. Activities associated with the no action alternative would not affect migration of existing groundwater contamination or impact off-site water supplies.

Potential impacts on groundwater quality from hypothetical releases of uranium from breached cylinders were also assessed. The maximum future concentration of uranium in groundwater directly below the Portsmouth site is estimated to be 5 µg/L, considerably below the 20-µg/L level used for comparison. It is estimated that if the rate of uranium migration was rapid, this concentration would occur sometime after 2070. A lower concentration would occur if uranium migration through the soil was slower than assumed for this analysis.

Calculations indicate that if no credit was taken for the reduction in corrosion as a result of cylinder painting and maintenance and if storage continued at the Portsmouth site indefinitely, uranium releases from future cylinder breaches occurring prior to about 2050 could result in a sufficient amount of uranium in the soil column to increase the groundwater concentration of uranium to 20 µg/L in the future (about 2100 or later). However, because of the ongoing maintenance program, it is not expected that breaches occurring prior to 2039 would be sufficient to increase the groundwater concentration to 20 µg/L at the site.

**5.1.2.4.3 Soil.** Potential impacts on soil that could receive contaminated rainwater runoff from the cylinder storage yards were estimated. The source is assumed to be uranium released from hypothetical breached cylinders. It is assumed that any releases from future cylinder painting activities would be controlled or treated to avoid soil contamination. The estimated maximum soil concentration is 1 µg/g for the Portsmouth site, considerably below the 230-µg/g guideline used for comparison.

### **5.1.2.5 Socioeconomics**

The potential socioeconomic impacts of operational activities at the Portsmouth site under the no action alternative would be low. No construction activities are planned for this site under this alternative. Operational activities would create 20 direct jobs and 40 total jobs per year. During operations, direct and total income would be \$0.8 million/yr and \$1.0 million/yr, respectively.

The employment created in the ROI for the Portsmouth site during continued cylinder maintenance would represent a change of less than 0.1 of a percentage point in the projected annual average growth in employment over the period 2004 to 2039. No migration into the ROI would occur, meaning that there would be no impact expected on local housing markets, local public service employment, or local public finances.

### **5.1.2.6 Ecology**

The no action alternative would have a negligible impact on ecological resources in the area of the Portsmouth site. Because no construction activities are planned, there would be no impacts on wetlands or on federal- and state-protected species.

The assessment results indicate that impacts to ecological resources from continued storage activities, including hypothetical cylinder breaches, would be negligible. Analysis of potential impacts was based on exposure of biota to airborne contaminants or contaminants released (e.g., from painting activities or from breached cylinders) to soil, groundwater, or surface water. Predicted concentrations of contaminants in environmental media were compared with benchmark values for toxic and radiological effects (see Appendix F). At the Portsmouth site, air, soil, and surface water concentrations would be below levels harmful to biota. However, as discussed in Section 5.1.2.4, cylinder painting activities may potentially result in future

reductions in surface water quality and may consequently result in impacts to aquatic biota downstream of the cylinder storage yards. Although groundwater uranium concentrations (5 to 20 µg/L) would be below the lowest effects level (150 µg/L) and below radiological benchmark levels ( $4.55 \times 10^3$  pCi/L), they would exceed the ecological screening value for surface water (2.6 µg/L). However, contaminants in groundwater discharging to a surface water body, such as a local stream, would be quickly diluted to negligible concentrations.

#### **5.1.2.7 Waste Management**

Under the no action alternative, operations at the Portsmouth site would generate relatively small amounts of LLW and LLMW (including PCB-containing wastes). The volume of LLW generated by continued storage activities would represent less than 1% of the annual generation at the site from all activities. The maximum annual amount of LLMW generation from stripping/painting operations at the Portsmouth site would generate less than 1% of the site's total annual LLMW load, resulting in negligible waste management impacts for this site. The overall impact on waste management operations from the no action alternative would be negligible.

#### **5.1.2.8 Resource Requirements**

Operations under the no action alternative would use electricity, fuel, concrete, steel and other metals, and miscellaneous chemicals. The total quantities of commonly used materials would be small compared with local sources and would not affect local, regional, or national availability of these materials. No strategic or critical materials are expected to be consumed. The anticipated utilities requirements would be within the supply capacities at the Portsmouth site. The required material resources would be readily available.

#### **5.1.2.9 Land Use**

Because no new construction is planned for the Portsmouth site under the no action alternative, no impacts to land use are expected.

#### **5.1.2.10 Cultural Resources**

Impacts to cultural resources at the Portsmouth site would not be likely under the no action alternative. The existing storage yards would continue to be used for cylinder storage. These yards are located in previously disturbed areas (graded during the original construction of the yards) and are unlikely to contain cultural properties or resources listed on or eligible for the NRHP. No new or expanded cylinder storage yards are proposed at Portsmouth under this alternative. Cylinder breaches are not expected to result in HF or criteria pollutant emissions sufficient to impact cultural resources (see Section 5.1.2.3).

### 5.1.2.11 Environmental Justice

A review of the potential human health and safety impacts anticipated under the no action alternative indicates that no disproportionately high and adverse effects to minority or low-income populations are expected on or in the vicinity of the Portsmouth site during DUF<sub>6</sub> cylinder storage. Although such populations occur in certain areas within the 50-mi (80-km) radius used to identify the maximum geographic extent of human health impacts (see Section 3.1.12), no noteworthy impacts to these populations are anticipated. The results of accident analyses for the no action alternative also did not identify high and adverse impacts to the general public; the risk of accidents (consequence × probability) yields less than 1 fatality for all accidents considered.

### 5.1.3 ETTP Site

The impacts described in this section are similar to those presented in Section 3.2 of the data compilation report for the ETTP site (Hartmann 1999b); however, they have been adjusted to account for changes in planned activities. For example, no construction activities are currently planned for the ETTP site under the no action alternative.

#### 5.1.3.1 Human Health and Safety

Potential impacts to human health and safety could result from operations during both routine conditions and accidents under the no action alternative. In general, the impacts during normal operations at the ETTP site would be limited to workers directly involved in handling cylinders. Under accident conditions, the health and safety of both workers and members of the general public around the site could potentially be affected.

##### 5.1.3.1.1 Normal Facility Operations

**Workers.** Cylinders containing DUF<sub>6</sub> emit low levels of gamma and neutron radiation. Involved workers would be exposed to this radiation when working near cylinders, such as during routine cylinder monitoring and maintenance activities, cylinder relocation and painting, and cylinder patching or repairing activities. It is estimated that an average of about 13 cylinder yard workers would be required at the ETTP site. These workers would be trained to work in a radiation environment, they would use protective equipment as necessary, and their radiation exposure levels would be measured and monitored by safety personnel at the sites. Radiation exposure of workers is required by law to be maintained ALARA and not to exceed 5,000 mrem/yr (10 CFR Part 835).

The radiation exposure of involved workers (cylinder yard workers) in future years through 2039 is estimated to be well within public health standards (10 CFR Part 835). It is estimated conservatively that if the same 13 workers conducted all cylinder management

activities, the average annual dose to individual involved workers would be about 410 mrem/yr. The estimated future doses do not account for standard ALARA practices that would be used to keep the actual doses as far below the limit as practicable. Thus, the future doses to workers are expected to be less than those estimated because of the conservatism incorporated into the assumptions and models used to generate the estimates. In fact, from 1990 through 1995, the average measured doses to cylinder yard workers at ETTP ranged from about 32 to 92 mrem/yr (Hodges 1996), and the maximum dose resulting from painting of 400 cylinders in 1998 was 107 mrem/yr (Cain 2002b). The radiation exposure of the noninvolved workers was estimated to be less than 0.048 mrem/yr.

It is estimated that the total collective dose to all involved workers at the ETTP site through 2039 would be about 200 person-rem. (The collective dose to noninvolved workers would be negligible [i.e., less than 0.01%] compared with the collective dose to involved workers.) This dose would be distributed among all of the workers involved with cylinder activities over the no action period. Although about 13 workers would be required each year, the actual number of different individuals involved over the period would probably be much greater than 13 because workers could be rotated to different jobs and could change jobs. This level of exposure could potentially result in less than 1 LCF (i.e., 0.1 LCF) among all the workers exposed, in addition to the cancer cases that would result from all other causes not related to activities under the no action alternative.

As discussed in Chapter 1 and Appendix B of this EIS, some portion of the DUF<sub>6</sub> inventory contains TRU and Tc contamination. The contribution of these contaminants to potential external radiation exposures under normal operations was evaluated on the basis of the bounding concentrations presented in Appendix B. The dose from these contaminants was estimated and compared with the dose from the depleted uranium and uranium decay products in the DUF<sub>6</sub>. It is estimated that under typical cylinder maintenance conditions, the TRU and Tc contaminants would make only a very small contribution to the radiation doses, amounting to approximately 0.2% of the dose from the depleted uranium and its decay products.

No impacts to involved workers from exposure to chemicals during normal operations are expected. Exposures to chemicals during cylinder painting operations would be monitored to ensure that airborne chemical concentrations were within applicable health standards that are protective of human health and safety. If planned work activities were likely to expose involved workers to chemicals, the workers would be provided with appropriate protective equipment as necessary.

Chemical exposures to noninvolved workers could result from airborne emissions of UO<sub>2</sub>F<sub>2</sub> and HF that would be dispersed from any cylinder breaches into the atmosphere and ground surfaces. The potential chemical exposures of noninvolved workers from any airborne releases during normal operations would be below levels expected to cause adverse effects. (The hazard index is estimated to be less than 0.1 for noninvolved workers.)

**General Public.** Potential health impacts to members of the general public could occur if material released from breached cylinders entered the environment and was transported from the

site through the air, surface water, or groundwater. Off-site releases of uranium and HF from breached cylinders are possible. However, the predicted off-site concentrations of these contaminants in the future would be much less than levels expected to cause adverse effects. Potential exposures of members of the general public would be well within public health standards. No adverse effects (LCFs or chemical effects) are expected to occur among members of the general public residing within 50 mi (80 km) of the ETTP site from continued DUF<sub>6</sub> storage activities.

It is estimated that if all the uranium and HF assumed to be released from breached cylinders through 2039 was dispersed from the site through the air, the total radiation dose to the general public (all persons within 50 mi [80 km]) would be less than 0.2 person-rem through 2039. This level of exposure would most likely result in zero cancer fatalities among members of the general public. For comparison, the average radiation dose from natural background and medical sources to the same population group over 40 years would be about  $1.3 \times 10^7$  person-rem. The maximum radiation dose to an individual near the site is estimated to be less than about 0.2 mrem/yr, well within health standards. Radiation doses to the general public are required by health regulations to be maintained below 10 mrem/yr from airborne sources (40 CFR Part 61) and below a total of 100 mrem/yr from all sources combined (DOE 1990). If an individual received the maximum estimated dose every year, the total dose would be about 8 mrem, resulting in an additional chance of dying from a latent cancer of about 1 in 250,000. No noncancer health effects from exposure to airborne uranium and HF releases are expected; the hazard index for an MEI is estimated to be less than 0.1. This means that the total exposure would be at least 10 times less than exposure levels that might cause adverse effects.

The material released from breached cylinders could also potentially be transported from the site in water, either in surface water runoff or by infiltrating the soil and contaminating groundwater. Members of the general public potentially could be exposed if they used this contaminated surface water or groundwater as a source of drinking water. The results of the surface water and groundwater analyses indicate that the maximum estimated uranium concentrations in surface water accessible to the general public and in groundwater beneath the site would be less than 20 µg/L (the EPA drinking water standard has now been finalized at 30 µg/L). Drinking water standards, meant to apply to water “at the tap” of the user, are set at levels protective of human health.

If a member of the public used contaminated water at the maximum concentrations estimated, adverse effects would be unlikely. Even if a member of the general public used contaminated surface water or groundwater as his or her primary water source, the maximum radiation dose in the future would be less than 0.5 mrem/yr. The corresponding risk to this individual of dying from a latent cancer would be less than 1 in 4 million per year. Noncancer health effects from exposure to possible water contamination are not expected; the estimated maximum hazard index for an individual assumed to use the groundwater is less than 0.05. This means that the total exposure would be 20 times less than the exposure that might cause adverse effects.

The groundwater analysis indicates that if no credit was taken for the reduction in cylinder corrosion rates as a result of cylinder maintenance and painting activities, the uranium

concentration in groundwater at the ETTP site could exceed 20 µg/L at some time in the future (see Section 5.1.3.4.2). This scenario is highly unlikely because ongoing cylinder inspections and maintenance would prevent significant releases from occurring, especially for as many cylinders as are assumed here (i.e., 213 breaches). Nonetheless, if contamination of groundwater used as drinking water occurred in the future, treating the water or supplying an alternative source of water might be required to ensure the safety of those potentially using the water.

#### 5.1.3.1.2 Facility Accidents

**Physical Hazards (On-the-Job Injuries and Fatalities).** Accidents occur in all work environments. In 2002, about 5,200 people in the United States were killed in accidents while at work, and approximately 3.9 million disabling work-related injuries were reported (National Safety Council 2002). Although all work activities would be conducted in as safe a manner as possible, there is a chance that workers could be accidentally killed or injured under the no action alternative, unrelated to any radiation or chemical exposures.

The numbers of accidental worker injuries and fatalities that might occur through 2039 were estimated on the basis of the number of workers required and on the historical accident fatality and injury rates in similar types of industries. It is estimated that a total of less than 1 accidental fatality (i.e., about 0.02, or about 2 chances in 100 of a single fatality) might occur at the ETTP site over the no action period evaluated. Similarly, a total of about 25 accidental injuries (defined as injuries resulting in lost workdays) are estimated. These rates are not unique to the activities required for the no action alternative but are typical of any industrial project of similar size and scope.

**Accidents Involving Radiation or Chemical Releases.** Accidents that could release radiation and chemicals from cylinders are possible under the no action alternative. Several types of accidents were evaluated, including those initiated by operational events, such as equipment or operator failure; external hazards; and natural phenomena, such as earthquakes. The assessment considered accidents ranging from those that would be reasonably likely to occur (estimated to occur one or more times in 100 years on average) to those that would be extremely rare (estimated to occur less than once in 1 million years on average). A listing of the cylinder accidents considered during storage is provided in the PEIS (DOE 1999a).

The accidents of most concern at the ETTP site would be accidents that could cause a release of UF<sub>6</sub> from cylinders. In a given accident, the amount potentially released would depend on the severity of the accident and the number of cylinders involved. Following a release, the UF<sub>6</sub> could combine with moisture in the air, forming gaseous HF and UO<sub>2</sub>F<sub>2</sub>, a soluble solid in the form of small particles. The depleted uranium and HF could be dispersed downwind, potentially exposing workers and members of the general public living near the site to radiation and chemical effects. The workers considered in the accident assessment were those noninvolved workers not immediately in the vicinity of the accident. Fatalities and injuries among involved workers would be possible if accidents were severe.

The estimated consequences of cylinder accidents are summarized in Table 5.1-4 for chemical effects and Table 5.1-5 for radiation effects. The impacts shown are the maximums estimated for the ETTP site. The impacts are presented separately for likely accidents and for rare, low-probability accidents estimated to result in the largest potential impacts. Although other accidents were evaluated (see Hartmann 1999b, Section 3.2.2), the estimated consequences of those other accidents would be less than the consequences of the accidents summarized in the tables. The estimated consequences are conservative in that they were based on the assumptions that at the time of the accident, the wind would be blowing in the direction of the greatest number of people. In addition, the effects of protective measures, such as evacuation, were not considered.

An exception to the discussion above would be a certain class of accidents that DOE investigated; however, because of security concerns, information about such accidents is not available for public review but is presented in a classified appendix to this EIS. All classified information will be presented to state and local officials, as appropriate.

**Chemical Effects.** The potential likely accident (defined as an accident that is estimated to occur one or more times in 100 years) that would cause the largest chemical health effects is the failure of a corroded cylinder, spilling part of its contents under dry weather conditions. Such an accident could occur, for example, during cylinder handling activities. It is estimated that about 24 lb (11 kg) of DUF<sub>6</sub> could be released in such an accident. The potential consequences from this type of accident would be limited to on-site workers. The off-site concentrations of HF and uranium were calculated to be less than the levels that would cause adverse effects from exposure to these chemicals, so that no adverse effects would occur among members of the general public. It is estimated that if such an accident did occur, up to 70 noninvolved workers might experience potential adverse effects from exposure to HF and uranium (mostly mild and transient effects, such as respiratory irritation or temporary decrease in kidney function). It is estimated that three noninvolved workers might experience potential irreversible adverse effects (such as lung or kidney damage). The number of fatalities following an HF or uranium exposure is expected to be somewhat less than 1% of the number of potential irreversible adverse effects (Policastro et al. 1997). Therefore, no fatalities are expected.

For assessment purposes, the estimated frequency of a corroded cylinder spill accident is assumed to be about once in 10 years. Therefore, over the no action period, about 4 such accidents are expected. The accident risk (defined as consequence  $\times$  probability) would be about 280 workers with potential adverse effects and 12 workers with potential irreversible adverse effects. The number of workers actually experiencing these effects would probably be considerably less, depending on the actual circumstances of the accidents and the individual chemical sensitivity of the workers. In previous accidental exposure incidents involving liquid UF<sub>6</sub> in gaseous diffusion plants, a few workers were exposed to amounts of uranium estimated to be approximately three times the guidelines used for assessing irreversible adverse effects in this EIS, and none actually experienced irreversible adverse effects (McGuire 1991).

**TABLE 5.1-4 No Action Alternative: Estimated Consequences of Chemical Exposures from Cylinder Accidents at the ETTP Site<sup>a</sup>**

Receptor <sup>b</sup>	Accident Scenario	Accident Frequency Category <sup>c</sup>	Potential Effect <sup>d</sup>	Consequence <sup>e</sup> (no. of persons affected)
<b><i>Likely Accidents</i></b>				
General public	Corroded cylinder spill, dry conditions	L	Adverse effects	0
	Corroded cylinder spill, dry conditions	L	Irreversible adverse effects	0
	Corroded cylinder spill, dry conditions	L	Fatalities	0
Noninvolved workers	Corroded cylinder spill, dry conditions	L	Adverse effects	0–70
	Corroded cylinder spill, dry conditions	L	Irreversible adverse effects	0–3
	Corroded cylinder spill, dry conditions	L	Fatalities	0
<b><i>Low Frequency-High Consequence Accidents</i></b>				
General public	Rupture of cylinders – fire	EU	Adverse effects	14–620
	Corroded cylinder spill, wet conditions – water pool	EU	Irreversible adverse effects	0
	Corroded cylinder spill, wet conditions – water pool	EU	Fatalities	0
Noninvolved workers	Rupture of cylinders – fire	EU	Adverse effects	0–770
	Corroded cylinder spill, wet conditions – rain	EU	Irreversible adverse effects	2–140
	Corroded cylinder spill, wet conditions – rain	EU	Fatalities	0–1

**Footnotes on next page.**

**TABLE 5.1-4 (Cont.)**

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- a The accidents listed are those estimated to result in the greatest impacts among all the accidents considered (except for certain accidents with security concerns). The site-specific impacts for a range of accidents at ETTP are given in Hartmann et al. (1999b).
- b Noninvolved workers are persons who work at the site but who are not involved in handling materials. Depending on the circumstances of the accident, injuries and fatalities among involved workers are possible for all accidents.
- c Accident frequencies: L = likely, estimated to occur one or more times in 100 years of facility operations ( $> 10^{-2}/\text{yr}$ ); EU = extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years of facility operations ( $10^{-4}$  to  $10^{-6}/\text{yr}$ ).
- d Potential adverse effects include exposures that could result in mild and transient injury, such as respiratory irritation. Potential irreversible adverse effects include exposures that could result in permanent injury (e.g., impaired organ function) or death. The majority of the adverse effects would be mild and temporary in nature. It is estimated that less than 1% of the predicted potential irreversible adverse effects would result in fatalities (see text).
- e The consequence is expressed as the number of individuals with a predicted exposure level sufficient to cause the corresponding health endpoint. The range of consequences reflects different atmospheric conditions at the time of an accident assumed to occur at the cylinder yard closest to the site boundary. In general, maximum risks would occur under the atmospheric conditions of a 1-m/s (2-mph) wind speed; minimum risks would occur under D stability with a 4-m/s (9-mph) wind speed. For both conditions, it was assumed that the wind would be blowing in the direction with the highest density of worker or public populations.

Accidents that are less likely to occur could have higher consequences. The potential cylinder accident at any of the sites estimated to result in the greatest total number of adverse chemical effects would be an accident involving several cylinders in a fire. It is estimated that if this accident occurred, up to 635 members of the general public and 770 noninvolved workers might experience adverse effects from HF and uranium exposure (mostly mild and transient effects, such as respiratory irritation or temporary decrease in kidney function). This accident is considered extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years. If the frequency is assumed to be once in 100,000 years, the accident risk over the no action period would be less than 1 adverse effect for both workers and members of the general public.

The potential cylinder accident estimated to result in the largest total number of irreversible adverse effects is a corroded cylinder spill under wet conditions, for which the UF<sub>6</sub> is assumed to be released into a pool of standing water. This accident is also considered extremely unlikely, expected to occur only between once in 10,000 years and once in 1 million years. It is estimated that if this accident did occur, no members of the general public but about 140 noninvolved workers might experience irreversible adverse effects (such as lung damage) from HF and uranium exposure. The number of fatalities would be somewhat less than 1% of the estimated number of potential irreversible adverse effects (Policastro et al. 1997). Thus, no fatalities are expected among the general public, but one fatality could occur among noninvolved

**TABLE 5.1-5 No Action Alternative: Estimated Consequences from Radiation Exposures for Cylinder Accidents at the ETTP Site<sup>a</sup>**

Receptor <sup>b</sup>	Accident Scenario	Accident Frequency Category <sup>c</sup>	MEI		Population	
			Dose (rem)	Lifetime Risk of LCF	Dose (person-rem)	Number of LCFs
<i>Likely Accidents</i>						
General public	Corroded cylinder spill, dry conditions	L	0.003	$1 \times 10^{-6}$	0.49	0.0002
Noninvolved workers	Corroded cylinder spill, dry conditions	L	0.077	$3 \times 10^{-5}$	1.3	0.0005
<i>Low Frequency-High Consequence Accidents</i>						
General public	Rupture of cylinders – fire	EU	0.013	$7 \times 10^{-6}$	73	0.04
Noninvolved workers	Rupture of cylinders – fire	EU	0.02	$8 \times 10^{-6}$	16	0.006

<sup>a</sup> The accidents listed are those estimated to have the greatest impacts among all accidents considered (except for certain accidents with a security concern). The impacts for a range of accidents at each of the three current storage sites are listed in Appendix D of the DUF<sub>6</sub> PEIS (DOE 1999a). The estimated consequences were based on the assumption that at the time of the accident, the wind would be blowing in the direction of the highest worker or public population density and that meteorological conditions would limit dispersion.

<sup>b</sup> Noninvolved workers are persons who work at the site but who are not involved in handling of materials. Depending on the circumstances of the accident, injuries and fatalities among involved workers are possible for all accidents.

<sup>c</sup> Accident frequencies: L = likely, estimated to occur one or more times in 100 years of facility operations ( $> 1 \times 10^{-2}/\text{yr}$ ); EU = extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years of facility operations ( $1 \times 10^{-4}$  to  $1 \times 10^{-6}/\text{yr}$ ).

workers (1% of 140). If this accident is assumed to occur once in 100,000 years, the accident risk through 2039 would be less than 1 (0.1) irreversible adverse health effect among workers and the general public combined.

**Radiation Effects.** Potential cylinder accidents could release uranium, which is radioactive in addition to being chemically toxic. The potential radiation exposures of members of the general public and noninvolved workers were estimated for the same cylinder accidents as those for which chemical effects were estimated (Table 5.1-5). For all cylinder accidents considered, the radiation doses from released uranium would be considerably below levels likely to cause radiation-induced effects among noninvolved workers and the general public and below the 25-rem total effective dose equivalent established by DOE as a guideline for assessing the adequacy of protection of public health and safety from potential accidents (DOE 2000c).

For the corroded cylinder spill accident (dry conditions), it is estimated that the radiation dose to a maximally exposed member of the general public would be less than 3 mrem (lifetime dose), resulting in an increased risk of death from cancer of about 1 in 1 million. The total population dose to the general public within 50 mi (80 km) would be less than 1 person-rem, most likely resulting in zero LCFs. Among noninvolved workers, the dose to an MEI would be 77 mrem, resulting in an increased risk of death from cancer of about 1 in 30,000. The total dose to all noninvolved workers would be about 1.3 person-rem. This dose to workers would result in zero LCFs. The risk (consequence  $\times$  probability) of additional LCFs among members of the general public and workers combined would be much less than 1 through 2039.

The cylinder accident estimated to result in the largest potential radiation doses would be an accident involving several cylinders in a fire. For this accident, it is estimated that the radiation dose to a maximally exposed member of the general public would be about 13 mrem, resulting in an increased risk of death from cancer of about 1 in 150,000. The total population dose to the general public within 50 mi (80 km) would be 73 person-rem, most likely resulting in zero LCFs. Among noninvolved workers, the dose to an MEI would be about 20 mrem, resulting in an increased risk of death from cancer of about 1 in 100,000. The total dose to all noninvolved workers would be about 16 person-rem. This dose to workers would result in zero LCFs. The risk (consequence  $\times$  probability) of additional LCFs among members of the general public and workers combined would be much less than 1 through 2039.

### **5.1.3.2 Transportation**

Continued cylinder storage under the no action alternative would have the potential to generate small amounts of LLW and LLMW during cylinder monitoring and maintenance activities. This material could require transportation to a treatment or disposal facility. Shipments would be made in accordance with all DOE and DOT regulations and guidelines. It is estimated that less than one waste shipment would be required each year. Because of the small number of shipments and the low concentrations of contaminants expected, the potential environmental impacts from these shipments would be negligible.

### **5.1.3.3 Air Quality and Noise**

The assessment of potential impacts to air quality under the no action alternative at the ETTP site included a consideration of air pollutant emissions from continued cylinder storage activities, including emissions from operations (cylinder painting and vehicle emissions) and HF emissions from breached cylinders. No cylinder yard construction activities are planned at the ETTP site. Atmospheric dispersion models were used to estimate the concentrations of criteria pollutants at the site boundaries: SO<sub>2</sub>, NO<sub>2</sub>, CO, O<sub>3</sub>, PM (PM<sub>10</sub> and PM<sub>2.5</sub>), and Pb. The site boundary concentrations were compared with existing air quality standards or with guidelines for pollutants that do not have corresponding standards as given in Chapter 3. The air concentrations of all criteria pollutants resulting from no action alternative activities would be less than 1% of the respective standards.

Painting activities could generate hydrocarbon emissions. No explicit air quality standard has been set for hydrocarbon emissions, but these emissions are associated with O<sub>3</sub> formation. Standards have been set for O<sub>3</sub>. For the ETTP site, hydrocarbon emissions from painting activities would be about 0.1% of the hydrocarbon emissions from the entire surrounding county. Because O<sub>3</sub> formation is a regional issue affected by emissions for an entire area, this small additional contribution to the county total would be unlikely to substantially alter the O<sub>3</sub> levels of the county. In addition, the actual frequency of cylinder painting would likely be much reduced in comparison with the frequency assumed for these analyses.

When credit is taken for reduced corrosion from better maintenance and painting, the estimated maximum 24-hour and annual average site boundary HF concentrations from hypothetical cylinder breaches occurring under the no action alternative at the ETTP site are 0.67 µg/m<sup>3</sup> and 0.084 µg/m<sup>3</sup>, respectively. Tennessee's primary HF 24-hour maximum average air standard is 2.9 µg/m<sup>3</sup> (there is no annual average standard). The estimated maximum 24-hour average would be about 23% of the standard.

Calculations indicate that if no credit was taken for the reduction in corrosion as a result of painting and continued maintenance and if storage continued at the ETTP site indefinitely, cylinder breaches occurring at the site by around 2020 could result in maximum 24-hour average HF concentrations at the site boundaries of 2.9 µg/m<sup>3</sup>, approximately equal to the Tennessee standard. However, because of the ongoing cylinder maintenance program, it is not expected that a breach rate this high would occur at the ETTP site.

No construction activities are planned under the no action alternative at the ETTP site; therefore, there would be no adverse noise impacts.

Continued storage operations could result in somewhat increased noise levels as a result of projected activities such as painting cylinders or repairing any infrequent cylinder breaches. However, it is expected that noise levels at off-site residences would not increase noticeably. Noise impacts are expected to be negligible under the no action alternative.

#### **5.1.3.4 Water and Soil**

Under the no action alternative, impacts on surface water, groundwater, and soil could result from continued storage of the cylinders. Important elements in assessing potential impacts on surface water include changes in runoff, floodplain encroachment, and water quality. Groundwater impacts were assessed in terms of changes in recharge to the underlying aquifers, depth to groundwater, direction of groundwater flow, and groundwater quality. Potential soil impacts considered were changes in topography, permeability, erosion potential, and soil quality.

For the no action alternative at the ETTP site, the assessment area in which potentially important impacts might occur was determined to be quality of surface water, groundwater, and soil. The other potential impacts include changes in water use and effluent volumes. Maximum water use during continued cylinder maintenance operations at the site would be 32,000 gal/yr (120,000 L/yr).

A contaminant of concern in evaluating surface water, groundwater, and soil quality is uranium. Surface water and groundwater concentrations of contaminants are generally evaluated through comparison with EPA MCLs, as given in Safe Drinking Water Act regulations (40 CFR Part 141), although these limits are only directly applicable “at the tap” of the water user. The water concentration value used for comparison in this EIS is 20 µg/L (the proposed MCL for uranium has now been finalized at 30 µg/L and became effective in December 2003 [EPA 2003a]). The 20-µg/L value is used as a guideline for evaluating surface water and groundwater concentrations of uranium in this EIS, even though it is not directly applicable as a standard. There is also no standard available for limiting concentrations of uranium in soil. A health-based value of 230 µg/g (EPA 1995), applicable for residential settings, is used as a guideline for comparison.

The nearest surface water to the ETTP site is Poplar Creek, which is a tributary of the Clinch River. The Clinch River is used as a drinking water source. Because of very large dilution effects, even high levels of contaminants in Poplar Creek would not be expected to cause concentrations to exceed guidelines at the drinking water intakes of the Clinch River.

**5.1.3.4.1 Surface Water.** Potential impacts on the nearest receiving water at the site (i.e., Poplar Creek) were estimated for uranium released from hypothetical cylinder breaches occurring through 2039. The estimated potential maximum concentration of uranium in Poplar Creek was calculated to be 0.02 µg/L, considerably below the 20-µg/L level used for comparison.

Cylinder painting activities have been associated with increased toxicity in runoff at the Paducah site. If such an impact occurred at the ETTP site as a result of future cylinder painting, mitigating actions, such as treating runoff, might be required.

**5.1.3.4.2 Groundwater.** Groundwater in the vicinity of the ETTP site discharges to nearby surface waters and is not known to be used as a domestic or industrial source. (See Chapter 3 for a discussion of existing groundwater quality at the site.) Activities associated with the no action alternative would not affect migration of existing groundwater contamination or impact off-site water supplies.

Potential impacts on groundwater quality from hypothetical releases of uranium from breached cylinders were assessed, taking credit for reduced corrosion from better maintenance and painting. The maximum future concentration of uranium in groundwater directly below the ETTP site is estimated to be 7 µg/L, which is considerably below the 20-µg/L level used for comparison. It was estimated that if the rate of uranium migration was rapid, this concentration would occur sometime after 2070. A lower concentration would occur if uranium migration through the soil was slower than assumed for this analysis.

Calculations indicate that if no credit was taken for the reduction in corrosion resulting from cylinder painting and maintenance and if storage continued at the ETTP site indefinitely, uranium releases from future cylinder breaches occurring before about 2025 could result in a

sufficient amount of uranium in the soil column to increase the groundwater concentration of uranium to 20 µg/L in the future. The groundwater concentration would not actually reach 20 µg/L at the site until about 2100 or later. However, because of the ongoing maintenance program, it is expected that breaches occurring before 2039 would not be sufficient to increase the groundwater concentration to 20 µg/L at the site.

**5.1.3.4.3 Soil.** Potential impacts on soil that could receive contaminated rainwater runoff from the cylinder storage yards were estimated. The contaminant source is assumed to be uranium released from hypothetical breached cylinders. It is assumed that any releases from future cylinder painting activities would be controlled or treated to avoid soil contamination. The estimated maximum soil concentration is 3 µg/g for the ETTP site, considerably below the 230-µg/g guideline used for comparison.

### **5.1.3.5 Socioeconomics**

The potential socioeconomic impacts of activities at the ETTP site under the no action alternative would be low. No construction activities are planned for the site under the no action alternative, and operational activities would create 30 direct jobs and 90 total jobs per year. During operations, direct and total income would be \$3.1 million/yr and \$4.2 million/yr, respectively.

The employment created in the ROI for the ETTP site during continued cylinder maintenance activities would represent a change of less than 0.1 of a percentage point in the projected annual average growth in employment over the period 2004 to 2039. No migration into the ROI would occur because of the ETTP activities; thus, no impacts are expected on local housing markets, local public service employment, or local public finances.

### **5.1.3.6 Ecology**

The no action alternative would have a negligible impact on ecological resources in the area of the ETTP site. Because no construction activities are planned, there would be no new impacts on wetlands or on federal- and state-protected species.

The assessment results indicate that impacts to ecological resources from continued storage activities, including hypothetical cylinder breaches, would be negligible. Analysis of potential impacts was based on exposure of biota to airborne contaminants or contaminants released to soil, groundwater, or surface water (e.g., from painting activities or from breached cylinders). Predicted concentrations of contaminants in environmental media were compared with benchmark values of toxic and radiological effects (see Appendix F). At the ETTP site, air, soil, and surface water concentrations would be below levels harmful to biota. However, as discussed in Section 5.1.3.4, cylinder painting activities may potentially cause future reductions in surface water quality, and they may consequently result in impacts to aquatic biota downstream of the cylinder storage yards. Although groundwater uranium concentrations

(7 to 20 µg/L) would be below the lowest effects level (150 µg/L) and below radiological benchmark levels ( $4.55 \times 10^3$  pCi/L), they would exceed the ecological screening value for surface water (2.6 µg/L). However, contaminants in groundwater discharging to a surface water body, such as a local stream, would be quickly diluted to negligible concentrations.

#### **5.1.3.7 Waste Management**

Under the no action alternative, operations at the ETTP site would generate relatively small amounts of LLW and LLMW. The volume of LLW generated by continued storage activities would represent less than 1% of the annual generation at the site from all activities. The maximum annual amount of LLMW generation from stripping/painting operations at the ETTP site would generate less than 1% of the site's total annual LLMW load, resulting in negligible waste management impacts for this site. Thus, the overall impact on waste management operations from the no action alternative would be negligible.

#### **5.1.3.8 Resource Requirements**

Operations under the no action alternative would use electricity, fuel, concrete, steel and other metals, and miscellaneous chemicals. The total quantities of commonly used materials would be small compared with local sources and would not affect local, regional, or national availability of these materials. No strategic or critical materials are expected to be consumed. The anticipated utilities requirements would be within the supply capacities at the ETTP site. The required material resources would be readily available.

#### **5.1.3.9 Land Use**

Because no new construction is planned for the ETTP site, no impacts on land use are anticipated for the no action alternative.

#### **5.1.3.10 Cultural Resources**

Impacts to cultural resources at the ETTP site would not be likely under the no action alternative. The existing cylinder storage yards would continue to be used for cylinder storage. These yards are currently located in previously disturbed areas (graded during the original construction of the yards) and are unlikely to contain cultural properties or resources listed on or eligible for listing on the NRHP. No new or expanded cylinder storage yards are proposed at ETTP. Cylinder breaches are not expected to result in HF or criteria pollutant emissions sufficient to impact cultural resources (see Section 5.1.2.3).

### 5.1.3.11 Environmental Justice

A review of the potential human health and safety impacts anticipated under the no action alternative indicates that no disproportionately high and adverse effects to minority or low-income populations are expected on or in the vicinity of the ETTP site during DUF<sub>6</sub> cylinder storage. Although such populations occur in certain areas within the 50-mi (80-km) radius used to identify the maximum geographic extent of human health impacts (see Section 3.2.12), no noteworthy impacts to these populations are anticipated. The results of accident analyses for the no action alternative also did not identify high and adverse impacts to the general public; the risk of accidents (consequence × probability) yields less than 1 fatality for all accidents considered.

## 5.2 PROPOSED ACTION ALTERNATIVES

This section presents the estimated potential environmental impacts for the proposed action alternatives, including:

- Impacts from construction of a new cylinder storage yard at two possible locations at the Portsmouth site (Section 5.2.1);
- Impacts from construction of the conversion facility at the three alternative locations within the Portsmouth site (Section 5.2.2);
- Impacts from operation of the conversion facility at the three alternative locations (Section 5.2.3);
- Impacts at ETTP from preparing cylinders for transportation to Portsmouth (Section 5.2.4);
- Impacts from the transportation of UF<sub>6</sub> cylinders from ETTP to Portsmouth, and uranium conversion products and waste materials from the Portsmouth site to a disposal facility (Section 5.2.5);
- Impacts associated with the potential sale and use of HF and CaF<sub>2</sub> (Section 5.2.6);
- Impacts that would occur if the cylinders at ETTP were shipped to Paducah for conversion rather than to Portsmouth (Section 5.2.7); and
- Impacts from expanded plant operations, including extending the operational period and increasing throughput (Section 5.2.8).

In general, within each technical area, impacts are discussed for the construction and operation of the facility at the preferred location (Location A) as well as for two alternative locations (Locations B and C). The time period considered is a construction period of approximately 2 years and an operational period of 18 years.

### 5.2.1 Portsmouth Site — Cylinder Storage Yard Construction Impacts

As discussed in Chapter 2, it may be necessary to construct an additional yard at Portsmouth for the storage of the ETTP cylinders, depending on when and at what rate the ETTP cylinders are shipped. DOE will not know if a new yard is required, or if existing storage yard space could be used for the ETTP cylinders, until some time in the future. The potential environmental impacts from the construction of a new cylinder storage yard are included in this section to account for current uncertainties. Two possible areas for new cylinder yard construction are evaluated, as shown in Figure 2.2-4. (Also identified in Figure 2.2-4 is an existing concrete pad being evaluated for temporary storage of the ETTP cylinders.) Both areas are adjacent to current DOE cylinder storage yards. Proposed Area 1 consists of three smaller sections, with a total area of about 5.5 acres (2.2 ha). Proposed Area 2 consists of two smaller sections, with a total area of about 6.3 acres (2.5 ha). A new yard would be constructed of concrete and would be similar to other concrete yards constructed at the Portsmouth site.

#### 5.2.1.1 Human Health and Safety — Normal Construction Activities

**5.2.1.1.1 Radiological Impacts.** Proposed Area 1 includes three separate sections in close proximity to the existing cylinder yards (X-745E and X-745C). While constructing concrete pads in this area, construction workers, due to proximity to the DUF<sub>6</sub> cylinders, would be exposed to external radiation. On the basis of thermoluminescence dosimeter (TLD) monitoring data at these cylinder yards and the assumption that a worker would spend a total of 500 hours close to the cylinders, potential radiation exposure is estimated to be about 30 mrem.

Proposed Area 2 includes two separate sections. The smaller section to the north is close to existing cylinder yard X-745C; the larger one to the south is away from existing cylinder yards. Construction workers working in the smaller section would receive radiation exposure from cylinders in the X-745C yards. On the basis of the assumption that the total exposure duration would be the same here as at Proposed Area 1 (500 hours), the potential radiation dose to a construction worker would be about 30 mrem. The exposures estimated are conservative because of the use of the TLD data taken from the cylinder yards. Furthermore, the construction work is expected to last for only 3 months (Folga 2003); therefore, the actual time a worker would spend at a distance close to the cylinder yard boundary would be less than 500 hours. For comparison, the average annual dose received by cylinder yard workers was 64 mrem/yr in year 2001 (DOE 2002e). The radiation dose limit set to protect the general public is 100 mrem/yr (DOE 1990), and workers are limited to a dose of 5,000 mrem/yr (10 CFR 835).

**5.2.1.1.2 Chemical Impacts.** Chemical exposures during construction of the new Portsmouth cylinder storage yard are expected to be low and mitigated by using personal protective equipment and engineering controls to comply with OSHA PELs that are applicable for construction activities.

**5.2.1.2 Human Health and Safety — Accidents**

The risk of on-the-job fatalities and injuries to cylinder storage yard construction workers was calculated by using industry-specific statistics from the BLS, as reported by the National Safety Council (2002). Annual fatality and injury rates from the BLS construction industry division were used for the 3-month construction phase. Construction of the cylinder storage yard is estimated to require approximately 21 or 24 FTEs over 3 months for Areas 1 or 2, respectively. No on-the-job fatalities are predicted during the cylinder storage yard construction phase; however, approximately 1 injury is predicted (Table 5.2-1).

**5.2.1.3 Air Quality and Noise**

**5.2.1.3.1 Air Quality Impacts.** Emissions of criteria pollutants — SO<sub>2</sub>, NO<sub>x</sub>, CO, and PM (PM<sub>10</sub> and PM<sub>2.5</sub>) — and of VOCs would occur during the construction period, which would last about 3 months. These emissions would include fugitive dust emissions from earthmoving activities and exhaust emissions from heavy equipment and commuter/delivery vehicles. The total emissions from fugitive and exhaust sources are estimated to be 0.02 ton (0.02 t) for SO<sub>2</sub>, 0.28 ton (0.25 t) for NO<sub>x</sub>, 0.19 ton (0.17 t) for CO, 2.96 tons (2.69 t) for PM<sub>10</sub>, 0.46 ton (0.42 t) for PM<sub>2.5</sub>, and 0.08 ton (0.07 t) for VOCs (Folga 2003). Estimated maximum pollutant concentrations during construction are shown in Table 5.2-2.

All of the pollutant concentration increments would remain below NAAQS and SAAQS. For SO<sub>2</sub>, NO<sub>2</sub>, and CO, it is predicted that maximum concentration increments would be about 2% of their applicable standards. The highest concentration increment would occur for 24-hour average PM<sub>10</sub>, which is predicted to be about 49% of the standard for PM<sub>10</sub>. The highest concentration increment for PM<sub>2.5</sub> is predicted to be about 12% of its standard.

To obtain the total concentrations for comparison with applicable air quality standards, the modeled concentration increments were added to measured background values (see Table 3.1-3). The total concentrations for SO<sub>2</sub>, NO<sub>2</sub>, CO, and PM<sub>10</sub> are estimated to be below 91% of applicable ambient standards. Total PM<sub>2.5</sub> concentrations are estimated to be near or above applicable ambient standards. In fact, concentrations of PM<sub>2.5</sub> at most statewide monitoring stations either approach or are above the standards. Construction activities should be conducted so as to minimize potential impacts on ambient air quality. Water could be sprayed on disturbed areas frequently, as needed, and dust suppressant or pavement could be applied to roads with frequent traffic.

**TABLE 5.2-1 Potential Impacts to Human Health from Physical Hazards during Construction of an Additional Cylinder Storage Yard at the Portsmouth Site**

Area	Impacts to Cylinder Storage Yard Workers <sup>a</sup>	
	Incidence of Fatalities	Incidence of Injuries
1	0.003	1
2	0.003	1

<sup>a</sup> Potential hazards were estimated for all cylinder storage yard workers over the 3-month construction phase.

Source: Injury and fatality rates used in calculations were taken from National Safety Council (2002).

**TABLE 5.2-2 Maximum Air Quality Impacts at the Construction Site Boundary Due to Emissions from Activities Associated with Construction of a New Cylinder Storage Yard at the Portsmouth Site**

Candidate Area	Pollutant <sup>a</sup>	Averaging Time	Concentration (µg/m <sup>3</sup> )			NAAQS and SAAQS	Percent of NAAQS/SAAQS <sup>e</sup>		
			Maximum Increment <sup>b</sup>	Back-ground <sup>c</sup>	Total <sup>d</sup>		Increment	Total	
1	SO <sub>2</sub>	3 hours	29.5	307	337	1,300	2.3	25.9	
		24 hours	5.5	110	115	365	1.5	31.6	
		Annual	0.2	18.7	18.9	80	0.2	23.6	
	NO <sub>2</sub>	Annual	0.2	54.7	54.9	100	0.2	54.9	
	CO	1 hour	68.0	13,400	13,500	40,000	0.2	33.7	
		8 hours	15.7	4,780	4,800	10,000	0.2	48.0	
	PM <sub>10</sub>	24 hours	63.0	64.0	127	150	42.0	84.7	
		Annual	2.4	32.0	34.4	50	4.7	68.7	
	PM <sub>2.5</sub>	24 hours	7.4	57.5	64.9	65	11.4	99.9	
		Annual	0.36	24.1	24.5	15	2.4	163	
	2	SO <sub>2</sub>	3 hours	29.1	307	336	1,300	2.2	25.9
			24 hours	6.7	110	117	365	1.8	32.0
			Annual	0.1	18.7	18.8	80	0.1	23.5
		NO <sub>2</sub>	Annual	0.2	54.7	54.9	100	0.2	54.9
		CO	1 hour	59.5	13,400	13,500	40,000	0.1	33.6
8 hours			19.7	4,780	4,800	10,000	0.2	48.0	
PM <sub>10</sub>		24 hours	72.8	64.0	137	150	48.6	91.2	
		Annual	1.7	32.0	33.7	50	3.4	67.4	
PM <sub>2.5</sub>		24 hours	7.5	57.5	65.0	65	11.5	100	
		Annual	0.3	24.1	24.4	15	1.7	162	

<sup>a</sup> Emissions are from equipment and vehicle engine exhaust, except for PM<sub>10</sub> and PM<sub>2.5</sub>, which are also from soil disturbance.

<sup>b</sup> Data represent the maximum concentration increments estimated, except that the fourth- and eighth-highest concentration increments estimated are listed for 24-hour PM<sub>10</sub> and PM<sub>2.5</sub>.

<sup>c</sup> See Table 3.1-3.

<sup>d</sup> Total equals the maximum modeled concentration increment plus background concentration.

<sup>e</sup> The values in the next-to-last column are maximum concentration increments as a percent of NAAQS and SAAQS. The values presented in the last column are total concentration increments as a percent of NAAQS and SAAQS.

The potential impacts of PM (PM<sub>10</sub> and PM<sub>2.5</sub>) released from near-ground level would be limited to the immediate vicinity of the construction site boundaries — areas that the general public is expected to occupy only infrequently. The PM concentrations would decrease rapidly with distance from the source. At the nearest residence (about 1.5 km [0.9 mi] west of the construction Area 2), predicted concentration increments would be less than 2% of the highest concentration increments at construction site boundaries.

Potential air quality impacts due to emissions from new cylinder yard construction activities were predicted to be comparable between the two alternative areas. However, potential impacts for Area 2 would be slightly higher than those for Area 1 if construction of the new cylinder yard occurred simultaneously with construction of the conversion facility.

**5.2.1.3.2 Noise Impacts.** During construction, the commuting/delivery vehicular traffic around the construction site would generate intermittent noise. However, the contribution to noise from these intermittent sources would be limited to the immediate vicinity of the traffic route and would be minor in comparison with the contribution from the continuous noise sources, such as a compressor or bulldozer, during construction. Noise sources during the construction of the cylinder yard would include site clearing followed by concrete padding. Noise levels from these activities would be comparable to those from other construction sites of similar size.

Average noise levels for construction equipment range from 76 dB(A) for a pump to 89 dB(A) for a scraper (Harris Miller Miller & Hanson, Inc. [HMMH] 1995). To estimate noise levels at the nearest residence, it was assumed that the two noisiest pieces of equipment would operate simultaneously (HMMH 1995). A scraper and a heavy truck operating continuously typically generate noise levels of 89 and 88 dB(A), respectively, at a distance of 15 m (50 ft) from the source, which results in a combined noise level of about 91.5 dB(A) at a distance of 15 m (50 ft).

The nearest residences to the proposed cylinder yard Areas 1 and 2 are located about 1.6 km (1.0 mi) and 1.5 km (0.9 mi) west-southwest and west of them, respectively. An analysis of the potential noise impacts was performed for the construction of cylinder yard Area 2, which is closer to the nearest residence. Noise levels decrease about 6 dB per doubling of distance from the point source because of the way sound spreads geometrically over an increasing distance. Thus, construction activities would result in an estimated noise level of about 52 dB(A) at the nearest residence. This level would be 47 dB(A) as DNL if it is assumed that construction activities would be limited to an 8-hour daytime shift. This value is below the EPA guideline of 55 dB(A) as DNL for residential zones (see Section 3.1.3.4), which was established to prevent interference with activity, annoyance, or hearing impairment. This 47-dB(A) estimate is probably an upper bound because it does not account for other types of attenuation, such as air absorption and ground effects due to terrain and vegetation. If other attenuation mechanisms were considered, noise levels at the nearest residence would decrease further. The resulting noise levels would be barely noticeable at the nearest residence.

Most of these construction activities would occur during the day, when noise is tolerated better than at night because of the masking effect of background noise. Nighttime noise levels

would drop to the background levels of a rural environment because construction activities would cease at night.

If construction of the cylinder yard would occur simultaneously with construction of the conversion facility, noise levels at the nearest residence would increase by about 3 dB at most, but resultant noise levels would still be below the EPA guideline level. At the end of the 3-month construction period, noise impacts associated with construction of the cylinder yard would cease to exist.

#### **5.2.1.4 Water and Soil**

Construction and operation of a new cylinder storage yard at Portsmouth could impact surface water, groundwater, and soil resources. Potential impacts are discussed below for the two alternative locations, Areas 1 and 2.

##### **5.2.1.4.1 Proposed Area 1**

**Surface Water.** Construction of the storage yard would require about 0.75 million gal (2.8 million L) of water. This water would be obtained from groundwater resources. Because all water needs would be met by using groundwater, there would be no direct impacts to surface waters.

Construction of the storage yard at Portsmouth would also generate sanitary wastewater (0.11 million gal [0.42 million L]). If it was discharged at a constant rate over a year, the rate of release would be about 0.2 gal/min (0.8 L/min). After treatment in the existing wastewater treatment facility, the wastewater would be released to Little Beaver Creek or piped directly to the Scioto River under an existing NPDES permit. For average flow conditions in Little Beaver Creek (940 gal/min [3,558 L/min]), contaminant concentrations would be diluted by a factor of about 4,700. Additional dilution would occur at the confluence with Big Beaver Creek and again at the confluence with the Scioto River. Even under low-flow conditions, contaminants would be diluted by a factor of about 140,000.

Although water resources would not be impacted by withdrawals, surface waters could be affected indirectly by receiving contaminated runoff from the construction sites. By following good construction practices (e.g., stockpiling materials away from surface drainage paths, covering construction materials with tarps, and cleaning up any spills thoroughly as soon as they occur), indirect impacts to surface water quality could be minimized.

**Groundwater.** Construction of the storage yard would require about 0.75 million gal (2.8 million L) of water. Construction is expected to be completed in about 3 months. However, even if it was completed in 1 year, and the rate of water use was constant, a withdrawal rate of about 1.4 gal/min (5.4 L/min) would be required. Current water use at the Portsmouth facility is

about 4,312 million gal/yr (16,323 million L/yr). The maximum capacity of the well system is about 13,900 million gal/yr (52,617 million L/yr). The water required for yard construction would, therefore, be about 0.02% of the existing use and 0.005% of the existing capacity. Groundwater withdrawal for construction would, therefore, have no measurable impact on the groundwater system beneath Portsmouth.

Construction of the storage yards at Portsmouth would also affect the permeability of the surface soil and its ability to transmit water as recharge to the underlying aquifers. However, impacts to recharge would not be measurable because the total area of land that would be permanently altered by construction of the yards would be very small (about 5.5 acres [2.2 ha] or about 0.2% of the total site area). Similarly, the quality of groundwater beneath the storage yards could be affected by construction activities through infiltration of surface water contaminated from spills of construction materials. By following good engineering and construction practices (e.g., covering chemicals with tarps to prevent contact with rainfall, promptly and thoroughly cleaning up spills, and providing retention basins to catch and hold any contaminated runoff), impacts to groundwater quality would be minimal.

**Soils.** Construction of the cylinder storage yard at Portsmouth would affect a total of 5.5 acres (2.2 ha). This amount of land is small (about 0.2% of the land area available), and impacts would be negligible. By following good engineering and construction practices, impacts to soil quality would also be minimal.

**Operations.** Operation of the proposed new cylinder storage areas at Portsmouth could affect water and soil resources, primarily from breached cylinders releasing a maximum of 4 lb (2 kg) of uranium over a 4-year period. As discussed above, approximately 5,000 cylinders containing DUF<sub>6</sub> would be stored in the new yards. This number of cylinders is less than 32% of the current inventory (about 16,000 cylinders). Because the number of additional cylinders stored would be less than the current inventory, impacts associated with their storage would be correspondingly smaller than the impacts predicted for continued cylinder storage at Portsmouth under the no action alternative (Section 5.1). For such conditions, impacts to surface water would not be measurable; a maximum groundwater concentration of 5 µg/L would occur somewhat before 2080 (assuming that the uranium in the groundwater was fairly mobile [Tomasko 1997]), and concentrations in the soil adjacent to the yards would be below the recommended EPA guideline of 230 µg/g for residential soil and 6,100 µg/g for industrial soil (EPA 2003a). These impacts could be reduced further by surrounding the storage yards with drainage ditches that could capture potentially contaminated runoff from the new yards and divert it for treatment, as needed.

**5.2.1.4.2 Proposed Area 2.** The quantity of water needed to construct the two storage yards for Proposed Area 2 would be about 0.85 million gal (3.2 million L). About 0.13 million gal (0.50 million L) of sanitary wastewater would be generated. Because the resources required to construct these yards are about the same as those discussed above for Proposed Area 1, the impacts would be about the same.

### 5.2.1.5 Socioeconomics

The potential socioeconomic impacts of construction and operation of a new cylinder yard at Portsmouth would be low. Construction activities would create short-term employment (60 direct jobs, 150 total jobs). Direct and total personal income from construction would be \$1.7 million and \$5.6 million, respectively.

The employment created in the ROI for the Portsmouth site would represent a change of less than 0.1 of a percentage point in the projected average annual growth in employment over the period of operations. Since no population in-migration is expected during either construction or operation, there would be no impact on local housing, local public finances, or local public service employment.

### 5.2.1.6 Ecology

Construction of a yard at Proposed Area 1 would result in the disturbance of approximately 6.1 acres (2.5 ha) of land, due to construction-related activities, and in the loss of previously disturbed managed grassland vegetation. The yard would not replace undisturbed natural communities. Managed grassland communities comprise most of the vegetation on the Portsmouth site, within the Perimeter Road. Thus, the loss of up to 6.1 acres (2.5 ha) would represent a minor decrease in this vegetation type on the Portsmouth site. Immediate replanting of areas disturbed by temporary construction-related activities with native species would help reduce impacts to vegetation.

Construction at Proposed Area 1 would primarily impact wildlife species commonly associated with managed grassland communities. Wildlife would be disturbed by land clearing, noise, and human presence. Wildlife with restricted mobility, such as burrowing species or juveniles of nesting species, would be destroyed during land clearing activities. More mobile individuals would relocate to adjacent areas with similar habitat, which is commonly available in the area. Wildlife in nearby woodland communities might also be disturbed by noise up to 91.5 dB(A) at 15 m (50 ft) during the construction period.

Wetlands do not occur within the areas that would be disturbed at Proposed Area 1. Therefore construction would not directly impact wetlands. Wetlands downgradient of the construction sites could be impacted by storm water runoff; however, the implementation of good construction practices, including erosion and sediment controls, would minimize impacts to surface water quality. Because surface water impacts from breached cylinders during use of the storage yards would be negligible, impacts to wetlands from cylinder storage would not be expected. The increase in impervious surface and discharge of storm water runoff from the yards could result in a greater fluctuation in flows within the stream northeast of the yards, across Perimeter Road. However, because the yard would not be located adjacent to the stream and only a small portion of the watershed would be involved, such effects would likely be very small.

Construction would not be expected to result in direct or indirect impacts to any federal- or state-listed species. Although the riparian forest along the stream north of Perimeter

Road might include trees that can be used by Indiana bats (federal- and state-listed as endangered) for roosting, this area has not been identified as summer roosting habitat. Although noise associated with construction activities might disturb wildlife, Indiana bats that might use habitats near the Portsmouth site are currently exposed to noise and other effects of human disturbance. Consequently, these effects related to construction activities would be expected to be minor.

Construction of a yard at Proposed Area 2 would result in the disturbance of approximately 6.9 acres (2.8 ha) of land, due to construction-related activities. Impacts to vegetation and wildlife would be similar to those for Proposed Area 1. Two intermittent streams originate in the area northeast of “A” Road and flow to the west, converging to form the stream immediately north of Location A. Storage yard construction would result in the elimination of the northernmost of these streams and partial filling of the other. Placement of a storage yard in this area could also result in a greater fluctuation in flows in downstream areas and reduced water quality. Impacts to federal- or state-listed species would not be expected.

**5.2.1.7 Waste Management**

The construction of a cylinder storage yard at Portsmouth would generate a total of about 353 yd<sup>3</sup> (270 m<sup>3</sup>) of nonhazardous solid waste and 130,000 gal (470,000 L) of nonhazardous sanitary wastewater (Folga 2003). Only minimal impacts would result from these construction-generated wastes.

**5.2.1.8 Resource Requirements**

A new storage yard would be an 8-in. (20-cm) thick concrete pad on top of a 12-in. (30-cm) layer of crushed stone. Table 5.2-3 provides an estimate of the construction requirements. None of the identified construction resources is in short supply, and all should be readily available in the local region.

**5.2.1.9 Land Use**

Both locations being considered for a storage yard are in an area of existing structures and on a site with more than 150 structures. Constructing an additional storage yard on the Portsmouth site would involve very slight modifications of existing land use. The resulting storage yard would be consistent with the heavy

**TABLE 5.2-3 Materials/Resources Consumed during Construction of a Cylinder Storage Yard at the Portsmouth Site**

Materials/Resources	Total Consumption	Unit
<i>Utilities</i>		
Water	840,000	gal
<i>Solids</i>		
Concrete	7,400	yd <sup>3</sup>
Aggregate (gravel)	11,000	yd <sup>3</sup>
Special coatings	33,000	yd <sup>2</sup>
<i>Liquids</i>		
Fuel	2.8 × 10 <sup>3</sup>	gal

industrialized land use currently found at the Portsmouth site — a consequence of producing enriched uranium and its DUF<sub>6</sub> by-product, as well as storing the latter. As a consequence, no land use impacts are anticipated as a result of construction of a new yard.

#### **5.2.1.10 Cultural Resources**

The construction of a new cylinder storage yard at Portsmouth could potentially impact cultural resources. The amount of data available on cultural resources within the project area at Portsmouth is not sufficient to determine whether or not the construction would adversely impact significant cultural resources. Consequently, the possibility of adverse effects on cultural resources as a result of the construction cannot be excluded.

Archaeological and architectural surveys were undertaken for Portsmouth in 1996. The findings of these surveys have not been finalized and have not received concurrence from the Ohio SHPO. Past ground disturbance resulting from grading and construction make it unlikely that intact archaeological remains are present at the proposed locations for a new cylinder storage yard (Anderson 2002). However, unless these findings receive SHPO concurrence, a separate archaeological assessment of the proposed location for the construction of the cylinder storage yard (conducted by a qualified professional archaeologist) would be required to ensure that cultural material is not present and that Section 106 obligations under the National Historic Preservation Act (NHPA) of 1966 are met. If archaeological resources were encountered and a site or sites were determined to be significant, a mitigation plan would have to be developed and executed in consultation with the Ohio SHPO prior to construction. In general, mitigation of an adverse effect of yard construction on cultural resources could entail site avoidance, site monitoring during construction, or site excavation/data recovery. No buildings or structures are located at the proposed construction locations for a new cylinder storage yard; thus, no impacts to historic structures are anticipated.

No Native American traditional cultural properties have been identified at Portsmouth to date. Consultations with the SHPO and Native American groups have been initiated (Appendix G). If construction of a cylinder storage yard would result in an adverse effect on any such property identified, appropriate mitigation, as determined through continued consultation, would have to be undertaken before construction could begin.

#### **5.2.1.11 Environmental Justice**

The evaluation of environmental justice impacts associated with constructing a cylinder storage yard at the Portsmouth site is based on the identification of high and adverse impacts in other impact areas considered in this EIS, followed by a determination if those impacts would affect minority and low-income populations disproportionately. Disproportionate impacts could take two forms: (1) when the environmental justice population is present at a higher percentage in the affected area than in the reference population (i.e., the state in which a potentially impacted population occurs) and (2) when the environmental justice population is more

susceptible to impacts than the population as a whole. In either case, high and adverse impacts are a necessary precondition for environmental justice concerns in an EIS.

Analyses of impacts from constructing a cylinder storage yard do not indicate the presence of high and adverse impacts for any of the other impact areas considered in this EIS (see Sections 5.2.1.1 through 5.2.1.10). Despite the presence of disproportionately high percentages of both minority and low-income populations within 50 mi (80 km) of the proposed cylinder yard, no environmental justice impacts from constructing this yard are anticipated. Similarly, no evidence indicates that minority or low-income populations would experience high and adverse impacts from the proposed construction in the absence of such impacts in the population as a whole.

## **5.2.2 Portsmouth Site — Conversion Facility Construction Impacts**

This section discusses the potential environmental impacts during construction of a conversion facility at the three alternative locations within the Portsmouth site. When completed, the conversion facility would occupy approximately 10 acres (4 ha), including process and support buildings and parking areas. However, up to 65 acres (26 ha) of land might be disturbed during construction, including temporary lay-down areas (areas for staging construction material and equipment or for excavated material) and areas for utility access. Some of the disturbed areas would not be adjacent to the construction area. The disturbed area would include access roads, rail lines, and utility corridors.

The preferred conversion facility location (Location A) is adjacent to the RCRA X-616 chromium sludge lagoon unit and its related monitoring wells, an area that has a deed notice and associated restrictions. The X-616 chromium sludge lagoon and monitoring wells are, at their nearest point, located approximately 100 ft (30 m) from the DUF<sub>6</sub> conversion facility site boundary. To prevent direct impacts and ensure the integrity of this area, it will be clearly marked and identified, a suitable buffer zone will be established around it, and the entry of conversion facility personnel or equipment into these areas will be prohibited. To prevent indirect impacts, best available technologies will be identified and implemented to prevent the transport of air particulates and liquid effluents or discharges originating at the conversion facility site from trespassing at or impacting the RCRA unit. Technologies to prevent air particulate transport could include covering and/or spraying exposed bare soil, prohibiting open burning, and using windbreaks around construction areas. Technologies to prevent impacts from liquid discharges could include storm water and sediment controls such as silt fences, sediment traps, and seeding; secondary containment around liquid storage areas; and prompt cleanup of any inadvertent spills.

### **5.2.2.1 Human Health and Safety — Normal Construction Activities**

**5.2.2.1.1 Radiological Impacts.** Of the three alternative locations at the Portsmouth site, none are close to the existing cylinder storage yards. According to site-specific external radiation

data (DOE 2001d), external gamma radiation at all three locations is close to the background level. Therefore, construction workers at Locations A, B, or C are not expected to incur any external radiation from the depleted uranium currently stored in the cylinder yards.

However, if Proposed Area 2 is selected as the new yard and the larger lot to the south is used, potential external exposure could result from constructing the conversion facility at Location A, the preferred alternative. The incurred radiation dose would be less than 60 mrem/yr, calculated by using the TLD data from cylinder yard X-745C and an exposure duration of 1,000 hours per year. Once the surrounding walls of the conversion facility were built, radiation exposure would be further reduced because of the shielding provided by the walls. No radiological impacts would be expected at alternative Locations B and C from the new cylinder yard because of the greater distance between them and the yard.

**5.2.2.1.2 Chemical Impacts.** Chemical exposures during construction at the Portsmouth site are expected to be low and mitigated by using personal protective equipment and engineering controls to comply with OSHA PELs that are applicable for construction activities. No differences among the three alternative locations are expected.

#### **5.2.2.2 Human Health and Safety — Accidents**

The risk of on-the-job fatalities and injuries to conversion facility construction workers would not be dependent on the location of the facility. The estimated injuries and fatalities were calculated by using industry-specific statistics from the BLS, as reported by the National Safety Council (2002). Annual fatality and injury rates from the BLS construction industry division were used for the 20-month construction phase. Construction of the conversion facility is estimated to require approximately 164 FTEs per year. For all three alternative locations, no on-the-job fatalities are predicted during the construction phase; however, approximately 11 injuries are predicted (Table 5.2-4).

#### **5.2.2.3 Air Quality and Noise**

**5.2.2.3.1 Air Quality Impacts.** Currently, detailed information on the location of facility boundaries is available only for the preferred Location A. For modeling air quality impacts at Locations B and C, the proposed facilities were assumed to be located in the middle of the alternative locations.

Emissions of criteria pollutants — SO<sub>2</sub>, NO<sub>x</sub> (emissions are in NO<sub>x</sub> but the ambient air quality standards are in NO<sub>2</sub>), CO, and PM (PM<sub>10</sub> and PM<sub>2.5</sub>) — and of VOCs would occur during the construction period. These emissions would include fugitive dust emissions from earthmoving activities and exhaust emissions from heavy equipment and commuter/delivery vehicles. The annual emissions of criteria pollutants and VOCs expected during facility

**TABLE 5.2-4 Potential Impacts to Human Health from Physical Hazards during Conversion Facility Construction and Operations at the Portsmouth Site**

Activity	Impacts to Conversion Facility Workers <sup>a</sup>			
	Incidence of Fatalities		Incidence of Injuries	
	Construction	Operations	Construction	Operations
Conversion to U <sub>3</sub> O <sub>8</sub>	0.04	0.10	11	142
Conversion to U <sub>3</sub> O <sub>8</sub> (without ETTP cylinders)	0.04	0.08	11	110

<sup>a</sup> Potential hazards were estimated for all conversion facility workers over the entire construction (20 months) and operation (18 and 14 years, with and without ETTP cylinders, respectively) phases.

Source: Injury and fatality rates used in calculations were taken from National Safety Council (2002).

construction are presented in Table 5.2-5. Estimated maximum pollutant concentrations during construction are shown in Table 5.2-6 for the three alternative locations.

All of the pollutant concentration increments would remain below NAAQS and SAAQS. For SO<sub>2</sub>, NO<sub>2</sub>, and CO, it is predicted that concentration increments would be below 32% of their applicable standards. The highest concentration increment would occur for 24-hour average PM<sub>10</sub>, which is predicted to be up to about 79% of the standard for PM<sub>10</sub>. The highest concentration increment for PM<sub>2.5</sub> is predicted to be less than 43% of its standard.

To obtain the total concentrations for comparison with applicable air quality standards, the modeled PM<sub>10</sub> concentration increments were added to measured background values (Table 3.1-3). The total concentrations for SO<sub>2</sub>, NO<sub>2</sub>, and CO would be below 86% of applicable ambient standards. Total PM<sub>10</sub> and PM<sub>2.5</sub> concentrations are estimated to either approach or be above their applicable ambient standards. In fact, concentrations of PM<sub>2.5</sub> at most statewide monitoring stations either approach or are above the standard. Predicted PM (PM<sub>10</sub> and PM<sub>2.5</sub>) concentration increments at the site boundaries would be high for the following two reasons: (1) the conversion facility would be constructed outside the current fenced site boundaries, so the general public would have access,<sup>2</sup> and (2) wind speeds measured at the on-site meteorological tower were relatively low, about half the speed of those at the Paducah GDP. Accordingly, construction activities should be conducted so as to minimize potential impacts on ambient air quality. Water could be sprayed on disturbed areas frequently, as needed, and/or dust suppressant or pavement could be applied to roads with frequent traffic.

<sup>2</sup> Formerly, the general public had access to the existing fenced boundaries. However, since the September 11, 2001, terrorist attack, site access for the general public has been restricted indefinitely to the DOE property boundaries.

**TABLE 5.2-5 Annual Criteria Pollutant and Volatile Organic Compound Emissions from Construction of the Conversion Facility at the Portsmouth Site**

Emission Source	Emission Rate (tons/yr)					
	SO <sub>2</sub>	NO <sub>x</sub>	CO	VOCs	PM <sub>10</sub>	PM <sub>2.5</sub>
Exhaust	1.7	24.9	16.8	7.0	2.5	2.5 <sup>a</sup>
Fugitive	– <sup>b</sup>	–	–	–	15.8 <sup>c</sup>	2.3 <sup>c</sup>

<sup>a</sup> For exhaust emissions, PM<sub>2.5</sub> emissions were conservatively assumed to be 100% of PM<sub>10</sub> emissions.

<sup>b</sup> A dash indicates no emissions.

<sup>c</sup> Fugitive dust emissions were estimated under the assumption that the conversion facility construction area would continuously disturb about 8.5 acres (3.4 ha). This is the maximum amount of the approximate 10-acre (4-ha) facility footprint that would be disturbed at one time. A conventional control measure of water spraying with an emission control efficiency of 50% would be applied over the disturbed area. For fugitive dust emissions from earthmoving activities, PM<sub>2.5</sub> emissions were assumed to be 15% of PM<sub>10</sub> emissions (EPA 2002).

Source: Folga (2003).

The potential impacts of PM (PM<sub>10</sub> and PM<sub>2.5</sub>) released from near-ground level would be limited to the immediate vicinity of the site boundaries — areas that the general public is expected to occupy only infrequently. The PM concentrations would decrease rapidly with distance from the source. At the nearest residence just off DOE's southern boundary (about 0.9 km [0.6 mi] from alternative Location B), predicted concentration increments would be less than 10% of the highest concentration increments at the site boundaries.

Among the three alternative locations, potential air quality impacts due to emissions from construction activities would be similar, with the highest at Location B and the lowest at Location A, as shown in Table 5.2-6. However, as mentioned previously, locations of facility boundaries for Locations B and C are assumed arbitrarily; thus, results for the two alternative locations should be interpreted in that context.

**5.2.2.3.2 Noise Impacts.** Noise levels from construction would be similar among the alternative locations. During construction, the commuting/delivery vehicular traffic around the facilities would generate intermittent noise. However, the contribution to noise from these intermittent sources would be limited to the immediate vicinity of the traffic route and would be minor in comparison with the contribution from continuous noise sources, such as compressors

**TABLE 5.2-6 Maximum Air Quality Impacts at the Construction Site Boundary Due to Emissions from Activities Associated with Construction of the Conversion Facility at the Portsmouth Site**

Location	Pollutant <sup>a</sup>	Averaging Time	Concentration ( $\mu\text{g}/\text{m}^3$ )						
			Maximum Increment <sup>b</sup>	Back-ground <sup>c</sup>	Total <sup>d</sup>	NAAQS and SAAQS	Percent of NAAQS/SAAQS <sup>e</sup>		
							Increment	Total	
A	SO <sub>2</sub>	3 hours	55.4	307	362	1,300	4.3	27.9	
		24 hours	13.7	110	124	365	3.8	33.9	
		Annual	1.5	18.7	20.2	80	1.8	25.2	
	NO <sub>2</sub>	Annual	21.8	54.7	76.5	100	21.8	76.5	
	CO	1 hour	1,100	13,400	14,500	40,000	2.7	36.2	
		8 hours	405	4,780	5,190	10,000	4.1	51.9	
	PM <sub>10</sub>	24 hours	95.8	64.0	160	150	63.9	107	
		Annual	16.7	32.0	48.7	50	33.3	97.3	
	PM <sub>2.5</sub>	24 hours	19.7	57.5	77.2	65	30.3	119	
		Annual	4.3	24.1	28.4	15	28.7	189	
	B	SO <sub>2</sub>	3 hours	63.5	307	371	1,300	4.9	28.5
			24 hours	15.2	110	125	365	4.2	34.3
			Annual	2.1	18.7	20.8	80	2.7	26.0
		NO <sub>2</sub>	Annual	31.5	54.7	86.2	100	31.5	86.2
		CO	1 hour	1,180	13,400	14,600	40,000	2.9	36.4
8 hours			441	4,780	5,220	10,000	4.4	52.2	
PM <sub>10</sub>		24 hours	118	64.0	182	150	78.6	121	
		Annual	25.7	32.0	57.7	50	51.4	115	
PM <sub>2.5</sub>		24 hours	24.0	57.5	81.5	65	37.0	126	
		Annual	6.5	24.1	30.6	15	43.1	204	
C		SO <sub>2</sub>	3 hours	56.6	307	364	1,300	4.4	28.0
			24 hours	13.0	110	123	365	3.6	33.7
			Annual	1.8	18.7	20.5	80	2.2	25.6
		NO <sub>2</sub>	Annual	26.4	54.7	81.1	100	26.4	81.1
		CO	1 hour	1,130	13,400	14,500	40,000	2.8	36.3
	8 hours		411	4,780	5,190	10,000	4.1	51.9	
	PM <sub>10</sub>	24 hours	115	64.0	179	150	76.7	119	
		Annual	21.5	32.0	53.5	50	43.0	107	
	PM <sub>2.5</sub>	24 hours	24.2	57.5	81.7	65	37.3	126	
		Annual	5.4	24.1	29.5	15	36.1	197	

Footnotes on next page.

**TABLE 5.2-6 (Cont.)**

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- <sup>a</sup> Emissions are from equipment and vehicle engine exhaust, except for PM<sub>10</sub> and PM<sub>2.5</sub>, which are also from soil disturbance.
  - <sup>b</sup> Data represent the maximum concentration increments estimated, except that the fourth- and eighth-highest concentration increments estimated are listed for 24-hour PM<sub>10</sub> and PM<sub>2.5</sub>.
  - <sup>c</sup> See Table 3.1-3.
  - <sup>d</sup> Total equals maximum modeled concentration plus background concentration.
  - <sup>e</sup> The values presented in the next-to-last column are maximum concentration increments as a percent of NAAQS and SAAQS. The values in the last column are total concentration increments as a percent of NAAQS and SAAQS.

or bulldozers during construction. Sources of noise during the construction of the conversion facility would include standard commercial and industrial activities for moving earth and erecting concrete and steel structures. Noise levels from these activities would be comparable to those from other construction sites of similar size.

The noise levels would be highest during the early phases of construction, when heavy equipment would be used to clear the site. This early phase of construction would last for about 6 months of the entire construction period of 1.5 years. Average noise levels for typical construction equipment range from 76 dB(A) for a pump, to 85 dB(A) for a bulldozer, to 101 dB(A) at peak for a pile driver (HMMH 1995). To estimate noise levels at the nearest residence, it was assumed the two noisiest pieces of equipment would operate simultaneously. A scraper and a heavy truck operating continuously typically generate noise levels of 89 and 88 dB(A), respectively, at a distance of 15 m (50 ft) from the source (HMMH 1995),<sup>3</sup> which results in a noise level of about 91.5 dB(A) at a distance of 15 m (50 ft).

The nearest residences to alternative Locations A, B, and C are located west, south-southeast, and northeast of them, respectively. The nearest residence, located about 0.9 km (0.6 mi) south-southeast of Location B and just off DOE's southern boundary, was selected as the receptor for the analysis of potential noise impacts. Noise levels decrease about 6 dB per doubling of distance from the point source because of the way sound spreads geometrically over an increasing distance. Thus, construction activities, which result in a combined noise level of about 91.5 dB(A) at a distance of 15 m (50 ft), would result in an estimated noise level of about 56 dB(A) at the nearest residence. This level would be 51 dB(A) as DNL, if it is assumed that construction activities would be limited to an 8-hour daytime shift. This 51-dB(A) estimate is below the EPA guideline of 55 dB(A) as DNL for residential zones (see Section 3.1.3.4), which was established to prevent interference with activity, annoyance, and hearing impairment. The 51-dB(A) estimate is probably an upper bound because it does not account for other types of attenuation, such as air absorption and ground effects due to terrain and vegetation. If only ground effects were considered (HMMH 1995), more than 10 dB(A) of attenuation would occur at the nearest residence, which would result in about 41 dB(A).

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<sup>3</sup> Pile drivers were excluded because piles would not be required for buildings at the site.

Most of these construction activities would occur during the day, when noise is tolerated better than at night because of the masking effects of background noise. The resulting noise levels would be barely noticeable to the nearest residence for all three alternative locations. Nighttime noise levels would drop to the background levels of a rural environment because construction activities would cease at night.

#### **5.2.2.4 Water and Soil**

Construction of a conversion plant at Portsmouth would disturb land, use water, and produce liquid wastes. Impacts from constructing a conversion plant on surface water, groundwater, and soil resources are discussed below. Because site-specific impacts were not identified, impacts to water and soil at alternative Locations A, B, and C would be the same.

**5.2.2.4.1 Surface Water.** Construction of a conversion facility at the Portsmouth site would result in increased runoff to nearby surface waters because soil and vegetation would be replaced by either buildings or paved areas. The amount of increased runoff from the new, impermeable land surface would be negligible compared with the existing area that contributes to runoff (less than about 2% of the site area). None of the construction activities would measurably affect the existing floodplains.

During construction, water would be needed. Peak water consumption would be 5,500 gal/d (20,800 L/d) or 2.0 million gal/yr (7.6 million L/yr). This water would include 1,500 gal/d (5,700 L/d) for construction use and 4,000 gal/d (15,100 L/d) for the workforce. Water requirements for construction would be independent of the specific location selected at Portsmouth. Although the Portsmouth site has the ability to use water from the Scioto River, almost all water is currently obtained from four on-site wells and 31 off-site wells. Because construction water needs would be met by using groundwater, there would be no impacts on surface water resources.

Wastewater would also be produced during construction. For the assumed workforce, about 4,000 gal/d (15,140 L/d) or 1.5 million gal/yr (5.7 million L/yr) of sanitary wastewater would be generated. There would be no sanitary wastewater discharge to the environment because portable toilets would be used.

**5.2.2.4.2 Groundwater.** Potential impacts to groundwater could occur during construction. These impacts could include changes in effective recharge to underlying aquifers, changes in the depth to groundwater, changes in the direction of groundwater flow, and changes in groundwater quality.

Current water use at Portsmouth is about 4,312 million gal/yr (16,323 million L/yr). The maximum capacity of the well system is about 13,900 million gal/yr (52,617 million L/yr). If the rate of withdrawal was constant over time, about 3.8 gal/min (14.4 L/min) would be needed to construct the conversion plant. This rate of withdrawal would be about 0.05% of the annual

average withdrawal and 0.01% of the excess well capacity. Direct impacts from such a withdrawal on groundwater resources (e.g., depth to groundwater and flow direction) would not be measurable and would be the same for all three alternative locations.

Construction could also affect the permeability of the surface soil and its ability to transmit water as recharge to the underlying aquifers. Because of the small associated operational areas (less than 2% of the land area available), these differences in permeability would produce changes in the effective recharge that would not be measurable. Similarly, the quality of groundwater beneath the selected location could be affected by surface construction activities through infiltration of contaminated surface water from spills. These impacts would be indirect because there would be no direct releases of contaminants to groundwater. Indirect contamination could result from the mobilization of exposed chemicals by precipitation, followed by infiltration of contaminated runoff water. Following good engineering and construction practices and implementing storm water and erosion control measures would minimize impacts to groundwater quality.

**5.2.2.4.3 Soils.** Potential impacts on soil could occur during construction and postulated accident scenarios. These impacts would include changes in topography, permeability, quality, and erosion potential.

Construction of a conversion facility at Portsmouth would disturb about 65 acres (26 ha) of land. Location A, however, has only 26 acres (11 ha) available. An additional 39 acres (16 ha) would be required for the disturbed area. An additional 19 acres (8 ha) of land would be required at the 46-acre (19-ha) Location B site. No additional land would be needed for the 78-acre (32-ha) Location C site. Because the conversion plant sites are relatively flat, there would be no significant changes in topography, and the maximum amount of land needed for construction would be small relative to the total land available at the site (less than about 2%). Erosion potential would increase during construction; the impacts, however, would be local and temporary.

Construction activities could also affect the quality of the land at the location selected for the conversion facility. The impacts could result from spills and other construction activities that could release contaminants to the surface. By following good engineering and construction practices (e.g., covering chemical stockpiles, cleaning up spills thoroughly as soon as they occur, and installing detention basins), impacts to soil quality would be minimized.

### **5.2.2.5 Socioeconomics**

The socioeconomic analysis covers the effects from construction on population, employment, income, regional growth, housing, and community resources in the ROI around the Portsmouth site. Impacts from construction are summarized in Table 5.2-7. The socioeconomic impacts are not dependent on the location of the conversion facility; thus, the impacts would be the same for alternative Locations A, B, and C.

The potential socioeconomic impacts would be relatively small. Construction activities would create direct employment of about 190 people in the peak construction year and about 90 additional indirect jobs in the ROI. Construction activities would increase the annual average employment growth rate by about 0.1 percentage point over the duration of construction. A conversion facility at Portsmouth would produce about \$9 million in personal income in the peak year of construction.

In the peak year of construction, it is estimated that about 300 people would in-migrate to the ROI. However, in-migration would only marginally affect population growth and would only require about 4% of vacant rental housing in the peak year. No significant impact on public finances would occur as a result of in-migration, and fewer than 5 local public service employees would be required to maintain existing levels of service in the various local public service jurisdictions in Pike and Scioto Counties.

**5.2.2.6 Ecology**

Potential impacts to vegetation, wildlife, wetlands, and threatened and endangered species that could result from the construction of a conversion facility are described below. Additional information regarding wetlands and federally listed species can be found in Van Lonkhuyzen (2004).

**5.2.2.6.1 Vegetation.** Existing vegetation within the disturbed area would be destroyed during land clearing activities. Construction of a conversion facility at any of the three alternative locations at the Portsmouth site is not expected to threaten the local population of any species. Replanting disturbed areas with native species would

**TABLE 5.2-7 Socioeconomic Impacts from Construction of the Conversion Facility at the Portsmouth Site**

Impact Area	Construction Impacts <sup>a</sup>
Employment	
Direct	190
Total	290
Income (millions of 2002 \$)	
Direct	5.3
Total	8.9
Population (no. of new ROI residents)	300
Housing (no. of units required)	110
Public finances (% impact on fiscal balance)	
Cities in Pike County <sup>b</sup>	0.3
Pike County	0.2
Schools in Pike County <sup>c</sup>	0.3
Cities in Scioto County <sup>d</sup>	0.2
Scioto County	0.2
Schools in Scioto County <sup>e</sup>	0.2
Public service employment (no. of new employees)	
Pike County	
Police officers	0
Firefighters	0
General	1
Physicians	0
Teachers	1
Scioto County	
Police officers	0
Firefighters	0
General	2
Physicians	0
Teachers	1
No. of new staffed hospital beds	
Pike County	1
Scioto County	1

<sup>a</sup> Impacts are shown for the peak year of construction (2005).

<sup>b</sup> Includes impacts that would occur in the cities of Waverly and Piketon.

<sup>c</sup> Includes impacts that would occur in Waverly and Pike County school districts.

<sup>d</sup> Includes impacts that would occur in the City of Portsmouth.

<sup>e</sup> Includes impacts that would occur in New Boston, Portsmouth, Wheelersburg, and Scioto County school districts.

comply with Executive Order 13148, *Greening the Government through Leadership in Environmental Management* (U.S. President 2000). Erosion of exposed soil at construction sites could reduce the effectiveness of restoration efforts and create sedimentation downgradient of the construction site. However, the implementation of standard erosion control measures, installation of storm water retention ponds, and immediate replanting of disturbed areas with native species would help minimize impacts to vegetation. Deposition of fugitive dust resulting from construction activities could adversely affect vegetation; however, the use of control measures to reduce dust production could minimize impacts (see Section 5.2.2.3).

Constructing a facility at Location A, the preferred alternative, would result in the loss of about 10 acres (4 ha) of previously disturbed managed grassland and old field vegetation. The facility would not replace undisturbed natural communities. Managed grassland and old field communities comprise most of the vegetation on the Portsmouth site, within the Perimeter Road. The loss of 10 acres (4 ha) would, therefore, represent a minor decrease in these habitats on the Portsmouth site. This area represents about 38% of the area available at the 26-acre (11-ha) Location A. The total area of construction-related disturbance, however, would be approximately 65 acres (26 ha) in size. Although construction-related activities would primarily affect managed grassland and old field vegetation, impacts to the wooded areas at this location would also occur during the construction period. Construction of the conversion facility access road and rail lines would result in impacts to several wooded areas within Location A. These areas, east of Building X-744-S (and "C" Road), north of Building X-744-U, and northwest of Building X-744-T, primarily support sapling and mature black locust. Additional impacts to wooded areas could occur unless temporary construction areas, such as lay-down areas, were positioned outside Location A in adjacent, previously disturbed areas. If facility construction required the disturbance of all of Location A, the entire wooded area at this location, including the riparian forest community, would potentially be eliminated. Riparian forest represents only a small portion (only about 4%) of the Portsmouth site. The construction of utility lines, access roads, and rail lines would extend beyond Location A and would result in additional impacts to vegetation. Construction of rail lines west of Location A would primarily affect managed grassland vegetation. However, impacts to the riparian forest community along the intermittent stream might occur near the point of connection of the new rail line with the existing line east of Perimeter Road.

Construction at Location B would affect previously disturbed managed grassland vegetation. The type of vegetation community affected by construction would not depend on the positioning of the facility within this 46-acre (19-ha) location. However, impacts to vegetation in the western portion of this location would be small because buildings and paved areas are already located there. A facility 10 acres (4 ha) in size would occupy approximately 22% of the area available at this location. However, the total area expected to be disturbed would likely require the use of areas outside Location B for construction-related activities.

The vegetation communities affected by construction at Location C would depend on the placement of the facility within the 78-acre (32-ha) area; however, construction at Location C would not directly affect undisturbed natural communities. A facility 10 acres (4 ha) in size would occupy only 13% of the area available at this location. Facility construction would primarily affect previously disturbed managed grassland vegetation. The wooded areas in the

west-central portion of Location C could be avoided by placing the facility in other areas of the location. Impacts to these wooded areas from construction-related activities could be avoided by positioning of the facility in the northern portion of Location C.

**5.2.2.6.2 Wildlife.** Wildlife would be disturbed by land clearing, noise, and human presence. Construction noise, up to 91.5 dB(A) at 15 m (50 ft), would disturb wildlife in the vicinity of the construction site during daylight construction hours. Wildlife with restricted mobility, such as burrowing species or juveniles of nesting species, would be destroyed during land clearing activities. More mobile individuals would relocate to adjacent available areas with suitable habitat. Population densities, and thus competition for food and nesting sites, would increase in these areas, potentially reducing the survivability or reproductive capacity of displaced individuals. Some wildlife species would be expected to recolonize replanted areas near the conversion facility following completion of construction. Construction of a conversion facility at any of the three locations is not expected to threaten the local population of any wildlife species because similar habitat would be available near the site.

Constructing a conversion facility at Location A would primarily impact those species commonly associated with managed grasslands and old field communities. Large areas of similar habitat would be available nearby. Construction would also affect the habitat of woodland species, such as neotropical migratory birds. Woodland habitat would be impacted by construction of the access roads and rail lines, and additional woodland habitat could be eliminated unless temporary construction areas were positioned outside Location A. However, the wooded areas that would be affected by rail line and access road construction are small and previously disturbed and do not represent a mature forest community. Similar habitat would be available nearby. The construction of the new rail line adjacent to the riparian woodland along the northern margin of Location A could limit the suitability of this habitat for some wildlife species. If facility construction required the disturbance of all of Location A, the entire wooded habitat at this location would potentially be eliminated. The construction of utility lines, access roads, and rail lines would extend beyond Location A and would result in additional impacts to wildlife habitat.

Constructing a conversion facility at Location B would affect the habitat of those species commonly associated with managed grasslands. Similar habitat would be abundant in areas near the Portsmouth site. Impacts to wildlife would be minimized in the western portion of Location B since buildings already exist there.

Facility construction at Location C would also affect the habitat of species associated with managed grasslands. However, similar habitat would be abundant in other areas of the Portsmouth site. Impacts to species associated with the open woodland areas in the west-central portion of Location C could be avoided by placing the facility in the northern portion of this location. Construction of a facility immediately adjacent to the woodlands could reduce the habitat's suitability for some wildlife species. However, the wooded areas that would be affected are small and previously disturbed and do not represent mature forest communities.

**5.2.2.6.3 Wetlands.** Wetlands could be affected by filling or draining during construction. Impacts to wetlands due to alteration of surface water runoff patterns, soil compaction, or groundwater flow could occur if the conversion facility was located immediately adjacent to wetland areas. Impacts to wetlands could be minimized, however, by maintaining a buffer area around them during facility construction. Executive Order 11990, *Protection of Wetlands* (U.S. President 1977a), requires federal agencies to minimize the destruction, loss, or degradation of wetlands and to preserve and enhance the natural and beneficial uses of wetlands. 10 CFR Part 1022 sets forth DOE regulations for implementing Executive Order 11990 as well as Executive Order 11988, *Floodplain Management* (U.S. President 1977b). Unavoidable impacts to wetlands that are within the jurisdiction of the USACE might require a CWA Section 404 Permit, which would trigger the requirement for a CWA 401 water quality certification from Ohio. An approved mitigation plan might be required prior to the initiation of construction.

Surface water sources are not expected to be used to meet water requirements during construction. Changes in groundwater as a result of withdrawing water for construction and the increase in the impermeable surface related to facility construction would be small to negligible (Section 5.2.2.4). Therefore, except for the potential local indirect impacts noted above, impacts to regional wetlands due to groundwater or surface water levels or flow patterns are not expected to occur.

Construction of a conversion facility at Location A would result in impacts to the small wetland located within the drainage channel in the east-central portion of this location (Figure 5.2-1). Construction of the south access road connecting to "C" Road would eliminate much of this wetland. Approximately 950 ft<sup>2</sup> (88 m<sup>2</sup>) of palustrine emergent wetland would likely be eliminated by direct placement of fill material. In addition, portions of the facility fence line cross this wetland, and a small building would be adjacent to the wetland. Portions of this wetland that are not filled might be indirectly affected by an altered hydrologic regime because of the proximity of construction, possibly resulting in a decreased frequency or duration of inundation or soil saturation, and potential loss of hydrology necessary to sustain wetland conditions, which would result in likely changes to the wetland plant and animal communities. However, the impact may potentially be avoided by an alternative routing of the entrance road, or mitigation may be developed in coordination with the appropriate regulatory agencies. Placement of temporary construction areas outside Location A might be necessary to avoid additional impacts to this wetland. Construction of a conversion facility could also affect the hydrology of the intermittent stream along the northern margin of Location A. The increase in impervious surface and discharge of storm water runoff could result in a greater fluctuation in flows, with a greater amplitude in high flows and extended low flows within the stream. However, because the facility would not be located adjacent to the stream and only a small portion of the watershed would be involved, impacts would likely be small. Downstream wetlands could be affected by sedimentation during construction; however, the implementation of erosion control measures would reduce the likelihood of impacts. Direct impacts to the stream would occur if a storm water outfall structure was located within the streambed.

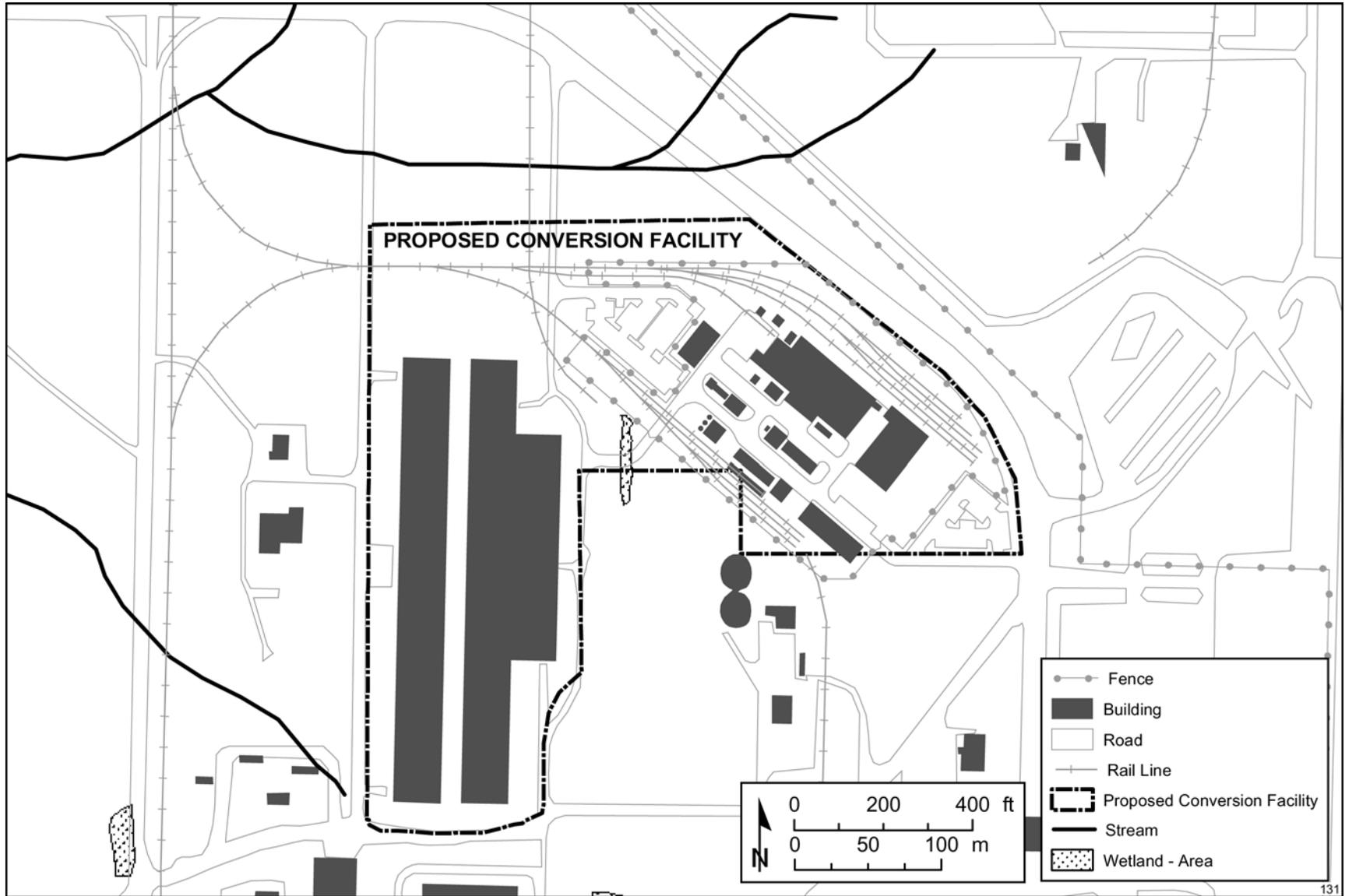


FIGURE 5.2-1 Wetlands within Location A at the Portsmouth Site

Construction of a facility at Location B would not result in direct impacts to wetlands. However, the hydrologic characteristics of wetlands in areas next to and south of this location could be indirectly affected by adjacent construction, possibly resulting in a decreased frequency or duration of inundation or soil saturation. Indirect impacts could be minimized by maintaining a buffer near adjacent wetlands. Downstream wetlands could be affected by sedimentation during construction; however, the implementation of erosion control measures would reduce the likelihood of sediment impacts.

Construction of a facility at Location C would not result in direct impacts to wetlands. However, the hydrologic characteristics of the wetland next to the northwest boundary of this location could be indirectly affected by adjacent construction, possibly resulting in a decreased frequency or duration of inundation or soil saturation. Indirect impacts could be minimized by maintaining a buffer near adjacent wetlands. Placement of a conversion facility next to the drainages along the western margin of Location C could alter the hydrology, including the X-230K Holding Pond, causing greater fluctuations in high and low flows. However, because only a small portion of the watershed would be involved, impacts would likely be small. Downstream wetlands could be affected by sedimentation during construction; however, the implementation of erosion control measures would reduce the likelihood of impacts.

**5.2.2.6.4 Threatened and Endangered Species.** Construction of a conversion facility at Location A is not expected to result in direct or indirect impacts to any federal- or state-listed species. However, impacts to wooded areas at Location A would occur as a result of the construction of facility access roads and rail lines, and additional woodland habitat could be eliminated unless temporary construction areas were positioned outside Location A. Trees with exfoliating bark, such as shagbark hickory or dead trees with loose bark, can be used by the Indiana bat (federal- and state-listed as endangered) for roosting during the summer. However, the wooded areas at Location A have not been identified as summer habitat. If facility construction required the disturbance of all of Location A, the entire wooded habitat at this location would potentially be eliminated. In addition, impacts to the riparian forest community along the intermittent stream might occur west of Location A, near the point of connection of the new rail line with the existing line east of Perimeter Road. If live or dead trees with exfoliating bark are encountered in construction areas, they should be saved if possible. If necessary, the trees should be cut before April 15 or after September 15. Disturbance due to increased noise, lighting, and human presence during the construction of the new rail line adjacent to the riparian forest habitat along the northern margin of Location A could decrease the quality of this habitat for the Indiana bat. However, Indiana bats that might use habitat near the Portsmouth site would be currently exposed to noise and other effects of human disturbance. Consequently, these effects related to construction activities would be expected to be minor.

Location B does not support habitat for federal- or state-listed species; therefore, construction at this location would not impact listed species. Although impacts to the woodland habitats at Location C could occur, these wooded areas have not been identified as Indiana bat summer habitat. In addition, impacts to the wooded areas at Location C could likely be avoided by facility placement in the northern portion of this location. Because of existing human disturbance in the vicinity of Locations A, B, and C, the construction of a conversion facility

would not affect the quality of potential Indiana bat habitat along Little Beaver Creek, the Northwest Tributary Stream, or the wooded area east of the X-100 facility.

### 5.2.2.7 Waste Management

Potential waste management impacts at Portsmouth during construction were evaluated by determining the types and estimating the volumes of wastes that would be generated. Waste management impacts would not depend on the location of the conversion facility within the site and would therefore be the same for alternative Locations A, B, and C. The estimates are presented in Table 5.2-8 and are compared with projected site generation volumes.

Construction of the conversion facility would generate both hazardous and nonhazardous wastes. Hazardous waste would be sent to off-site permitted contractors for disposal. Nonhazardous waste would be disposed of off site at a state-permitted landfill. No radioactive waste would be generated during the construction phase. Overall, only minimal waste management impacts would result from the construction-generated wastes.

### 5.2.2.8 Resource Requirements

The resources required for facility construction would not be dependent on the location of the facility. Materials related to construction would include concrete, sand, gravel, steel, and other metals (Table 5.2-9). At this time, no unusual construction material requirements have been identified. The construction resources, except for those that could be recovered and recycled with current technology, would be irretrievably lost. None of the identified construction resources are in short supply, and all should be readily available in the local region.

Small to moderate amounts of specialty materials (i.e., Monel and Inconel) would be required for construction of the conversion facility in quantities that would not seriously reduce the national or world supply. This material would be used throughout the facilities and is used in the generation of HF in the conversion process. The autoclaves and conversion units (process reactors) are long-lead-time procurements with few qualified bidders. Many suppliers are available for the remainder of the equipment.

**TABLE 5.2.8 Wastes Generated from Construction Activities for the Conversion Facility at the Portsmouth Site<sup>a</sup>**

Waste Category	Volume
Hazardous waste	115 m <sup>3</sup>
Nonhazardous waste	
Solids	700 m <sup>3</sup>
Wastewater	3.8 × 10 <sup>6</sup> L
Sanitary wastewater	1.1 × 10 <sup>7</sup> L

<sup>a</sup> Total waste generated during a construction period of 2 years. Because data were not available for the UDS conversion facility, data developed for the DUF<sub>6</sub> PEIS (Dubrin et al. 1997) were used.

**TABLE 5.2-9 Materials/Resources Consumed during Construction of the Conversion Facility at the Portsmouth Site**

Materials/Resources	Total Consumption	Unit	Peak Demand	Unit
<b>Utilities</b>				
Water	4 × 10 <sup>6</sup>	gal	1,500	gal/h
Electricity	1,500	MWh	7.2	MWh/d
<b>Solids</b>				
Concrete	9,139	yd <sup>3</sup>	NA <sup>a</sup>	NA
Steel	511	tons	NA	NA
Inconel/Monel	33	tons	NA	NA
<b>Liquids</b>				
Fuel	73,000	gal	250	gal/d
<b>Gases</b>				
Industrial gases (propane)	15,000	gal	50	gal/d

<sup>a</sup> NA = not applicable.

### 5.2.2.9 Land Use

The preferred location for the facility (Location A) covers 26 acres (10 ha) and presently features three structures on a site with more than 150 additional structures. Constructing a conversion facility at Location A would involve very slight modifications of existing land use. The resulting facility would be consistent with the heavy industrialized land use currently found at the Portsmouth site — a consequence of producing enriched uranium and its DUF<sub>6</sub> by-product. As a consequence, no land use impacts are anticipated as a result of constructing a conversion facility at Location A.

Use of either Location B or C considered for the conversion facility would have similar impacts. Location B is larger than the preferred location and covers about 50 acres (20 ha); it currently has two structures within its boundary. Location C also is larger than the preferred location, covering 78 acres (31 ha) and consisting of a grassy field. Land use impacts from construction on Location B would be very like those on Location A, with only slight modifications of existing land use. Land use impacts from construction on Location C would entail greater shifts in land use on the specific tract proposed, but within a site that already is heavily industrialized. In either case, the resulting facility would be consistent with current land use, and, as a result, negligible (for Location C) or no land use impacts are anticipated.

#### 5.2.2.10 Cultural Resources

Construction could potentially impact cultural resources. Currently, the amount of data on cultural resources within the project area at Portsmouth (Locations A, B, and C) is not sufficient to determine whether or not the proposed construction would adversely affect significant resources. Consequently, the possibility of adverse effects on cultural resources cannot be excluded.

Archaeological and architectural surveys were undertaken for Portsmouth in 1996. The findings from these surveys have not been finalized and have not received concurrence from the Ohio SHPO. Past ground disturbance resulting from grading and construction make it unlikely that intact archaeological remains are present at the proposed alternative locations. Preliminary results from the 1996 archaeological survey suggest that these locations are too disturbed to warrant subsurface testing (Anderson 2002). However, unless these findings receive SHPO concurrence, a separate archaeological assessment of the proposed area for the construction would be required to ensure that cultural material is not present and that Section 106 obligations under the NHPA are met. If archaeological resources were encountered and determined to be significant, a mitigation plan would have to be developed and executed in consultation with the Ohio SHPO prior to construction. In general, mitigation of an adverse effect of facility construction on cultural resources could entail site avoidance, monitoring during construction, or excavation/data recovery.

Two of the alternative locations (A and B) include existing structures dating to the Cold War era. It is possible that these structures would be demolished or modified during construction of a new facility. The historical significance of these structures, if any, has yet to be determined. Location A includes three warehouses formerly used to store lithium hydroxide. Location B includes two structures (X-3346 and X-1107F) associated with the Gaseous Centrifuge Enrichment Plant complex. The historical significance of these structures and any other standing structures that would be affected by the proposed action should be evaluated prior to any modification or demolition with respect to their contribution to the significance of the Portsmouth GDP operations during the Cold War. Following the Section 106 consultation process, if these structures were determined to be historically significant, either individually or as contributing members of a historic district, appropriate mitigation activities (e.g., avoidance, data recovery, monitoring) would have to be determined in consultation with the Ohio SHPO and implemented before the facility could be constructed. Location C does not contain standing structures.

No Native American traditional cultural properties have been identified at Portsmouth to date. Government-to-government consultations with Native American groups have been initiated (Appendix G). If the proposed action would result in an adverse effect on any such property identified, appropriate mitigation as determined through continued consultation would have to be undertaken before construction could begin.

### 5.2.2.11 Environmental Justice

The evaluation of environmental justice impacts associated with construction is based on the identification of high and adverse impacts in other impact areas considered in this EIS, followed by a determination if those impacts would affect minority and low-income populations disproportionately. Analyses of impacts from conversion facility construction under the action alternatives do not indicate the presence of high and adverse impacts for any of the other impact areas considered in this EIS (see Sections 5.2.2.1 through 5.2.2.10). Despite the presence of disproportionately high percentages of both minority and low-income populations within 50 mi (80 km) of the site, no environmental justice impacts from constructing the conversion facility are anticipated for Locations A, B, or C. Similarly, no evidence indicates that minority or low-income populations would experience high and adverse impacts from the proposed construction in the absence of such impacts in the population as a whole.

## 5.2.3 Portsmouth Site — Operational Impacts

This section discusses the potential environmental impacts during operation of a conversion facility at the three alternative locations within the Portsmouth site. During normal operations, the facility would emit only small amounts of contaminants through air emissions; no contaminated liquid effluents would be produced during the dry conversion process. The operational period would be 18 years, including conversion of the DUF<sub>6</sub> cylinders from ETTP. If the ETTP cylinders were not converted at Portsmouth, the operational period would be 14 years.

### 5.2.3.1 Human Health and Safety — Normal Facility Operations

**5.2.3.1.1 Radiological Impacts.** Radiological impacts to involved workers during normal operation of the conversion facility would result primarily from external radiation from the handling of depleted uranium materials. Impacts to noninvolved workers and members of the public would result primarily from trace amounts of uranium compounds released to the environment. Background information on radiation exposure is provided in Chapter 4; details on the methodologies are provided in Appendix F. Impacts to involved workers, noninvolved workers, and the general public would be similar for the three alternative locations.

Radiation exposures of the involved workers in the conversion facility were estimated on the basis of the measurement data on worker exposures in the Framatome ANP, Inc., facility in Richland, Washington. The Framatome facility uses a dry conversion process to convert UF<sub>6</sub> into uranium oxide and has been in operation since 1997. UDS would implement a similar conversion technology in the Portsmouth facility, and the key components would be similar to those of the Framatome ANP facility. Therefore, conditions for potential worker exposures at Portsmouth are expected to be similar to those at Framatome. However, the processing rate of uranium at Portsmouth (38 t [42 tons] of DUF<sub>6</sub> per day) would be greater than that at Framatome (9 t [10 tons] of UF<sub>6</sub> per day). To process more uranium materials, three conversion lines would be installed, and more workers or longer work hours from each worker would be required. On

the other hand, the specific activity of the uranium materials handled at Framatome (about  $3.5 \times 10^6$  pCi/g [Edgar 1994]) is greater than that of depleted uranium (about  $4.0 \times 10^5$  pCi/g). Consequently, the total radiological activities contained in each key component at Portsmouth would be less than those at Framatome, resulting in a smaller radiation dose rate from each component at Portsmouth. Because the actual worker activities and the activity duration and frequencies are not available for the conversion facility at this time, using worker exposure data from the Framatome facility is expected to provide a reasonable estimate of the potential radiation exposures of the involved workers at the Portsmouth facility. According to UDS (2003a,b), the conversion process would be very automated; therefore, the requirement of working at close distances to radiation sources would be limited. Potential radiation exposures of workers would be monitored by a dosimetry program and would be kept below the regulatory limit. The implementation of ALARA practices would further reduce the potential of exposures.

Potential radiation exposures of the involved cylinder yard workers would result mainly from the following activities: (1) receiving and inspecting ETTP cylinders upon arrival and putting them into storage; (2) regularly maintaining cylinders at the storage yards, including the current inventory of both DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders and the ETTP cylinders; and (3) preparing and transferring cylinders to the conversion facility. The first activity could last up to 6 years (from 2004 up to December 2009, when all cylinders are required to have been removed from ETTP); however, for the purpose of analysis and to provide bounding estimates of annual impacts, it is assumed to last for only 2 years. The other two activities would last for about 18 years — the operation period of the conversion facility. Under the action alternatives, cylinder maintenance activities during the conversion period would most likely stay the same as those currently implemented, except that the number of depleted uranium cylinders maintained would decrease steadily from the starting level. Therefore, potential radiation exposures caused by maintenance activities were estimated by scaling the current cylinder yard exposure data.

Potential exposures resulting from transferring cylinders to the conversion facility were estimated by using the following assumptions: (1) retrieving each cylinder to transportation equipment would involve two workers each spending half an hour at a distance of 3 ft (1 m) from the cylinder, (2) inspecting a cylinder would require two workers each spending half an hour at a distance of 1 ft (0.30 m) from the cylinder, and (3) each transfer from the cylinder yard to the conversion facility would require two workers for about half an hour at a distance of 6 ft (2 m) from the cylinders. Similar assumptions were used for estimating potential radiation exposures from receiving and placing the ETTP cylinders in storage. After inspection, the cylinder would be transported to the designated cylinder yard for storage. In the cylinder yard, each cylinder would be placed into storage position by two workers. This would take about half an hour at an exposure distance of 3 ft (1 m). All the above assumptions were developed for the purpose of modeling potential radiation exposures; in actuality, inspection, preparation, and transferring activities would probably take less time and involve fewer workers. As a result, radiation doses estimated on the basis of these assumptions are conservative.

Noninvolved workers would be those who would work in the conversion facility but would not perform hands-on activities and those who would work elsewhere on the Portsmouth site. Depending on the location of the conversion facility, the location of the MEI would be different, and the associated radiation exposure might also vary. However, according to the

previous analyses in the DUF<sub>6</sub> PEIS and the small uranium emission rate provided by UDS (2003b) for the conversion facility, potential radiation exposures of the noninvolved workers would be very small. An estimate of the bounding exposure, on the basis of the estimated maximum downwind air concentrations, is provided for the MEI in this section. According to the estimated bounding exposure, which is less than  $6 \times 10^{-6}$  mrem/yr, it is anticipated that the potential collective exposure of the noninvolved workers would also be very small and would be less than the product of the bounding MEI dose and the number of the noninvolved workers.

The location of the conversion facility within the Portsmouth site would have very little impact on collective exposures of the off-site public because of the much larger area (a circle with a radius of 50 mi [80 km]) considered for the collective exposures than the area of the Portsmouth site. The estimate of the collective exposure was obtained by using the emission rate ( $< 0.25$  g/yr for uranium) provided in UDS (2003b) and the population distribution information obtained from the 2000 census. The actual location of the off-site public MEI would depend on the selected location of the conversion facility and the site boundary. The potential exposure would be bounded by the exposure associated with the maximum air concentrations, which are the same as those used for estimating the bounding exposure of the noninvolved worker MEI. The bounding exposure of the off-site public MEI would be greater than that of the noninvolved worker MEI because of the longer exposure duration (8,760 h/yr versus 2,000 h/yr) assumed for the off-site public than for the noninvolved workers, and because of consideration of the food ingestion pathway for the off-site public (see Appendix F for more detailed information).

As discussed in Chapter 1 and Appendix B, some portion of the DUF<sub>6</sub> inventory contains TRU and Tc contamination. The TRU materials and most of the Tc material are expected to remain in the emptied cylinders after the withdrawal of DUF<sub>6</sub>. A small quantity of Tc might become vaporized and end up in the conversion process equipment, having been converted to technetium oxide. However, airborne emission of Tc is not anticipated because the oxide particles would be captured in the U<sub>3</sub>O<sub>8</sub> product. The contribution to the potential external radiation exposures from these contaminants under normal operations were evaluated on the basis of bounding concentrations presented in Appendix B. The dose from these contaminants was estimated and compared with the dose from the depleted uranium and uranium decay products in the DUF<sub>6</sub>. It is estimated that under normal operational conditions, the TRU and Tc contaminants would result in a very small contribution to the radiation doses — approximately 0.2% of the dose from the depleted uranium and its decay products.

Estimated potential annual radiation exposures and corresponding LCFs of the various receptors as a result of normal operations of the conversion facility are presented in Table 5.2-10 (impacts would be the same for all three alternative locations). The average individual dose for involved workers in the conversion facility is estimated to be about 75 mrem/yr (UDS 2003b). Collective exposures of the involved workers would depend on the number of workers required in the conversion facility. A total of about 135 involved workers would be required (UDS 2003b). The total collective exposure of the involved workers in the conversion facility would then be about 10.1 person-rem/yr. The estimated average cancer risk for individual workers would be about  $3 \times 10^{-5}$ /yr (1 chance in 33,000 of developing 1 LCF per year).

**TABLE 5.2-10 Estimated Radiological Doses and Cancer Risks under Normal Conversion Facility Operations at the Portsmouth Site<sup>a</sup>**

Location	Receptors					
	Involved Workers <sup>b</sup>		Noninvolved Workers <sup>c</sup>		General Public	
	Average Dose/Risk (mrem/yr) / (risk/yr)	Collective Dose/Risk (person-rem/yr) / (fatalities/yr)	MEI Dose/Risk <sup>d</sup> (mrem/yr) / (risk/yr)	Collective Dose/Risk (person-rem/yr) / (fatalities/yr)	MEI Dose/Risk <sup>e</sup> (mrem/yr) / (risk/yr)	Collective Dose/Risk <sup>f</sup> (person-rem/yr) / (fatalities/yr)
Radiation doses						
Conversion facility	75	10.1	$< 5.5 \times 10^{-6}$	$< 9.9 \times 10^{-6}$	$< 2.1 \times 10^{-5}$	$6.2 \times 10^{-5}$
Cylinder yards <sup>g</sup>	510 – 600 (1180)	2.6 – 3.0 (9.4)	– <sup>h</sup>	–	–	–
Cancer risks						
Conversion facility	$3 \times 10^{-5}$	$4 \times 10^{-3}$	$< 3 \times 10^{-12}$	$< 5 \times 10^{-9}$	$< 1 \times 10^{-11}$	$3 \times 10^{-8}$
Cylinder yards <sup>g</sup>	$2 \times 10^{-4}$ ( $5 \times 10^{-4}$ )	$1 \times 10^{-3}$ ( $4 \times 10^{-3}$ )	–	–	–	–

<sup>a</sup> Impacts are reported as best estimates or bounding values. They are the same regardless of the location of the conversion facility.

<sup>b</sup> Involved workers are those workers directly involved with handling radioactive materials. For the conversion facility, 135 involved workers were assumed. Calculation results are presented as average individual dose and collective dose for the worker population.

<sup>c</sup> Noninvolved workers include individuals who work at the conversion facility but are not directly involved in handling materials, and individuals who work at the Portsmouth site but not within the conversion facility. The population size of noninvolved workers is about 1,800.

<sup>d</sup> The noninvolved worker MEI doses are the bounding estimates corresponding to the estimated maximum downwind air concentrations. The exposures would result from inhalation, external radiation, and incidental soil ingestion.

<sup>e</sup> The general public MEI doses are the bounding estimates corresponding to the estimated maximum downwind air concentrations. The exposure would result from inhalation; external radiation; and ingestion of plant foods, meat, milk, and soil.

<sup>f</sup> Collective exposures were estimated for the population (about 670,000 persons) within a 50-mi (80 km) radius around the Portsmouth site. The exposure pathways considered were inhalation; external radiation; and ingestion of plant foods, meat, milk, and soil.

<sup>g</sup> Radiation exposures estimated for cylinder yard workers were obtained by considering maintenance, preparation, and transferring activities, with the assumption of a total of 5 workers every year. These exposures are expected to last for the entire conversion operation period. Results listed in parentheses include radiation exposures resulting from unloading, inspecting, and placing the ETTP cylinders into storage position, in addition to maintaining, preparing, and transferring cylinders. A total of 8 workers is assumed every year. These higher levels of exposures are assumed to last only for the first 2 years.

<sup>h</sup> A dash indicates that potential air emissions from cylinder maintenance or preparation activities are expected to be negligible. Therefore, no impacts were estimated for the noninvolved workers and the off-site general public.

The average individual dose for workers working at the cylinder yards would vary over the conversion period. For the first 2 years (based on the assumption discussed above), because of receiving, inspecting, and putting the ETTP cylinders into storage position, potential radiation exposures are expected to be greater than those in the following years. It is estimated that handling the arriving cylinders would result in a collective exposure of about 12.3 person-rem. The total person-hours estimated to be required for the handling activities is about 13,000. For the purpose of calculating an average individual exposure, a total of eight workers is assumed. The average individual exposure for the first 2 years is thus estimated to be about 1,180 mrem/yr. Beyond the first 2 years, it is judged that five workers would be sufficient to handle the planned activities. The average individual exposure for the remaining years is estimated to range from about 510 to 600 mrem/yr (the collective dose ranges from 2.5 to 3.0 person-rem/yr). The larger exposure corresponds to the third year of conversion operations, and the smaller exposure corresponds to the last year of operations. The estimated average doses for cylinder yard workers are well below the dose limit of 5,000 mrem/yr set for radiation workers (10 CFR Part 835). The corresponding latent cancer risk for an average worker would be about  $5 \times 10^{-4}$  per year (1 chance in 2,000 of developing 1 LCF per year) or less. UDS has proposed 28 workers for cylinder management activities (UDS 2003b); therefore, the actual average dose to individual workers is likely to be less than the above estimated values.

Because of the small airborne release rates of depleted uranium during normal operations, potential radiation exposures of the noninvolved workers would be very small regardless of where the conversion facility was located within the Portsmouth site. The radiation dose incurred by the MEI was modeled to be less than  $6.0 \times 10^{-6}$  mrem/yr. This small radiation dose would correspond to potential excess latent cancer risks of less than  $3 \times 10^{-12}$  per year (1 chance in 330 billion of developing 1 LCF per year). For comparison, the dose limit set for airborne releases from operations of DOE facilities is 10 mrem/yr (40 CFR 61).

Radiation exposures of the off-site public also would be very small regardless of the location of the conversion facility. The MEI dose was modeled to be less than  $3.0 \times 10^{-5}$  mrem/yr. This dose is much less than the radiation dose limits of 100 mrem/yr (DOE 1990) from all pathways and 10 mrem/yr (40 CFR Part 61) from airborne pathways set to protect the general public from operations of DOE facilities. The corresponding latent cancer risk would be less than  $1 \times 10^{-11}$  per year (1 chance in 100 billion of developing 1 LCF per year). Because of no waterborne discharge of uranium (UDS 2003b), radiation exposure to the off-site public from using surface water near the facility would be negligible.

**5.2.3.1.2 Chemical Impacts.** Potential chemical impacts to human health from normal operations at the conversion facility would result primarily from exposure to trace amounts of the insoluble uranium compound U<sub>3</sub>O<sub>8</sub> and to HF released from the process exhaust stack. Risks from normal operations were quantified on the basis of calculated hazard indices. General information concerning the chemical impact analysis methodology is provided in Chapter 4.

The hazard indices were calculated on the basis of air dispersion modeling, which identified the locations of maximum ground-level concentrations of uranium compounds and HF emitted from the conversion facility. Since the maximum concentration locations were used for

modeling both noninvolved worker and general public exposures, the impacts would be the same for the three alternative locations assessed.

Conversion to U<sub>3</sub>O<sub>8</sub> would result in very low levels of exposure to hazardous chemicals. No adverse health effects to noninvolved workers or the general public are expected during normal operations. Human health impacts resulting from exposure to hazardous chemicals during normal operations of the conversion facilities are estimated as hazard indices of  $3.8 \times 10^{-7}$  and  $4.1 \times 10^{-5}$  for the noninvolved worker and general public MEI, respectively. The hazard indices for the conversion process would be at least three orders of magnitude lower than the hazard index of 1, which is the level at which adverse health effects might be expected to occur in some exposed individuals.

Impacts to involved workers from exposure to chemicals during normal operations are not expected. The workplace would be monitored to ensure that airborne chemical concentrations were within applicable health standards that are protective of human health and safety. If planned work activities were likely to expose involved workers to chemicals, workers would be provided with appropriate protective equipment, as necessary.

### 5.2.3.2 Human Health and Safety — Facility Accidents

A range of accidents covering the spectrum from high-frequency/low-consequence events to low-frequency/high-consequence accidents was considered for DUF<sub>6</sub> conversion operations. The accident scenarios considered such events as releases due to cylinder damage, fires, plane crashes, equipment leaks and ruptures, hydrogen explosions, earthquakes, and tornadoes. The accident scenarios considered in the assessment were those identified in the DUF<sub>6</sub> PEIS (DOE 1999a), modified to take into account the specific conversion technology and facility design proposed by UDS (UDS 2003b; Folga 2003). A list of bounding radiological and chemical accidents – that is, those accidents expected to result in the highest consequences in each frequency category should the accident occur – for the UDS conversion facility is provided in UDS (2003b). The bounding accident scenarios and their estimated consequences are discussed below for both radiological and chemical impacts.

**5.2.3.2.1 Radiological Impacts.** Potential radiation doses from accidents were estimated for noninvolved workers at the Portsmouth site and members of the public within a 50-mi (80-km) radius of the site for both MEIs and the collective populations. Impacts to involved workers under accident conditions would likely be dominated by physical forces from the accident itself; thus, quantitative dose/effect estimates would not be meaningful. For these reasons, the impacts to involved workers during accidents are not quantified in this EIS. However, it is recognized that injuries and fatalities among involved workers would be possible if an accident did occur.

Table 5.2-11 lists the bounding accidents in each frequency category (i.e., the accidents that were found to have the highest consequences) for radiological impacts. The estimated

**TABLE 5.2-11 Bounding Radiological Accidents Considered for Conversion Operations at the Portsmouth Site<sup>a</sup>**

Accident Scenario	Accident Description	Chemical Form	Amount (lb)	Duration (min)	Release Level <sup>b</sup>
<i>Likely Accidents (frequency: 1 or more times in 100 years)</i>					
Corroded cylinder spill, dry conditions	A 1-ft (0.30 m) hole results during handling, with solid UF <sub>6</sub> forming a 4-ft <sup>2</sup> (0.37-m <sup>2</sup> ) area on the dry ground.	UF <sub>6</sub>	24	60	Ground
U <sub>3</sub> O <sub>8</sub> drum spill	A single U <sub>3</sub> O <sub>8</sub> drum is damaged by a forklift and spills its contents onto the ground outside the storage facility.	U <sub>3</sub> O <sub>8</sub>	2.4	30	Ground
<i>Extremely Unlikely Accidents (frequency: 1 time in 10,000 years to 1 time in 1 million years)</i>					
Earthquake	The U <sub>3</sub> O <sub>8</sub> storage building is damaged during a design-basis earthquake, and 10% of the stored containers are breached.	U <sub>3</sub> O <sub>8</sub>	135	30	Stack
Rupture of cylinders – fire	Several cylinders hydraulically rupture during a fire.	UF <sub>6</sub>	0 11,500 8,930 3,580	0–12 12 12–30 30–121	Ground
Tornado	A windblown missile from a design-basis tornado pierces a single U <sub>3</sub> O <sub>8</sub> container in the storage building.	U <sub>3</sub> O <sub>8</sub>	1,200	0.5	Ground

<sup>a</sup> Potential accidents in the unlikely and incredible frequency categories would not result in radiological releases, but they are considered in the chemical assessment. The accident assessment considered a spectrum of accidents in four categories: likely, unlikely, extremely unlikely, and incredible.

<sup>b</sup> Ground-level releases were assumed to occur outdoors on concrete pads in the cylinder storage yards. To prevent contaminant migration, cleanup of residuals was assumed to begin immediately after the release was stopped.

radiation doses to members of the public and noninvolved workers (both MEIs and collective populations) for these accidents are presented in Table 5.2-12. The corresponding risks of LCFs associated with the estimated doses for these accidents are given in Table 5.2-13. The doses and risks are presented as ranges (minimum and maximum) because two different atmospheric conditions were considered for each accident. The estimated doses and LCFs were calculated on the basis of the assumption that the accidents would occur, without taking into account the probability of the accident's occurring. The probability of occurrence for each accident is indicated by the frequency category to which it is assigned. For example, accidents in the extremely unlikely category have an estimated probability of occurrence of between 1 in 10,000 and 1 in 1 million per year.

**TABLE 5.2-12 Estimated Radiological Doses per Accident Occurrence during Conversion at the Portsmouth Site<sup>a</sup>**

Conversion Product/Accident <sup>b</sup>	Frequency Category <sup>c</sup>	Maximum Dose				Minimum Dose			
		Noninvolved Workers		General Public		Noninvolved Workers		General Public	
		MEI (rem)	Population <sup>d</sup> (person-rem)	MEI (rem)	Population (person-rem)	MEI (rem)	Population <sup>d</sup> (person-rem)	MEI (rem)	Population (person-rem)
Corroded cylinder spill, dry conditions	L	$7.8 \times 10^{-2}$	1.1/1.4/1.1	$7.8 \times 10^{-2}$	$1.2 \times 10^{-1}$	$3.3 \times 10^{-3}$	$(4.4/5.6/4.6) \times 10^{-2}$	$3.3 \times 10^{-3}$	$1.9 \times 10^{-2}$
Failure of U <sub>3</sub> O <sub>8</sub> container while in transit	L	$5.3 \times 10^{-1}$	7.3/9.6/7.4	$5.3 \times 10^{-1}$	$5.1 \times 10^{-1}$	$2.3 \times 10^{-2}$	$(3.0/3.8/3.1) \times 10^{-1}$	$2.3 \times 10^{-2}$	$1.2 \times 10^{-1}$
Earthquake	EU	30	$(4.0/5.3/4.3) \times 10^2$	30	30	1.2	$(1.7/2.1/1.8) \times 10^{-1}$	1.1	6.5
Rupture of cylinders – fire	EU	$2.0 \times 10^{-2}$	3.9/3.3/5.1	$2.0 \times 10^{-2}$	23	$3.7 \times 10^{-3}$	$(2.4/2.5/6.1) \times 10^{-1}$	$3.7 \times 10^{-3}$	$7.3 \times 10^{-1}$
Tornado <sup>e</sup>	EU	7.5	100/130/110	7.5	17	7.5	100/130/110	7.5	17

<sup>a</sup> Maximum and minimum doses reflect differences in meteorological conditions at the time of the accident. In general, maximum doses would occur under meteorological conditions of F stability with a 1-m/s (2-mph) wind speed, whereas minimum doses would occur under D stability with a 4-m/s (9-mph) wind speed.

<sup>b</sup> The bounding accident chosen to represent each frequency category is the one that would result in the highest dose to the general public MEI. Health impacts in that row represent that accident only and not the range of impacts among accidents in that category. Absence of an accident in a certain frequency category indicates that the accident would not result in a release of radioactive material.

<sup>c</sup> Accident frequencies: L = likely, estimated to occur one or more times in 100 years of facility operations ( $> 10^{-2}/\text{yr}$ ); EU = extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years of facility operations ( $10^{-4}$  to  $10^{-6}/\text{yr}$ ).

<sup>d</sup> For the noninvolved worker population dose, three estimates are provided, corresponding to Locations A, B, and C within the Portsmouth site.

<sup>e</sup> Meteorological conditions analyzed for the tornado were D stability with a 20-m/s (45-mph) wind speed.

**TABLE 5.2-13 Estimated Radiological Health Risks per Accident Occurrence during Conversion at the Portsmouth Site<sup>a</sup>**

Conversion Product/Accident <sup>b</sup>	Frequency Category <sup>c</sup>	Maximum Risk <sup>d</sup> (LCFs)				Minimum Risk <sup>d</sup> (LCFs)			
		Noninvolved Workers		General Public		Noninvolved Workers		General Public	
		MEI	Population <sup>d</sup>	MEI	Population	MEI	Population <sup>d</sup>	MEI	Population
Corroded cylinder spill, dry conditions	L	$3 \times 10^{-5}$	$(0.4/1/0.2) \times 10^{-3}$	$3 \times 10^{-5}$	$3 \times 10^{-5}$	$1 \times 10^{-6}$	$(2/3/2) \times 10^{-5}$	$1 \times 10^{-6}$	$9 \times 10^{-6}$
U <sub>3</sub> O <sub>8</sub> drum spill	L	$2 \times 10^{-4}$	$(3/7/2) \times 10^{-3}$	$3 \times 10^{-4}$	$3 \times 10^{-4}$	$9 \times 10^{-6}$	$(1/2/2) \times 10^{-4}$	$1 \times 10^{-5}$	$6 \times 10^{-5}$
Earthquake	EU	$2 \times 10^{-2}$	$(2/2/2) \times 10^{-1}$	$2 \times 10^{-2}$	$2 \times 10^{-2}$	$4 \times 10^{-4}$	$(8/10/9) \times 10^{-3}$	$5 \times 10^{-4}$	$3 \times 10^{-3}$
Rupture of cylinders – fire	EU	$8 \times 10^{-6}$	$(4/3/3) \times 10^{-3}$	$8 \times 10^{-6}$	$1 \times 10^{-2}$	$1 \times 10^{-6}$	$(1/1/3) \times 10^{-4}$	$1 \times 10^{-6}$	$5 \times 10^{-4}$
Tornado <sup>e</sup>	EU	$3 \times 10^{-3}$	$(5/6/5) \times 10^{-2}$	$4 \times 10^{-3}$	$8 \times 10^{-3}$	$3 \times 10^{-3}$	$(5/6/5) \times 10^{-1}$	$4 \times 10^{-3}$	$8 \times 10^{-3}$

<sup>a</sup> Maximum and minimum risks reflect differences in meteorological conditions at the time of the accident. In general, maximum risks would occur under meteorological conditions of F stability with a 1-m/s (2-mph) wind speed; minimum risks would occur under D stability with a 4-m/s (9-mph) wind speed. Values shown are the consequences if the accident did occur. The risk of an accident is the consequence (LCFs) times the estimated frequency times 18 years of operations.

<sup>b</sup> The bounding accident chosen to represent each frequency category is the one that would result in the highest risks to the general public MEI. Health impacts in that row represent that accident only and not the range of impacts among accidents in that category. Absence of an accident in a certain frequency category indicates that the accident would not result in a release of radioactive material.

<sup>c</sup> Accident frequencies: L = likely, estimated to occur one or more times in 100 years of facility operations ( $> 10^{-2}/\text{yr}$ ); EU = extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years of facility operations ( $10^{-4} - 10^{-6}/\text{yr}$ ).

<sup>d</sup> For the noninvolved worker population dose, three estimates are provided, corresponding to Locations A, B, and C within the Portsmouth site.

<sup>e</sup> Meteorological conditions analyzed for the tornado were D stability with a 20-m/s (45-mph) wind speed.

The accident assessment took into account the three alternative locations within the Portsmouth site. Because of the close proximity of the alternative locations to the site boundary and the uncertainty associated with both the wind direction at the time of the accident and the exact location of the release point, it was conservatively assumed that both the noninvolved worker MEI and the general public MEI would be located 328 ft (100 m) from accidents with a ground-level release. For accidents with the potential for plume rise due to a fire or for releases from a stack, both the worker and public MEIs were assumed to be located at the point of maximum ground-level concentrations of the released contaminants. As discussed in Chapter 4, the noninvolved worker MEI was assumed to be exposed to the passing plume for 2 hours after the accident, after which time he or she would be evacuated; the public MEI was assumed to remain indefinitely in the path of the passing plume and consume contaminated food grown on site.

The estimated doses and risks to the noninvolved worker and public MEIs are presented in Tables 5.2-12 and 5.2-13. The estimated impacts to the noninvolved worker MEI and public MEI are similar because 99% of the dose is due to the inhalation pathway within the first 2 hours after the accident.

For the off-site public, the location of the conversion facility within the Portsmouth site would have very little impact on collective exposures because the area considered (a circle with a radius of 80 km [50 mi]) would be so much larger than the area of the Portsmouth site. The population dose estimates are based on population distributions from the 2000 census. The collective dose to noninvolved workers, however, would depend on the location of the conversion facility with respect to other buildings within the site. Therefore, for the noninvolved worker population, three estimates are provided in Tables 5.2-12 and 5.2-13, corresponding to Locations A, B, and C within the site.

The postulated accident estimated to have the largest consequence is the extremely unlikely accident caused by an earthquake involving the conversion facility. In this scenario, it is assumed that the U<sub>3</sub>O<sub>8</sub> storage building would be damaged during the earthquake and that 10% of the stored containers would be breached. Under conservative meteorological conditions (F stability class with a 1-m/s [2-mph] wind speed) expected to result in the highest possible exposures, it is estimated that the dose to the MEI member of the public and noninvolved worker from this accident would be approximately 30 rem, if it is assumed that the product storage building contained 6 month's worth of production. The RFP for conversion services required the bidders to provide enough capacity to be able to store up to 6 month's worth of inventory on site. The estimated MEI doses are well below levels expected to cause immediate fatalities from radiation exposure (approximately 450 rem) and would result in a lifetime increase in the probability of developing an LCF of about 0.02 (about 1 chance in 50) in the public MEI and about 0.02 (about 1 chance in 50) in the worker MEI.

It is estimated that the collective doses from the U<sub>3</sub>O<sub>8</sub> storage building earthquake accident would be 400 to 530 person-rem to the worker population and 30 person-rem to the off-site general population. These collective doses would result in less than 1 additional LCF in the worker population (0.2 LCF) and in the general population (0.02 LCF).

The accident scenario with the second-highest impacts was the extremely unlikely scenario caused by a tornado strike. In this scenario, it is assumed that a windblown missile from a tornado would pierce a single U<sub>3</sub>O<sub>8</sub> container in storage. In this hypothetical accident, if bulk bags were used to transport and dispose of the U<sub>3</sub>O<sub>8</sub> product, approximately 1,200 lb (550 kg) of U<sub>3</sub>O<sub>8</sub> could be released at ground level. Under conservative meteorological conditions, it is estimated that the dose to the MEI and noninvolved worker would be 7.5 rem. The collective doses would be up to 130 person-rem to the worker population and up to 17 person-rem to the general population. If the emptied cylinders rather than the bulk bags were used as U<sub>3</sub>O<sub>8</sub> containers, the resulting doses would be approximately half of the above results.

To account for the possible TRU and Tc contamination in some of the cylinders, a ratio of the dose from the TRU and Tc radionuclides at bounding maximum concentrations to the dose from the depleted uranium was calculated (see Appendix B for details). For accidents involving full DUF<sub>6</sub> cylinders, the relative dose contribution from TRU and Tc was found to be less than 0.02% of the dose from the depleted uranium. This approach is conservative because only a fraction of the cylinders in the inventory are contaminated with TRU and because it is expected that the concentration in any one cylinder would be less than the bounding concentrations assumed in the analysis.

The following conclusions may be drawn from the radiological health impact results:

- No cancer fatalities are predicted for any of the accidents.
- The maximum radiological dose to the noninvolved worker and general public MEIs (assuming that an accident occurred) would be about 30 rem. This dose would thus be greater than the 25-rem total effective dose equivalent established by DOE as a guideline for assessing the adequacy of protection of public health and safety from potential accidents (DOE 2000c). Therefore, more detailed analysis during facility design and siting may be necessary.
- The overall radiological risk to noninvolved worker and general public MEI receptors (estimated by multiplying the risk per occurrence [Table 5.2-13] by the annual probability of occurrence by the number of years of operations) would be less than 1 for all of the conversion facility locations.
- The differences in noninvolved worker population impacts among the three locations would be relatively small.

**5.2.3.2.2 Chemical Impacts.** This section presents the results for chemical health impacts for the highest-consequence accident in each frequency category for conversion operations at the Portsmouth site. The estimated numbers of adverse and irreversible adverse effects among noninvolved workers and the general public were calculated separately for each of the three alternative locations within the site by using 2000 census data for the off-site population. The methodology and assumptions used in the calculations are summarized in Appendix F, Section F.2.

The bounding conversion facility chemical accidents are listed in Table 5.2-14 and cover events that could occur during conversion. Note that an anhydrous NH<sub>3</sub> tank rupture is one of the bounding chemical accidents and the accident expected to cause the greatest impacts. NH<sub>3</sub> is used to produce hydrogen required for the conversion process. Although the use of NH<sub>3</sub> for hydrogen production is part of the UDS facility design, the use of natural gas for hydrogen production, which would eliminate the need for NH<sub>3</sub>, is also possible.

The consequences from accidental chemical releases derived from the accident consequence modeling for conversion are presented in Tables 5.2-15 and 5.2-16. The results are presented as the number of people with the potential for (1) adverse effects and (2) irreversible adverse effects. Within each frequency category, the tables present the results for the accident that would affect the largest number of people (total of workers and off-site population). The numbers of noninvolved workers and members of the off-site public represent the impacts if the associated accident occurred. The accident scenarios given in Tables 5.2-15 and 5.2-16 are not identical because an accident with the largest impacts for adverse effects might not lead to the largest impacts for irreversible adverse effects.

The impacts may be summarized as follows:

- The largest impacts would be caused by the following accident scenarios: an HF storage tank rupture; a corroded cylinder spill under wet conditions (i.e., rain and formation of a water pool); an NH<sub>3</sub> tank rupture; and the rupture of several cylinders in a fire. Accidents involving stack emissions would have smaller impacts compared with accidents involving releases at ground level because of the relatively larger dilution and smaller release rates (due to filtration) involved with the stack emissions.
- If the accidents identified in Tables 5.2-15 and 5.2-16 did occur, the number of persons in the off-site population with the potential for adverse effects would range from 0 to around 2,300 (maximum corresponding to an HF tank rupture), and the number of off-site persons with the potential for irreversible adverse effects would range from 0 to around 210 (maximum corresponding to an NH<sub>3</sub> pressurized tank rupture).
- The maximum number of adverse effects among noninvolved workers would occur for Location B for most accident scenarios. For the general public, maximum impacts may occur at Locations A or C, depending on the specific scenario; however, the differences are relatively small among the three locations.
- The greatest number of irreversible adverse effects among the noninvolved workers would occur at Location C for most scenarios and at Location B for the NH<sub>3</sub> tank rupture. Among members of the public, impacts are very similar for all three locations.

**TABLE 5.2-14 Bounding Chemical Accidents during Conversion Operations at the Portsmouth Site**

Frequency Category/ Accident Scenario	Accident Description	Chemical Form of Release	Release Amount (lb)	Release Duration (min)	Release Level/ Medium
<b>Likely Accidents (frequency: 1 or more times in 100 years)</b>					
Corroded cylinder spill, dry conditions	A 1-ft (0.30-m) hole results during handling, with solid UF <sub>6</sub> forming a 4-ft <sup>2</sup> (0.37-m <sup>2</sup> ) area on the dry ground.	UF <sub>6</sub>	24	60	Ground/ air
<b>Unlikely Accidents (frequency: 1 in 100 years to 1 in 10,000 years)</b>					
Corroded cylinder spill, wet conditions – rain	A 1-ft (0.30-m) hole results during handling, with solid UF <sub>6</sub> forming a 4-ft <sup>2</sup> (0.37-m <sup>2</sup> ) area on the wet ground	HF	96	60	Ground/ air
Aqueous HF pipe rupture	An earthquake ruptures an aboveground pipeline transporting aqueous HF, releasing it to the ground.	HF	910 <sup>a</sup>	10	Ground/ air
Anhydrous NH <sub>3</sub> line leak	An NH <sub>3</sub> fill line is momentarily disconnected, and NH <sub>3</sub> is released at grade.	NH <sub>3</sub>	255	1	Ground/ air
<b>Extremely Unlikely Accidents (frequency: 1 in 10,000 years to 1 in 1 million years)</b>					
Corroded cylinder spill, wet conditions – water pool	A 1-ft (0.30-m) hole results during handling, with solid UF <sub>6</sub> forming a 4-ft <sup>2</sup> (0.37-m <sup>2</sup> ) area into a 0.25-in. (0.64-cm)-deep water pool.	HF	147	60	Ground/ air
Rupture of cylinders – fire	Several cylinders hydraulically rupture during a fire.	UF <sub>6</sub>	0 11,500 8,930 3,580	0 to 12 12 12 to 30 30 to 121	Ground/ air
<b>Incredible Accidents (frequency: less than 1 in 1 million years)</b>					
Aqueous HF (70%) tank rupture	Large seismic or beyond-design-basis event causes rupture of a filled HF storage tank.	HF	F1: 8,710 <sup>b</sup> D4: 25,680 <sup>b</sup>	120	Ground/ air
Anhydrous NH <sub>3</sub> tank rupture	Large seismic or beyond-design-basis event causes rupture of a filled anhydrous NH <sub>3</sub> storage tank.	NH <sub>3</sub>	29,500	20	Ground/ air

<sup>a</sup> The estimate assumes that 10% of the spill evaporates, with the remainder absorbed into the soil. It should be noted that the soil/groundwater assessment conservatively assumed that 100% of the spill is absorbed into the soil.

<sup>b</sup> The two separate atmospheric conditions considered would cause different amounts to be released. These release amounts were computed based on evaporation rates estimated by assuming 77°F (25°C; F-1 conditions) and 95°F (35°C; D-4 conditions).

**TABLE 5.2-15 Consequences of Chemical Accidents during Conversion at the Portsmouth Site: Number of Persons with the Potential for Adverse Effects<sup>a</sup>**

Accident <sup>b</sup>	Freq. Cat. <sup>c</sup>	Maximum No. of Persons per Location <sup>d</sup>												Minimum No. of Persons per Location <sup>d</sup>											
		Noninvolved Worker						General Public						Noninvolved Workers						General Public					
		MEI <sup>e</sup>			No. Affected			MEI <sup>e</sup>			No. Affected			MEI <sup>e</sup>			No. Affected			MEI <sup>e</sup>			No. Affected		
		A	B	C	A	B	C	A	B	C	A	B	C	A	B	C	A	B	C	A	B	C	A	B	C
Corroded cylinder spill, dry conditions	L	Yes	Yes	Yes	4	22	48	No	No	Yes <sup>f</sup>	0	0	0	Yes	Yes	Yes	0	0	0	No	No	No	0	0	0
Corroded cylinder spill, wet conditions – rain	U	Yes	Yes	Yes	490	480	480	Yes	Yes	Yes	13	13	14	Yes	Yes	Yes	0	14	0	No	No	No	0	0	0
Rupture of cylinders – fire	EU	Yes	Yes	Yes	540	660	450	Yes	Yes	Yes	650	600	570	Yes	Yes	Yes	110	110	160	Yes	Yes	Yes	5	5	5
HF tank rupture	I	Yes	Yes	Yes	660	920	330	Yes	Yes	Yes	2,200	2,000	2,300	Yes	Yes	Yes	600	800	330	Yes	Yes	Yes	29	30	33
NH <sub>3</sub> tank rupture	I	Yes	Yes	Yes	810	1,400	1,100	Yes	Yes	Yes	1,700	1,500	1,500	Yes	Yes	Yes	580	880	850	Yes	Yes	Yes	21	21	24

<sup>a</sup> Values shown are the consequences if the accident did occur. The risk of an accident is the consequence (number of persons) times the estimated frequency, times 18 years of operations. The estimated frequencies are as follows: L = likely, 0.1; U = unlikely, 0.001; EU = extremely unlikely, 0.00001; I = incredible, 0.000001.

<sup>b</sup> The bounding accident chosen to represent each frequency category is the one in which the largest number of people (workers plus off-site population) would be affected. Health impacts in that row represent that accident only and not the range of impacts among accidents in that category.

<sup>c</sup> Accident frequencies: L = likely, estimated to occur one or more times in 100 years of facility operations (> 10<sup>-2</sup>/yr); U = unlikely, estimated to occur between once in 100 years and once in 10,000 years of facility operations (10<sup>-2</sup> to 10<sup>-4</sup>/yr); EU = extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years of facility operations (10<sup>-4</sup> to 10<sup>-6</sup>/yr); I = incredible, estimated to occur less than one time in 1 million years of facility operations (< 10<sup>-6</sup>/yr).

<sup>d</sup> Maximum and minimum values reflect differences in assumed meteorological conditions at the time of the accident. In general, the maximum risks would occur under meteorological conditions of F stability with a 1-m/s (2-mph) wind speed; the minimum risks would occur under D stability with a 4-m/s (9-mph) wind speed.

<sup>e</sup> At the MEI location, the determination is either “Yes” or “No” for potential adverse effects to an individual.

<sup>f</sup> MEI locations were evaluated at 100 m (328 ft) from ground-level releases for workers and at the location of highest off-site concentration for members of the general public; the population risks are 0 because the worker and general public population distributions for the site were used, which did not show receptors at the MEI locations.

**TABLE 5.2-16 Consequences of Chemical Accidents during Conversion at the Portsmouth Site: Number of Persons with the Potential for Irreversible Adverse Effects<sup>a</sup>**

Conversion Product/Accident <sup>b</sup>	Freq. Cat. <sup>c</sup>	Maximum No. of Persons per Location <sup>d</sup>												Minimum No. of Persons per Location <sup>d</sup>											
		Noninvolved Worker						General Public						Noninvolved Workers			General Public								
		MEI <sup>e</sup>			No. Affected			MEI <sup>e</sup>			No. Affected			MEI <sup>e</sup>			No. Affected			MEI <sup>e</sup>			No. Affected		
		A	B	C	A	B	C	A	B	C	A	B	C	A	B	C	A	B	C	A	B	C	A	B	C
<b>Conversion to U<sub>3</sub>O<sub>8</sub></b>																									
Corroded cylinder spill, dry conditions	L	Yes <sup>f</sup>	Yes	Yes	0	0	0	No	No	No	0	0	0	Yes	Yes	Yes	0	0	0	No	No	No	0	0	0
Corroded cylinder spill, wet conditions – rain	U	Yes	Yes	Yes	97	120	130	Yes	Yes	Yes	0	0	0	Yes	Yes	Yes	0	0	0	No	No	No	0	0	0
Corroded cylinder spill, wet conditions – water pool	EU	Yes	Yes	Yes	170	170	190	Yes	Yes	Yes	0	0	1	Yes	Yes	Yes	0	0	0	No	No	No	0	0	0
NH <sub>3</sub> tank rupture <sup>g</sup>	I	Yes	Yes	Yes	810	1,400	1,100	Yes	Yes	Yes	200	210	210	Yes	Yes	Yes	400	370	50	Yes	Yes	Yes	2	2	4

<sup>a</sup> The values shown are the consequences if the accident did occur. The risk of an accident is the consequence (number of persons) times the estimated frequency, times 18 years of operations. The estimated frequencies are as follows: L = likely, 0.1; U = unlikely, 0.001; EU = extremely unlikely, 0.00001; I = incredible, 0.000001.

<sup>b</sup> The bounding accident chosen to represent each frequency category is the one in which the largest number of people (workers plus off-site population) would be affected. Health impacts in that row represent that accident only and not the range of impacts among accidents in that category.

<sup>c</sup> Accident frequencies: L = likely, estimated to occur one or more times in 100 years of facility operations (> 10<sup>-2</sup>/yr); U = unlikely, estimated to occur between once in 100 years and once in 10,000 years of facility operations (10<sup>-2</sup> to 10<sup>-4</sup>/yr); EU = extremely unlikely, estimated to occur between once in 10,000 years and once in 1 million years of facility operations (10<sup>-4</sup> to 10<sup>-6</sup>/yr); I = incredible, estimated to occur less than one time in 1 million years of facility operations (< 10<sup>-6</sup>/yr).

<sup>d</sup> Maximum and minimum values reflect differences in assumed meteorological conditions at the time of the accident. In general, the maximum risks would occur under meteorological conditions of F stability with a 1-m/s (2-mph) wind speed; the minimum risks would occur under D stability with a 4-m/s (9-mph) wind speed.

<sup>e</sup> At the MEI location, the determination is either “Yes” or “No” for potential adverse effects to an individual.

<sup>f</sup> MEI locations were evaluated at 100 m (328 ft) from ground-level releases for workers and at the location of highest off-site concentration for members of the general public; the population risks are 0 because the worker and general public population distributions for the site were used, which did not show receptors at the MEI locations.

<sup>g</sup> Under D-stability, 4-m/s (9-mph) meteorological conditions (minimum no. of persons affected), an aqueous HF tank rupture would have higher consequences to noninvolved workers than would the NH<sub>3</sub> tank rupture, resulting in about 150 to 200 more irreversible adverse effects at all three proposed locations. However, under F-stability, 1-m/s (2-mph) meteorological conditions (maximum no. of persons affected), the NH<sub>3</sub> tank rupture would have the maximum consequences to noninvolved workers and the general public.

- If the accidents identified in Tables 5.2-15 and 5.2-16 did occur, the number of noninvolved workers with the potential for adverse effects would range from 0 to around 1,400 (maximum corresponding to an NH<sub>3</sub> tank rupture), and the number of noninvolved workers with the potential for irreversible adverse effects would range from 0 to around 1,400 (maximum also corresponding to an NH<sub>3</sub> tank rupture).
- For the most severe accidents in each frequency category, the noninvolved worker MEI and the public MEI would have the potential for both adverse effects and irreversible adverse effects. The likely accidents for each conversion option (frequency of more than 1 chance in 100 per year) would result in no potential adverse or irreversible adverse effects for the general public.
- The maximum risk was computed as the product of the consequence (number of people) times the frequency of occurrence (occurrences per year) times the number of years of operations (18 years). These risk values are conservative because the numbers of people affected were based on the following assumptions: (1) occurrence of very low wind speed and moderately stable meteorological conditions that would result in the maximum reasonably foreseeable plume size (i.e., F stability and a 1-m/s [2-mph] wind speed) and (2) steady or nonmeandering wind direction, lasting up to 3 hours and blowing toward locations that would lead to the maximum number of individuals exposed for noninvolved workers or for the general population. The results indicate that the maximum risk values would be less than 1 for all accidents except the following:
  - *Potential Adverse Effects:*
    - Corroded cylinder spill, dry conditions (L, likely), workers  
Assuming the accident occurred once every 10 years, 7, 40, and 90 workers would potentially experience adverse effects at Locations A, B, and C, respectively, over the entire 18-year operational period.
    - Corroded cylinder spill, wet conditions – rain (U, unlikely), workers  
Assuming the accident occurred once every 1,000 years (frequency = 10<sup>-3</sup>/yr), about 9 workers would potentially experience adverse effects over the 18-year operational period at any of the three alternative locations.
  - *Potential Irreversible Adverse Effects:*
    - Corroded cylinder spill, wet conditions – rain (U, unlikely), workers  
Assuming the accident occurred once every 1,000 years (frequency = 10<sup>-3</sup>/yr), about 2 workers would potentially experience an irreversible adverse health effect over the 18-year operational period at all three locations.

The number of fatalities that could potentially be associated with the estimated irreversible adverse effects was also calculated. Previous analyses indicated that exposure to HF and uranium compounds, if sufficiently high, could result in death to 1% or fewer of the persons experiencing irreversible adverse effects (Policastro et al. 1997). Similarly, it was estimated that exposure to NH<sub>3</sub> could result in death to about 2% of the persons experiencing irreversible adverse effects (Policastro et al. 1997). Therefore, if the corroded cylinder spill, wet conditions – rain accident occurred (Table 5.2-16), about one fatality might be expected among the noninvolved workers at any of the three locations: A, B, or C. However, this accident is classified as an unlikely accident, meaning that it is estimated to occur between once in 100 years and once in 10,000 years of facility operation. Assuming that it would occur once every 1,000 years, the risk of fatalities among the noninvolved workers from this accident over the 18-year operational period would be less than 1 ( $1 \times 0.0001 \times 18 = \approx 0.02$ ). (See Section 4.3 for discussion on the interpretation of risk numbers that are less than 1.)

Similarly, if the higher-consequence accident in the extremely unlikely frequency category (corroded cylinder spill, wet conditions – water pool) in Table 5.2-16 occurred, approximately 2 fatalities might be expected among the noninvolved workers, irrespective of the location chosen. However, because of the low frequency of this accident, the risk of a fatality over the lifetime of the conversion facility would be about 0.0004, assuming a frequency of 0.00001 per year.

For the NH<sub>3</sub> tank rupture accident, which belongs to the incredible frequency category (frequency of less than 0.000001 per year), the expected numbers of fatalities among the noninvolved workers would be about 16, 28, and 22 for Locations A, B, and C, respectively. However, the risk of a fatality would be much less than 1 at any of the locations (0.0001 at Location A, 0.0003 at Location B, and 0.0002 at Location C, assuming a frequency of  $5 \times 10^{-7}$  per year) over the facility lifetime. Among the general public, 4 fatalities might be expected if the same accident occurred. However, because of the low frequency of the accident, the risk of fatalities would be much less than 1 (about 0.00004).

Even though the risks are relatively low, the consequences for a few of the accidents are considered to be high. These high-consequence accidents are generally associated with the storage of anhydrous NH<sub>3</sub> and aqueous HF on site. The consequences can be reduced or mitigated through design (e.g., by limiting tank capacity), operational procedures (e.g., by controlling accessibility to the tanks), and emergency response actions (e.g., by sheltering, evacuation, and interdiction of contaminated food materials following an accident). For example, UDS is proposing to reduce the size of the anhydrous NH<sub>3</sub> storage tanks from 9,200 to 3,300 gal (35,000 to 12,000 L). This change would reduce the consequences of an NH<sub>3</sub> release accident. However, to conservatively estimate the consequences of an anhydrous NH<sub>3</sub> tank rupture and preserve process flexibility, this analysis retained the assumption of a 9,200-gal (35,000-L) tank size.

**5.2.3.2.3 Physical Hazards.** The risk of on-the-job fatalities and injuries to conversion facility workers was calculated by using industry-specific statistics from the BLS, as reported by the National Safety Council (2002). Annual fatality and injury rates from the BLS manufacturing

industry division were used for the 18-year operations phase, assuming ETTP cylinders are processed there. Operation of the conversion facility is estimated to require approximately 175 FTEs per year. No on-the-job fatalities are predicted during the conversion facility operational phase. It is estimated, however, that about 142 injuries would occur (Table 5.2-4).

### 5.2.3.3 Air Quality and Noise

**5.2.3.3.1 Air Quality Impacts.** Three alternative locations (Locations A, B, and C) were considered for air quality impacts. Detailed information on facility boundaries and the orientations and locations of buildings and stacks is currently available for the preferred Location A only. For Locations B and C, the layout of the facility for Location A was assumed to be placed in the middle of the other two locations.

At the conversion facility, air pollutants would be emitted from four point sources: the boiler stack, backup generator stack, conversion building stack, and HF processing building stack. UDS is proposing to use electrical heating in the conversion facility, but it is evaluating other options. If natural gas was chosen, furnaces or boilers could be used. To assess bounding air quality impacts, a boiler option was analyzed because it would result in more emissions than furnaces or electric heat. The boiler could be used to generate process steam and building heat, and a backup generator would be used to provide emergency electricity. Primary emission sources for criteria pollutants and VOCs would be the boiler and the emergency generator. The conversion building stack would release uranium, fluoride, criteria pollutants, and VOCs in minute amounts, while the HF processing building stack would release fluorides into the atmosphere. Although nitrogen would be used as a purge gas in the process, its use would not generate additional NO<sub>x</sub> emissions because of the absence of oxygen in contact with the nitrogen stream at high temperatures. Annual total stack emission rates during operations are given in the Engineering Support Document (Folga 2003); these emission rates are presented in Table 5.2-17. Other sources during operations would include vehicular traffic to and from the facility, associated with cylinder transfer, commuting, and material delivery. Parking lots and access roads to the facility would be paved with asphalt or concrete to minimize fugitive dust emissions. In addition, fugitive emissions would include those from storage tanks, silos, cooling towers, etc., but in negligible amounts.

The modeling results for concentration increments of SO<sub>2</sub>, NO<sub>2</sub>, CO, PM<sub>10</sub>, PM<sub>2.5</sub>, and HF due to emissions from the proposed facility operations are summarized in Table 5.2-18. The results are maximum modeled concentrations at or beyond the conversion facility boundary. The total concentrations (modeled concentration increments plus background concentrations) are also presented in the table for comparison with applicable NAAQS and SAAQS.

Because of low emissions during operations, all air pollutant concentration increments would be well below applicable standards. As shown in Table 5.2-18, the estimated maximum concentration increments due to operation of the proposed facility would amount to about 16% of the applicable standard for 3-hour average SO<sub>2</sub>. These concentration increments are primarily

**TABLE 5.2-17 Annual Point Source Emissions of Criteria Pollutants, Volatile Organic Compounds, Uranium, and Fluoride from Operation of the Conversion Facility at the Portsmouth Site**

Pollutant	Emission Rate <sup>a</sup>			
	Boiler <sup>b</sup>	Backup Generator	Conversion Building Stack	HF Processing Building Stack
SO <sub>2</sub>	0.01	0.17	$9.7 \times 10^{-4}$	– <sup>c</sup>
NO <sub>x</sub>	2.09	1.20	$2.5 \times 10^{-2}$	–
CO	1.25	0.17	$4.0 \times 10^{-2}$	–
VOC	0.08	0.17	$1.2 \times 10^{-2}$	–
PM <sub>10</sub> <sup>d</sup>	0.11	0.07	$6.8 \times 10^{-3}$	–
Uranium	–	–	< 0.25 g/yr	–
Fluoride	–	–	<0.005 ppm <sup>e</sup>	< 0.05 ppm <sup>f</sup>

<sup>a</sup> Tons/yr unless otherwise noted.

<sup>b</sup> Boiler emissions were estimated on the basis of annual natural gas usage given in Table 5.2-22.

<sup>c</sup> A dash indicates no or negligible emissions.

<sup>d</sup> PM<sub>2.5</sub> emissions are assumed to be the same as PM<sub>10</sub> emissions.

<sup>e</sup> Annual emission is about 0.8 kg (1.8 lb) as HF.

<sup>f</sup> Annual emission is about 55.8 kg (123 lb) as HF.

due to a backup generator, which is located next to the conversion building and the site boundaries and within the building cavity/wake region. However, the generator would be operating on an intermittent basis; thus, air quality impacts would be limited to the period of its operation. The maximum total concentrations, except for PM<sub>2.5</sub>, would be about 64%, well below their applicable standards. However, it is estimated that total PM<sub>2.5</sub> concentration would be approaching (91%) or above (161%) the standard. However, concentration increments from operations are predicted to account for only 2.8% of the standard. As previously mentioned, the annual average PM<sub>2.5</sub> concentration at most statewide monitoring stations would either approach or exceed the standard.

The air quality impacts would be limited to the immediate vicinity of the site boundaries. For example, maximum predicted concentrations at the nearest residence would be about 11% of

**TABLE 5.2-18 Maximum Air Quality Impacts Due to Emissions from Activities Associated with Operation of the Conversion Facility at the Portsmouth Site**

Location	Pollutant	Averaging Time	Maximum Increment <sup>a</sup>	Background <sup>b</sup>	Total <sup>c</sup>	NAAQS and SAAQS	Concentration (µg/m <sup>3</sup> )	
							Percent of NAAQS/SAAQS <sup>d</sup>	
							Increment	Total
A	SO <sub>2</sub>	3 hours	127	307	434	1,300	9.8	33.4
		24 hours	57.1	110	167	365	15.6	45.8
		Annual	0.08	18.7	18.8	80	0.1	23.5
	NO <sub>2</sub>	Annual	0.6	54.7	55.3	100	0.6	55.3
	CO	1 hour	245	13,400	13,600	40,000	0.6	34.1
		8 hours	84.9	4,780	4,860	10,000	0.8	48.6
	PM <sub>10</sub>	24 hours	11.8	64	75.8	150	7.8	50.5
		Annual	0.03	32	32.0	50	0.1	64.1
	PM <sub>2.5</sub>	24 hours	1.7	57.5	59.2	65	2.6	91.1
		Annual	0.03	24.1	24.1	15	0.2	161
	HF <sup>e</sup>	12 hours	0.07	0.45	0.52	3.68	1.9	14.3
		24 hours	0.05	0.37	0.42	2.86	1.8	14.8
		1 week	0.02 <sup>f</sup>	0.21	0.23	1.64	1.1	13.9
		1 month	0.01	0.14	0.14	0.82	0.9	17.6
		Annual	0.003	0.07	0.07	400	0.001	0.02
B	SO <sub>2</sub>	3 hours	161	307	468	1,300	12.4	36.0
		24 hours	47.8	110	158	365	13.1	43.2
		Annual	0.06	18.7	18.8	80	0.1	23.5
	NO <sub>2</sub>	Annual	0.5	54.7	55.2	100	0.5	55.2
	CO	1 hour	258	13,400	13,700	40,000	0.6	34.1
		8 hours	86.7	4,780	4,870	10,000	0.9	48.7
	PM <sub>10</sub>	24 hours	14.8	64	78.8	150	9.8	52.5
		Annual	0.03	32	32.0	50	0.1	64.1
	PM <sub>2.5</sub>	24 hours	1.9	57.5	59.4	65	2.8	91.3
		Annual	0.03	24.1	24.1	15	0.2	161
	HF <sup>e</sup>	12 hours	0.07	0.45	0.52	3.68	1.8	14.1
		24 hours	0.05	0.37	0.42	2.86	1.6	14.6
		1 week	0.02 <sup>f</sup>	0.21	0.23	1.64	1.0	13.8
		1 month	0.01	0.14	0.14	0.82	0.6	17.4
		Annual	0.003	0.066	0.07	400	0.001	0.02

**TABLE 5.2-18 (Cont.)**

Location	Pollutant	Averaging Time	Maximum Increment <sup>a</sup>	Concentration (µg/m <sup>3</sup> )				
				Background <sup>b</sup>	Total <sup>c</sup>	NAAQS and SAAQS	Percent of NAAQS/SAAQS <sup>d</sup>	
							Increment	Total
C	SO <sub>2</sub>	3 hours	208	307	515	1,300	16.0	39.6
		24 hours	45.3	110	155	365	12.4	42.6
		Annual	0.08	18.7	18.8	80	0.1	23.5
	NO <sub>2</sub>	Annual	0.6	54.7	55.3	100	0.6	55.3
	CO	1 hour	260	13,400	13,700	40,000	0.7	34.2
		8 hours	88.1	4,780	4,870	10,000	0.9	48.7
	PM <sub>10</sub>	24 hours	14.2	64	78.2	150	9.5	52.1
		Annual	0.04	32	32.0	50	0.1	64.1
	PM <sub>2.5</sub>	24 hours	1.7	57.5	59.2	65	2.5	91.0
		Annual	0.04	24.1	24.1	15	0.2	161
	HF <sup>e</sup>	12 hours	0.15	0.45	0.61	3.68	4.1	16.5
		24 hours	0.11	0.37	0.48	2.86	3.7	16.7
		1 week	0.04 <sup>f</sup>	0.21	0.25	1.64	2.2	15.0
		1 month	0.01	0.14	0.15	0.82	1.3	18.1
Annual		0.006	0.066	0.07	400	0.001	0.02	

<sup>a</sup> Data represent the maximum concentration increments estimated, except that the fourth- and eighth-highest concentration increments estimated are listed for 24-hour PM<sub>10</sub> and PM<sub>2.5</sub>.

<sup>b</sup> See Table 3.1-3 for criteria pollutants and DOE (2002b) for highest weekly and annual HF. Background HF for other averaging times was estimated based on highest weekly annual background concentrations.

<sup>c</sup> Total equals the maximum modeled concentration increment plus background concentration.

<sup>d</sup> The values in the next-to-last column are maximum concentration increments as a percent of NAAQS and SAAQS. The values presented in the last column are total concentrations as a percent of NAAQS and SAAQS.

<sup>e</sup> State HF standards in Ohio are not available, so Kentucky standards were used for comparative purposes.

<sup>f</sup> Estimated by interpolation.

the highest concentration. It is also expected that potential impacts from the proposed facility operations on the air quality of nearby communities would be insignificant.<sup>4</sup>

The maximum 3-hour, 24-hour, and annual SO<sub>2</sub> concentration increments predicted to result from the proposed facility operations would be about 63% of the applicable PSD

<sup>4</sup> Formerly, the general public had access to the existing fenced gaseous diffusion plant boundaries. However, since the September 11, 2001, terrorist attack, site access for the general public has been restricted indefinitely to the DOE property boundaries.

increments (Table 3.2-3). The maximum predicted increments in annual average NO<sub>2</sub> concentrations due to the proposed facility operations would be about 3% of the applicable PSD increments. The 24-hour and annual PM<sub>10</sub> concentration increases predicted to result from the proposed operations would be about 49% of the applicable PSD increments. The predicted concentration increment at a receptor located 30 mi (50 km) from the proposed facility (the maximum distance for which the Industrial Source Complex [ISC3] short-term model [EPA 1995] could reliably estimate concentrations) in the direction of the nearest Class I PSD area (Otter Creek Wilderness Area, West Virginia) would be far less than 0.5% of the applicable PSD increments. Concentration increments at this wilderness area, which is located about 177 mi (285 km) west of Portsmouth, would be negligible.

Concentration increments for the two remaining criteria pollutants, Pb and O<sub>3</sub>, were not modeled. As a direct result of the phase-out of leaded gasoline in automobiles, average Pb concentrations in urban areas throughout the country have decreased dramatically. It is expected that emissions of Pb from the proposed facility operations would be negligible and would therefore have no adverse impacts on Pb concentrations in surrounding areas. Contributions to the production of O<sub>3</sub>, a secondary pollutant formed from complex photochemical reactions involving O<sub>3</sub> precursors, including NO<sub>x</sub> and VOCs, cannot be accurately quantified. As discussed in Section 3.1.3.2, Pike County, including the Portsmouth site, is currently in attainment for O<sub>3</sub> (40 CFR 81.336). The O<sub>3</sub> precursor emissions from the proposed facility stacks would make up about 0.7% and 3.8% of the year 2001 combined Portsmouth DOE and USEC emissions of NO<sub>x</sub> and VOCs, respectively (see Table 3.1-2). These emission levels would be negligible in absolute terms (compared with statewide emissions). As a consequence, the cumulative impacts of potential releases from Portsmouth facility operations on regional O<sub>3</sub> concentrations would not be of any concern.

Maximum HF air quality impacts are also listed in Table 5.2-18. State HF standards in Ohio are not available; thus, Kentucky standards were used for comparative purposes. The estimated maximum short-term ( $\leq 1$  month) HF concentration increment and total concentrations would be about 4.1% and 18.1% of the state standard, respectively, which are still well below the standards. The annual average concentration increment and total concentration would be several orders of magnitude lower than the HF air quality standard.

In summary, except for annual average PM<sub>2.5</sub>, total concentrations of criteria pollutants would be well below their respective standards. Total maximum estimated concentrations of criteria pollutants, except PM<sub>2.5</sub>, would be less than 64% of NAAQS and SAAQS. Predicted total concentrations of 24-hour and annual average PM<sub>2.5</sub> would be near or above their respective standards, respectively; however, their concentration increments associated with site operations would account for only about 2.8% of the standards. In particular, the annual average PM<sub>2.5</sub> concentration at most statewide monitoring stations would either approach or exceed the standard.

**Accidents.** Among chemicals released due to accidents, HF is the only one subject to an ambient air quality standard (the state of Ohio does not have ambient air quality standards for HF, so those for the state of Kentucky were used for comparison purposes). Most accidental

releases would occur over a short duration, about 2 hours at most. The passage time of an elevated-concentration plume for any receptor location would be a little longer than its release duration. The HF concentration in the plume's path would exceed the 12-hour or 24-hour ambient standard for the HF tank rupture accident scenario; however, when concentrations are averaged over a year, the annual ambient air quality standard would not be exceeded. Therefore, potential impacts of accidental releases on ambient air quality would be short-term and limited to along the plume path, and long-term impacts would be negligible.

**5.2.3.3.2 Noise Impacts.** Many noise sources associated with operation would be inside the buildings. The highest noise levels are expected inside the conversion facility in the area of the powder receiver vessels, with measured readings at 77 to 79 dB(A), and in the area of the dry conversion, with a reading of 72 to 74 dB(A) (UDS 2003b). Ambient facility noise levels, measured in various processing areas (inside buildings) for continuous operations of a facility at Richland, Washington, ranged from 70 to 79 dB(A). Major outdoor noise sources associated with operation would include the cooling tower, trucks and heavy equipment moving cylinders, and traffic moving to and from the facility, which are typical industrial noise sources. Heavy equipment and truck traffic would be intermittent, so noise levels would be low except when the equipment was moving or operating. For noise impact analyses, a continuous noise source during operation was assumed to be about 79 dB(A) at a distance of 15 m (50 ft), on the basis of the highest noise level measured inside buildings at the Richland facility (UDS 2003b).<sup>5</sup>

The nearest residence, located about 0.9 km (0.6 mi) south-southeast of Location B and just off DOE's southern boundary, was selected as the receptor for the analysis of potential noise impacts. Noise levels decrease about 6 dB per doubling of distance from the point source because of the way sound spreads geometrically over an increasing distance. The estimated noise level would result in about 43 dB(A) at the nearest residence. This level would be about 49 dB(A) as DNL, if 24-hour continuous operation is assumed. The 49-dB(A) estimate is just below the EPA guideline of 55 dB(A) as DNL for residential zones (see Section 3.1.3.4), which was established to prevent interference with activity, annoyance, and hearing impairment. If other attenuation mechanisms, such as ground effects or air absorption, are considered, noise levels at the nearest residence would considerably decrease. If only ground effects are considered (HMMH 1995), more than 10 dB(A) of attenuation would occur at the nearest residence, which would result in about 39 dB(A) as DNL, well below the EPA guideline.

Most trains would blow their whistle loud enough to ensure that all motorists and pedestrians nearby would be aware of an approaching train. These excessive noises could disturb those who live or work near the train tracks. Typical noise levels of train whistles would range from 95 to 115 dB(A) at a distance of 30 m (100 ft), comparable to noise levels of low-flying aircraft or emergency vehicle sirens (DOT 2003a). The total number of shipments (railcars) associated with facility operations would be less than 5,000. This would be equivalent to about one train per week, assuming five railcars per train. Accordingly, the noise level from train

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<sup>5</sup> The noise level from one of the continuous outdoor noise sources, a cooling tower, to be used at this size of facility would be less than 79 dB(A) at a distance of 15 m (50 ft).

operations would be high along the rail tracks and particularly near the crossings. However, noise impacts would be infrequent and of short duration.

In general, facility operations produce less noise than construction activities. For all three alternative locations, except for intermittent vehicular traffic and infrequent rail traffic, the noise level at the nearest residence would be somewhat higher than the ambient background level discussed in Section 3.1.3.4, and it would be barely distinguishable from the background level, depending on the time of the day. In conclusion, noise levels generated by plant operation would have minor impacts on the residence located nearest to the proposed facility and would be well below the EPA guideline limits for residential areas.

#### 5.2.3.4 Water and Soil

Operating a conversion facility at Portsmouth could disturb land, use water, and produce liquid wastes. Impacts on surface water, groundwater, and soil resources are discussed below. Because no site-specific impacts to water and soil were identified, impacts at alternative Locations A, B, and C would be the same.

**5.2.3.4.1 Surface Water.** Impacts from operating a conversion facility at Portsmouth would be independent of the location selected at Portsmouth; all of the water needed would be withdrawn from the system of on-site and off-site wells. Because all of the water needed for operating a conversion plant at Portsmouth would be obtained from groundwater wells, there would be no impacts on surface water resources.

During facility operations, about 4,000 to 8,000 gal/d (15,140 to 30,280 L/d) of sanitary wastewater would be processed. There would also be about 3,000 gal/d (11,400 L/d) of process wastewater produced during normal operations. This water would not contain any radionuclides. Another 23,000 gal/d (87,100 L/d) (8.4 million gal/yr [31.8 million L/yr]) of wastewater would be produced by cooling tower blowdown, and 36,000 gal/d (136,300 L/d) of wastewater would be produced if HF neutralization was required. These wastewaters would not contain any radionuclides and could be disposed of to the existing process wastewater treatment system at Portsmouth, or discharged under a NPDES permit, or treated and reused at the conversion facility. Disposition of these wastewaters is under evaluation.

Discharge effluent would be treated prior to discharge. The existing water treatment plant processes about 4,533 million gal (17,160 million L) of wastewater per year. The additional wastewater produced by a conversion plant would be a maximum of about 0.2% of the current treatment volume. Once in surface water, the effluent would be diluted. At Portsmouth, effluent discharge would go to Little Beaver Creek or the Scioto River. If released at a constant rate, the approximately 30,000 gal/d (114,000 L/d) of wastewater would flow at about 21 gal/min (80 L/min). This small increase in flow would produce negligible impacts to Little Beaver Creek, Big River Creek, and the Scioto River. Because the release water would be treated, impacts to

water quality would also be negligible, even without the additional dilution expected (45 for Little Beaver Creek).

**Accidents.** An earthquake could rupture an aboveground HF pipeline that would carry liquid HF from the conversion building to the HF storage building at a rate of 10 gal/min (38 L/min). Approximately 910 lb (410 kg) of liquid HF would be released. Because response and cleanup would occur within a relatively short time after the release (i.e., days or weeks), the HF would have little time to migrate into the soil, and very little would be transported by runoff to nearby surface waters. Removal of the contaminated soil would prevent any contamination of surface water or groundwater resources. Therefore, there would be no impacts on surface water or groundwater from this accident. A similar quick response and cleanup would minimize impacts for an HF spill to the ground during transfer to railcars.

**5.2.3.4.2 Groundwater.** All operational water needs at the Portsmouth site would be satisfied by using groundwater resources. Peak potable and nonpotable water use for the Portsmouth plant would be about 33 million gal/yr (125 million L/yr). An additional 1.1 million gal (4.2 million L) of process water per year would be required. If this water was withdrawn at a constant rate, the withdrawal would represent an increase of about 0.8% of the current water use and 0.3% of the existing capacity. Impacts from this rate of extraction would be small.

In addition, the quality of groundwater beneath the selected location could be affected by infiltrating contaminated surface water from spills. Indirect contamination could result from the dissolution and mobilization of exposed chemicals by precipitation and subsequent infiltration of the contaminated runoff into the surficial aquifers. By following good engineering and operating practices (e.g., covering chemicals to prevent interaction with rain, promptly and thoroughly cleaning up any spills, and providing retention basins to catch and hold any contaminated runoff), impacts on groundwater quality would be minimized.

**Accidents.** An earthquake could rupture the aboveground HF pipeline that would carry liquid HF from the conversion building to the HF storage building. Because of rapid response and cleanup times, the travel distance of the released HF would be small. Removal of the contaminated soil would prevent any contamination of underlying groundwater resources. Therefore, there would be no impacts on groundwater from this type of accident. A similar quick response and cleanup would minimize impacts for an HF spill to the ground during transfer to railcars.

**5.2.3.4.3 Soils.** Normal operations of a conversion facility at the Portsmouth site would have no direct impacts on soil at all three alternative locations.

**Accidents.** The only accidents identified that could potentially affect soil would be an HF pipeline rupture and an HF spill to the ground during transfer to railcars. Because mitigation would be initiated rapidly and because the volume of HF released would be small (910 lb [410 kg]), impacts on soil would be negligible.

**5.2.3.5 Socioeconomics**

The socioeconomic analysis covers the effects on population, employment, income, regional growth, housing, and community resources in the ROI around the Portsmouth site. Impacts from operations, which are the same for all three alternative locations, are summarized in Table 5.2-19.

The potential socioeconomic impacts from operations would be relatively small. Operational activities would create about 160 direct jobs annually and about 160 more indirect jobs in the ROI. A conversion facility would produce about \$13 million in personal income annually during operations.

It is estimated that about 220 people would move to the area at the beginning of operations. However, in-migration would have only a marginal effect on population growth and would require about 1% of vacant owner-occupied housing during facility operations. No significant impact on public finances would occur as a result of in-migration, and fewer than five new local public service employees would be required to maintain existing levels of service in the various local public service jurisdictions in Pike and Scioto Counties.

**TABLE 5.2-19 Socioeconomic Impacts from Operation of the Conversion Facility at the Portsmouth Site<sup>a</sup>**

Impact Area	Operation
Employment	
Direct	160
Total	320
Income (millions of 2002 \$)	
Direct	5.8
Total	12.9
Population (no. of new ROI residents)	220
Housing (no. of units required)	80
Public finances (% impact on fiscal balance)	
Cities in Pike County <sup>b</sup>	0.2
Pike County	0.1
Schools in Pike County <sup>c</sup>	0.2
Cities in Scioto County <sup>d</sup>	0.2
Scioto County	0.2
Schools in Scioto County <sup>e</sup>	0.2
Public service employment (no. of new employees)	
Pike County	
Police officers	0
Firefighters	0
General	1
Physicians	0
Teachers	1
Scioto County	
Police officers	0
Firefighters	0
General	1
Physicians	0
Teachers	1
No. of new staffed hospital beds	
Pike County	1
Scioto County	1

<sup>a</sup> Impacts are shown for the first year of operations (2006).

<sup>b</sup> Includes impacts that would occur in the cities of Waverly and Piketon.

<sup>c</sup> Includes impacts that would occur in Waverly and Pike County school districts.

<sup>d</sup> Includes impacts that would occur in the City of Portsmouth.

<sup>e</sup> Includes impacts that would occur in New Boston, Portsmouth, Wheelersburg, and Scioto County school districts.

### 5.2.3.6 Ecology

**5.2.3.6.1 Vegetation.** A portion of the conversion product released from the process stack of the conversion facility would become deposited on the soils surrounding the site. Uptake of uranium-containing compounds could cause adverse effects to vegetation. Deposition of uranium compounds on soils, resulting from atmospheric emissions, would result in soil uranium concentrations considerably below the lowest concentration known to produce toxic effects in plants. Because there would not be a release of process effluent from the facility to surface waters, impacts to vegetation along nearby streams would not occur. Therefore, toxic effects on vegetation due to uranium uptake would be expected to be negligible.

**5.2.3.6.2 Wildlife.** Noise generated by the operation of a conversion facility at Location A and disturbance from human presence would likely result in a minor disturbance to wildlife in the vicinity. Movement of railcars along the new rail line west of the facility might potentially render the adjacent riparian forest habitat unsuitable for some species. In addition, the rail line might impede the movement of some small wildlife species.

During operations, ecological resources in the vicinity of the conversion facility would be exposed to atmospheric emissions from the boiler stack, cooling towers, and process stack; nevertheless, emission levels are expected to be extremely low. The highest average air concentration of uranium compounds would result in a radiation exposure to the general public (nearly 100% due to inhalation) of  $2.07 \times 10^{-5}$  mrem/yr, well below the DOE guideline of 100 mrem/yr (DOE 2002f). Wildlife species are less sensitive to radiation than humans. (DOE guidelines require an absorbed dose limit to terrestrial animals of less than 0.1 rad/d [DOE 2002f].) Therefore, impacts on wildlife due to radiation effects are expected to be negligible. Toxic effect levels of chronic inhalation of uranium are many orders of magnitude greater than expected emissions. Therefore, toxic effects on wildlife as a result of inhalation of uranium compounds are also expected to be negligible.

The maximum annual average air concentration of HF that would result from operation of a conversion facility would be  $0.0028 \mu\text{g}/\text{m}^3$ . Toxic effect levels of chronic inhalation of HF are many orders of magnitude greater than expected emissions. Therefore, toxic effects on wildlife from HF emissions are expected to be negligible.

Impacts to wildlife from the operation of a conversion facility at Locations B or C would be similar to impacts at Location A. Noise and human presence would likely result in a minor disturbance to wildlife in the vicinity.

**5.2.3.6.3 Wetlands.** Liquid process effluents would not be discharged to surface waters during the operation of the conversion facility (Section 5.2.3.4). Surface water sources are also not expected to be used to meet water requirements during operations. Changes in groundwater as a result of the withdrawal of groundwater for facility operations would be small to negligible (Section 5.2.2.4). Therefore, except for potential local indirect impacts near the facility, impacts

to regional wetlands due to changes in groundwater or surface water levels or flow patterns are not expected to occur. As a result, adverse effects on wetlands or aquatic communities from effluent discharges or water use are not expected.

Storm water runoff from conversion facility parking areas and other paved surfaces might carry contaminants commonly found on these surfaces to local streams. Biota in receiving streams might be affected by these contaminants, resulting in reduced species diversity or changes in community composition. Storm water discharges from the conversion facility would be addressed under a new or existing NPDES permit for industrial facility storm water discharge. The streams near Locations A, B, and C currently receive runoff and associated contaminants from various roadways on the Portsmouth site, and their biotic communities are likely indicative of developed areas.

**5.2.3.6.4 Threatened and Endangered Species.** Impacts to federal- or state-listed species during operation of a conversion facility at Location A are not expected. However, although the wooded areas at Location A have not been identified as summer roosting habitat for the Indiana bat (federal- and state-listed as endangered), disturbances from increased noise, lighting, and human presence due to facility operation and the movement of railcars along the new rail line west of the facility might decrease the quality of the adjacent riparian forest habitats for use by Indiana bats. However, Indiana bats that might currently be using habitat near the Portsmouth site would already be exposed to noise and other effects of human disturbance due to operation of the site, including vehicle traffic. In addition, Indiana bats have been observed to tolerate increased noise levels (U.S. Fish and Wildlife Service [USFWS] 2002). Consequently, disturbance effects related to conversion facility operation are expected to be minor. The operation of a conversion facility at Location C might similarly decrease the quality of wooded areas at that location for Indiana bat summer habitat, although these locations have also not been identified as containing Indiana bat habitat. Location B does not support habitat suitable to the Indiana bat.

#### **5.2.3.7 Waste Management**

Operations at the conversion facility would generate radioactive, hazardous, and nonhazardous waste, as shown in Table 5.2-20. Waste volumes generated would be the same for all three alternative locations. The total waste volumes for 18 years of operation would be 772 yd<sup>3</sup> (590 m<sup>3</sup>) of LLW and 98 yd<sup>3</sup> (74 m<sup>3</sup>) of hazardous waste. These volumes would result in low impacts on site annual projected volumes. If ETTP cylinders were not processed at Portsmouth, the waste volumes would be reduced by 26 yd<sup>3</sup> (20 m<sup>3</sup>) of LLW, 5 yd<sup>3</sup> (4 m<sup>3</sup>) of hazardous waste, and 125 yd<sup>3</sup> (96 m<sup>3</sup>) of nonhazardous solid waste.

CaF<sub>2</sub> would be produced in the U<sub>3</sub>O<sub>8</sub> conversion process and is assumed to have a low uranium content. It is currently unknown whether this CaF<sub>2</sub> could be sold (e.g., as feedstock for commercial production of anhydrous HF) or whether the low uranium content would force disposal. If CaF<sub>2</sub> disposal is necessary, it could be either as a nonhazardous solid waste (provided that authorized limits have been established in accordance with DOE Order 5400.5

[DOE 1990] and its associated guidance) or as LLW. The nonhazardous solid waste generation estimate for conversion to U<sub>3</sub>O<sub>8</sub>, as shown in Table 5.2-20, is based on the assumption that CaF<sub>2</sub> would be disposed of as nonhazardous solid waste at a rate of approximately 13 yd<sup>3</sup>/yr (10 m<sup>3</sup>/yr). This represents a negligible impact to the annual site generation rate for this waste type. If CaF<sub>2</sub> was disposed of as LLW, it would represent less than 1% of the projected site annual LLW load.

If the HF was not marketable, neutralization of HF to CaF<sub>2</sub> would produce approximately 3,745 yd<sup>3</sup>/yr (2,860 m<sup>3</sup>/yr) of CaF<sub>2</sub>. This volume represents approximately 89% and 4% of nonhazardous solid waste and LLW, respectively, of the projected annual generation volumes for Portsmouth. It is unknown whether CaF<sub>2</sub> LLW would be considered DOE waste if the conversion was conducted by a private commercial enterprise. If CaF<sub>2</sub> could be sold, the nonhazardous solid waste or LLW management impacts would be lower.

The U<sub>3</sub>O<sub>8</sub> produced from the conversion process would generate about 4,700 yd<sup>3</sup>/yr (3,570 m<sup>3</sup>/yr) of LLW. This volume is about 5% of the annual site-projected volume for LLW and constitutes a low impact on site LLW management.

Current UDS plans are to leave the heels in the emptied cylinders, fill them with the depleted U<sub>3</sub>O<sub>8</sub> product, and dispose of them at either Envirocare or NTS. This approach is expected to meet the waste acceptance criteria of the disposal facilities and eliminate the potential for generating TRU waste (see Appendix B for additional information concerning TRU and PCB contamination). However, it is possible that the heels could be washed from the emptied cylinders if it was decided to reuse the cylinders for other purposes. In this case, the TRU in the heels of some cylinders at the maximum postulated concentrations could also result in the generation of some TRU waste at the conversion facility (see Appendix B). It is estimated that up to 30% (or 244 drums) of the heels could contain enough TRU to qualify this material as TRU waste if it was disposed of as waste. In this case, it is estimated that a volume of about 2.6 yd<sup>3</sup>/yr (2.0 m<sup>3</sup>/yr) of TRU and 6.0 yd<sup>3</sup>/yr (4.4 m<sup>3</sup>/yr) of LLW would be generated.

**TABLE 5.2-20 Wastes Generated from Operation of the Conversion Facility at the Portsmouth Site**

Waste Category	Annual Volume <sup>a</sup>
<b>LLW</b>	
Combustible waste	26 m <sup>3</sup>
Noncombustible	6.4 m <sup>3</sup>
Others	<1.0 m <sup>3</sup>
Total <sup>b</sup>	33 m <sup>3</sup>
Hazardous waste <sup>c</sup>	4.1 m <sup>3</sup>
<b>Nonhazardous waste</b>	
Solids <sup>d</sup>	144 m <sup>3</sup>
Sanitary wastewater	5.5 × 10 <sup>6</sup> L

- <sup>a</sup> Represents annual volume generated from Portsmouth cylinders only.
- <sup>b</sup> Includes LLW from high-efficiency particulate air (HEPA) filters and laboratory acids and residues. The total volume of LLW from ETTP cylinders is about 20 m<sup>3</sup> (26 yd<sup>3</sup>).
- <sup>c</sup> Includes the total volume of hazardous waste from ETTP cylinders of 4 m<sup>3</sup> (5 yd<sup>3</sup>).
- <sup>d</sup> Includes CaF<sub>2</sub> generation from the conversion process. The total volume of nonhazardous waste from ETTP cylinders is about 95 m<sup>3</sup> (125 yd<sup>3</sup>).

Source: UDS (2003b).

In addition, a small quantity of TRU could be entrained in the gaseous DUF<sub>6</sub> during the cylinder emptying operations and carried out of the cylinders. These contaminants would be captured in the filters between the cylinders and the conversion equipment. The filters would be monitored and replaced routinely to prevent buildup of TRU. The spent filters would be disposed of as LLW. It is estimated that the amount of LLW generated in the form of spent filters would be about 1 drum per year for a total of 18 drums (drums are 55 gal [208 L] in size) for the duration of the conversion operations (see Appendix B). This converts to a total volume of 5.0 yd<sup>3</sup> (3.7 m<sup>3</sup>) of LLW. In the unlikely event that small amounts of TRU waste are generated from the conversion facility, the waste would be managed in accordance with DOE's policy for TRU waste, which includes the packaging and transport of these wastes to the Waste Isolation Pilot Plant (WIPP) in New Mexico for disposal.

### 5.2.3.8 Resource Requirements

Resource requirements during operations would not depend on the location of the conversion facility. Facility operations would consume electricity, fuel, and miscellaneous chemicals that are generally irretrievable resources. Estimated annual consumption rates of operating materials are provided in Table 5.2-21. The total quantity of commonly used materials is not expected to be significant and would not affect their local, regional, or national availability. In general, facility operational resources required are not considered rare or unique.

Operation of the facility could include the consumption of fossil fuels used to generate steam and heat and electricity (Table 5.2-22). Energy would also be expended in the form of diesel fuel and gasoline for cylinder transport equipment and transportation vehicles. The existing infrastructure at the site appears to be sufficient to supply the required utilities.

### 5.2.3.9 Land Use

Because the preferred location (Location A) for the facility already contains structures, operations would be generally consistent with current land use. As a consequence, no land use impacts are anticipated as a result of operating the facility and cylinder storage pad.

**TABLE 5.2-21 Materials Consumed Annually during Normal Conversion Facility Operations at the Portsmouth Site<sup>a</sup>**

Chemical	Quantity (tons/yr)
<b>Solid</b>	
Lime (CaO) <sup>b</sup>	14
<b>Liquid</b>	
Ammonia (99.95% minimum NH <sub>3</sub> )	510
Potassium hydroxide (KOH)	6
<b>Gas</b>	
Nitrogen (N <sub>2</sub> )	7,800

<sup>a</sup> Material estimates are based on conceptual-design-status facility design data (UDS 2003b). A number of studies are planned to evaluate design alternatives, the results of which may affect the above materials needs.

<sup>b</sup> Assuming lime is used only for potassium hydroxide regeneration. If HF neutralization is required, the annual lime requirement would be approximately 7,000 tons/yr (6,350 t/yr).

**TABLE 5.2-22 Utilities Consumed during Conversion Facility Operations at the Portsmouth Site<sup>a</sup>**

Utility	Annual Average Consumption	Unit	Peak Demand <sup>b</sup>	Unit
Electricity	31,084	MWh	6.2	MW
Liquid fuel	3,000	gal	NA <sup>c</sup>	NA
Natural gas <sup>d,e</sup>	$4.0 \times 10^7$	scf <sup>f</sup>	180	scfm <sup>f</sup>
Process water	$30 \times 10^6$	gal	215	gal/min
Potable water	$3 \times 10^6$	gal	350	gal/min

<sup>a</sup> Utility estimates are based on facility conceptual-design-status data (UDS 2003b). A number of studies are planned to evaluate design alternatives, the results of which may affect the above utility needs.

<sup>b</sup> Peak demand is the maximum rate expected during any hour.

<sup>c</sup> NA = not applicable.

<sup>d</sup> Standard cubic feet measured at 14.7 psia and 60°F (16°C).

<sup>e</sup> The current facility design uses electrical heating. However, an option of using natural gas is being evaluated.

<sup>f</sup> scf = standard cubic feet; scfm = standard cubic feet per minute.

Alternative Locations B and C would have impacts similar to those at the preferred Location A during operations. Both locations occur on a site developed for the production of enriched uranium (and its DUF<sub>6</sub> by-product); as a consequence, operations would be generally consistent with current land use.

### 5.2.3.10 Cultural Resources

The routine operation of a DUF<sub>6</sub> conversion facility at Portsmouth is unlikely to adversely affect cultural resources at all three alternative locations because no ground-disturbing activities are associated with facility operation.

Air emissions or chemical releases from the facility were evaluated to determine their potential to affect significant cultural resources, predominantly historic structures, in the surrounding area. On the basis of the analysis of air emissions presented in Section 5.2.3.3, there would be only a negligible contribution of PM<sub>2.5</sub> within 150 m (500 ft) of the facility. This would not result in an adverse effect to cultural resources.

Accidental radiological and chemical releases, including HF, uranium compounds, and NH<sub>3</sub>, would be possible, although unlikely, during the operation of the plant (Section 5.2.3.2). HF emissions are not projected to exceed secondary standards beyond site boundaries and would have no effect on cultural resources. Any release of uranium compounds would be as PM and could affect building surfaces in close proximity to the facility. NH<sub>3</sub> releases would be gaseous

and would quickly disperse, although some surface deposits could occur. Careful washing of building surfaces could be required to remove such deposits if any contamination was detected following an accidental release.

#### **5.2.3.11 Environmental Justice**

The evaluation of environmental justice impacts is predicated on the identification of high and adverse impacts in other impact areas considered in this EIS, followed by a determination if those impacts would affect minority and low-income populations disproportionately. Analyses of impacts from operating the proposed facilities do not indicate high and adverse impacts for any of the other impact areas considered in this EIS (see Sections 5.2.3.1 through 5.2.3.10). Despite the presence of disproportionately high percentages of both minority and low-income populations within 50 mi (80 km) of the Portsmouth site, no environmental justice impacts are anticipated at any of the three alternative locations because of the lack of high and adverse impacts. Similarly, no evidence exists indicating that minority or low-income populations would experience high and adverse impacts from operating the facility or storage pad in the absence of such impacts in the population as a whole.

#### **5.2.4 Cylinder Preparation Impacts at ETTP**

Transporting the cylinders at ETTP to Portsmouth could result in potential environmental impacts at ETTP from the preparation of the cylinders for shipment. As described in Chapter 2, some of the DUF<sub>6</sub> cylinders in storage no longer meet DOT requirements for the shipment of radioactive materials. It is currently unknown exactly how many cylinders do not meet DOT requirements, although current estimates are that 1,700 cylinders are DOT-compliant. Before transportation, cylinders would have to be prepared to meet the requirements. As described in Chapter 2, for the purposes of this EIS, environmental impacts were evaluated for three options for preparing cylinders for shipment: use of cylinder overpacks, cylinder transfer and obtaining a DOT exemption.

An overpack is a container into which a cylinder would be placed for shipment. The overpack would be designed, tested, and certified to meet all DOT shipping requirements. The overpack would be suitable to contain, transport, and store the cylinder contents regardless of cylinder condition. According to UDS (2003b), the use of cylinder overpacks is considered the most likely approach for shipping noncompliant cylinders.

The cylinder transfer option would involve the transfer of the DUF<sub>6</sub> from noncompliant cylinders to cylinders that meet all DOT requirements. If selected, this option would likely require the construction of a cylinder transfer facility at ETTP. Currently, there are no plans or proposals to build or use a cylinder transfer facility to prepare DUF<sub>6</sub> cylinders for shipment. If such a decision were made, additional NEPA review would be conducted. The use of a cylinder transfer facility for cylinder preparation is considered much less likely than the use of overpacks,

because the former approach would be more resource intensive and costly and would generate additional contaminated emptied cylinders requiring treatment and disposal.

The third option is to obtain an exemption from DOT that would allow the DUF<sub>6</sub> cylinders to be transported either “as is” or following repairs. The primary finding that DOT would have to make to justify granting an exemption is this: the proposed alternative would have to achieve a safety level that would be at least equal to the level required by the otherwise applicable regulation or, if the otherwise applicable regulation did not establish a required safety level, would be consistent with the public interest and adequately protect against the risks to life and property that are inherent when transporting hazardous materials in commerce. It is likely that some type of compensatory measures during the transportation would have to be employed to justify the granting of an exemption. No specific measures were evaluated in this EIS. However, because the granting of an exemption would be based on a demonstration of equivalent safety, the transportation impacts for this option would be similar to those presented for the overpack and cylinder transfer options. Therefore, transportation impacts for the exemption option are not presented separately in this section.

The site-specific impacts of preparing both compliant and noncompliant cylinders (using overpacks and cylinder transfer) for shipment at ETTP were evaluated in Appendix E of the DUF<sub>6</sub> PEIS (DOE 1999a). In that evaluation, it was assumed for ETTP that the total number of cylinders not meeting DOT requirements ranged from 2,342 to 4,683 (50% to 100% of the ETTP DUF<sub>6</sub> inventory); correspondingly, from 0 to 2,342 compliant cylinders would require preparation for shipment.

The following paragraphs summarize the impacts from the cylinder preparation activities at ETTP as presented in Appendix E of the DUF<sub>6</sub> PEIS (DOE 1999a). The site-specific impacts from operation of a transfer facility at ETTP were evaluated on the basis of the assumption that the facility would be located at the center of the site, since no proposal exists for such a facility and no specific location has been proposed. For the same reasons, the site-specific impacts from construction were not evaluated. Therefore, an additional NEPA review might be required to construct a cylinder transfer facility if a decision was made to do so in the future.

#### **5.2.4.1 Cylinder Overpack Option**

For normal operations, the PEIS analysis concluded that the potential on-site impacts from preparing compliant cylinders and from placing noncompliant cylinders into overpacks would be small and limited to involved workers. No impacts to the off-site public or the environment would occur, since no releases are expected and no construction activities would be required. The only equipment required would be similar to the equipment currently used during routine cylinder handling and maintenance activities.

It is estimated that at ETTP, the total collective dose to involved workers would range from 42 to 85 person-rem (resulting in less than 0.03 LCF) for overpacking operations and from 0 to 27 person-rem (resulting in less than 0.01 LCF) for preparation of compliant cylinders. The total collective dose to workers preparing all the ETTP cylinders would range from 69 to

85 person-rem (resulting in less than 0.03 LCF). This dose to workers would be incurred over the duration of the cylinder preparation operations (annual doses can be estimated by dividing the total dose by the duration of the operation in years). It should be noted that the assumptions used in the PEIS for estimating worker exposure were very conservative, with the purpose of bounding potential exposures. In practice, cylinder preparation activities, such as inspecting, unstacking, and loading cylinders, would involve fewer workers and be of shorter duration, resulting in significantly lower worker exposures than the estimates presented here.

The PEIS also evaluated the potential for accidents during cylinder preparation operations. The types of accident considered were the same as those considered for the continued storage of cylinders under the no action alternative in this EIS, such as spills from corroded cylinders during wet and dry conditions and vehicle accidents causing cylinders to be involved in fires. The consequences of such accidents are described under the no action alternative in Section 5.1.

#### 5.2.4.2 Cylinder Transfer Facility Option

A summary of environmental parameters associated with the construction and operation of a cylinder transfer facility with various throughputs is presented in Table 5.2-23. In the PEIS, it was assumed that the ETTP transfer facility would process 320 cylinders per year, requiring about 15 years to transfer 4,683 cylinders. Although the three facility sizes shown in Table 5.2-23 have vastly different throughputs (ranging over a factor of 5), the differences in the environmental parameters among them are relatively small because of economies of scale. If transfer operations at ETTP occurred over a shorter period of time than 15 years, a larger facility would be required, with environmental parameters similar to those listed for the 1,600-cylinder/yr facility or the 960-cylinder/yr facility.

**TABLE 5.2-23 Summary of Environmental Parameters for a Cylinder Transfer Facility at ETTP**

Affected Parameter	Facility Size (annual throughput)		
	1,600 Cylinders	960 Cylinders	320 Cylinders
Disturbed land area (acres)	21	14	12
Paved area (acres)	15	10	8
Construction water (million gal/yr)	10	8	6.5
Construction wastewater (million gal/yr)	5	4	3.3
Operations water (million gal/yr)	9	7	6
Operations wastewater (million gal/yr)	7.1	5.7	4.4
Radioactive release (Ci/yr)	0.00078	0.00063	0.00049

Source: Appendix E in DOE (1999a).

For the cylinder transfer option, impacts during construction and normal operations would generally be small and limited primarily to involved workers. It is estimated that at ETTP, the total collective dose to involved workers would range from 410 to 480 person-rem (resulting in less than 0.2 LCF) for cylinder transfer operations, and it would range from 0 to 27 person-rem (resulting in less than 0.01 LCF) for preparing compliant cylinders. The total collective dose to workers preparing all the ETTP cylinders would range from 437 to 480 person-rem (resulting in less than 0.2 LCF). This dose to workers would be incurred over the duration of the cylinder preparation operations (annual doses can be estimated by dividing the total dose by the duration of the operation in years).

In the PEIS, the size of the transfer facility was estimated to be less than about 20 acres (8 ha); such a facility would likely be constructed in a previously disturbed area. Some small off-site releases of hazardous and nonhazardous materials could occur, although such releases would have negligible impacts on the off-site public and the environment. Construction activities could temporarily impact air quality; however, all criteria pollutants concentrations would be within applicable standards.

Impacts on cultural resources would be possible if a transfer facility was built at ETTP. Depending on the location chosen, the K-25 Main Plant Historical District, significant archaeological resources, or traditional cultural properties could be adversely affected. The ORR CRMP has been approved by the Tennessee SHPO. It includes procedures for determining the effect of an undertaking on cultural resources, consulting with the Tennessee SHPO and Native American groups, and mitigating adverse effects (Souza et al. 2001). These procedures, including additional surveys and any necessary mitigation, would have to be completed before any ground-disturbing activities for construction of a new facility could begin.

### **5.2.5 Transportation**

The action alternatives involve transportation of DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders from ETTP to Portsmouth, in addition to transportation of the conversion products to a disposal site or to commercial users. The ETTP cylinders are expected to be shipped by truck and the conversion products by rail. However, a viable option is to ship some ETTP cylinders via rail and the conversion products by truck. For purposes of this EIS, transportation of all cargo is considered for both truck and rail modes of transport. In a similar fashion, conversion products declared to be wastes are expected to be sent to Envirocare of Utah for disposal; another viable option is to send the products to NTS. Thus, both options are evaluated. If not used as disposal containers for depleted U<sub>3</sub>O<sub>8</sub> products, the emptied heel cylinders would be crushed and shipped in 20-ft (6-m) cargo containers, approximately 10 to a container. However, up to 10% of these cylinders might not meet Envirocare acceptance criteria and would be shipped as-is to NTS for disposal (UDS 2003b).

As discussed in Appendix F, Section F.3, the impacts of transportation were calculated in three areas: (1) collective population risks during routine conditions and accidents (Section 5.2.5.1), (2) radiological risks to MEIs during routine conditions (Section 5.2.5.2), and

(3) consequences to individuals and populations after the most severe accidents involving a release of radioactive or hazardous chemical material (Section 5.2.5.3).

### 5.2.5.1 Collective Population Risk

The collective population risk is a measure of the total risk posed to society as a whole by the actions being considered. For a collective population risk assessment, the persons exposed are considered as a group, without specifying individual receptors. The collective population risk is used as the primary means of comparing various options. Collective population risks are calculated for both vehicle- and cargo-related causes for routine transportation and accidents. Vehicle-related risks are independent of the cargo in the shipment and include risks from vehicular exhaust emissions and traffic accidents (fatalities caused by physical trauma).

**5.2.5.1.1 ETTP Cylinders.** The total collective population risks for shipment of the entire ETTP inventory to Portsmouth are presented in Table 5.2-24 for DUF<sub>6</sub> and non-DUF<sub>6</sub> cylinders. Annual impacts would depend on the duration of the shipping campaign and can be computed by dividing the total risk by the campaign duration. No fatalities are expected as a result of the shipping campaign because all estimated collective fatality risks would be much less than 0.5. The estimated radiation doses from the shipments are much less than levels expected to cause an appreciable increase in the risk of cancer in crew members and the public. The highest fatality risks are from vehicle-related causes, with the risks for truck shipments being higher than for rail.

The highest radiological risks would be for routine transport by general train (0.03 crew LCFs) followed by truck (0.01 crew LCFs). In RADTRAN (Neuhauser and Kanipe 1992), rail crew risks are calculated for railcar inspectors in rail yards. During transport, members of the rail crew are assumed to be shielded completely by the locomotive(s) and any intervening railcars. The radiological risks from accidents are approximately 10 times lower than those for routine transport. No chemical impacts would occur under normal transport conditions because the package contents are assumed to remain confined. Chemical accident risks for the entire shipping campaign would be negligible for any transport option. No adverse effects ( $3.6 \times 10^{-6}$  or less) or irreversible adverse effects ( $2.6 \times 10^{-6}$  or less) are expected.

**5.2.5.1.2 Ammonia.** Anhydrous NH<sub>3</sub> would be transported to the conversion facility for generation of hydrogen, which is used in the conversion process. Collective population risks associated with the transport of NH<sub>3</sub> to the site are shown in Table 5.2-25 for three different distances between the origin of NH<sub>3</sub> and the site. When a distance of 620 mi (1,000 km) from the site is assumed and average accident rates and population densities are used, the number of adverse effects that are expected among the crew and the population along the transportation route would be about 5 for the truck option and about 1 for the rail option. For the same distance, less than 1 irreversible adverse effect or fatality would be expected for either transportation mode. As expected, the risks would be smaller for distances of less than 620 mi (1,000 km) and higher for greater distances.

**TABLE 5.2-24 ETPP UF<sub>6</sub> Cylinder Shipments to Portsmouth**

Mode	DUF <sub>6</sub>		Non-DUF <sub>6</sub>	
	Truck	Rail <sup>a</sup>	Truck	Rail <sup>a</sup>
<b>Shipment summary</b>				
Number of shipments	4,900	1,225	503	181
Total distance traveled (km)	2,380,000	872,000	244,000	129,000
<b>Cargo-related<sup>b</sup></b>				
<b>Radiological impacts</b>				
Dose risk (person-rem)				
Routine crew	26	82	3.5	17
Routine public				
Off-link	0.28	1.2	0.11	0.25
On-link	0.82	0.046	0.32	0.0094
Stops	7.8	1.4	3.1	0.29
Total	8.9	2.6	3.5	0.55
Accident <sup>c</sup>	0.24	0.022	0.0011	5.2 × 10 <sup>-5</sup>
Latent cancer fatalities <sup>d</sup>				
Crew fatalities	0.01	0.03	0.001	0.007
Public fatalities	0.005	0.001	0.002	0.0003
<b>Chemical impacts</b>				
Adverse effects	3.6 × 10 <sup>-6</sup>	9.9 × 10 <sup>-8</sup>	0	0
Irreversible adverse effects	2.6 × 10 <sup>-6</sup>	7.6 × 10 <sup>-8</sup>	0	0
<b>Vehicle-related<sup>e</sup></b>				
Emission fatalities	0.2	0.01	0.02	0.002
Accident fatalities	0.069	0.029	0.007	0.0043

<sup>a</sup> Risks are presented on a railcar basis. One shipment is equivalent to one railcar.

<sup>b</sup> Cargo-related impacts are impacts attributable to the radioactive or chemical nature of the material being transported.

<sup>c</sup> Dose risk is a societal risk and is the product of accident probability and accident consequence.

<sup>d</sup> Latent cancer fatalities are calculated by multiplying dose by the ICRP Publication 60 health risk conversion factors of 4 × 10<sup>-4</sup> fatal cancers per person-rem for workers and 5 × 10<sup>-4</sup> for the public (ICRP 1991).

<sup>e</sup> Vehicle-related impacts are impacts independent of the cargo in the shipment.

**TABLE 5.2-25 Collective Population Transportation Risks for Shipment of Anhydrous NH<sub>3</sub> to the Portsmouth Conversion Facility**

Mode	Distance to Conversion Facility (km)		
	250	1,000	5,000
<b>Truck Option</b>			
Shipment summary			
Number of shipments	704	704	704
Total distance (km)	176,000	704,000	3,520,000
Cargo-related <sup>a</sup>			
Chemical impacts			
Adverse effects	1.3	5.3	26
Irreversible adverse effects	0.19	0.77	3.9
Vehicle related <sup>b</sup>			
Emission fatalities	0.02	0.07	0.3
Accident fatalities	0.0026	0.01	0.052
<b>Rail Option</b>			
Shipment summary			
Number of shipments	352	352	352
Total distance (km)	88,000	352,000	1,760,000
Cargo-related <sup>a</sup>			
Chemical impacts			
Adverse effects	0.29	1.2	5.8
Irreversible adverse effects	0.041	0.17	0.83
Vehicle-related <sup>b</sup>			
Emission fatalities	0.0009	0.004	0.02
Accident fatalities	0.0069	0.028	0.14

<sup>a</sup> Cargo-related impacts are impacts attributable to the radioactive or chemical nature of the material being transported.

<sup>b</sup> Vehicle-related impacts are impacts independent of the cargo in the shipment.

**5.2.5.1.3 Conversion Products.** The transportation assessment for the shipment of depleted uranium conversion products for disposal considers several options. The proposed disposal site is the Envirocare facility. (A small number of empty cylinders may require disposal at NTS.) For shipments to Envirocare, rail is evaluated as the proposed mode and truck is evaluated as an alternative. In addition, NTS is considered as an alternative disposal site. For this alternative, both truck and rail modes are evaluated, although neither is currently proposed.

For assessment of the rail option to NTS, it is assumed that a rail spur would be built in the future to provide rail access to NTS. Currently, the nearest rail terminal is about 70 mi (113 km) from NTS. If a rail spur was not available in the future and if NTS was selected as the disposal site, shipments could be made by truck, or rail could be used with an intermodal transfer

to trucks at some place near NTS. (Transportation impacts for the intermodal option would be slightly greater than those presented for rail assuming NTS rail access, but less than those presented for the truck alternative.) If a rail spur to NTS was built, the impacts would require additional NEPA review.

Estimates of the collective population risks for shipment of the U<sub>3</sub>O<sub>8</sub>, emptied cylinders, and CaF<sub>2</sub> to Envirocare over the entire 18-year operational period are presented in Table 5.2-26, by assuming the U<sub>3</sub>O<sub>8</sub> product is shipped in bulk bags. As an option, risks for the shipment of these materials to NTS are provided in Table 5.2-27. No radiological LCFs, traffic fatalities, or emission fatalities are expected for rail transport under either option. If the truck option was used, about 1 traffic fatality would occur and up to 7 fatalities from vehicle emissions might occur over the project period. No LCFs are expected.

If the emptied DUF<sub>6</sub> cylinders were refilled with the U<sub>3</sub>O<sub>8</sub> product and used to transport the product to the disposal facility, as proposed, the risks shown in Tables 5.2-26 and 5.2-27 for transportation of emptied cylinders would not be applicable, and the risks associated with transportation of CaF<sub>2</sub> would be the same. The risks of transporting the U<sub>3</sub>O<sub>8</sub> product in cylinders would be about the same as the sum of the risks for transporting the product in bulk bags plus the risk of shipping the crushed cylinders for the truck option (Table 5.2-28), assuming two refilled cylinders per truck. If one cylinder per truck were shipped, routine risks to the crew and vehicle-related risks would approximately double because the number of shipments would double. If the rail option was used, the risks would be slightly higher for the cylinder refill option, primarily because the quantity of U<sub>3</sub>O<sub>8</sub> shipped in a single railcar would be less under the cylinder refill option than under the bulk bag option, and the number of shipments would be proportionally higher.

The risks for shipping the HF co-product are presented in Table 5.2-29 for representative shipment distances of 250, 1,000, and 5,000 km (155, 620, and 3,100 mi) by using average accident rates and population densities. For shipment distances up to 5,000 km (3,100 mi), 1 traffic fatality might be expected for shipment of the HF by either truck or rail and up to 4 emission fatalities could occur for shipment by truck, with none expected for rail shipments. For chemical risks, approximately 1 irreversible adverse effect is estimated for both truck and rail transport. Thus, no chemical fatalities are expected because approximately 1% of the cases with irreversible adverse effects are expected to result in fatality (Policastro et al. 1997). Table 5.2-30 presents the risks associated with the shipment of CaF<sub>2</sub> to either Envirocare or NTS should the HF be neutralized and disposed of as waste. Shipment of the CaF<sub>2</sub> to either Envirocare or NTS would have similar impacts, approximately 10 and 0 emission fatalities for truck or rail, respectively, and about 1 traffic fatality if shipped by truck.

The results of the transportation analysis discussed above indicate that the largest impact during normal transportation conditions would be associated with vehicle exhaust and fugitive dust emissions (unrelated to the cargo). Health risks from cardiovascular and pulmonary diseases have been linked to incremental increases in particulate concentrations in air. However, estimating the health risks associated with vehicle emissions is subject to a great deal of

**TABLE 5.2-26 Collective Population Transportation Risks for Shipment of Conversion Products to Envirocare as the Primary Disposal Site, Assuming the U<sub>3</sub>O<sub>8</sub> Is Disposed of in Bulk Bags**

Mode	U <sub>3</sub> O <sub>8</sub>		Emptied Cylinders				CaF <sub>2</sub>	
	Portsmouth to Envirocare		Portsmouth to Envirocare <sup>a</sup>		Portsmouth to NTS <sup>b</sup>		Portsmouth to Envirocare	
	Truck (option)	Rail (proposed) <sup>c</sup>	Truck (option)	Rail (proposed) <sup>c</sup>	Truck (proposed)	Rail (option) <sup>c</sup>	Truck (option)	Rail (proposed) <sup>c</sup>
<b>Shipment summary</b>								
Number of shipments	8,846	2,212	2,007	1,004	2,232	558	15	4
Total distance (km)	25,860,000	7,315,000	5,866,000	3,320,000	7,504,000	2,240,000	43,850	13,230
<b>Cargo-related<sup>d</sup></b>								
<b>Radiological impacts</b>								
<b>Dose risk (person-rem)</b>								
Routine crew	150	350	35	88	79	170	NA <sup>e</sup>	NA
Routine public								
Off-link	2.6	12	0.7	2.9	1.2	3.9	NA	NA
On-link	7.2	0.31	1.9	0.077	3.0	0.12	NA	NA
Stops	60	5.4	16	1.3	23	2.7	NA	NA
Total	70	17	19	4.3	27	6.6	NA	NA
Accident <sup>f</sup>	28	9.3	0.24	0.075	0.02	0.0062	NA	NA
<b>Latent cancer fatalities<sup>g</sup></b>								
Crew fatalities	0.06	0.1	0.01	0.04	0.03	0.07	NA	NA
Public fatalities	0.05	0.01	0.009	0.002	0.01	0.003	NA	NA
<b>Chemical impacts</b>								
Adverse effects	0.0009	0.0003	NA	NA	NA	NA	NA	NA
Irreversible adverse effects	0.0001	0.00009	NA	NA	NA	NA	NA	NA
<b>Vehicle-related<sup>h</sup></b>								
Emission fatalities	5	0.2	1	0.1	2	0.05	0.008	0.0005
Accident fatalities	0.53	0.24	0.12	0.11	0.13	0.061	0.0009	0.00043

<sup>a</sup> Emptied cylinders are crushed and shipped 10 per cargo container, with 1 container per truck or 2 containers per railcar.

<sup>b</sup> Cylinders assumed not to meet waste acceptance criteria for Envirocare. Shipped “as-is” one per truck or four per railcar.

<sup>c</sup> Risks are presented on a railcar basis. One shipment is equivalent to one railcar. For assessment purposes, it was assumed that rail access to NTS would be available in the future.

<sup>d</sup> Cargo-related impacts are impacts attributable to the radioactive or chemical nature of the material being transported.

<sup>e</sup> NA = not applicable.

<sup>f</sup> Dose risk is a societal risk and is the product of accident probability and accident consequence.

<sup>g</sup> Latent cancer fatalities were calculated by multiplying the dose by the ICRP Publication 60 health risk conversion factors of  $4 \times 10^{-4}$  fatal cancers per person-rem for workers and  $5 \times 10^{-4}$  for the public (ICRP 1991).

<sup>h</sup> Vehicle-related impacts are impacts independent of the cargo in the shipment.

**TABLE 5.2-27 Collective Population Transportation Risks for Shipment of Conversion Products to NTS as an Optional Disposal Site, Assuming the U<sub>3</sub>O<sub>8</sub> Is Disposed of in Bulk Bags**

Mode	U <sub>3</sub> O <sub>8</sub>		Emptied Cylinders				CaF <sub>2</sub>	
	Portsmouth to NTS		Portsmouth to NTS <sup>a</sup>		Portsmouth to NTS <sup>b</sup>		Portsmouth to Envirocare	
	Truck (option)	Rail (option) <sup>c</sup>	Truck (option)	Rail (option) <sup>c</sup>	Truck (option)	Rail (option) <sup>c</sup>	Truck (option)	Rail (option) <sup>c</sup>
<b>Shipment summary</b>								
Number of shipments	8,846	2,212	2,007	1,004	2,232	558	15	4
Total distance (km)	29,740,000	8,879,000	6,748,000	4,030,000	7,504,000	2,240,000	43,850	13,230
<b>Cargo-related<sup>d</sup></b>								
<b>Radiological impacts</b>								
<b>Dose risk (person-rem)</b>								
Routine crew	180	410	41	100	79	170	NA <sup>e</sup>	NA
Routine public								
Off-link	3.6	9.2	0.96	2.3	1.2	3.9	NA	NA
On-link	9.0	0.28	2.4	0.069	3.0	0.12	NA	NA
Stops	69	6.4	18	1.6	23	2.7	NA	NA
Total	82	16	22	3.9	27	6.6	NA	NA
Accident <sup>f</sup>	20	7.5	0.18	0.053	0.02	0.0062	NA	NA
<b>Latent cancer fatalities<sup>g</sup></b>								
Crew fatalities	0.07	0.2	0.02	0.04	0.03	0.07	NA	NA
Public fatalities	0.05	0.01	0.01	0.002	0.01	0.003	NA	NA
<b>Chemical impacts</b>								
Adverse effects	0.001	0.0004	NA	NA	NA	NA	NA	NA
Irreversible adverse effects	0.0002	0.0001	NA	NA	NA	NA	NA	NA
<b>Vehicle-related<sup>h</sup></b>								
Emission fatalities	6	0.2	1	0.09	2	0.05	0.008	0.0005
Accident fatalities	0.53	0.24	0.12	0.11	0.13	0.061	0.0009	0.00043

<sup>a</sup> Cylinders are crushed and shipped 10 per cargo container, with 1 container per truck or 2 containers per railcar.

<sup>b</sup> Cylinders assumed not to meet waste acceptance criteria for Envirocare. Shipped “as-is” one per truck or four per railcar.

<sup>c</sup> Risks are presented on a railcar basis. One shipment is equivalent to one railcar. For assessment purposes, it was assumed that rail access to NTS would be available in the future.

<sup>d</sup> Cargo-related impacts are impacts attributable to the radioactive or chemical nature of the material being transported.

<sup>e</sup> NA = not applicable.

<sup>f</sup> Dose risk is a societal risk and is the product of accident probability and accident consequence.

<sup>g</sup> Latent cancer fatalities were calculated by multiplying the dose by the ICRP Publication 60 health risk conversion factors of  $4 \times 10^{-4}$  fatal cancers per person-rem for workers and  $5 \times 10^{-4}$  for the public (ICRP 1991).

<sup>h</sup> Vehicle-related impacts are impacts independent of the cargo in the shipment.

**TABLE 5.2-28 Collective Population Transportation Risks for Shipment of U<sub>3</sub>O<sub>8</sub> Conversion Products in Emptied Cylinders**

Mode	Portsmouth to Envirocare (proposed)			Portsmouth to NTS (option)		
	Truck (option)		Rail (proposed)	Truck (option)		Rail <sup>a</sup> (option)
	1 cylinder	2 cylinders		1 cylinder	2 cylinders	
<b>Shipment summary</b>						
Number of shipments	21,000	10,500	4,200	21,000	10,500	4,200
Total distance (km)	61,380,000	30,690,000	13,890,000	70,600,000	35,300,000	16,860,000
<b>Cargo-related<sup>b</sup></b>						
<b>Radiological impacts</b>						
Dose risk (person-rem)						
Routine crew	330	180	520	390	210	600
Routine public						
Off-link	4.5	4.5	19	6.1	6.2	15
On-link	12	12	0.52	15	15	0.46
Stops	100	100	8.8	120	120	10
Total	120	120	29	140	140	26
Accident	31	31	10	21	21	8
Latent cancer fatalities						
Crew fatalities	0.1	0.07	0.2	0.2	0.08	0.2
Public fatalities	0.07	0.08	0.02	0.08	0.08	0.02
<b>Chemical impacts</b>						
Adverse effects	0.0008	0.0008	0.0004	0.0009	0.0009	0.0005
Irreversible adverse effects	0.0001	0.0001	0.0001	0.0001	0.0001	0.0001
<b>Vehicle-related<sup>c</sup></b>						
Emission fatalities	10	5	0.5	10	7	0.4
Accident fatalities	1.3	0.63	0.45	1.3	0.63	0.46

<sup>a</sup> For assessment purposes, it was assumed that rail access to NTS would be available in the future.

<sup>b</sup> Cargo-related impacts are impacts attributable to the radioactive or chemical nature of the material being transported.

<sup>c</sup> Vehicle-related impacts are impacts independent of the cargo in the shipment.

uncertainty. The estimates presented in this EIS were based on very conservative health risk factors presented in Biwer and Butler (1999) and should be considered an upper bound. For perspective, in a recently published EIS for a geologic repository at Yucca Mountain, Nevada, (DOE 2002h), the same risk factors were used for vehicle emissions; however, they were adjusted to reduce the amount of conservatism in the estimated health impacts. As reported in the Yucca Mountain EIS, the adjustments resulted in a reduction in the emission risks by a factor of about 30.

**TABLE 5.2-29 Collective Population Transportation Risks for Shipment of the HF Conversion Co-Product from the Portsmouth Site to Commercial Users**

Mode	49% HF			70% HF		
	250 km	1,000 km	5,000 km	250 km	1,000 km	5,000 km
<b>Truck Option</b>						
Shipment summary						
Number of shipments	5,792	5,792	5,792	2,417	2,417	2,417
Total distance (km)	1,448,000	5,792,000	28,960,000	604,250	2,417,000	12,085,000
Cargo-related <sup>a</sup>						
Chemical impacts						
Adverse effects	0.13	0.54	2.7	0.50	2.0	10
Irreversible adverse effects	0.011	0.045	0.23	0.040	0.16	0.81
Vehicle-related <sup>b</sup>						
Emission fatalities	0.1	0.5	3	0.06	0.2	1
Accident fatalities	0.022	0.086	0.43	0.0090	0.036	0.18
<b>Rail Option</b>						
Shipment summary						
Number of shipments	1,159	1,159	1,159	484	484	484
Total distance (km)	289,750	1,159,000	5,795,000	121,000	484,000	2,420,000
Cargo-related <sup>a</sup>						
Chemical impacts						
Adverse effects	0.19	0.74	3.7	0.48	1.9	9.7
Irreversible adverse effects	0.012	0.047	0.23	0.04	0.16	0.79
Vehicle-related <sup>b</sup>						
Emission fatalities	0.003	0.01	0.06	0.001	0.005	0.02
Accident fatalities	0.023	0.091	0.45	0.0095	0.038	0.19

<sup>a</sup> Cargo-related impacts are impacts attributable to the radioactive or chemical nature of the material being transported.

<sup>b</sup> Vehicle-related impacts are impacts independent of the cargo in the shipment.

### 5.2.5.2 Maximally Exposed Individuals during Routine Conditions

During the routine transportation of radioactive material, specific individuals may be exposed to radiation in the vicinity of a shipment. RISKIND (Yuan et al. 1995) has been used to estimate the risk to these individuals for a number of hypothetical exposure-causing events. The receptors include transportation crew members, inspectors, and members of the public exposed during traffic delays, while working at a service station, or while living near an origin or a destination site. The assumptions about exposure are given in Biwer et al. (2001). The scenarios for exposure are not meant to be exhaustive; they were selected to provide a range of

**TABLE 5.2-30 Collective Population Transportation Risks for Shipment of CaF<sub>2</sub> for the Neutralization Option**

Parameter	Truck (option)	Rail (proposed) <sup>a</sup>
Number of shipments	13,559	3,390
Portsmouth to Envirocare option		
Total distance (km)	39,630,000	11,210,000
Emission fatalities	7	0.4
Accident fatalities	0.81	0.37
Portsmouth to NTS option		
Total distance (km)	45,590,000	13,610,000
Emission fatalities	10	0.3
Accident fatalities	0.82	0.37

<sup>a</sup> Risks are presented on a railcar basis. One shipment is equivalent to one railcar.

representative potential exposures. Doses were assessed and are presented in Table 5.2-31 on a per-event basis for the shipments of all radioactive materials.

On a per-shipment basis, the radiological risks to an MEI during routine transportation would be slightly higher for non-DUF<sub>6</sub> shipments than for depleted uranium shipments because a higher external dose rate is assumed. The highest potential routine radiological exposure to an MEI, with an LCF risk of  $3 \times 10^{-7}$ , would be for a person stopped in traffic near a rail shipment of non-DUF<sub>6</sub> cylinders from ETTP for 30 min at a distance of 3 ft (1 m). There is also the possibility for multiple exposures. For example, if an individual lived near the Portsmouth site and all shipments of U<sub>3</sub>O<sub>8</sub> were made by rail in bulk bags, the resident could receive a combined dose of approximately  $2.4 \times 10^{-5}$  rem if present for all shipments (calculated as the product of about 2,200 shipments and an estimated exposure per shipment of  $1.1 \times 10^{-8}$  rem). The individual dose would increase by a factor of 2 approximately if the U<sub>3</sub>O<sub>8</sub> product was shipped in refilled cylinders. This dose is still very low, however — more than 6,000 times lower than the individual average annual exposure of 0.3 rem from natural background radiation.

### 5.2.5.3 Accident Consequence Assessment

Whereas the collective accident risk assessment considers the entire range of accident severities and their related probabilities, the accident consequence assessment assumes that an accident of the highest severity category has occurred. The consequences, in terms of committed dose (rem) and LCFs for radiological impacts and in terms of adverse affects and irreversible adverse effects for chemical impacts, were calculated for both exposed populations and

**TABLE 5.2-31 Estimated Radiological Impacts to the MEI from Routine Shipment of Radioactive Materials from the Portsmouth Conversion Facility**

Material	Mode	Inspector	Resident	Person in Traffic	Person at Gas Station	Person near Rail Stop
<b><i>Routine Radiological Dose from a Single Shipment (rem)</i></b>						
DUF <sub>6</sub>	Truck	$6.3 \times 10^{-5}$	$5.4 \times 10^{-9}$	$2.3 \times 10^{-4}$	$7.5 \times 10^{-6}$	NA <sup>a</sup>
	Rail	$1.1 \times 10^{-4}$	$1.5 \times 10^{-8}$	$2.6 \times 10^{-4}$	NA	$9.3 \times 10^{-7}$
Non-DUF <sub>6</sub>	Truck	$1.4 \times 10^{-4}$	$2.0 \times 10^{-8}$	$5.0 \times 10^{-4}$	$2.7 \times 10^{-5}$	NA
	Rail	$1.8 \times 10^{-4}$	$2.5 \times 10^{-8}$	$5.0 \times 10^{-4}$	NA	$1.6 \times 10^{-6}$
Depleted U <sub>3</sub> O <sub>8</sub> (in bulk bags) <sup>b</sup>	Truck	$4.0 \times 10^{-5}$	$3.1 \times 10^{-9}$	$1.6 \times 10^{-4}$	$4.4 \times 10^{-6}$	NA
	Rail	$9.3 \times 10^{-5}$	$1.1 \times 10^{-8}$	$2.7 \times 10^{-4}$	NA	$6.9 \times 10^{-7}$
Crushed heel cylinders <sup>c</sup>	Truck	$5.3 \times 10^{-5}$	$5.7 \times 10^{-9}$	$1.6 \times 10^{-4}$	$7.7 \times 10^{-6}$	NA
	Rail	$6.6 \times 10^{-5}$	$9.4 \times 10^{-9}$	$1.7 \times 10^{-4}$	NA	$6.1 \times 10^{-7}$
Heel cylinders <sup>d</sup>	Truck	$6.8 \times 10^{-5}$	$5.4 \times 10^{-9}$	$2.7 \times 10^{-4}$	$7.5 \times 10^{-6}$	NA
	Rail	$1.5 \times 10^{-4}$	$2.0 \times 10^{-8}$	$4.0 \times 10^{-4}$	NA	$1.3 \times 10^{-6}$
<b><i>Routine Radiological Risk from a Single Shipment (lifetime risk of a LCF)<sup>e</sup></i></b>						
DUF <sub>6</sub>	Truck	$3 \times 10^{-8}$	$3 \times 10^{-12}$	$1 \times 10^{-7}$	$4 \times 10^{-9}$	NA
	Rail	$6 \times 10^{-8}$	$8 \times 10^{-12}$	$1 \times 10^{-7}$	NA	$5 \times 10^{-10}$
Non-DUF <sub>6</sub>	Truck	$9 \times 10^{-8}$	$1 \times 10^{-11}$	$3 \times 10^{-7}$	$1 \times 10^{-8}$	NA
	Rail	$9 \times 10^{-8}$	$1 \times 10^{-11}$	$3 \times 10^{-7}$	NA	$8 \times 10^{-10}$
Depleted U <sub>3</sub> O <sub>8</sub> (in bulk bags) <sup>b</sup>	Truck	$2 \times 10^{-8}$	$2 \times 10^{-12}$	$8 \times 10^{-8}$	$2 \times 10^{-9}$	NA
	Rail	$5 \times 10^{-8}$	$6 \times 10^{-12}$	$1 \times 10^{-7}$	NA	$4 \times 10^{-10}$
Crushed heel cylinders <sup>c</sup>	Truck	$3 \times 10^{-8}$	$3 \times 10^{-12}$	$8 \times 10^{-8}$	$4 \times 10^{-9}$	NA
	Rail	$3 \times 10^{-8}$	$5 \times 10^{-12}$	$8 \times 10^{-8}$	NA	$3 \times 10^{-10}$
Heel cylinders <sup>d</sup>	Truck	$3 \times 10^{-8}$	$3 \times 10^{-12}$	$1 \times 10^{-7}$	$4 \times 10^{-9}$	NA
	Rail	$7 \times 10^{-8}$	$1 \times 10^{-11}$	$2 \times 10^{-7}$	NA	$6 \times 10^{-10}$

<sup>a</sup> Not applicable.

<sup>b</sup> Per-shipment doses and LCFs would be approximately the same for the cylinder refill option.

<sup>c</sup> Crushed heel cylinders are shipped 10 per cargo container, with 1 container per truck or 2 containers per railcar.

<sup>d</sup> Cylinders assumed not to meet waste acceptance criteria for Envirocare. Shipped “as-is,” one per truck or four per railcar.

<sup>e</sup> LCFs were calculated by multiplying the dose by the ICRP Publication 60 health risk conversion factors of  $4 \times 10^{-4}$  fatal cancers per person-rem for workers and  $5 \times 10^{-4}$  for the public (ICRP 1991).

individuals in the vicinity of an accident. Tables 5.2-32 and 5.2-33 present the radiological and chemical consequences, respectively, to the population from severe accidents involving shipment of DUF<sub>6</sub>, depleted U<sub>3</sub>O<sub>8</sub>, emptied heel cylinders, anhydrous NH<sub>3</sub>, and aqueous HF.

Because the average uranium content of each non-DUF<sub>6</sub> cylinder shipment is much less than that of a DUF<sub>6</sub> cylinder shipment (the *total* amount of UF<sub>6</sub> in the non-DUF<sub>6</sub> cylinders is approximately 25 t [28 tons], compared with approximately 12 t [13 tons] in *each* DUF<sub>6</sub> cylinder), a separate accident consequence assessment was not conducted for non-DUF<sub>6</sub> cylinder shipments. The potential impacts of the highest-consequence accidents for non-DUF<sub>6</sub> cylinder shipments would be much less than those presented in Tables 5.2-32 and 5.2-33 for DUF<sub>6</sub> shipments.

The nuclear properties of DUF<sub>6</sub> are such that the occurrence of a nuclear criticality is not a concern, regardless of the amount of DUF<sub>6</sub> present. However, criticality is a concern for the handling, packaging, and shipping of enriched UF<sub>6</sub>. For enriched UF<sub>6</sub>, criticality control is accomplished by employing, individually or collectively, specific limits on uranium-235 enrichment, mass, volume, geometry, moderation, and spacing for each type of cylinder. The amount of enriched UF<sub>6</sub> that may be contained in an individual cylinder and the total number of cylinders that may be transported together are determined by the nuclear properties of enriched UF<sub>6</sub>. Spacing of cylinders of enriched UF<sub>6</sub> in transit during routine and accident conditions is ensured by use of regulatory approval packages that provide protection against impact and fire. Consequently, because of these controls and the relatively small number of shipments containing enriched UF<sub>6</sub>, the occurrence of an inadvertent criticality is not considered to be credible and therefore is not analyzed in the accident consequence assessment in this EIS.

No LCFs are expected for accidents involving heel cylinders; however, up to 3 or 60 LCFs might occur following a severe urban rail accident involving a railcar of U<sub>3</sub>O<sub>8</sub> or DUF<sub>6</sub>, respectively. Severe rail accidents could have higher consequences than truck accidents because each railcar would carry more material than each truck. The highest consequences were estimated on the basis of the assumption that the accident occurred in an urban area under stable weather conditions (such as at nighttime).

In a highly populated urban area, it is estimated that about 3 million people could be exposed to small amounts of uranium as it was dispersed by the wind. Among those exposed, it is estimated that approximately 60 LCFs could occur in the urban population in addition to those occurring from all other causes. For comparison, in a population of 3 million people, approximately 700,000 are expected to die of cancer from all causes. The occurrence of a severe rail accident in an urban area under stable weather conditions are expected to be rare. The consequences of cylinder accidents occurring in rural environments, during unstable weather conditions (typical of daytime) or involving a truck shipment, were also assessed. The consequences of all other accident conditions are estimated to be considerably less than those described above for the severe urban rail accident.

A comparison of Tables 5.2-32 and 5.2-33 indicates that severe accidents involving chemicals transported to and from the conversion facility site could have higher consequences

**TABLE 5.2-32 Potential Radiological Consequences to the Population from Severe Transportation Accidents<sup>a</sup>**

Material	Mode	Neutral Meteorological Conditions			Stable Meteorological Conditions		
		Rural	Suburban	Urban <sup>b</sup>	Rural	Suburban	Urban <sup>b</sup>
<b>Radiological Dose (person-rem)</b>							
DUF <sub>6</sub>	Truck	590	580	1,300	15,000	15,000	32,000
	Rail	2,400	2,300	5,200	60,000	58,000	130,000
Depleted U <sub>3</sub> O <sub>8</sub> (in bulk bags)	Truck	250	250	550	630	610	1,400
	Rail	1,000	990	2,200	2,500	2,400	5,400
Depleted U <sub>3</sub> O <sub>8</sub> (1 cylinder)	Truck	120	110	250	280	280	620
	Rail	290	280	630	710	690	1,500
Depleted U <sub>3</sub> O <sub>8</sub> (2 cylinders)	Truck	230	230	500	570	550	1,200
	Rail	580	560	1,300	1,400	1,400	3,100
Crushed heel cylinders <sup>c</sup>	Truck	2.5	0.67	1.5	4.4	1.2	2.6
	Rail	5.0	1.3	3.0	8.7	2.3	5.2
Heel cylinders <sup>d</sup>	Truck	0.25	0.067	0.15	0.44	0.12	0.26
	Rail	1.0	0.27	0.60	1.7	0.47	1.0
<b>Radiological Risk (LCF)<sup>e</sup></b>							
DUF <sub>6</sub>	Truck	0.3	0.3	0.6	7	7	20
	Rail	1	1	3	30	30	60
Depleted U <sub>3</sub> O <sub>8</sub> (in bulk bags)	Truck	0.1	0.1	0.3	0.3	0.3	0.7
	Rail	0.5	0.5	1	1	1	3
Depleted U <sub>3</sub> O <sub>8</sub> (1 cylinder)	Truck	0.06	0.06	0.1	0.1	0.1	0.3
	Rail	0.1	0.1	0.3	0.4	0.3	0.8
Depleted U <sub>3</sub> O <sub>8</sub> (2 cylinders)	Truck	0.1	0.1	0.3	0.3	0.3	0.6
	Rail	0.3	0.3	0.6	0.7	0.7	2
Crushed heel cylinders <sup>c</sup>	Truck	0.001	0.0003	0.0007	0.002	0.0006	0.001
	Rail	0.002	0.0007	0.001	0.004	0.001	0.003
Heel cylinders <sup>d</sup>	Truck	0.0001	3 × 10 <sup>-5</sup>	7 × 10 <sup>-5</sup>	0.0002	6 × 10 <sup>-5</sup>	0.0001
	Rail	0.0005	0.0001	0.0003	0.0009	0.0002	0.0005

<sup>a</sup> National average population densities were used for the accident consequence assessment, corresponding to densities of 6 persons/km<sup>2</sup>, 719 persons/km<sup>2</sup>, and 1,600 persons/km<sup>2</sup> for rural, suburban, and urban zones, respectively. Potential impacts were estimated for the population within a 50-mi (80-km) radius, assuming a uniform population density for each zone.

<sup>b</sup> It is important to note that the urban population density generally applies to a relatively small urbanized area — very few, if any, urban areas have a population density as high as 1,600 persons/km<sup>2</sup> extending as far as 50 mi (80 km). The urban population density corresponds to approximately 32 million people within the 50-mi (80-km) radius, well in excess of the total populations along the routes considered in this assessment.

<sup>c</sup> Crushed heel cylinders are shipped 10 per cargo container, with 1 container per truck or 2 containers per railcar.

<sup>d</sup> Cylinders assumed not to meet waste acceptance criteria for Envirocare. Shipped “as-is,” one per truck or four per railcar.

<sup>e</sup> LCFs were calculated by multiplying the dose by the ICRP Publication 60 health risk conversion factors of 4 × 10<sup>-4</sup> fatal cancers per person-rem for workers and 5 × 10<sup>-4</sup> for the public (ICRP 1991).

**TABLE 5.2-33 Potential Chemical Consequences to the Population from Severe Transportation Accidents<sup>a</sup>**

Chemical Effect	Mode	Neutral Meteorological Conditions			Stable Meteorological Conditions		
		Rural	Suburban	Urban <sup>b</sup>	Rural	Suburban	Urban <sup>b</sup>
<i>Number of Persons with the Potential for Adverse Health Effects</i>							
DUF <sub>6</sub>	Truck	0	2	4	6	760	1,700
	Rail	4	420	940	110	13,000	28,000
Depleted U <sub>3</sub> O <sub>8</sub> (in bulk bags)	Truck	0	1	1	0	12	28
	Rail	0	3	9	0	47	103
Depleted U <sub>3</sub> O <sub>8</sub> (in cylinders)	Truck (1 cylinder)	0	0	1	0	6	13
	Truck (2 cylinders)	0	1	1	0	11	26
	Rail	0	2	5	0	27	58
Anhydrous NH <sub>3</sub>	Truck	6	710	1,600	55	6,600	15,000
	Rail	10	1,100	2,500	90	11,000	24,000
49% HF	Truck	0.35	42	93	3.4	400	900
	Rail	0.99	120	270	7.3	880	1,900
70% HF	Truck	2.8	340	760	44	5,200	12,000
	Rail	9.3	1,100	2,500	110	14,000	30,000
<i>Number of Persons with the Potential for Irreversible Adverse Health Effects<sup>c</sup></i>							
DUF <sub>6</sub>	Truck	0	1	2	0	1	3
	Rail	0	1	3	0	2	4
Depleted U <sub>3</sub> O <sub>8</sub> (in bulk bags)	Truck	0	0	0	0	5	10
	Rail	0	0	0	0	17	38
Depleted U <sub>3</sub> O <sub>8</sub> (in cylinders)	Truck (1 cylinder)	0	0	0	0	2	5
	Truck (2 cylinders)	0	0	0	0	4	8
	Rail	0	1	1	0	10	22
Anhydrous NH <sub>3</sub>	Truck	0.8	100	200	10	1,000	3,000
	Rail	1	200	400	20	2,000	5,000
49% HF	Truck	0.025	3.0	6.6	0.25	30	66
	Rail	0.081	9.7	22	0.62	74	160
70% HF	Truck	0.23	27	60	2.0	240	540
	Rail	0.77	92	210	6.7	800	1,800

Footnotes on next page.

**TABLE 5.2-33 (Cont.)**

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- <sup>a</sup> National average population densities were used for the accident consequence assessment, corresponding to densities of 6 persons/km<sup>2</sup>, 719 persons/km<sup>2</sup>, and 1,600 persons/km<sup>2</sup> for rural, suburban, and urban zones, respectively. Potential impacts were estimated for the population within a 50-mi (80-km) radius, assuming a uniform population density for each zone.
- <sup>b</sup> It is important to note that the urban population density generally applies to a relatively small urbanized area — very few, if any, urban areas have a population density as high as 1,600 persons/km<sup>2</sup> extending as far as 50 mi (80 km). The urban population density corresponds to approximately 32 million people within the 50-mi (80-km) radius, well in excess of the total populations along the routes considered in this assessment.
- <sup>c</sup> The potential for irreversible adverse effects from chemical exposures. Exposure to HF or uranium compounds is estimated to result in fatality to approximately 1% or less of those persons experiencing irreversible adverse effects (Policastro et al. 1997). Exposure to anhydrous NH<sub>3</sub> is estimated to result in fatality to approximately 2% of those persons experiencing irreversible adverse effects (Policastro et al. 1997).

than radiological accidents. For example, a severe rail accident involving transportation of anhydrous NH<sub>3</sub> to a site in an urban area under stable meteorological conditions could lead to 5,000 irreversible adverse effects. Among the individuals experiencing these irreversible effects, there could be close to 100 fatalities (about 2% of the irreversible adverse effects [Policastro et al. 1997]). Similarly, a 70% aqueous HF rail accident under the same conservative assumptions could result in approximately 1,800 irreversible adverse effects and 18 fatalities. As indicated in Table 5.2-33, the consequences would be considerably less if the accident occurred in a less populated area under neutral meteorological conditions. Consequences would also be less if a truck was involved in the accident rather than a railcar, because the truck would carry less material than a railcar.

Accidents for which consequences are provided in Tables 5.2-32 and 5.2-33 are extremely rare. For example, the average accident rate for interstate-registered heavy combination trucks is approximately  $3.0 \times 10^{-7}$  per kilometer (Saricks and Tompkins 1999). The conditional probability that a given accident would be a severe accident is on the order of 0.06 in rural and suburban areas and about 0.007 in urban areas (NRC 1977). Therefore, the frequency of a severe accident per kilometer of travel in an urban area is about  $2 \times 10^{-9}$ . For shipment of NH<sub>3</sub> to the site, the total distance traveled is estimated to be about 435,000 mi (700,000 km) if the NH<sub>3</sub> is transported from a location 620 mi (1,000 km) away from the conversion site (Table 5.2-25). The fraction of the distance traveled in urban areas is generally less than 5% (DOE 2002g, Table 6.10). If 5% is assumed, the total distance traveled in urban areas would be about 22,000 mi (35,000 km). On the basis of these assumptions, the probability of a severe NH<sub>3</sub> accident occurring in an urban area is about  $7 \times 10^{-5}$ . In general, stable weather conditions occur only about one-third of the time, resulting in a probability for the most severe anhydrous NH<sub>3</sub> accident listed in Table 5.2-33 of about  $2 \times 10^{-5}$  (or a 1-in-50,000 chance of occurrence) during the 18-year operational period. This means that such an accident is expected to occur about once

every 900,000 years. Similarly, the severe aqueous 70% HF transportation truck accident is expected to occur about once in every 250,000 or more years of operation (i.e., it has about a 1-in-10,000 chance of occurring over the 18-year operational period).

The probability of a rail accident involving anhydrous NH<sub>3</sub> or 70% HF is even less than  $2 \times 10^{-5}$  or  $1 \times 10^{-4}$ , respectively, over the 18-year operational period, because the accident rates for railcars are lower (generally by about a factor of 5, see Table 6 in Saricks and Tompkins [1999]) and the total distance traveled by train is less (generally by about a factor of 2 to 4) for shipments of the same quantity of material over the same distance (because the railcar capacity is larger than the truck capacity). The conditional probability of a severe rail accident is about the same as that of a severe truck accident (about 0.05 in rural and suburban areas and about 0.008 in urban areas). Therefore, the probabilities of severe rail accidents over the same operational period are about 10 to 20 times less than the severe truck accidents.

Conservative estimates of consequences to the MEI located 100 ft (30 m) away from the accident site along the transportation route are also made for shipment of DUF<sub>6</sub> cylinders, depleted U<sub>3</sub>O<sub>8</sub>, emptied heel cylinders (assuming they are not used as containers for depleted U<sub>3</sub>O<sub>8</sub>), anhydrous NH<sub>3</sub>, and aqueous HF. The results for radiological impacts are shown in Table 5.2-34. Under the conservative assumptions described above for consequences to the population, it is estimated that the MEI could receive a dose of up to 3.7 rem in accidents involving DUF<sub>6</sub> cylinders and up to 1.3 rem in accidents involving emptied cylinders. However, for shipment of the depleted U<sub>3</sub>O<sub>8</sub> product by train, the MEI dose could be as high as 670 rem if the product was shipped in bulk bags and 380 rem if it was shipped in emptied DUF<sub>6</sub> cylinders. For shipment by truck, the MEI dose would be 170 rem with bulk bags and 150 rem with refilled cylinders (two per truck). The dose received by the individual would decrease quickly as the person's distance from the accident site increased. For example, at a distance of 328 ft (100 m), the dose would be reduced by a factor of about 6 (to about 110 rem and 60 rem for train accidents with bulk bags and refilled cylinders, respectively, and to about 28 rem and 25 rem for truck accidents with bulk bags and refilled cylinders, respectively). If the person was located at a distance of 100 ft (30 m) and if the accident occurred under the most severe conditions described above, the individual could suffer acute and potentially lethal consequences from both radiation exposure and the chemical effects of uranium. At 328 ft (100 m) or farther from the accident, the MEI would not be expected to suffer acute effects. However, the chance of the MEI developing a latent cancer would increase by about 10% for the train accident and about 3% for the truck accident under those conditions. For accidents involving DUF<sub>6</sub> cylinders, anhydrous NH<sub>3</sub>, and aqueous HF, the MEI would likely experience an irreversible health effect or death, depending on the severity of the accident, weather conditions, and distance at the time of the accident.

Even though the risks are relatively low, the consequences of a few of the transportation accidents are considered to be high. These high-consequence accidents are generally associated with the transportation of anhydrous NH<sub>3</sub> to the site and aqueous HF and depleted U<sub>3</sub>O<sub>8</sub> from the site. The consequences can be reduced or mitigated through design (e.g., by limiting the quantity of material per vehicle), operational procedures (e.g., by judicious selection of routes and times of travel, increased protection and tracking of transport vehicles), and emergency response actions (e.g., by sheltering, evacuation, and interdiction of contaminated food materials following an accident.)

**TABLE 5.2-34 Potential Radiological Consequences to the MEI from Severe Transportation Accidents Involving Shipment of Radioactive Materials**

Mode	Neutral Meteorological Conditions		Stable Meteorological Conditions	
	Dose (rem)	Radiological Risk (LCF) <sup>a</sup>	Dose (rem)	Radiological Risk (LCF) <sup>a</sup>
DUF <sub>6</sub>				
Truck	0.43	0.0002	0.91	0.0004
Rail	1.7	0.0009	3.7	0.002
Depleted U <sub>3</sub> O <sub>8</sub> (in bulk bags)				
Truck	11	0.005	170 <sup>b</sup>	0.08
Rail	42	0.02	670 <sup>b</sup>	0.3
Depleted U <sub>3</sub> O <sub>8</sub> (1 cylinder)				
Truck	4.8	0.002	76	0.04
Rail	12	0.006	190	0.09
Depleted U <sub>3</sub> O <sub>8</sub> (2 cylinders)				
Truck	9.6	0.005	150 <sup>b</sup>	0.08
Rail	24	0.01	380 <sup>b</sup>	0.2
Crushed heel cylinders <sup>c</sup>				
Truck	0.28	0.0001	0.63	0.0003
Rail	0.55	0.0003	1.3	0.0006
Heel cylinders <sup>d</sup>				
Truck	0.028	1 × 10 <sup>-5</sup>	0.063	3 × 10 <sup>-5</sup>
Rail	0.11	6 × 10 <sup>-5</sup>	0.25	0.0001

<sup>a</sup> LCFs were calculated by multiplying the dose by the ICRP Publication 60 health risk conversion factors of  $4 \times 10^{-4}$  fatal cancers per person-rem for workers and  $5 \times 10^{-4}$  for the public (ICRP 1991).

<sup>b</sup> See text for discussion. Because of the conservative assumptions made in deriving the numbers in this table, the MEI is likely to receive a dose that is less than shown here. However, if the doses were as high as those shown in the table, the MEI could develop acute radiation effects. The individual might also suffer from chemical effects due to uranium intake.

<sup>c</sup> Crushed heel cylinders are shipped 10 per cargo container, with 1 container per truck or 2 containers per railcar.

<sup>d</sup> Shipped "as is," one cylinder per truck or four cylinders per railcar.

#### 5.2.5.4 Historical Safety Record of Anhydrous NH<sub>3</sub> and HF Transportation in the United States

Anhydrous NH<sub>3</sub> is routinely shipped commercially in the United States for industrial and agricultural applications. Information provided in the DOT *Hazardous Material Incident System (HMIS) Database* (DOT 2003b) for 1990 through 2002 indicates that 2 fatalities and 19 major injuries to the public or to transportation or emergency response personnel occurred as a result of anhydrous NH<sub>3</sub> releases during truck and rail operations. These fatalities and injuries occurred during transportation or loading and unloading operations. Over that period, truck and rail NH<sub>3</sub> spills resulted in more than 1,000 and 6,000 evacuations, respectively. Five very large spills, greater than 10,000 gal (38,000 L), occurred; however, these spills were en route derailments from large rail tank cars. The two largest spills, both around 20,000 gal (76,000 L), occurred in rural or lightly populated areas of Texas and Idaho and resulted in 1 major injury. The Idaho spill in 1990 required the evacuation of 200 people. For highway shipments, 1 truck transport and 3 loading/unloading accidents occurred that involved large anhydrous NH<sub>3</sub> spills of between 4,000 and 8,000 gal (15,000 and 30,000 L). The 1 en route truck accident involving the largest truck spill (in Iowa on May 3, 1996) resulted in 1 fatality and the evacuation of 40 people. The other 3 large truck shipment spills occurred during loading/unloading operations but did not result in any fatalities. However, one of the spills involved a major injury and required the evacuation of 14 people in addition to the treatment of 26 with minor injuries.

Over the past 30 years, the safety record for transporting anhydrous NH<sub>3</sub> has significantly improved as a result of several factors. Hazardous compressed gas truck shipment loading and unloading operations require strict conformance with DOT standards for safety valve design and specifications, in addition to requirements on the installation of measuring and sampling devices. Federal rules governing the transportation of hazardous materials (49 CFR 173) require that valves installed for tank venting, loading, and unloading operations must be “of approved design, made of metal not subject to rapid deterioration by the lading, and must withstand the tank test pressure without leakage.” The MC331 compressed gas tanker trucks, which would most likely be used to ship anhydrous NH<sub>3</sub> to the DUF<sub>6</sub> conversion facility, must be equipped with check valves to prevent the occurrence of a large spill (e.g., a spill from a feed line disconnection during a loading operation). These valves are typically located near the front end of a MC331 tanker truck and close to the driver’s cab. Although not specifically required by DOT regulations, excess flow valves may be installed to prevent a catastrophic spill in the event that the driver is unable to reach the manual check valve to cut off flow from a failed feed line or loading tank valve. Safety measures contributing to the improved safety record over the past 30 years include the installation of protective devices on railcars, fewer derailments, closer manufacturer supervision of container inspections, and participation of shippers in the Chemical Transportation Emergency Center.

Most of the HF transported in the United States is anhydrous HF, which is more hazardous than the aqueous HF. Since 1971, which is the period covered by DOT records (DOT 2003b), no fatal or serious injuries to the public or to transportation or emergency response personnel have occurred as a result of anhydrous HF releases during transportation. Over the period 1971 to 2003, 11 releases from railcars were reported to have no evacuations or injuries associated with them. The only major release (estimated at 6,400 lb [29,000 kg] of HF)

occurred in 1985 and resulted in approximately 100 minor injuries. Another minor HF release during transportation occurred in 1990. The safety record for transporting HF has improved in the past 10 years for the same reasons discussed above for NH<sub>3</sub>.

### 5.2.6 Impacts Associated with HF and CaF<sub>2</sub> Conversion Product Sale and Use

During the conversion of the DUF<sub>6</sub> inventory to depleted uranium oxide, products having some potential for reuse would be produced. These products would include HF and CaF<sub>2</sub>, which are commonly used as commercial materials. An analysis of impacts associated with their potential reuse has been included as part of this EIS. Areas examined include the characteristics of these materials as produced within the conversion process, the current markets for these products, and the potential socioeconomic impacts within the United States if the products were sold. Because there would be some residual radioactivity associated with these materials, a description of the DOE process for authorizing release of materials for unrestricted use (referred to as “free release”) and a bounding estimate of the potential human health effects of such free release were included in the analysis. Details on the analysis are presented in Appendix E and are summarized below.

One of the chemicals produced during conversion would be an aqueous HF acid-water solution of 55% strength. The predominant markets for HF acid call for 49% and 70% HF solutions; consequently, this product would be further processed to yield these strengths. In the preferred design, a small amount of solid CaF<sub>2</sub> would also be produced.

Table 5.2-35 gives the approximate quantities of HF and CaF<sub>2</sub> that would be produced annually in the preferred designs. The quantities are based on the assumption that there would be a viable economic market for the aqueous HF produced. If such a market did not exist, UDS proposes that it would convert all of the HF to CaF<sub>2</sub> and then either sell this product or dispose of it as LLW or solid waste. The approximate quantity of CaF<sub>2</sub> produced in this scenario would be 8,800 t (9,700 tons) at the Portsmouth site.

Because it is expected that the UDS-produced HF and CaF<sub>2</sub> would contain small amounts of volumetrically distributed residual radioactive material, neither could be sold for unrestricted use, and CaF<sub>2</sub> could not be disposed of as solid waste, unless DOE established authorized limits for radiological contamination in HF and CaF<sub>2</sub>. UDS would be required to apply for appropriate authorized limits, according to whether HF and CaF<sub>2</sub> were sold, or CaF<sub>2</sub> was disposed of as solid

**TABLE 5.2-35 Products from DUF<sub>6</sub> Conversion (t/yr)**

Product	Portsmouth	Paducah	Total
Depleted uranium oxide	10,800	14,300	25,100
HF acid (55% solution)	8,200	11,000	19,300
CaF <sub>2</sub>	18	24	42

waste. In this context, authorized limits would be the maximum concentrations of radioactive contaminants allowed to remain volumetrically distributed within the HF or CaF<sub>2</sub>. The dose analysis presented in this EIS was not conducted to establish authorized limits.

The potential, bounding exposure rate for a hypothetical worker working in close proximity to an HF storage tank was estimated to be 0.034 mrem/yr on the basis of very conservative assumptions. Similar bounding estimates of the exposure rate to a worker in close proximity to a CaF<sub>2</sub> handling process yielded 0.23 mrem/yr. The radiation sources contributing to the bounding exposure rate for HF were external radiation and inhalation. For CaF<sub>2</sub>, in addition to external radiation and inhalation, the bounding exposure also resulted from an assumed incidental ingestion. Given more realistic exposure conditions, the potential dose would be much smaller than the bounding estimates. Potential exposures to product users would be much smaller than those to workers. Detailed discussions on the assumptions for bounding exposure are provided in Appendix E.

Socioeconomic impact analyses were conducted to evaluate the impacts of the introduction of the UDS-produced HF or CaF<sub>2</sub> into the commercial marketplace. The current aqueous HF acid producers have been identified as a potential market for the aqueous HF acid (UDS 2003b), with UDS-produced aqueous HF replacing some or all of current U.S. production. The impact of HF sales on the local economy in which the existing producers were located and on the U.S. economy as a whole would likely be minimal.

No market for the 22,000 t (24,000 tons) of CaF<sub>2</sub> that might be produced in the proposed conversion facilities at Paducah and Portsmouth has been identified (UDS 2003a). Should such a market be found, the impact of CaF<sub>2</sub> sales on the U.S. economy would likely be minimal.

In the event that no market for either HF or CaF<sub>2</sub> is established, the HF would be neutralized in a process that would produce additional CaF<sub>2</sub>. It is likely that the CaF<sub>2</sub> would be disposed of as waste. This would require shipping it to an approved solid waste or LLW disposal facility. While disposal activities would produce a small number of transportation jobs and might lead to additional jobs at the waste disposal facility, the impact of these activities in the transportation corridors, at the waste disposal site(s), and on the U.S. economy would be minimal.

### **5.2.7 Impacts If ETTP Cylinders Are Shipped to Paducah Rather Than to Portsmouth**

Current DOE plans call for the cylinders at ETTP to be shipped to Portsmouth. However, the option of sending the ETTP cylinders to Paducah instead is considered in this section.

If the ETTP DUF<sub>6</sub> cylinders were shipped to Paducah, the Portsmouth conversion plant would operate for 14 years rather than 18 years to convert the Portsmouth inventory. Potential impacts associated with transportation to and conversion of the ETTP cylinders at Paducah are evaluated in detail in the site-specific Paducah conversion facility EIS (DOE/EIS-0359). Facility construction impacts would be the same as discussed in Section 5.2.2. The annual operational impacts would be the same as described in Section 5.2.3 because the facility throughput would

be the same; however, impacts would occur over only a 14-year period rather than 18 years. In addition, the radiation doses to cylinder yard workers handling the ETTP cylinders, described in Section 5.2.2.1, would not be incurred.

### **5.2.8 Potential Impacts Associated with the Option of Expanding Conversion Facility Operations**

As discussed in Section 2.2.7, several reasonably foreseeable activities could result in a future decision to increase the conversion facility throughput or extend the operational period at one or both of the conversion facility sites. Specifically, the throughput of the facility could be increased through process improvements or a fourth process line could be added at Portsmouth. The facility also could be operated beyond the currently planned 18-year period in order to process additional DUF<sub>6</sub> that might be transferred to DOE at some time in the future (such as DUF<sub>6</sub> generated by USEC or another commercial enrichment facility). In addition, it is possible that DUF<sub>6</sub> cylinders could be transferred from Paducah to Portsmouth to facilitate conversion of the entire inventory, particularly if DOE assumes responsibility for additional DUF<sub>6</sub> at Paducah and not at Portsmouth.

To account for these future possibilities and provide future planning flexibility, this section includes an evaluation of the environmental impacts associated with expanding conversion facility operations at Portsmouth, either by increasing throughput or by extending operations. In addition, potential environmental impacts associated with possible Paducah-to-Portsmouth cylinder shipments are also evaluated in this section.

#### **5.2.8.1 Potential Impacts Associated with Increasing Plant Throughput**

The throughput of the Portsmouth facility could be increased either by process efficiency improvements or by adding an additional (fourth) process line. DOE believes that higher throughput rates can be achieved by improving the efficiency of the planned equipment (DOE 2004b). The conversion contract provides significant incentives to the conversion contractor to improve efficiency. For example, the current facility designs are based on an assumption that the conversion plant would have an 84% on-line availability (percent of time system is on line and operational). However, on the basis of Framatome's experience at the Richland plant, the on-line availability is expected to be at least 90%. Therefore, there is additional capacity expected to be realized in the current design.

If the plant throughput was marginally increased by process improvements, the environmental impacts during operations could increase for some areas but still would be similar to those discussed in Section 5.2.3 for the base design. For example, annual radiation doses to workers and the public from site emissions might increase in proportion to throughput. Slight variations in plant throughput are not unusual from year to year because of operational factors (e.g., equipment maintenance or replacement) and are generally accounted for by the conservative nature of the impact calculations. As discussed in Section 5.2.3, the estimated

annual impacts during operations are well within applicable guidelines and regulations, with collective and cumulative impacts being quite low.

In contrast to process efficiency improvements, the addition of a fourth process line at the Portsmouth facility would require the installation of additional plant equipment and would result in a nominal 33% increase in throughput when compared with the current base design. The plant capacity would be similar to the capacity planned for the Paducah site (evaluated in DOE/EIS-0359). This throughput increase would reduce the time necessary to convert the Portsmouth and ETTP DUF<sub>6</sub> inventories by about 5 years.

The potential environmental impacts associated with a 33% increase in throughput (for example, by the addition of a fourth conversion process line) at Portsmouth are discussed below by technical discipline. In general, the potential impacts are discussed relative to the operational impacts presented previously in Section 5.2.3 for the base design facility (i.e., three process lines). The construction impacts presented in Section 5.2.2 for three process lines were already based on a process building large enough to accommodate a fourth process line.

A parametric analysis was conducted for conversion facilities of different sizes as part of the PEIS (DOE 1999a). As discussed in Appendix K of the PEIS, potential environmental impacts resulting from the construction and operation of a conversion facility were estimated for throughputs ranging from 7,000 to 28,000 t/yr (7,716 to 30,865 tons/yr) of DUF<sub>6</sub>. In comparison, the throughput of the Portsmouth conversion facility is 13,500 t/yr (14,881 tons/yr) with three process lines and 18,000 t/yr (19,842 tons/yr) when a 33% increase is assumed — well within the range analyzed in the parametric study conducted for the PEIS.

The results presented in Appendix K of the PEIS indicated that some impacts would not vary with throughput (e.g., certain accident consequences), whereas other impacts would. However, it was found that in most cases, impacts would not increase in direct proportion with throughput because of economies of scale. For example, if the throughput increased by 33%, the expected increase in the impacts generally would be less than 33%. In spite of this less than one-to-one relationship, in some cases, the analyses that follow conservatively assume that impacts would increase in the same proportion as throughput.

In addition, DOE analyzed the impacts of a larger conversion facility with four process lines at Paducah in a separate EIS (DOE/EIS-0359). The resource requirements, environmental releases, and product and waste generation rates would be the same irrespective of where the facility was constructed. In addition, some of the impacts (e.g., the involved worker doses) would also be same. Whenever applicable, the results from the Paducah conversion facility EIS were used in the evaluation of impacts for the expanded capacity conversion facility option at Portsmouth in the following sections.

**5.2.8.1.1 Human Health and Safety — Normal Operations.** In general, a 33% increase in throughput at Portsmouth would result in an annual increase in the radiation exposure of workers and members of the public. However, it is expected that the cumulative doses for conversion of the entire inventory of Portsmouth and ETTP DUF<sub>6</sub> would be the same, regardless

of the annual throughput or number of process lines. This is because the higher annual doses associated with increased throughput would be offset by a shorter operational duration.

When an increase in the annual radiation dose to individual involved workers of 33% (proportional to the throughput increase) is assumed, the maximum annual individual worker doses would be approximately 100 mrem/yr to workers in the conversion facility and approximately 800 mrem/yr to cylinder yard workers (on the basis of results presented in Table 5.2-10). These doses would remain well below applicable regulatory limits and below levels expected to cause appreciable health effects. The annual collective dose to involved workers would increase from approximately 10.1 person-rem/yr to 10.7 person-rem/yr (on the basis of the involved worker doses estimated for the Paducah conversion facility [DOE 2004a]).

It is estimated that the annual airborne emissions of uranium would be the same for the Portsmouth conversion facility (three process lines) and the Paducah conversion facility (four process lines) (UDS 2003b). Therefore, annual doses to off-site members of the public and noninvolved workers from uranium emissions would be expected to be the same as presented in Table 5.2-10. However, even if it was assumed that emissions would increase 33% proportionally with throughput, the estimated dose to the MEI public and noninvolved workers would be much less than  $1 \times 10^{-4}$  mrem/yr. This dose is much less than the radiation dose limits of 100 mrem/yr (DOE 1990) from all pathways and 10 mrem/yr (40 CFR Part 61) from airborne pathways set to protect the general public from operations of DOE facilities.

Potential chemical exposures would also remain well below levels expected to cause health effects, even with a 33% increase in throughput. Human health impacts resulting from exposure to hazardous chemicals during normal operations of the conversion facilities are estimated as hazard indices of  $5 \times 10^{-6}$  and  $5.4 \times 10^{-5}$  for the noninvolved worker and general public MEI, respectively. The hazard indices for the conversion process would be at least three orders of magnitude lower than the hazard index of 1, which is the level at which adverse health effects might be expected to occur in some exposed individuals.

**5.2.8.1.2 Human Health and Safety — Facility Accidents.** As discussed in Section 5.2.3, there is a risk of on-the-job fatalities and injuries to conversion facility workers because of the industrial nature of the work environment. This risk is directly related to the amount of labor required (measured in terms of full-time equivalent employees). UDS estimated that there would be the same number of workers employed in the conversion facility at Paducah (four process lines) and at Portsmouth (three process lines) (UDS 2003b). Therefore, when it is assumed that the total amount of labor required to convert the Portsmouth and ETTP DUF<sub>6</sub> inventories would be the same regardless of throughput (e.g., whether three or four process lines were used), the risks from physical hazards if the throughput was increased 33% would be the same as those described in Section 5.2.3 for the base design. No on-the-job fatalities are predicted during the conversion facility operational phase. It is estimated, however, that about 142 injuries would occur over the life of the project (Table 5.2-4). Therefore, if the processing time was reduced by 5 years, about 40 fewer on-the-job injuries would be expected.

In general, for accidents involving the release of radioactive or hazardous materials, the consequences and risks if the throughput was increased by 33% would be the same as those discussed in Sections 5.2.3.2.1 and 5.2.3.2. This is because most of the bounding accidents would involve a limited amount of material that would be at risk under accident conditions, regardless of the facility throughput. For example, the consequences of accidents involving cylinders do not depend on the facility throughput. Similarly, the HF and NH<sub>3</sub> storage tanks would be the same size regardless of the facility throughput; therefore the consequences of a tank rupture would be the same.

The one exception would be the bounding radiological accident involving an earthquake that affects 6 months' worth of conversion product storage (an extremely unlikely accident). If the throughput was increased 33% (for instance, by adding a fourth process line), the amount of uranium oxide in storage could be 33% greater than the amount under the base design. Therefore, the amount of material potentially released would be 33% greater than that shown in Table 5.3-11. The resulting consequences (Tables 5.2-12 and 5.2-13) would also increase by 33%. However, because of the low probability of such an accident, the overall accident risk (calculated as the product of the accident consequence and the accident probability) would remain the same as discussed in Section 5.2.3.2.1; that is, no fatalities would be expected.

Although the estimated frequencies of some accidents could increase somewhat in association with an increased throughput, this increase would not be large enough to change the frequency category designations of the accidents given in Section 5.2.3. Any small increase in the annual frequency of some accidents would be offset by the reduced operational period of the facility. Therefore, the overall probability of occurrence of the accidents over the operational periods would be about the same. As a result, the total accident risk would not change.

**5.2.8.1.3 Air Quality and Noise.** If the throughput was increased 33% at the Portsmouth facility, emissions of criteria pollutants would increase in negligible amounts. However, emissions of HF would increase by 33% as a result of the increase in throughput. Potential impacts of criteria pollutants on ambient air quality would remain almost the same as presented in Table 5.2-18. In other words, total (background plus project increment) concentrations would be well below their applicable standards, except for PM<sub>2.5</sub>, which would approach or exceed the standards because of the regionally high background concentrations (similar to the case with three process lines). The background data used are the maximum values from the last 5 years of monitoring at the nearest monitoring location (operated by the OEPA) to the site, located about 20 mi (32 km) away in the town of Portsmouth. On the basis of these values, exceedance of the annual PM<sub>2.5</sub> standard would be unavoidable, because the background concentration already exceeds the standard (background is 24.1 µg/m<sup>3</sup>, in comparison with the standard of 15 µg/m<sup>3</sup>).

The potential impacts of HF on ambient air quality would increase by about 33%, with estimated maximum HF concentration increments and total concentrations remaining well below their state standards: about 6% and 20% for the standards, respectively.

With respect to noise, a throughput increase of 33% is estimated to result in an increase in the noise level within the conversion facility of about 1 dB. This increase would attenuate

significantly while passing through the conversion building walls. Accordingly, noise levels at the nearest residence would be almost the same as those for three processing lines, which would be below the EPA guideline of 55 dB(A).

**5.2.8.1.4 Water and Soil.** Increasing the throughput 33% at Portsmouth (for example, by increasing the number of process lines from three to four) would increase the quantity of process water needed for operations from 30 million gal/yr (114 million L/yr) to 37 million gal/yr (141 million L/yr), the same amount of process water needed at the Paducah facility. Groundwater withdrawn from wells for average use would still represent an increase of less than 1% of the current water use at the facility and 0.3% of the existing well capacity. Such impacts would remain small. No additional impacts to surface water or soils would be expected.

**5.2.8.1.5 Socioeconomics.** The socioeconomic impacts of a 33% increase in throughput at Portsmouth would be minimal. There could be a slight increase in capital and material expenditures if an additional process line was constructed (estimated to be \$5.6 million by the OIG), with a corresponding increase in labor expenditures to install the necessary equipment and facilities. However, as would be the case with capital expenditures associated with a three-process-line facility, it is assumed that there would be no local vendors or a limited number of them for the required specialized equipment, with a large majority of capital expenditures being made outside the ROI at the Portsmouth site. The impact of capital expenditures for an additional process line would therefore be minimal in the ROI.

Wage and salary spending associated with the installation of additional process line equipment would produce impacts in the ROI. The size of these impacts would depend on the size of the additional labor force required and the timing of the corresponding labor expenditures. However, since the additional process-line installation would most likely require no increase or only a small increase in the size of the overall labor force beyond that required for the three-process-line facility, the relative impact of the additional wage and salary expenditures in the ROI would likely be small. No additional impacts on local housing or local public services and education would be expected.

Operation of the facility with the additional process line would not require any increase in employment at the Portsmouth site. Impacts of operating the additional process line would be limited to any increase in expenditures on materials that might be made in the ROI. These expenditures would be unlikely to differ significantly from those associated with a three-process-line facility, meaning that the local impacts of the additional process line are also likely to be minimal.

A 33% increase in the throughput at Portsmouth would reduce the operational period of the facility by approximately 5 years. Consequently, positive socioeconomic impacts associated with employment of the conversion facility workforce would last approximately 13 years, compared to 18 years under the base design.

**5.2.8.1.6 Ecology.** Because a 33% increase in throughput at Portsmouth would not require the disturbance of any areas beyond those disturbed for the base design facility, and because the emissions would remain well below levels expected to have adverse effects on vegetation and biota, no impacts to ecological resources would be expected.

**5.2.8.1.7 Waste Management.** Over the life of the project, the total amounts of conversion products and waste (including low level, hazardous, and non-hazardous waste) generated at the conversion facility for conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories would be the same regardless of the annual facility throughput. However, the annual amounts of waste produced, provided in Table 5.2-20, would increase by approximately 33% as a result of the higher plant throughput when compared with that of the base design. This annual increase would not be expected to appreciably increase the annual impacts to waste management capabilities discussed in Section 5.2.3.7. As noted in Section 5.2.3.7, in the event that the HF was not marketable and it was neutralized to CaF<sub>2</sub>, the site's projected generation of nonhazardous waste would increase substantially (increasing by approximately 90% with three process lines and 120% with four process lines, assuming the CaF<sub>2</sub> was determined to be a nonhazardous waste).

**5.2.8.1.8 Resource Requirements.** A 33% increase in annual throughput at Portsmouth could require an increase of up to 33% in the quantities of materials required for operations, as shown in Table 5.2-21. As noted in Section 5.2.3.8, the material resources required during operations are not considered rare or unique, and the total quantities required would not affect their local, regional, or national availability. Therefore, negligible impacts on resource requirements would be expected if the throughput was increased 33% at the Portsmouth facility.

**5.2.8.1.9 Land Use.** A 33% increase in the annual throughput at Portsmouth would not increase the amount of land required for the conversion facility and would not alter the current or proposed site land use. The base design facility is already large enough to accommodate a fourth process line if one is required. Therefore, no impacts on land use would occur.

**5.2.8.1.10 Cultural Resources.** A 33% increase in the annual throughput at Portsmouth is unlikely to adversely affect cultural resources at all three alternative locations because no ground-disturbing activities would be associated with the throughput increase. In addition, facility air emissions would be well below levels that would adversely affect cultural resources.

**5.2.8.1.11 Environmental Justice.** As discussed in Section 5.2.3.11, the evaluation of environmental justice impacts is predicated on the identification of high and adverse impacts in other impact areas considered in this EIS, followed by a determination of whether those impacts would affect minority and low-income populations disproportionately. Analyses of impacts from operating the conversion facility with an increased throughput do not indicate high and adverse impacts for any of the other impact areas considered. Despite the presence of disproportionately

high percentages of low-income populations within 50 mi (80 km) of the Portsmouth site, no environmental justice impacts are anticipated at any of the three alternative locations because of the lack of high and adverse impacts.

**5.2.8.1.12 Transportation.** The transportation impacts presented in Section 5.2.5 for the base design (three process lines) are cumulative totals for the shipment of all materials associated with the conversion of the Portsmouth and ETTP DUF<sub>6</sub> inventories. Therefore, the overall transportation impacts would be the same regardless of whether or not the annual throughput was increased 33%. However, the annual number of shipments would increase 33%. The annual transportation impacts can be estimated by dividing the collective population impacts presented in Section 5.2.5 by the shipping campaign duration. Thus, annual impacts would be greater if the throughput was increased 33% because the inventory would be converted and transported at a higher rate, but the total impacts would be the same as for the three-process-line base design.

**5.2.8.1.13 Cumulative Impacts.** The potential cumulative impacts at the Portsmouth site from operation of the conversion facility are discussed in Section 5.3 for the base design, a three-process-line facility. As discussed in that section, the cumulative impacts, including the proposed action and other current or reasonably foreseeable activities at the site, are within regulatory limits and generally well below levels expected to cause adverse environmental impacts (with the exception of PM<sub>2.5</sub> concentrations, which might exceed standards because of the regionally high background level). Because the incremental impacts of increasing the throughput by 33% at the Portsmouth facility would not significantly increase the potential environmental impacts from the conversion facility, as discussed above, the cumulative impacts would be the same as those discussed in Section 5.3.

**5.2.8.1.14 Decontamination and Decommissioning.** Potential environmental impacts associated with the D&D of the conversion facility after the facility is closed are discussed in Section 5.9 for the three-process-line base design. If the throughput was increased by adding a fourth process line, additional process equipment would require D&D. This would be expected to result in a potential increase in the radiation dose to involved workers and an increase in the amount of LLW generated, when compared with a three-process-line facility. However, there is a large amount of uncertainty concerning D&D activities because they will not likely occur for 15 to 20 years, and the activities required would be very dependent on the operational history of the facility. Thus, the D&D impacts presented in Section 5.9 are considered representative of both a three- and a four-process-line facility. As noted in Section 5.9, additional NEPA review would likely need to be performed before D&D occurred. It is also expected that such a review would be based on the actual condition of the facilities and a more definite identification of the resulting waste materials.

**5.2.8.1.15 Other Issues and Impacts.** Sections 5.4 through 5.8 of this EIS discuss mitigation, unavoidable adverse impacts, irreversible and irretrievable commitment of resources, the relationship between short-term use of the environment and long-term productivity, and

pollution prevention and waste minimization. The discussion in these sections would also apply if the throughput of the Portsmouth facility was increased 33%.

#### **5.2.8.2 Potential Impacts Associated with Extending the Plant Operational Period**

As noted above, the Portsmouth conversion facility is currently being designed to process the Portsmouth and ETTP DUF<sub>6</sub> cylinder inventories over 18 years. There are no current plans to operate the conversion facilities beyond this period. However, with routine facility and equipment maintenance and periodic equipment replacements or upgrades, it is believed the conversion facility could be operated safely beyond this time period to process additional DUF<sub>6</sub> for which DOE might assume responsibility.

The estimated annual environmental impacts during conversion facility operations were presented and discussed previously in Section 5.2.3; these impacts are expected to continue each year for the planned 18 years of operations at Portsmouth. If operations were extended beyond 18 years and if the operational characteristics (e.g., estimated releases of contaminants to air and water) of the facility remained unchanged, the annual impacts would be expected to be essentially the same as those presented in Section 5.2.3. However, continued operations would result in the impacts being incurred over a greater number of years. The total radiation dose to the workers and the public would increase in proportion to the number of additional years that the facility operated. Although the annual frequency of accidents would remain unchanged, the overall probability of a severe accident would increase proportionately with the additional operational time period. In addition, the total quantities of depleted uranium and secondary waste products requiring disposal would increase proportionately, as would the amount of HF or CaF<sub>2</sub> produced. As discussed in Section 5.2.3, the estimated annual impacts during operations are within applicable guidelines and regulations, with collective and cumulative impacts being quite low. This would also be expected during extended operations.

#### **5.2.8.3 Potential Impacts Associated with Possible Future Paducah-to-Portsmouth Cylinder Shipments**

As noted above, it is possible that in the future, DUF<sub>6</sub> cylinders could be transferred from Paducah to Portsmouth to facilitate conversion of the entire inventory, particularly if DOE assumes responsibility for additional DUF<sub>6</sub> at Paducah. At this time, it is uncertain whether such transfers would take place and how many cylinders would be transferred if such a decision was made. Therefore, for comparative purposes, this section provides estimates of the potential impacts from transporting 1,000 DUF<sub>6</sub> cylinders from Paducah to Portsmouth by either truck or rail. Shipment of 1,000 cylinders per year roughly corresponds to the annual base design throughput of the Portsmouth conversion facility.

The transportation assessment methodology discussed in Appendix F, Section F.3, was used to estimate the collective population risk for shipment of 1,000 cylinders between Paducah and Portsmouth by both truck and rail. It was assumed that only compliant cylinders that met DOT requirements would be shipped between the sites. The estimated highway and rail route

distances between the sites are 395 mi (636 km) and 478 mi (769 km), respectively. The estimated collective risks are provided in Table 5.2-36. No cargo-related or vehicle-related fatalities are expected for the shipment of 1,000 cylinders per year between the sites.

The estimated consequences of severe accidents and the potential impacts to MEIs would be the same as those presented and described in Section 5.2.5 for the shipment of ETPP cylinders.

## 5.3 CUMULATIVE IMPACTS

### 5.3.1 Issues and Assumptions

The CEQ guidelines for implementing NEPA define cumulative effects as the impacts on the environment resulting from the incremental impacts of an action when added to other past, present, and reasonably foreseeable future actions (40 CFR 1508.7). Cumulative effects include other actions regardless of what agency (federal or nonfederal), organization, or person undertakes them. Noteworthy cumulative impacts can result from individually minor, but collectively significant, effects of all actions.

The activities considered in this cumulative analysis comprise those that might affect environmental conditions at or near the Portsmouth site, including activities occurring on the site itself and activities occurring nearby whose impacts could affect the site. A summary of impacts associated with various actions is presented in Table 5.3-1 for impacts associated with most of the technical areas assessed in this EIS. When possible, these summaries are quantitative;

**TABLE 5.2-36 Annual Transportation Impacts for the Shipment of DUF<sub>6</sub> Cylinders from Paducah to Portsmouth, Assuming 1,000 DUF<sub>6</sub> Cylinders Shipped per Year**

Route	Mode	No. of Shipments	Total Distance (10 <sup>6</sup> mi)	Cargo-Related		Vehicle-Related		
				Radiological Risk (LCF) <sup>a</sup>		Irreversible Adverse Effects	Latent Emission Fatalities	Accident Fatalities
				Crew	Public			
Paducah to Portsmouth	Truck	1,000	0.395	0.002	0.001	5 × 10 <sup>-7</sup>	0.1	0.01
	Rail <sup>b</sup>	250	0.12	0.007	0.0003	2 × 10 <sup>-8</sup>	0.008	0.006

<sup>a</sup> The lifetime risk of an LCF for an individual was estimated from the calculated doses by using a dose-to-risk conversion factor of 0.0005 fatality per person-rem for members of the general public, as recommended in ICRP Publication 60 (ICRP 1991). The approximate corresponding dose received for each radiological fatality risk listed in this table may be obtained by multiplying the fatality risk by 2,000 (i.e., 1 ÷ 0.0005).

<sup>b</sup> Assumes four DUF<sub>6</sub> cylinders per railcar.



**TABLE 5.3-1 (Cont.)**

Impact Category	Existing Conditions	Impacts of DUF <sub>6</sub> Management <sup>a</sup>		Impacts of Other Actions <sup>c</sup>	Cumulative Impacts <sup>d</sup>	
		No Action	Action Alternatives <sup>b</sup>		No Action	Action Alternatives <sup>b</sup>
Cultural resources (adverse impacts)	None	None	Unlikely	Unlikely	Unlikely	Unlikely
Environmental justice (impacts)	None	None	None	None	None	None

<sup>a</sup> Based on results presented in Sections 5.1 and 5.2 of this EIS. No action impacts were considered over 40 years. Proposed action impacts were considered for both construction (over 2 years) and operation (over 18 years), with calculations shown including whichever had the greatest impacts.

<sup>b</sup> For purposes of estimating cumulative impacts, all three facility locations would yield identical environmental consequences and, as a result, are not presented in separate columns.

<sup>c</sup> Includes impacts of current UF<sub>6</sub> management activities by DOE and USEC (DOE 1999a); waste management activities (DOE 1997a) and continued storage of cylinders under the no action alternative; converting the Portsmouth GDP to standby (DOE 2001c); reindustrialization of the Portsmouth GDP (DOE 2001b); and current environmental restoration activities that have proceeded to the point that their consequences can be defined: X-749 Contaminated Materials Disposal Facility, Quadrant I Groundwater Investigative Area, X-701C Neutralization Pit/X-701A Lime House Removal, X-720 Neutralization Pit, X-740 Waste Oil Handling Facility (with associated phytoremediation), X-701B in situ chemical oxidation, X-326 L-cage Glove Box, X-744G Glove Box, X-623 Groundwater Treatment Facility, and X-624 Groundwater Treatment Facility (DOE 2002d). Future actions include construction and operation of a gas centrifuge enrichment facility at Portsmouth (U.S. Energy Research and Development Administration [ERDA] 1977).

<sup>d</sup> Cumulative impacts represent the sum of the impacts of the DUF<sub>6</sub> management alternatives and other past, present, and reasonably foreseeable future actions.

<sup>e</sup> Estimated for 18 years, to enable comparison with proposed action.

<sup>f</sup> No dose estimates given for surrogate reuse activities for Portsmouth in the assessment of impacts from reindustrialization (DOE 2001b), apart from suggesting that the magnitude would be similar to the estimated public dose (which is estimated at 0.02% of the DOE limit for public exposure).

<sup>g</sup> Assumes 0.0005 LCF/person-rem.

<sup>h</sup> Cumulative impacts assume all facilities operate simultaneously and are located at the same point.

<sup>i</sup> No worker dose given for possible enrichment facility or Lead Cascade test facility for enrichment, thus cumulative figures will be slightly low; the individual dose would still be monitored to remain under 5 rem/person annually.

<sup>j</sup> NA = Not available.

<sup>k</sup> Includes both facility workers and noninvolved workers; assumes 0.0004 LCF/person-rem.

<sup>l</sup> Concerns shipments of radioactive materials; all estimates of numbers of shipments rounded upward to nearest hundred.

**TABLE 5.3-1 (Cont.)**

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- <sup>m</sup> Assumes monthly average of 1 LLW shipment and 0.67 LLMW shipment from USEC, and 1 LLW shipment from DOE activities (Coriell 2003; Hawk 2003; Kelly 2003), rounded upward to the nearest hundred for the 18-yr duration of shipments.
- <sup>n</sup> Estimates for transportation under the action alternatives consider the proposed mode of transport of radiological materials, to or from Portsmouth when such a mode has been specified. In the cases of transporting DUF<sub>6</sub> and non-DUF<sub>6</sub> from ETTP, this analysis assumes truck transport (in the absence of a proposed mode) since trucks would result in the greatest impacts to an MEI.
- <sup>o</sup> Actual shipments are monitored to ensure external dose is below regulatory limits; calculations here reflect estimates based on empirical data recorded in DOE complex of  $1.6 \times 10^{-8}$  rem to public from passing truck shipment (DOE 1997a).
- <sup>p</sup> Although currently classified as an attainment area, measured concentrations for both O<sub>3</sub> and PM<sub>2.5</sub> (of regional concern) currently are higher than state and national air quality standards.
- <sup>q</sup> Air impacts are not discussed for the enrichment facility (see ERDA 1977).
- <sup>r</sup> PM<sub>2.5</sub> exceedance is primarily due to higher background concentrations, already above the standards
- <sup>s</sup> Drinking water standards exceeded for alpha activity, americium, beta activity, beryllium, chloroethane, TCE, and uranium.

however, some are, by necessity, qualitative. For technical areas without data that can be aggregated, this analysis evaluates potential cumulative impacts in a qualitative manner as systematically as possible. When it is not appropriate for estimates of impacts to be accumulated, they are not included in the table. For example, it is not appropriate to accumulate chemical impacts (anticipated to be extremely small under the alternatives considered in this EIS) because hazard index estimates are not expected to be additive for different materials and conditions.

### 5.3.2 Portsmouth Site

Past, ongoing, and future actions at the Portsmouth site include continued waste management activities (DOE 1997a), waste disposal activities (DOE 2002d), environmental restoration activities (DOE 2002d), industrial reuse of sections of the site (DOE 2001b), consolidation of reusable uranium from other sites in the DOE complex (DOE 2003c), continued management of DUF<sub>6</sub> cylinders by USEC and DOE, and other DUF<sub>6</sub> management activities considered in this EIS (see also DOE 1999a). Uranium enrichment activities at Portsmouth were discontinued early in 2002 (see DOE 2001c). However, in late 2002, Portsmouth was identified as the future location of USEC's Lead Cascade test enrichment facility (NRC 2004). Table 5.3-1 identifies the anticipated cumulative impacts that could result from the construction and operation of a DUF<sub>6</sub> conversion facility at the Portsmouth site, as well as impacts from continued management of DUF<sub>6</sub> at the Portsmouth site under the no action alternative.

One action that is considered in this analysis to be reasonably foreseeable and that deserves special mention is the future development of a permanent uranium enrichment facility at the Portsmouth site. In January 2004, USEC announced that it had selected Portsmouth as the site of the American Centrifuge Facility. This cumulative assessment assumes that the facility would use existing gas centrifuge technology. The assessment further assumes that the impacts of such a facility would be the same as those outlined in a 1977 analysis of environmental consequences for such an action (ERDA 1977). (The facility proposed in 1977 was never completed.)

Together with the alternatives assessed in Sections 5.1 and 5.2 of this EIS, the cumulative analysis (the final two columns of Table 5.3.1) includes the following:

- *No Action Alternative:* The cumulative impacts of no action include impacts of UF<sub>6</sub> generation and management activities by USEC and DOE (management only) (DOE 1999a) and continued, long-term storage of cylinders under the no action alternative; waste management activities at the Portsmouth site (DOE 1997a; see also DOE 2002d); conversion of the Portsmouth GDP to standby (DOE 2001b); construction, operation, and D&D of the Lead Cascade test uranium enrichment facility at Portsmouth (NRC 2004); construction, operation, and D&D of a uranium enrichment facility at the Portsmouth site (ERDA 1977); consolidation of reusable uranium in the DOE complex at the Portsmouth site (DOE 2003c); and current environmental restoration activities that have proceeded to the point that their consequences can be defined (DOE 2002d).

- *Proposed Action Alternatives:* The cumulative impacts of the proposed action alternatives include impacts related to the preferred alternative, including the impacts of constructing an additional storage pad and facility to convert DUF<sub>6</sub> to U<sub>3</sub>O<sub>8</sub> by using UDS technology; conversion of DUF<sub>6</sub> currently stored at the Portsmouth and ETTP sites to U<sub>3</sub>O<sub>8</sub> at the proposed facility; waste management activities at the Portsmouth site (DOE 1997a; see also DOE 2002d); conversion of the Portsmouth GDP to standby (DOE 2001c); construction, operation, and D&D of the Lead Cascade test uranium enrichment facility at Portsmouth (NRC 2004); construction, operation and D&D of a uranium enrichment facility at the Portsmouth site (ERDA 1977); consolidation of reusable uranium in the DOE complex at the Portsmouth site (DOE 2003c); and environmental restoration activities that have proceeded to the point that their consequences can be defined (DOE 2002d).

The results of the cumulative analysis are summarized in Table 5.3-1. The first data column of the table summarizes existing conditions at the site, as presented in Section 3.1 of this EIS. The second and third data columns of the table, in turn, summarize the results of the assessment of impacts of alternatives presented in Sections 5.1 and 5.2 of this EIS. The fourth data column summarizes aggregated impacts of past, present, and reasonably foreseeable future actions at the Portsmouth site, while the final two columns present cumulative impacts under the no action and proposed action alternatives. Transporting cylinders currently stored at the ETTP site to Portsmouth is considered as part of the proposed action.

#### **5.3.2.1 Radiological Releases — Normal Operations**

For both the no action alternative and the action alternatives, impacts to human health and safety could result from radiological facility operations and accidents. As shown in Table 5.3-1, cumulative collective radiological exposure to the off-site population would be well below the maximum DOE dose limit of 100 mrem/yr to the off-site MEI for both alternatives and below the limit of 25 mrem/yr specified in 40 CFR 190 for uranium fuel cycle facilities. Annual radiological doses to individual involved workers would be monitored to maintain exposure below the regulatory limits.

#### **5.3.2.2 Accidental Releases — Radiological and Chemical Materials**

For both the no action alternative and the action alternatives, doses and consequences of releases of radiological materials were considered for a range of accidents from *likely* (occurring an average of 1 or more times in 100 years) to *extremely rare* (occurring an average of less than 1 time in a million years). Because of the low probability of two accidents happening at the same time, the consequences of these accidents are not considered to be cumulative. The probability of even *likely* accidents occurring at the same time is very low, even for the most frequently expected accidents — the likelihood of this co-occurrence being the product of their individual probabilities (1 in 100 years multiplied by 1 in 100 years equals 1 in 10,000 years [ $0.01 \times 0.01 =$

0.0001]). Moreover, in the event that two facility accidents from the *likely* category occurred at the same time, the consequences for the public would be low.

### **5.3.2.3 Transportation**

The number of shipments of DUF<sub>6</sub>, non-DUF<sub>6</sub>, U<sub>3</sub>O<sub>8</sub>, crushed heel cylinders, and heel cylinders associated with the action alternatives at the Portsmouth site would involve rail and truck transport. Calculations prepared for cumulative impacts, which are based on analytical results presented in Section 5.2.5, consider proposed transport modes for the various materials or items moved. Results indicate a total of 12,300 truck shipments and 6,800 rail shipments, with radiological impacts presented as an annual dose to the MEI. Radiological impacts resulting from transportation of all materials under both modes would be very small, as would the cumulative impacts.

### **5.3.2.4 Chemical Exposure — Normal Operations**

Impacts associated with chemical exposure are expected to be very small under the alternatives considered in this EIS. As noted previously, the calculation of cumulative impacts is not possible because of the absence of necessary measures (hazard indices) for other actions and the inappropriateness of aggregating these measures across the different chemicals used in different industries. Under normal operations, no impacts to the public are expected from chemical exposure for the action or the no action alternatives.

### **5.3.2.5 Air Quality**

The Portsmouth site is currently located in an attainment region, although measured concentrations for certain criteria pollutants (O<sub>3</sub> and PM<sub>2.5</sub>) were above the state and national air quality standards (see Section 3.1.3.3). During construction at the site for additional on-site storage or the conversion facility, total PM<sub>10</sub> and/or PM<sub>2.5</sub> concentrations would be higher than applicable ambient standards, due in part to their high background concentrations. Because of their near-ground-level releases, high concentrations would be limited to the immediate vicinity of the site. However, these impacts would be temporary and could be minimized by using good engineering and construction practices and standard dust suppression methods. During the period of conversion at the Portsmouth site, total annual-average PM<sub>2.5</sub> concentrations would exceed state and national standards, primarily because of higher background concentrations.

### **5.3.2.6 Noise**

No cumulative noise impacts are expected for the alternatives considered in this EIS. Noise energy dissipates within short distances from the sources, and significant noise impacts are not expected in the vicinity of the conversion facility.

### 5.3.2.7 Water and Soil

Cumulative impacts on surface water at the Portsmouth site for construction and normal operations would not exceed the 30 µg/L of uranium used for comparison in discharges to Little Beaver Creek, Big Beaver Creek, or the Scioto River, even under low-flow conditions for the first two. Cumulative impacts on surface water would be localized and temporary even for small creeks, with adequate dilution occurring once such a creek entered larger waterways. Under the no action alternative, care would be taken during cylinder painting to prevent a further toxicity effect.

Data from the 2000 annual groundwater monitoring at the Portsmouth site indicated that seven pollutants exceeded primary drinking water standards in groundwater: alpha activity, americium, beta activity, beryllium, chloroethane, TCE, and uranium (DOE 2001d,e). Such impacts would continue under cumulative impacts, although site management practices that continue to stabilize plume movement and improve current groundwater quality should not allow further noteworthy contamination under the cumulative case. The groundwater analysis indicates that current cylinder maintenance practices would control cylinder corrosion under the no action alternative; thus, the maximum uranium concentration in groundwater (from cylinder breaches) would be 5 µg/L, considerably below the 30-µg/L guideline level used for comparison. Direct contamination of groundwater could occur during the construction and operation of a conversion facility (e.g., from the dissolution and infiltration of stockpiled chemicals into aquifers). However, good engineering and construction practices should ensure that impacts associated with construction would be minimal and not change existing groundwater conditions. Slight contamination similarly could occur during normal operation of a conversion facility. However, the contamination is not anticipated to reach a noteworthy magnitude. Cumulative impacts might contribute slightly to groundwater contamination, although the combination of efforts to address existing contaminants and practices to minimize increasing contamination should limit the magnitude of increases.

No noteworthy cumulative impacts to soils are anticipated.

### 5.3.2.8 Ecology

Cumulative ecological impacts are anticipated to be negligible under the no action alternative and negligible to minor under the action alternatives, in conjunction with the effects of existing conditions and other activities. Habitat disturbance would involve settings commonly found in this part of Ohio, in many cases previously disturbed. Construction of a conversion facility at Location A could directly affect a small wetland. Construction of a conversion facility at Location C would also remove trees that could provide habitat for the Indiana bat; this federally endangered species is not known to utilize this area. No impacts on this or other state- or federal-listed species are anticipated.

### **5.3.2.9 Land Use**

All DUF<sub>6</sub> activities under the alternatives would be confined to the Portsmouth site, which is already used for similar activities. Other activities on the site similarly are consistent with existing land use at Portsmouth, while activities already in the vicinity of the site change land uses to, at most, only relatively very small areas. No cumulative land use impacts are anticipated.

### **5.3.2.10 Cultural Resources**

The probability of encountering significant archaeological resources at the Portsmouth site would vary, depending on the area disturbed by a proposed activity or activities and the amount of disturbance. Further cultural resource surveys in consultation with the SHPO would be required for areas as yet unsurveyed that have not been previously disturbed. Consultation with Native Americans, conducted under this project, similarly would have to occur. If significant cultural resources were encountered during any of the activities under cumulative impacts, adverse effects would need to be mitigated. If any structures at the Portsmouth GDP were determined to be historically significant and there was a potential for a short-term adverse effect from the deposit of particulate matter on building surfaces, these adverse effects would be mitigated. All additional survey and mitigation would be conducted in consultation with the Ohio SHPO.

### **5.3.2.11 Environmental Justice**

No environmental justice cumulative impacts are anticipated for the Portsmouth site. Although disproportionately high percentages of minority and low-income populations occur in the vicinity of the site, no cumulative impacts in the vicinity of Portsmouth are high and adverse.

### **5.3.2.12 Socioeconomics**

Socioeconomic impacts under all alternatives are anticipated to be generally positive, often temporary, and relatively small. Growth in population could occur to meet labor demands during construction and operation, but it would not be so great as to place excessive demands on existing housing or public services. Cumulative socioeconomic impacts similarly are expected to be relatively small and positive, although some would be more long-lived than others.

## **5.3.3 ETPP Site**

Because some of the DUF<sub>6</sub> processed at the Portsmouth conversion facility under the action alternatives would come from the ETPP site, cumulative impacts also would involve activities at this locality. Under the no action alternative, in contrast, existing DUF<sub>6</sub> at ETPP would continue to be stored at the site, similarly causing cumulative impacts. Although the focus

of this EIS is on impacts (including cumulative impacts) associated with the Portsmouth site, this section briefly examines cumulative impacts at ETTP.

Cumulative impacts associated with the no action alternative would involve the effects of continued storage of DUF<sub>6</sub> at ETTP in conjunction with other activities at or near that site, as summarized in the PEIS for long-term storage of this material (DOE 1999a). Reasonably foreseeable future actions at or in the vicinity of ETTP include waste management activities (DOE 1997a, 2000b, 2001a); stockpile, stewardship, and management activities (DOE 1996b); the disposition of highly enriched uranium (DOE 1996c); the disposition of potentially reusable uranium (DOE 2002b); interim storage of enriched uranium (DOE 1994b); construction and operation of the Spallation Neutron Source Facility (DOE 1999d); tritium production in a commercial light-water reactor (DOE 1999g); transfer of non-nuclear functions (DOE 1993); changes in the sanitary sludge land application program (DOE 1996d); reindustrialization of ETTP (DOE 1997b, 2002a); and environmental restoration activities at ETTP (DOE 2001f). The absence of noteworthy negative impacts under the no action alternative, described in Section 5.1.3, is consistent with the absence of large cumulative impacts in the no action case (see also DOE 1999a).

Cumulative impacts at ETTP under the action alternatives would involve activities associated with preparing cylinders stored at this site for transportation, followed by their shipment to the Portsmouth site. The other past, present, and reasonably foreseeable activities listed in the preceding paragraph for ETTP would be the same. Cylinder preparation impacts, described in Section 5.2.4, are anticipated to be minimal. When aggregated with other activities at or near the ETTP site, cumulative impacts would not be large or serious for any impact area. Transportation impacts associated with ETTP cylinders, described in Section 5.2.5, similarly are not anticipated to be large. Cumulative impacts of transportation, discussed in Section 5.3.2 and presented in Table 5.3-1, likewise would not be large or serious.

## 5.4 MITIGATION

In general, the impacts of the alternatives presented in this chapter are conservative estimates of impacts expected for each alternative. Factors such as flexibility in siting at and within the three alternative locations at Portsmouth and facility design and construction options could be used to reduce impacts from these conservative levels. This section identifies what impacts could be mitigated to reduce adverse impacts. On the basis of the analyses conducted for this EIS, the following recommendations can be made:

- Potential future impacts on site air and groundwater could be avoided by inspecting cylinders, carrying out cylinder maintenance activities (such as painting), and promptly cleaning up releases from any breached DUF<sub>6</sub> cylinders. In addition, runoff from cylinder yards should be collected and sampled so that contaminants can be detected and their release to surface water or groundwater can be avoided. If future cylinder painting results in permit violations, treating cylinder yard runoff prior to release may be required.

- Temporary impacts on air quality from fugitive dust emissions during construction of any new facility should be controlled by the best available practices to avoid temporary exceedances of the PM<sub>10</sub> and PM<sub>2.5</sub> standard. Technologies that would be used to mitigate air quality impacts during construction include using water sprays on dirt roadways and on bare soils in work areas for dust control; covering open-bodied trucks transporting materials likely to become airborne when full and at all times when in motion; water spraying and covering bunkered or staged excavated and replacement soils; maintaining paved roadways in good repair and in a clean condition; using barriers and windbreaks around construction areas such as soil banks, temporary screening, and/or vegetative cover; mulching or covering exposed bare soil areas until vegetation has time to recover or paving has been installed; and prohibiting any open burning.
- During construction, impacts to water quality and soil can be minimized through implementing storm water management, sediment and erosion controls (e.g., temporary and permanent seeding; mulching and matting; sediment barriers, traps, and basins; silt fences; runoff and earth diversion dikes), and good construction practices (e.g., covering chemicals with tarps to prevent interaction with rain; promptly cleaning up any spills).
- Potential impacts to wetlands at the Portsmouth site could be minimized or eliminated by maintaining a buffer near adjacent wetlands during construction. Impacts at Location A may potentially be avoided by an alternative routing of the entrance road, or mitigation may be developed in coordination with the appropriate regulatory agencies.
- If trees (either live or dead) with exfoliating bark are encountered on construction areas, they should be saved if possible to avoid destroying potential habitat for the Indiana bat. If necessary, the trees should be cut before April 15 or after September 15.
- The quantity of radioactive and hazardous materials stored on site, including the products of the conversion process, should be minimized.
- The construction of a DUF<sub>6</sub> conversion facility at Portsmouth would have the potential to impact cultural resources. Neither an archaeological nor an architectural survey has been completed for the Portsmouth site as a whole or for any of the alternative locations, although an archaeological sensitivity study has been conducted. In accordance with Section 106 of the NHPA, the adverse effects of this undertaking must be evaluated once a location is chosen.
- Testing should be conducted either prior to or during the conversion facility startup operations to determine if the air vented from the autoclaves should be

monitored or if any alternative measures would need to be taken to ensure that worker exposures to PCBs above allowable OSHA limits do not occur.

- The nuclear properties of DUF<sub>6</sub> are such that the occurrence of a nuclear criticality is not a concern, regardless of the amount of DUF<sub>6</sub> present. However, criticality is a concern for the handling, packaging, and shipping of enriched UF<sub>6</sub>. For enriched UF<sub>6</sub>, criticality control is accomplished by employing, individually or collectively, specific limits on uranium-235 enrichment, mass, volume, geometry, moderation, and spacing for each type of cylinder. The amount of enriched UF<sub>6</sub> that may be contained in an individual cylinder and the total number of cylinders that may be transported together are determined by the nuclear properties of enriched UF<sub>6</sub>. Spacing of cylinders of enriched UF<sub>6</sub> in transit during routine and accident conditions is ensured by use of regulatory approval packages that provide protection against impact and fire.
- Because of the relatively high consequences estimated for some accidents, special attention will be given to the design and operational procedures for components that may be involved in such accidents. For example, the tanks holding hazardous chemicals on site such as anhydrous NH<sub>3</sub> and aqueous HF would be designed to all applicable codes and standards, and special procedures would be in place for gaining access to the tanks and for filling of the tanks. In addition, although the probabilities of occurrence for high consequence accident are extremely low, emergency response plans and procedures would be in place to respond to any emergencies should an accident occur. Additional details are discussed below.

Although the probability of transportation accidents involving hazardous chemicals such as HF and NH<sub>3</sub> is very low, the consequences could be severe. For this EIS, the assessment of transportation accidents involving HF assumed conservative conditions. Currently, a number of industry practices are commonly employed to minimize the potential for large HF releases, as discussed below.

HF is usually shipped in 100-ton (91-t), 23,000-gal (87,000-L) shell, full, noncoiled, noninsulated tank cars. Most HF railcars today meet DOT Classification 112S500W, which represents the current state of the art. To minimize the potential for accidental releases, these railcars have head protection and employ shelf couplers, which help prevent punctures during an accident. The use of these improved tank cars has led to an improved safety record with respect to HF accidents over the last several years. In fact, the HF transportation accident rate has steadily decreased since 1985. Industry recommendations for the new tank car guideline appear in *Recommended Practices for the Hydrogen Fluoride Industry* (Hydrogen Fluoride Industry Practices Institute 1995b).

Accidents involving HF and NH<sub>3</sub> at a conversion facility could have potentially serious consequences. However, a wide variety of good engineering and mitigative practices are available that are related to siting, design, and accident mitigation for HF and NH<sub>3</sub> storage tanks,

which might be present at a conversion facility. Many are summarized in *Guideline for the Bulk Storage of Anhydrous Hydrogen Fluoride* (Hydrogen Fluoride Industry Practices Institute 1995a). There is an advanced set of accident prevention and mitigative measures that are recommended by industry for HF storage tanks, including storage tank siting principles (e.g., evaluating seismic, high wind, and drainage conditions), design recommendations, and tank appurtenances, as well as spill detection, containment, and mitigation. Measures to mitigate the consequences of an accident include detection systems, spill containment systems such as dikes, remote storage tank isolation valves, water spray systems, and rapid acid deinventory systems (that rapidly remove acid from a leaking vessel). Details on these mitigative strategies are also provided in the Hydrogen Fluoride Industry Practices Institute (1995a) guidelines.

## 5.5 UNAVOIDABLE ADVERSE IMPACTS

Unavoidable adverse impacts are those impacts that cannot be mitigated by choices associated with siting and facility design options. They are impacts that would be unavoidable, no matter which options were selected.

The cylinders currently in storage would require continued monitoring and maintenance under all alternatives. These activities would result in the exposure of workers in the vicinity of the cylinders to low levels of radiation. The radiation exposure of workers could be minimized, but some level of exposure would be unavoidable. The radiation doses to workers are estimated to be well within public health standards under all alternatives. Radiation exposures of workers would be monitored at each facility and would be kept ALARA. Cylinder monitoring and maintenance activities would also emit air pollutants, such as vehicle exhaust and dust (PM<sub>10</sub>), and produce small amounts of sanitary waste and LLW. Concentrations of air emissions during operations are estimated to be within applicable standards and guidelines, and waste generation would not appreciably affect waste management operations.

Under all alternatives, workers would have a potential for accidental on-the-job injuries and fatalities that would be unrelated to radiation or chemical exposures. These would be a consequence of unanticipated events in the work environment, typical of all workplaces. On the basis of statistics in similar industries, it is estimated that less than 1 fatality and on the order of several hundred injuries would occur under the alternatives, including the required transportation among sites associated with the alternatives. The chance of fatalities and injuries occurring would be minimized by conducting all work activities in as safe a manner as possible, in accordance with occupational health and safety rules and regulations. However, the chance of these types of impacts cannot be completely avoided.

Conversion would require the construction of a new facility at the Portsmouth site. Up to 65 acres (26 ha) of land could be disturbed during construction, with approximately 10 acres (4 ha) required for the facility footprint. Construction of the facility could result in losses of terrestrial and aquatic habitats. Dispersal of wildlife and temporary elimination of habitats would result from land clearing and construction activities involving movement of construction personnel and equipment. The construction of the facility could cause both short-term and long-term disturbances of some biological habitats. Although some destruction would be

inevitable during and after construction, these losses could be minimized by careful site selection and construction practices.

## **5.6 IRREVERSIBLE AND IRRETRIEVABLE COMMITMENT OF RESOURCES**

The major irreversible and irretrievable commitments of natural and man-made resources related to the alternatives analyzed in this EIS are discussed below. A commitment of a resource is considered *irreversible* when the primary or secondary impacts from its use limit the future options for its use. An *irretrievable* commitment refers to the use or consumption of a resource that is neither renewable nor recoverable for later use by future generations.

The decisions to be made in the ROD following the publication of this EIS would commit resources required for implementing the selected alternative. Three major resource categories would be committed irreversibly or irretrievably under the alternatives considered in this EIS: land, materials, and energy.

### **5.6.1 Land**

Land that is currently occupied by UF<sub>6</sub> cylinder storage or selected for the conversion facility could ultimately be returned to open space if the yards, buildings, roads, and other structures were removed, the areas cleaned up, and the land revegetated. Future use of these tracts of land, although beyond the scope of this EIS, could include restoring them for unrestricted use. Therefore, the commitment of this land would not necessarily be irreversible. However, the land used to dispose of any conversion products or construction or D&D wastes would represent an irretrievable commitment, because wastes in belowground disposal areas could not be completely removed, the land could not be restored to its original condition, and the site could not feasibly be used for other purposes following the closure of the disposal facility. All disposal activities associated with alternatives analyzed in this EIS would take place at DOE or commercial disposal facilities that would be permitted or licensed to accept such wastes.

### **5.6.2 Materials**

The irreversible and irretrievable commitment of material resources for the various EIS alternatives would include construction materials that could not be recovered or recycled, materials rendered radioactive that could not be decontaminated, and materials consumed or reduced to unrecoverable forms of waste. Materials related to construction could include wood, concrete, sand, gravel, steel, aluminum, and other metals (Table 5.6-1). At this time, no unusual construction material requirements have been identified. The construction resources, except for those that could be recovered and recycled with current technology, would be irretrievably lost. None of the identified construction resources is in short supply, and all should be readily available in the local region.

**TABLE 5.6-1 Materials/Resources Consumed during Conversion Facility Construction at the Portsmouth Site**

Materials/Resources	Total Consumption	Unit	Peak Demand	Unit
<b>Utilities</b>				
Water	550,000	gal	1,500	gal/h
Electricity	1,500	MWh	7.2	MWh/d
<b>Solids</b>				
Concrete	9,139	yd <sup>3</sup>	NA <sup>a</sup>	NA
Steel	511	tons	NA	NA
Inconel/Monel	33	tons	NA	NA
<b>Liquids</b>				
Fuel	73,000	gal	250	gal/d
<b>Gases</b>				
Industrial gases (propane)	15,000	gal	50	gal/d

<sup>a</sup> NA = not applicable.

Strategic and critical materials (e.g., Monel and Inconel) would not be required in quantities that would seriously reduce the national or world supply. This material would be used throughout the facilities and would be used in the generation of HF in the conversion process. The autoclaves and conversion units (process reactors) are long-lead-time procurements with few qualified bidders. Many suppliers are available for the remainder of the equipment.

Estimated annual consumption rates of raw materials are provided in Table 5.6-2. Consumption of operating supplies (e.g., miscellaneous chemicals such as lime and potassium hydroxide, and gases such as nitrogen), although irretrievable, would not constitute a permanent drain on local sources or involve any material in critically short supply in the United States as a whole.

### 5.6.3 Energy

The irretrievable commitment of energy resources during the operation of the various facilities considered under the alternatives would include the consumption of fossil fuels used to generate steam and heat and electricity for the facilities (Table 5.6-3). Energy also would be expended in the form of diesel fuel and gasoline for cylinder transport equipment and transportation vehicles. Consumption of these utilities, although irretrievable, would not constitute a permanent drain on local sources or involve any utility in critically short supply in the United States as a whole.

## 5.7 RELATIONSHIP BETWEEN SHORT-TERM USE OF THE ENVIRONMENT AND LONG-TERM PRODUCTIVITY

For this EIS, *short term* is considered the period of construction activities for the alternatives analyzed — the time when most short-term (or temporary) environmental impacts would occur. Disposal of solid nonhazardous waste resulting from new facility construction, operations, and D&D would require additional land at a sanitary landfill site, which would be unavailable for other uses in the long term. Any radioactive or hazardous waste generated by the various alternatives would involve the commitment of associated land, transportation, and disposal resources and resources associated with the processing facilities for waste management.

For the construction and operation the of conversion facility, the associated construction activities would result in both short-term and long-term losses of terrestrial and aquatic habitats from natural productivity. Dispersal of wildlife and temporary elimination of habitats would result from land clearing and construction activities involving movement and staging of construction personnel and equipment. The building of new facilities could cause long-term disturbances of some biological habitats, potentially causing long-term reductions in the biological activity of an area. Although some habitat loss would be inevitable during and after construction, these losses would be minimized by careful site selection and by thorough environmental reviews of specific proposals. Short-term impacts would be reduced and mitigated as necessary. After closure of the new facilities, they would be decommissioned and could be reused, recycled, or remediated.

## 5.8 POLLUTION PREVENTION AND WASTE MINIMIZATION

Implementation of the EIS alternatives would be conducted in accordance with all applicable pollution prevention and waste minimization guidelines. Pollution prevention is designed to reduce risk to public health, safety, welfare, and the environment through source reduction techniques and environmentally acceptable recycling processes. The Pollution Prevention Act of 1990 (42 USC 11001–11050) established a national policy that pollution should be prevented or reduced at the source, whenever feasible. The act indicates that when pollution cannot be prevented, polluted products should be recycled in an environmentally safe

**TABLE 5.6-2 Materials Consumed Annually during Conversion Facility Operations at the Portsmouth Site<sup>a</sup>**

Chemical	Quantity (tons/yr)
Solid	
Lime (CaO) <sup>b</sup>	14
Liquid	
Ammonia (99.95% minimum NH <sub>3</sub> )	510
Potassium hydroxide (45% KOH)	6
Gaseous	
Nitrogen (N <sub>2</sub> )	7,800

<sup>a</sup> Material estimates are based on facility conceptual-design-status data (UDS 2003b). A number of studies are planned to evaluate design alternatives, the results of which may affect the above materials needs.

<sup>b</sup> Assuming lime is used only for potassium hydroxide regeneration. If HF neutralization is required, the annual lime requirement would be approximately 7,000 tons/yr (6,350 t/yr).

**TABLE 5.6-3 Utilities Consumed during Conversion Facility Operations at the Portsmouth Site<sup>a</sup>**

Utility	Annual Average Consumption	Unit	Peak Demand <sup>b</sup>	Unit
Electricity	31,084	MWh	6.2	MW
Liquid fuel	3,000	gal	NA <sup>c</sup>	NA
Natural gas <sup>d,e</sup>	$4.0 \times 10^7$	scf <sup>f</sup>	180	scfm <sup>f</sup>
Process water	$30 \times 10^6$	gal	215	gal/min
Potable water	$3 \times 10^6$	gal	350	gal/min

<sup>a</sup> Utility estimates are based on facility conceptual-design-status data (UDS 2003b). A number of studies are planned to evaluate design alternatives, the results of which may affect the above utility needs.

<sup>b</sup> Peak demand is the maximum rate expected during any hour.

<sup>c</sup> NA = not applicable.

<sup>d</sup> Standard cubic feet measured at 14.7 psia and 60°F (16°C).

<sup>e</sup> The current facility design (UDS 2003b) uses electrical heating. However, an option of using natural gas is being evaluated.

<sup>f</sup> scf = standard cubic feet; scfm = standard cubic feet per minute.

manner. Disposal or other releases into the environment should be employed only as a last resort. Executive Order 12856, *Federal Compliance with Right-to-Know Laws and Pollution Prevention Requirements* (U.S. President 1993), and DOE Order 5400.1, *General Environmental Protection Program* (DOE 1988), implement the provisions of the Pollution Prevention Act of 1990. Pollution prevention measures could include source reduction, recycling, treatment, and disposal. The emphasis would be on source reduction and recycling to prevent the creation of wastes (i.e., waste minimization).

Waste minimization is the reduction, to the extent feasible, of the generation of radioactive and hazardous waste. Source reduction and waste minimization techniques include good operating practices, technology modifications, changes in input material, and product changes. An example of waste minimization would be to substitute nonhazardous materials, when possible, for materials that contribute to the generation of hazardous or mixed waste.

A consideration of opportunities for reducing waste generation at the source, as well as for recycling and reusing material, will be incorporated to the extent possible into the engineering and design process for the conversion facility. Pollution prevention and waste minimization will be major factors in determining the final design of any facility to be constructed. Specific pollution prevention and waste minimization measures will be considered in designing and operating the final conversion facility.

## 5.9 DECONTAMINATION AND DECOMMISSIONING OF THE CONVERSION FACILITY

When operations at the conversion facility are complete, D&D would be performed to protect both public health and safety and the environment from accidental releases of any remaining radioactivity and hazardous materials. The conversion facility is being designed to facilitate D&D activities. This analysis assumes that the D&D activity would provide for the disassembly and removal of all radioactive and hazardous components, equipment, and structures associated with the conversion facility. The objective assumed in this EIS would be to completely dismantle the various buildings and achieve “greenfield” (unrestricted use) conditions. The design requirements for the D&D of this facility can be found in two DOE Directives from 1999: DOE Guide 430.1-3, *Deactivation Implementation Guide*, and DOE Guide 430.1-4, *Decommissioning Implementation Guide* (DOE 1999e,f).

Because the D&D of the conversion facility is not expected to occur for at least 18 years, it is likely that an additional environmental review would need to be performed before it occurred. It is also expected that such a review would be based on the actual condition of the facilities and a more definite identification of the resulting waste materials.

### 5.9.1 Human Health and Safety — Off-Site Public

It is expected that D&D of the DUF<sub>6</sub> conversion facility would result in low radiation doses to members of the public and would be accomplished with no significant adverse environmental impacts.

DOE has established a primary dose limit for any member of the public of 0.1 rem (1 mSv) total effective dose equivalent (TEDE) per year for protection of public health and safety. Compliance with the limit is based not just on an individual DOE source or practice but on the sum of internal and external doses resulting from all modes of exposure to all radiation sources other than background and medical sources (DOE 1993). However, it could be very difficult to determine doses from all radiation sources for the purpose of demonstrating compliance. Therefore, DOE elements are instructed to apply a public dose constraint of 0.025 rem (0.25 mSv) of TEDE per year to each DOE source or practice (DOE 2002h). Also, DOE elements are required to implement a process to ensure, on a case-specific basis, that public radiation exposures will be ALARA below the dose constraint (DOE 1993).

To be consistent with DOE’s general approach to protecting the public from radiation exposure as explained above, the release of radioactive material from D&D activities at a DOE-controlled site, such as a DUF<sub>6</sub> conversion or cylinder treatment facility, would be limited to an amount determined on a case-specific basis through the ALARA process to be ALARA but, in any event, less than 0.025 rem/yr (0.25 mSv/yr). This would ensure that doses to the public from DOE real property releases following D&D were consistent with NRC requirements for commercial nuclear facilities, as stated in 10 CFR 20, Subpart E, “Radiological Criteria for License Termination.”

In its final generic EIS for decommissioning of NRC-licensed nuclear facilities (NRC 1994), the NRC concluded that at any site where the 0.025-rem/yr (0.25-mSv/yr) dose criterion established in 10 CFR 20, Subpart E, is met, the likelihood that individuals who use the site would be exposed to multiple sources with cumulative doses approaching 0.1 rem/yr (1 mSv/yr) would be very low. Accordingly, the likelihood would also be very low that a member of the public would be exposed in excess of the DOE primary dose limit after D&D of the DUF<sub>6</sub> conversion and cylinder treatment facilities to meet site-specific limits that are ALARA below the dose constraint of 0.025 mrem/yr (0.25 mSv/yr).

The total public dose from D&D of the DUF<sub>6</sub> conversion facility is estimated to range from 4 to 5 person-rem. This estimate was scaled from data on public exposure doses found in NRC (1988) to account for the capacity of the conversion facility and the effort required for its D&D. Because of the low specific activity of uranium, the estimate is very small and primarily would result from the transportation of D&D wastes for ultimate disposition (NRC 1988). Radiation doses to the public resulting from accidents during D&D activities would be low enough to be considered insignificant (NRC 1988).

### **5.9.2 Human Health and Safety — On-Site Workforce**

Radiological impacts to involved workers during D&D of the conversion facility would result primarily from external radiation due to the handling of depleted uranium materials. Because of the low radiation exposures from depleted uranium, one of the initial D&D activities would be removal of any residual uranium from the process equipment, significantly reducing radiation exposure to the involved workforce.

Radiation exposure estimates for the involved workforce during D&D activities involving nuclear facilities licensed by the NRC are provided in NRC (1988) and NRC (1994). These nuclear facilities include UF<sub>6</sub> production plants and uranium fuel fabrication plants that are similar to the conversion facilities considered in this EIS. Average radiation dose rates in the conversion facility during the initial cleaning are expected to be much less than 2 mrem/h, which is the radiation dose rate from bulk quantities of uranium (NRC 1988).

Table 5.9-1 lists the estimated LCFs of the involved workforce during decontamination and cleanup activities at the facility as a function of the residual dose rate (NRC 1994). The radiological impacts in Table 5.9-1 were estimated on the basis of the dose rates to which the workers are subjected and the collective effort required to reduce the residual contamination levels.

One of the most critical parameters in developing the decommissioning plan would be the release criterion applicable for the project. Subpart E of 10 CFR Part 20 addresses release criteria for NRC licensees, while DOE Order 5400.5 (DOE 1990) governs the development of release limits for DOE facilities. On the basis of a residual dose rate of 25 mrem/yr, the estimated LCFs of the involved workforce would be much lower than unity (i.e., no radiation-related fatalities), since the radiation dose to involved workers would be a small fraction of the exposure

experienced over the operating lifetime of the facility and well within the occupational exposure limits imposed by regulatory requirements.

Radiation exposure of the involved D&D workers would be monitored by a dosimetry program and maintained below regulatory limits.

The risk of on-the-job fatalities and injuries to conversion facility D&D workers was calculated by using industry-specific statistics from the BLS, as reported by the National Safety Council (2002). Annual fatality and injury rates from the BLS construction industry division were used for the D&D phase. On the basis of D&D cost information provided in Elayat et al. (1997), it is assumed that the D&D workforce would be approximately 10% of the construction workforce. On the basis of these assumptions and information provided in UDS (2003b), the estimated incidences of fatalities and injuries for the D&D of the conversion facilities are 0.01 and 5, respectively.

### 5.9.3 Air Quality

Before structural dismantlement, all contaminated surfaces would be cleaned manually. Best construction management practices, such as dust control measures, would be used to protect air quality and to mitigate any airborne releases during the D&D process. As discussed in Section 5.9.1, it is anticipated that the D&D activities would not produce any significant radiological emissions that would affect the off-site public.

D&D can be considered to be the reverse of the construction of buildings and structures. Available information (Elayat et al. 1997) indicates that the level of construction-related activities during D&D would be an order of magnitude lower than during conversion facility construction. Air quality during D&D activities would thus be bounded by the results presented in Sections 5.2.1.3 and 5.2.2.3 for construction activities, if it is assumed that the existing emission control systems were efficiently maintained.

**TABLE 5.9-1 Estimated Latent Cancer Fatalities from Radiation Exposure Resulting from Conversion Facility D&D Activities at the Portsmouth Site<sup>a</sup>**

Residual Dose Rate (mrem/yr)	Residual Dose	
	Low <sup>b</sup>	High <sup>c</sup>
100	$2.12 \times 10^{-3}$	$3.61 \times 10^{-3}$
60	$2.12 \times 10^{-3}$	$3.63 \times 10^{-3}$
30	$2.12 \times 10^{-3}$	$3.65 \times 10^{-3}$
15	$2.14 \times 10^{-3}$	$3.66 \times 10^{-3}$
10	$2.16 \times 10^{-3}$	$3.67 \times 10^{-3}$
3	$2.18 \times 10^{-3}$	$3.68 \times 10^{-3}$
1	$2.19 \times 10^{-3}$	$3.69 \times 10^{-3}$
0.3	$2.19 \times 10^{-3}$	$3.70 \times 10^{-3}$
0.1	$2.20 \times 10^{-3}$	$3.71 \times 10^{-3}$
0.03	$2.20 \times 10^{-3}$	$3.72 \times 10^{-3}$

<sup>a</sup> Values in this table are unscaled values taken directly from NRC (1994).

<sup>b</sup> Based on the D&D of a uranium fuel fabrication plant that converts enriched UF<sub>6</sub> into UO<sub>2</sub> for production of light-water reactor fuel (DOE 1999g).

<sup>c</sup> Based on the D&D of a UF<sub>6</sub> production plant where yellowcake is converted to UF<sub>6</sub>.

#### 5.9.4 Socioeconomics

The potential consequences from D&D of the conversion facilities would be lower than those discussed in Section 5.2.1.5 for conversion facility construction, because the total D&D workforce would be smaller for facility D&D than for facility construction.

To decommission the conversion facility, many of the same people who operated the facility could do the cleaning; however, the dismantling and moving of equipment would have to be performed by electricians, plumbers, mechanics, and equipment operators, most of whom would be hired or contracted (NRC 1988) specifically for this purpose.

#### 5.9.5 Waste Management

The major challenge of the D&D activity would be to remove and dispose of radioactive and hazardous wastes while keeping occupational and other exposures ALARA. Section 3.7 of DOE Guide 420.1-1 (DOE 2000c) requires facilities where radioactive or other hazardous contaminating materials will be used to be designed so as to simplify periodic decontamination and ultimate decommissioning. For example, if necessary, all cracks, crevices, and joints would have to be caulked or sealed and finished smooth to prevent the accumulation of contaminated material in inaccessible areas. These design features should minimize the generation of radioactive and/or hazardous materials during D&D activities.

There are three major classes of D&D waste, based on the composition and radioactivity of the materials involved: LLW, mixed LLW, and hazardous waste. It is assumed that TRU waste would not be present (any TRU waste generated during facility operations would be removed prior to D&D activities). A fourth class is “clean” material; this is any material resulting from D&D activities, including metal, which can be safely reused or recycled without any further radiological or hazardous controls. If no further need is established for these clean materials, they can be disposed of at sanitary landfills without requiring any further radiological or hazardous controls.

D&D-related waste can also be categorized into two general groups: contaminated materials and other wastes. Contaminated materials are standard materials such as steel and concrete that contain or have embedded trace amounts of radioactivity. In general, contamination is caused by the settling or adherence of uranium and its progeny products on internal surfaces such as piping. The average concentrations of the radionuclides contaminating the conversion facility are expected to be generally low enough to rank these materials as Class-A LLW.

Other wastes, the second general group of D&D-related wastes, are composed of materials that can become radioactively contaminated when plant workers use them. They include gloves, rags, tools, plastic sheeting, and chemical decontaminants. These wastes are also expected to have an average radioactivity low enough to be ranked as Class-A LLW. This analysis assumes that the quantities of other wastes would be much lower than those generated during facility deconstruction.

It is assumed that the soil within the conversion facility perimeters would not be contaminated with radiological or hazardous materials as a result of normal facility operations and, therefore, would not require excavation and subsequent treatment and disposition. If soil was contaminated due to an accidental release, it would be cleaned up as quickly as feasible after the release occurred and would not be part of the D&D wastes.

The methodology outlined in Forward et al. (1994) was used to estimate the volumes and types of wastes that would be generated from the D&D of the conversion facilities. Because contaminant inventories for these facilities are unavailable, reference data on the contaminant inventory data compiled by the NRC were applied. Facilities are categorized in Forward et al. (1994) into different types on the basis of their function, structure, design, and degree of D&D difficulty. This analysis assumes that the conversion facilities could be considered to be “radioactively contaminated buildings” with a “low” degree of D&D difficulty.

On the basis of the above assumptions and information provided in UDS (2003a), the annual and total waste generation rates from the D&D of the conversion facility were estimated and are provided in Table 5.9-2. Of the total materials generated during the D&D of the conversion facility, both LLMW and hazardous wastes would make up 2% to 3% of the total, and LLW would constitute about 6% to 7%. The majority of the D&D materials (approximately 88% of the total) would be “clean.”

The “clean” waste would be sent to a landfill that accepts construction debris. Low-level waste would be sent to a licensed disposal facility where it will likely be buried in accordance with the waste acceptance criteria and other requirements in effect at that time. Hazardous and mixed waste would be disposed of in a licensed facility in accordance with applicable regulatory requirements.

**TABLE 5.9-2 Annual and Total Waste Volume Estimates from Conversion Facility D&D Activities at the Portsmouth Site**

Waste Type	Annual D&D Waste (m <sup>3</sup> /yr) <sup>a</sup>	Total D&D Waste (m <sup>3</sup> )
LLMW	40	110
Hazardous waste	40	110
LLW	70	200
Clean	1,200	4,000

<sup>a</sup> Annual rates based on 3-year D&D.

## 6 ENVIRONMENTAL AND OCCUPATIONAL SAFETY AND HEALTH PERMITS AND COMPLIANCE REQUIREMENTS

### 6.1 DUF<sub>6</sub> CYLINDER MANAGEMENT AND CONSTRUCTION AND OPERATION OF A DUF<sub>6</sub> CONVERSION FACILITY

DUF<sub>6</sub> cylinder management as well as construction and operation of the proposed DUF<sub>6</sub> conversion facility would be subject to many federal, state, and local requirements. In accordance with such legal requirements, a variety of permits, licenses, and other consents must be obtained. Table 6.1 at the end of this chapter lists those that may be needed. The status of each is indicated on the basis of currently available information. However, because the DUF<sub>6</sub> project is still at an early stage, the information in Table 6.1 should not be considered comprehensive or binding. UDS may determine that additional consents not listed in Table 6.1 apply, or that the DUF<sub>6</sub> cylinder management and/or conversion facility qualify for exemptions or exclusions from some listed consents.

### 6.2 TRANSPORTATION OF UF<sub>6</sub>

Transportation of UF<sub>6</sub> (depleted, natural, or slightly enriched) is governed by the Hazardous Materials Transportation Act (HMTA), as amended by the Hazardous Materials Transportation Uniform Safety Act of 1990 and other acts (49 USC 5101 et seq.). This law is implemented by the DOT through its hazardous materials regulations (HMRs) (i.e., 49 CFR Parts 171 through 180). Since UF<sub>6</sub> presents hazards because of both its radioactivity and corrosivity, the DOT HMRs impose specific packaging requirements on UF<sub>6</sub> shipments in addition to the otherwise applicable radioactive material transportation requirements. The specific packaging requirements for shipments of UF<sub>6</sub> appear in 49 CFR 173.420 and are summarized below.

- Other than Model 30A cylinders and certain cylinders manufactured before June 30, 1987, DUF<sub>6</sub> packaging must be designed, fabricated, inspected, tested, and marked in accordance with the version of ANSI Standard N14.1, *Uranium Hexafluoride — Packaging for Transport*, that was in effect at the time the packaging was manufactured.
- Each UF<sub>6</sub> packaging must be designed so that it will withstand a hydraulic test at an internal pressure of at least 1.4 megapascals (MPa) (200 lb/in.<sup>2</sup>) without leakage.
- Each UF<sub>6</sub> packaging must be designed so that it will withstand a free drop test without loss or dispersal of UF<sub>6</sub>. The specimen must drop onto a flat, horizontal surface of such a character that any increase in its resistance to displacement or deformation upon impact by the specimen would not significantly increase the damage to the specimen. The drop must occur so that the specimen will suffer maximum damage in respect to the safety

features to be tested. Mandatory drop heights, which must be measured from the lowest point of the specimen to the upper surface of the target, vary depending on the packaging mass from 1 ft (0.3 m) if the packaging mass exceeds 33,000 lb (15,000 kg), to 4 ft (1.2 m) if the packaging mass is less than 11,000 lb (5,000 kg).

- Each UF<sub>6</sub> packaging must be designed so that it will withstand, without rupture of the containment system, a thermal test as follows: Exposure for a period of 30 minutes to a thermal environment that provides a heat flux at least equivalent to that of a hydrocarbon fuel/air fire in sufficiently quiescent ambient conditions to give a minimum average flame emissivity coefficient of 0.9 and an average temperature of at least 800°C (1,475°F), fully engulfing the specimen, with a surface absorptivity coefficient that is the greater of 0.8, or the value the package may be expected to possess if exposed to the fire specified and a convective coefficient that must be the value that the package may be demonstrated to have if exposed to the fire specified.
- The UF<sub>6</sub> must be in solid form.
- The volume of solid DUF<sub>6</sub> must not exceed 62% of the certified capacity of the package at 20°C (68°F). For natural and slightly enriched UF<sub>6</sub>, this requirement is 61%.
- The pressure in the package at 20°C (68°F) must be less than 101.3 kPa (14.8 lb/in.<sup>2</sup> absolute [psi]).
- Before initial filling and during periodic inspection and tests, UF<sub>6</sub> packaging must be cleaned in accordance with ANSI N14.1.
- UF<sub>6</sub> packaging must be periodically inspected, tested, marked, and otherwise conform to ANSI N14.1.
- Each repair to UF<sub>6</sub> packaging must be performed in accordance with ANSI N14.1.

If, at the time transportation occurs, the DUF<sub>6</sub> is being stored in a cylinder for which compliance with the then-applicable transportation requirements in 49 CFR 173.420 cannot be verified, UDS may implement one of the following options before shipping the DUF<sub>6</sub>:

- Obtain an exception, pursuant to 49 CFR 173.3(b), to allow the cylinder to be transported either “as is” or following repairs, or
- Transfer the DUF<sub>6</sub> from its noncompliant cylinder into a compliant cylinder.
- Ship the noncompliant cylinder in a compliant overpack.

A detailed discussion of regulatory considerations associated with transporting UF<sub>6</sub> is presented in Biwer et al. (2001).

### **6.3 WORKER SAFETY AND HEALTH**

The Occupational Safety and Health Act of 1970 (P.L. 91-596) gives OSHA the authority to prescribe and enforce standards and regulations affecting the occupational safety and health of private-sector employees. However, at facilities where another federal agency has exercised its statutory authority to prescribe or enforce occupational safety and health standards, Section 4(b)(1) of the act waives OSHA's jurisdiction. Relying on this section of the act, in 1974, OSHA explicitly recognized the authority of the AEC to establish and enforce occupational safety and health standards at AEC-sponsored, contractor-operated facilities covered by the AEA. Since then, the AEC and its successor agencies, including DOE, have regulated worker health and safety at most of their own facilities. This approach will be used to regulate worker safety at DUF<sub>6</sub> cylinder management and conversion facilities.

DOE exercises its authority over working conditions at its facilities through an extensive program of internal oversight and a system of DOE regulations and directives that require DOE contractors to comply with relevant worker protection standards and regulations (e.g., 29 CFR Part 1910, *Occupational Safety and Health Standards*, and 29 CFR Part 1926, *Safety and Health Regulations for Construction*) and impose additional radiation and chemical exposure standards developed by DOE (DOE Order 440.1A). DOE enforces its regulations, which have the power of law, by levying fines or by referring the offending contractor to the Department of Justice for other punishment. Most of DOE's worker radiation protection regulations are located in 10 CFR Part 835, *Occupational Radiation Protection*. Pertinent DOE directives are listed in site-specific contract provisions and are enforced by invoking contractual remedies such as contract cancellation. Accordingly, UDS is required by its contract to comply with applicable health, safety, and environmental laws, orders, regulations, and national consensus standards and to develop and execute a radiation protection plan and an integrated safety management plan (DOE 2000d).

**TABLE 6.1 Potentially Applicable Consents for the Construction and Operation of a DUF<sub>6</sub> Conversion Facility**

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<i>Air Quality Protection</i>			
<p><b>Title V Operating Permit:</b> Required for sources that are not exempt and are major sources, affected sources subject to the Acid Rain Program, sources subject to new source performance standards (NSPS), or sources subject to National Emission Standards for Hazardous Air Pollutants (NESHAPs).</p>	<p>Ohio Environmental Protection Agency (OEPA); U.S. Environmental Protection Agency (EPA)</p>	<p>Clean Air Act (CAA), Title V, Sections 501–507 (<i>U.S. Code</i>, Title 42, Sections 7661–7661f [42 USC 7661–7661f]); <i>Ohio Administrative Code</i> (OAC) 3745-77-02</p>	<p>Uranium Disposition Services, LLC (UDS), has determined that the DUF<sub>6</sub> conversion facility is not an affected source subject to the Acid Rain Program and is not a source subject to NSPS. Nevertheless, UDS has not yet confirmed whether the DUF<sub>6</sub> conversion facility would be a major source of hazardous air pollutants (HAPs). Also, the facility is subject to <i>Code of Federal Regulations</i>, Title 40, Part 61, Subpart H (40 CFR Part 61, Subpart H), “National Emission Standards for Emissions of Radionuclides Other Than Radon from Department of Energy Facilities” (NESHAPs), although emissions are expected to result in an effective dose equivalent to the maximally exposed individual (MEI) of well below the standard (i.e., 10 mrem/yr). Accordingly, UDS is seeking official verification from the OEPA as to whether this permit is needed. OEPA representatives have verbally stated that no Title V Operating Permit will be required.</p>
<p><b>Ohio Permit to Install:</b> Required for (1) any source to which one or more of the following CAA programs would apply: prevention of significant deterioration (PSD), nonattainment area, NSPS, and/or NESHAPs; and (2) any source to which one or more of the following state air quality programs would apply: Gasoline Dispensing Facility Permit, Direct Final Permit, and/or Small Maximum Uncontrolled Emission Unit Registration.</p>	<p>OEPA</p>	<p>CAA, Title I, Sections 160–169 (42 USC 7470–7479); OAC 3745-31-02</p>	<p>UDS has determined that the PSD, nonattainment area, and NSPS programs do not apply to the DUF<sub>6</sub> conversion facility. In addition, UDS has determined that none of the state air quality programs that would trigger the need for an Ohio Permit to Install would apply. Nevertheless, the facility is subject to the NESHAPs program (40 CFR Part 61, Subpart H). Accordingly, an Ohio Permit to Install will be required for the DUF<sub>6</sub> conversion facility. UDS will submit a timely permit application to the OEPA.</p>

**TABLE 6.1 (Cont.)**

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<i>Air Quality Protection (Cont.)</i>			
<b>Ohio Permit to Operate:</b> Required for (1) any source to which one or more of the following CAA programs would apply: PSD, nonattainment area, NSPS, NESHAPs; and (2) any source to which one or more of the following state air quality programs would apply: State Permit to Operate and/or registration of operating unit with potential air emissions of an amount and type considered minimal; this permit is not required, however, for any facility that must obtain a Title V Operating Permit.	OEPA	CAA, Title I, Sections 160–169 (42 USC 7470–7479); OAC 3745-35-02	UDS has determined that the PSD, nonattainment area, and NSPS programs do not apply to the DUF <sub>6</sub> conversion facility. Nevertheless, the facility is subject to 40 CFR Part 61, Subpart H, “National Emission Standards for Emissions of Radionuclides Other Than Radon from Department of Energy Facilities” (NESHAPs). Therefore, UDS believes the State Permit to Operate program would apply. UDS will submit a timely application for an Ohio Permit to Operate.
<b>Risk Management Plan (RMP):</b> Required for any stationary source that has a regulated substance (e.g., hydrogen fluoride, anhydrous ammonia, ammonia, nitric acid) in any process (including storage) in a quantity that is over the threshold level.	EPA; OEPA	CAA, Title 1, Section 112(r)(7) (42 USC 7412); 40 CFR Part 68; OAC 3745-104	UDS has determined that certain regulated substances would be stored at the DUF <sub>6</sub> conversion facility in quantities that potentially exceed the threshold levels. Accordingly, an RMP may be required. UDS will verify this with the OEPA and, if necessary, prepare an RMP.
<b>CAA Conformity Determination:</b> Required for each criteria pollutant (i.e., sulfur dioxide, particulate matter, carbon monoxide, ozone, nitrogen dioxide, and lead) where the total of direct and indirect emissions in a nonattainment or maintenance area caused by a federal action would equal or exceed threshold rates.	DOE; OEPA; Tennessee Department of Environment and Conservation (TDEC)	CAA, Title 1, Section 176(c) (42 USC 7506); 40 CFR 93; OAC 3745-102; TDEC Regulations 1200-3-34-.02	Pike County, Ohio, and Roane County, Tennessee, have both been designated as “Cannot be Classified or Better Than Standard” for all criteria pollutants. Because these counties are in attainment with National Ambient Air Quality Standards for all criteria pollutants and contain no maintenance areas, no CAA conformity determination is required for any criteria pollutant that would be emitted as a result of the proposed federal action.

TABLE 6.1 (Cont.)

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<b>Water Resources Protection</b>			
<p><b>National Pollutant Discharge Elimination System (NPDES) Permit – Construction Site Storm Water:</b> Required before making point source discharges into waters of the state of storm water from a construction project that disturbs more than 5 acres (2 ha) of land.</p>	OEPA	Clean Water Act (CWA) (33 USC 1251 et seq.); 40 CFR Part 122; OAC-3745-33-02, 3745-38-02, and 3745-38-06	UDS has determined that construction of the DUF <sub>6</sub> conversion facility and new cylinder storage yard would require an NPDES Permit for construction site storm water discharges. A general NPDES Permit for Storm Water Discharges in Ohio (OEPA Permit No. OHR100000 and proposed renewal OHC000002), which covers storm water discharges during construction, including storm water discharges from an on-site concrete batch plant if one is installed, is expected to satisfy this requirement. Accordingly, UDS will submit a Notice of Intent (NOI) to discharge under the General NPDES Permit and, if requested, a Storm Water Pollution Prevention Plan (SWPP) to the OEPA at the appropriate time.
<p><b>National Pollutant Discharge Elimination System (NPDES) Permit – Industrial Facility Storm Water:</b> Required before making point source discharges into waters of the state of storm water from an industrial site.</p>	OEPA	CWA (33 USC 1251 et seq.); 40 CFR Part 122; OAC-3745-33-02, 3745-38-02, and 3745-38-06	UDS has determined that storm water would be discharged from the DUF <sub>6</sub> conversion facility site during operations. Therefore, an NPDES Permit for industrial facility storm water discharge may be required, unless arrangements can be made to discharge such storm water through existing outfalls covered by an NPDES Permit already held by United States Enrichment Corporation (USEC) for the Portsmouth site. UDS plans to consult with USEC concerning discharges of storm water during operations through existing outfalls. If this cannot be arranged, a General NPDES Permit for Storm Water Discharges Associated with Industrial Activity (NPDES Permit No. OHR000003) may apply. Thus, if storm water cannot be discharged through existing USEC outfalls, UDS plans to consult with the OEPA about the applicability of the General NPDES Permit, and if it applies, submit a NOI to the OEPA at the appropriate time. Otherwise, UDS will submit an application for an individual NPDES permit at the appropriate time.

TABLE 6.1 (Cont.)

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<i>Water Resources Protection (Cont.)</i>			
<b>National Pollutant Discharge Elimination System (NPDES) Permit – Process Water Discharge:</b> Required before making point source discharges into waters of the state of industrial process wastewater.	OEPA	CWA (33 USC 1251 et seq.); 40 CFR Part 122; OAC-3745-33-02, 3745-38-02, and 3745-38-06	UDS is studying options for management of process water/blowdown discharges. The need for an NPDES permit for such discharges will be determined based on the outcome of the study. If it is determined that an NPDES permit is required, UDS will apply for the permit at the appropriate time.
<b>Ohio Surface Water Permit to Install:</b> Required before constructing sewers or pump stations.	OEPA	OAC-3745-31-02	UDS has determined that a Surface Water Permit to Install would be required before construction of sewer lines and pump stations at the DUF <sub>6</sub> conversion facility site. Accordingly, UDS plans to submit an application to the OEPA at the appropriate time.
<b>Ohio Surface Water Permit to Install:</b> Required before constructing any wastewater treatment or collection system or disposal facility.	OEPA	OAC-3745-31-02	If it is determined that the DUF <sub>6</sub> conversion facility would have an on-site wastewater treatment facility, UDS plans to submit an application for a Surface Water Permit to Install at the appropriate time.
<b>CWA Section 404 (Dredge and Fill) Permit:</b> Required to place dredged or fill material into waters of the United States, including areas designated as wetlands, unless such placement is exempt or authorized by a nationwide permit or a regional permit; a notice must be filed if a nationwide or regional permit applies.	U.S. Army Corps of Engineers (USACE)	CWA (33 USC 1251 et seq.); 33 CFR Parts 323 and 330	UDS believes that construction of the DUF <sub>6</sub> conversion facility would not result in dredging or placement of fill material into wetlands within the jurisdiction of the USACE. However, construction of a storm water discharge outfall requiring dredging in waters of the United States may be necessary. If construction activities are subject to the CWA Section 404 Permit program, they may be covered under a USACE Nationwide CWA Section 404 Permit (i.e., No. 14 [Linear Transportation Projects], 18 [Minor Discharges], or 19 [Minor Dredging]). Accordingly, UDS plans to consult with the USACE concerning the project and, if appropriate, submit either a preconstruction notification about activities covered by a nationwide permit or an application for an individual Section 404 Permit.

**TABLE 6.1 (Cont.)**

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<i>Water Resources Protection (Cont.)</i>			
<b>Ohio General Permit for Filling Category 1 and Category 2 Isolated Wetlands:</b> Required where the proposed project involves the filling or discharge of dredged material into Category 1 and Category 2 isolated wetlands, causing impacts that total 0.5 acre (0.20 ha) or less.	OEPA	<i>Ohio Revised Code</i> (ORC) Sections 6111.021–6111.029	UDS believes that construction of the DUF <sub>6</sub> conversion facility would not result in dredging or placement of fill material into wetlands within the jurisdiction of the OEPA isolated wetlands program. Accordingly, UDS plans to consult with the OEPA concerning the project and, only if appropriate, submit to the OEPA a Pre-Activity Notice of activities covered under the General Permit for Filling Isolated Wetlands.
<b>Ohio Individual Isolated Wetland Permit:</b> Required where the proposed project involves the filling or discharge of dredged material into Category 1 and Category 2 isolated wetlands, causing impacts that total greater than 0.5 acre (0.20 ha) for Category 1 isolated wetlands and/or greater than 0.5 acre (0.20 ha) but not exceeding 3 acres (1.21 ha) for Category 2 isolated wetlands.	OEPA	ORC Sections 6111.021–6111.029	UDS believes that construction of the DUF <sub>6</sub> conversion facility would not result in dredging or placement of fill material into wetlands within the jurisdiction of the OEPA isolated wetlands program. Accordingly, UDS plans to consult with the OEPA concerning the project and, only if appropriate, submit to the OEPA an application for an Individual Isolated Wetland Permit.
<b>Spill Prevention Control and Countermeasures (SPCC) Plan:</b> Required for any facility that could discharge oil in harmful quantities into navigable waters or onto adjoining shorelines.	EPA	CWA (33 USC 1251 et seq.); 40 CFR Part 112	If it is determined that a SPCC plan would be required, UDS will submit the plan to the EPA and the OEPA at the appropriate time.
<b>CWA Section 401 Water Quality Certification:</b> Required to be submitted to the agency responsible for issuing any federal license or permit to conduct an activity that may result in a discharge of pollutants into waters of a state.	OEPA	CWA, Section 401 (33 USC 1341); ORC Chapters 119 and 6111; OAC Chapters 3745-1, 3745-32, and 3745-47	UDS would be required to obtain a CWA Section 401 Water Quality Certification if construction or operation of the DUF <sub>6</sub> conversion facility or new cylinder storage yard requires a federal license or permit. If UDS determines that a federal license or permit is required (e.g., a CWA Section 404 Permit), a CWA Section 401 Water Quality Certification will be requested from the OEPA at the appropriate time.

TABLE 6.1 (Cont.)

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<b>Waste Management and Pollution Prevention</b>			
<b>Submit Determination Results:</b> Required when a person who generates waste in the State of Ohio or a person who generates waste outside the state that is managed inside the state determines that the waste he/she generates is hazardous waste.	OEPA	OAC 3745-52-11	At the appropriate time, UDS will submit to the OEPA the results of its determination that any waste generated at the DUF <sub>6</sub> conversion facility is a hazardous waste.
<b>Registration and Hazardous Waste Generator Identification Number:</b> Required before a person who generates over 220 lb (100 kg) per calendar month of hazardous waste ships the hazardous waste off site.	EPA; OEPA	Resource Conservation and Recovery Act (RCRA), as amended (42 USC 6901 et seq.), Subtitle C; OAC 3745-52-12	At the appropriate time, UDS plans to apply to the OEPA for an EPA Hazardous Waste Generator Identification Number.
<b>Hazardous Waste Treatment, Storage, or Disposal Facility Permit:</b> Required if hazardous or mixed waste will undergo nonexempt treatment by the generator, be stored on site for longer than 90 days by the generator of 2,205 lb (1,000 kg) or more of hazardous waste per month, be stored on site for longer than 180 days by the generator of between 220 and 2,205 lb (100 and 1,000 kg) of hazardous waste per month, disposed of on site, or be received from off site for treatment or disposal.	EPA; OEPA	RCRA, as amended (42 USC 6901 et seq.), Subtitle C; OAC 3745-50-40	Hazardous waste would not be disposed of on site at the DUF <sub>6</sub> conversion facility. Also, UDS does not plan to store any hazardous wastes that are generated on site for more than 90 days. Accordingly, UDS believes that no Hazardous Waste Treatment, Storage, or Disposal Facility Permit would be required.
<b>Industrial Solid Waste Landfill Permit to Install:</b> Required before constructing or expanding a solid waste landfill facility in Ohio.	OEPA	OAC 3745-29-06	Industrial solid waste would not be disposed of on site at the DUF <sub>6</sub> conversion facility. Therefore, no Industrial Solid Waste Landfill Permit to Install would be required.

TABLE 6.1 (Cont.)

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<b>Waste Management and Pollution Prevention (Cont.)</b>			
<b>Construction and Demolition Debris Facility License:</b> Required before establishing, modifying, operating, or maintaining a facility to dispose of debris from the alteration, construction, destruction, or repair of a man-made physical structure; however, the debris to be disposed of must not qualify as solid or hazardous waste; also, no license is required if debris from site clearing is used as fill material on the same site.	OEPA or the authorized local board of health	OAC 3745-37-01	Construction debris would not be disposed of on site at the DUF <sub>6</sub> conversion facility. Therefore, no Construction and Demolition Debris Facility License would be required.
<b>Low-Level Radioactive Waste Generator Report:</b> Required within 60 days of commencing the generation of low-level waste in Ohio.	Ohio Department of Health	OAC 3701:1-54-02	UDS will file a Low-Level Radioactive Waste Generator Report with the Ohio Department of Health at the appropriate time.
<b>Underground Storage Tank (UST) Installation Permit:</b> Required before beginning installation of a UST system (i.e., a tank and/or piping of which 10% or more of the volume is underground and that contains petroleum products or substances defined as hazardous by the Comprehensive Environmental Response, Compensation, and Liability Act [CERCLA], except those hazardous substances that are also defined as hazardous waste by the RCRA).	Ohio Department of Commerce, Ohio Bureau of Underground Storage Tank Regulations (BUSTR)	OAC 1301:7-9-06(D)	No UST systems would be installed at the DUF <sub>6</sub> conversion facility. Therefore, no UST Installation Permit would be required.
<b>New UST System Registration:</b> Required within 30 days of bringing a new UST system into service.	EPA; Ohio BUSTR	RCRA, as amended, Subtitle I (42 USC 6991a-6991i); 40 CFR 280.22; OAC 1301:7-9-04	No UST systems would be installed at the DUF <sub>6</sub> conversion facility. Therefore, no New UST System Registration would be required.
<b>Notification of PCB Waste Activity</b>	EPA	Toxic Substances Control Act (TSCA), as amended (15 USC 2601 et seq.); 40 CFR Part 761	UDS would be required to notify EPA of PCB waste activities at the time that DUF <sub>6</sub> cylinders to which paints containing PCBs have been applied are designated for disposal, either alone or as containers for depleted uranium oxide. At the appropriate time, UDS will notify the EPA by filing the required form.

**TABLE 6.1 (Cont.)**

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<i>Emergency Planning and Response</i>			
<b>List of Material Safety Data Sheets:</b> Submission of a list of Material Safety Data Sheets is required for hazardous chemicals (as defined in 29 CFR Part 1910) that are stored on site in excess of their threshold quantities.	Local Emergency Planning Commission (LEPC); Ohio State Emergency Response Commission (SERC)	Emergency Planning and Community Right-to-Know Act of 1986 (EPCRA), Section 311 (42 USC 11021); 40 CFR 370.20; OAC 3750-30-15	UDS will prepare and submit a List of Material Safety Data Sheets at the appropriate time.
<b>Annual Hazardous Chemical Inventory Report:</b> Submission of the report is required when hazardous chemicals have been stored at a facility during the preceding year in amounts that exceed threshold quantities.	LEPC; Ohio SERC; local fire department	EPCRA, Section 312 (42 USC 11022); 40 CFR 370.25; OAC 3750-30-01	UDS will cooperate with other DOE tenants at the Portsmouth GDP site regarding submission of a site-wide Annual Hazardous Chemical Inventory Report each year. For the purpose of preparing the site-wide report, the total quantities of hazardous chemicals stored by all tenants at the Portsmouth GDP site, including those stored at the depleted UF <sub>6</sub> conversion facility, will be considered.
<b>Notification of On-Site Storage of an Extremely Hazardous Substance:</b> Submission of the notification is required within 60 days after on-site storage begins of an extremely hazardous substance in a quantity greater than the threshold planning quantity.	Ohio SERC	EPCRA, Section 304 (42 USC 11004); 40 CFR 355.30; OAC 3750-20-05	UDS will prepare and submit the Notification of On-Site Storage of an Extremely Hazardous Substance at the appropriate time, if such substances are determined to be stored in a quantity greater than the threshold planning quantity at the DUF <sub>6</sub> conversion facility.

**TABLE 6.1 (Cont.)**

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<b>Transportation of Radioactive Wastes and Conversion Products</b>			
<b>Certificate of Registration:</b> Required to authorize the registrant to transport hazardous material or cause a hazardous material to be transported or shipped.	U.S. Department of Transportation (DOT)	Hazardous Materials Transportation Act (HMTA), as amended by the Hazardous Materials Transportation Uniform Safety Act of 1990 and other acts (49 USC 1501 et seq.); 49 CFR 107.608(b)	UDS will obtain a Certificate of Registration at the appropriate time.
<b>Packaging, Labeling, and Routing Requirements for Radioactive Materials:</b> Required for packages containing radioactive materials that will be shipped by truck or rail.	DOT	HMTA (49 USC 1501 et seq.); Atomic Energy Act (AEA), as amended (42 USC 2011 et seq.); 49 CFR Parts 172, 173, 174, 177, and 397	When shipments of radioactive materials are made, UDS will comply with DOT packaging, labeling, and routing requirements.
<b>Biotic Resources</b>			
<b>Threatened and Endangered Species Consultation:</b> Required between the responsible federal agencies and affected states to ensure that the project is not likely to (1) jeopardize the continued existence of any species listed at the federal or state level as endangered or threatened or (2) result in destruction of critical habitat of such species.	U.S. Department of Energy (DOE); U.S. Fish and Wildlife Service; Ohio Department of Natural Resources	Endangered Species Act of 1973, as amended (16 USC 1531 et seq.); ORC 1531.25–26 and 1531.99	Neither a species listed at the federal or state level as endangered or threatened, nor the critical habitat of such a species, has been identified that would be affected by construction or operation of the DUF <sub>6</sub> conversion facility or new cylinder storage yard.

TABLE 6.1 (Cont.)

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<i>Nuclear Facility Operations</i>			
<b>Approval to Start Up a Nuclear Facility:</b> Required before start-up of new nuclear facilities, which are activities or operations that involve radioactive and/or fissionable materials in such form or quantity that a nuclear hazard potentially exists to the employees or the general public.	DOE	AEA, as amended (42 USC 2011 et seq.); DOE Order 425.1B	UDS will obtain approval from DOE to start up the DUF <sub>6</sub> conversion facility at the appropriate time.
<b>Approval to Release Materials Containing Residual Radioactive Contamination:</b> Required before releasing (1) nonuranium products from the DUF <sub>6</sub> conversion process (such as hydrogen fluoride [HF] or calcium fluoride [CaF <sub>2</sub> ]) for unregulated use and (2) decontaminated DUF <sub>6</sub> cylinders for unregulated use as scrap metal.	DOE	AEA, as amended (42 USC 2011 et seq.); DOE Order 5400.5	UDS will obtain approval from DOE before releasing HF, CaF <sub>2</sub> , or decontaminated cylinders for unregulated use.
<i>Cultural Resources</i>			
<b>Archaeological and Historical Resources Consultation:</b> Required before a federal agency approves a project in an area where archaeological or historic resources might be located.	DOE; Advisory Council on Historic Preservation; Ohio State Historic Preservation Officer (SHPO)	National Historic Preservation Act of 1966, as amended (16 USC 470 et seq.); Archaeological and Historical Preservation Act of 1974 (16 USC 469-469c-2); Antiquities Act of 1906 (16 USC 431 et seq.); Archaeological Resources Protection Act of 1979, as amended (16 USC 470aa-mm)	DOE has coordinated with the Advisory Council on Historic Preservation and the Ohio SHPO regarding previous archeological and architectural surveys at the Portsmouth Gaseous Diffusion Plant site. Discussion of the results of such surveys is ongoing.

**TABLE 6.1 (Cont.)**

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<i>Cultural Resources (Cont.)</i>			
<b>Government-to-Government Tribal Consultation:</b> Required to ensure that project activities have been designed to protect access to, physical integrity of, and confidentiality of traditional cultural and religious sites.	DOE	American Indian Religious Freedom Act of 1978 (42 USC 1996 and 1996a); Native American Graves Protection and Repatriation Act of 1990 (25 USC 3001 et seq.); National Historic Preservation Act of 1966, as amended (16 USC 470F); 36 CFR Part 800, Subpart B; 43 CFR Part 10	DOE has initiated government-to-government consultations with Native American tribes in the area of the DUF <sub>6</sub> conversion facility. No religious or sacred sites, burial sites, or resources significant to Native Americans have been identified to date.
<i>Other</i>			
<b>Environmental Impact Statement (EIS):</b> Required to evaluate the potential environmental impacts of a proposed major federal action that may significantly affect the quality of the human environment and to consider alternatives to the proposed action.	DOE	National Environmental Policy Act of 1969, as amended (NEPA) (42 USC 4321 et seq.); 40 CFR Parts 1500–1508; 10 CFR Part 1021	The requirements of NEPA are satisfied by publication of this EIS for the DUF <sub>6</sub> conversion facility and cylinder management area.
<b>Annual Toxic Release Inventory (TRI) Report:</b> Required for facilities that have 10 or more full-time employees and are assigned certain Standard Industrial Classification (SIC) codes.	EPA; OEPA	EPCRA, Section 313 (42 USC 11023); 40 CFR Part 372; OAC 3745-100-07	UDS will prepare and submit a TRI Report to the EPA each year.

TABLE 6.1 (Cont.)

License, Permit, or Other Consent	Responsible Agency	Authority	Relevance and Status
<i>Other (Cont.)</i>			
<b>OEPA Director's Final Findings and Orders (issued February 24, 1998):</b> Establishes requirements for management, surveillance, testing, and maintenance associated with the DUF <sub>6</sub> storage yards and cylinders owned by DOE at the Portsmouth site.	DOE; OEPA	ORC 3734 and 3745	UDS will implement the requirements of the OEPA Director's Final Findings and Orders, including preparation and submission to the OEPA of an annual report outlining DOE's good faith efforts to evaluate potential use or reuse of DUF <sub>6</sub> .
<b>Tennessee Department of Environment and Conservation Consent Order (issued February 2, 1999):</b> Establishes requirements for management, surveillance, testing, maintenance, and disposition of the UF <sub>6</sub> cylinders at the East Tennessee Technology Park.	DOE; Tennessee Department of Environment and Conservation (TDEC)		UDS will implement the requirements of the TDEC Consent Order.

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## 8 LIST OF PREPARERS

Name	Education/Expertise	Contribution
<b><i>U.S. Department of Energy</i></b>		
Gary S. Hartman	B.A., Geology; 23 years of experience in NEPA compliance and environmental compliance and regulation	DOE Document Manager
<b><i>Argonne National Laboratory</i></b> <sup>1</sup>		
Timothy Allison	M.S., Mineral and Energy Resource Economics; M.A., Geography; 16 years of experience in regional analysis and economic impact analysis	Socioeconomic analysis
Halil I. Avci	Ph.D., Nuclear Engineering; 19 years of experience in environmental assessment, waste management, accident analysis, and project management	Project Leader
Bruce M. Biwer	Ph.D., Chemistry; 13 years of experience in radiological pathway analysis, dose calculations, and radiological transportation risk analysis	Radiological transportation risk analysis
James P. Butler	Ph.D., Environmental Health Sciences; 22 years of experience in health risk assessment and exposure analysis	Chemical human health impacts — normal operations
Young-Soo Chang	Ph.D., Chemical Engineering; 17 years of experience in air quality impact analysis	Air quality, noise
Jing-Jy Cheng	Ph.D., Polymer Science and Engineering; 13 years of experience in radiological risk assessment and computer model development	Radiological impacts — normal operations
Stephen M. Folga	Ph.D., Gas Engineering; 9 years of experience in technology assessment and waste management	Technology assessment, accident assessment, resources/materials

<sup>1</sup> The contractor disclosure statement appears in Appendix H.

Name	Education/Expertise	Contribution
John R. Gasper	M.S., M.P.H., Environmental Health Science; 28 years of experience in environmental and energy assessment and program management	Program Coordinator/Liaison
Jerry L. Gillette	M.S., Nuclear Engineering; 34 years of experience in energy and environmental technologies and accident analysis	Technology assessment, accident analysis
Larry J. Gorenflo	Ph.D., Geography, M.A., Anthropology; 18 years of experience in environmental impact assessment and anthropological and geographical research	Land use, environmental justice, cumulative impacts
Heidi M. Hartmann	M.S., Environmental Toxicology and Epidemiology; 15 years of experience in exposure and risk analysis and public health assessment	Assistant Project Leader/Technical Coordinator; chemical human health impacts, cylinder management
Patricia Hollopeter	A.M., Philosophy; 22 years of experience in editing and writing	Technical Editor
Michael Lazaro	M.S., Environmental Science (Atmospheric Physics), M.S., Nuclear Engineering; 30 years of experience in atmospheric modeling, environmental engineering, policy analysis, and environmental assessment	Chemical accidents
David J. LePoire	M.S., Computer Science, B.S., Physics; 13 years of experience in computer models development for radiological human health risk assessments	Radiological accidents
Frederick A. Monette	M.S., Health Physics; 13 years of experience in radiological risk assessment, environmental impact assessment, and document management	Assistant Project Leader/ Document Manager
Marita Moniger	B.A., English; 24 years of experience in editing and writing	Technical Editor
Dan O'Rourke	M.S., Industrial Archaeology; 11 years of experience in cultural resource management; 6 years of experience in historical property issues	Cultural resources

Name	Education/Expertise	Contribution
Mary H. Picel	M.S., Environmental Health Sciences; 17 years of experience in environmental assessment, risk assessment, and waste management	Waste management
Nancy L. Ranek	J.D., M.S., Nuclear Engineering, B.S., Physics; 19 years of experience in environmental permitting, management, and assessment	Environmental, occupational safety, and health permits and compliance requirements
Elisabeth A. Stull	Ph.D., Ecology; 34 years of experience in ecological research and environmental assessment	Cumulative impacts, affected environment, summary
David Tomasko	Ph.D., Civil Engineering; 24 years of experience in hydrogeology and fluid mechanics	Water and soil
Robert A. VanLonkhuyzen	B.A., Biology; 13 years of experience in ecological research and environmental assessment	Ecological resources
Bruce T. Verhaaren	Ph.D., Archaeology; 16 years of experience in archaeological analysis; 13 years of experience in environmental assessments and records management	Cultural resources, references
Konnie L. Wescott	B.A., Mathematics and Sociology/Anthropology, M.A., Anthropology; 15 years of experience in archaeological research; 13 years of experience in environmental assessment	Cultural resources

## 9 GLOSSARY

**Accident:** An unplanned sequence of events resulting in undesirable consequences, such as the release of radioactive or hazardous material to the environment.

**Accident consequence assessment:** An assessment of the impacts following the occurrence of an accident, independent of the probability of that accident. The environmental impact statement (EIS) provides estimates of the consequences of a number of possible accidents, ranging from those with low probability (rare) to those with relatively high probability (frequent).

**Accident frequency:** The likelihood that a specific accident will occur, that is, the probability of occurrence. If an accident is estimated to happen once every 50 years, the accident frequency is generally reported as 0.02 per year (1 occurrence divided by 50 years = 0.02 occurrence per year). For the EIS, accident frequencies were grouped as follows:

- I, likely (L) — The average frequency of occurrence is estimated to be greater than or equal to 1 in 100 years.
- II, unlikely (U) — The average frequency of occurrence is estimated to be 1 in 100 to 1 in 10,000 years.
- III, extremely unlikely (EU) — The average frequency of occurrence is estimated to be 1 in 10,000 to 1 in 1 million years.
- IV, incredible (I) — The average frequency of occurrence is estimated to be less than 1 in 1 million years.

**Accident risk:** Risk based on both the severity of an accident (consequence) and the probability that the accident will occur. High-consequence accidents that are unlikely to occur (low probability) may pose a low overall risk. For purposes of comparison, accident risk is typically calculated by multiplying the accident consequence (e.g., dose or expected fatalities) by the accident probability.

**Accident risk assessment:** An assessment that considers the probabilities and consequences of a range of possible accidents, including low-probability accidents that have high consequences and high-probability accidents that have low consequences. The overall risk associated with an accident is generally estimated by multiplying the accident consequence by the probability of occurrence.

**Accident source term:** The amount of radioactive or hazardous material released to the environment in dispersible form following an accident.

**Adsorption:** Process in which solid surfaces attract and retain a layer of ions from a solution.

**Advection:** The process by which material is transported by the bulk motion of flowing gas or liquid.

**Air quality:** Measure of the health-related and visual characteristics of the air, often derived from quantitative measurements of the concentrations of specific injurious or contaminating substances. Air quality standards are the prescribed level of constituents in the outside air that cannot be exceeded during a specific time in a specified area.

***Air Quality Control Region (AQCR):*** An interstate or intrastate area designated by the U.S. Environmental Protection Agency (EPA) for the attainment and maintenance of National Ambient Air Quality Standards (NAAQS).

***Alpha particle (α):*** A positively charged particle consisting of two protons and two neutrons that is emitted during radioactive decay from the nucleus of certain nuclides. It is the least penetrating of the three common types of radiation (alpha, beta, and gamma).

***Ambient air:*** The surrounding atmosphere as it exists around people, plants, and structures.

***American Indian Religious Freedom Act of 1978:*** The Act that established national policy to protect and preserve for Native Americans their inherent right of freedom to believe, express, and exercise their traditional religions, including the rights of access to religious sites, use and possession of sacred objects, and freedom to worship through traditional ceremonies and rites.

***Aquifer:*** A saturated subsurface geologic formation that can transmit significant quantities of water.

***Archaeological and Historic Preservation Act:*** Act directed at the preservation of historic and archaeological data that would otherwise be lost as a result of federal construction. It authorizes the U.S. Department of the Interior to undertake recovery, protection, and preservation of archaeological and historic data.

***As low as reasonably achievable (ALARA):*** An approach to control or manage radiation exposures (both individual and collective to the workforce and the public) and releases of radioactive material to the environment as low as social, technical, economic, practical,

and public policy considerations permit. ALARA is not a dose limit; it is a practice that has as its objective the attainment of dose levels as far below applicable limits as possible.

***Atomic Energy Act of 1954 (AEA):*** The Act that, along with other related legislation, provided the Atomic Energy Commission (a predecessor of the U.S. Department of Energy) with authority to develop generally applicable standards for protecting the environment from radioactive materials.

***Attainment area:*** An area considered to have air quality as good as or better than the National Ambient Air Quality standards as defined in the Clean Air Act (CAA). An area may be an attainment area for one pollutant and a nonattainment area for others (see also *nonattainment area*).

***Bald and Golden Eagle Protection Act, as amended:*** The Act making it unlawful to take, pursue, molest, or disturb bald (American) and golden eagles, their nests, or their eggs anywhere in the United States.

***Beta particle (β):*** An elementary particle emitted from a nucleus during radioactive decay; it is negatively or positively charged, identical in mass to an electron, and in most cases easily stopped, as by a thin sheet of metal or plastic.

***Biota:*** The plant and animal life of a region.

***Bounding:*** In the case of accident analysis, bounding is a condition, consequence, or risk that provides an upper limit that is not exceeded by other conditions, consequences, or risks. This term is also used to identify conservative assumptions that will likely overestimate actual risks or consequences.

**Breach:** A general term referring to a hole in a cylinder or container. A breach may be caused by corrosion or by mechanical forces, such as those caused by a drop or contact with handling equipment.

**Cancer:** A group of diseases characterized by uncontrolled cellular growth. Increased incidence of cancer can be caused by exposure to radiation.

**Candidate species:** Plant or animal species that are not yet officially listed as threatened or endangered but are undergoing status review by the U.S. Fish and Wildlife Service (USFWS). These species are candidates for possible addition to the list of threatened and endangered species.

**Carbon monoxide (CO):** A colorless, odorless gas that is toxic if breathed in high concentration over a period of time. Carbon monoxide is one of six criteria air pollutants specified under Title I of the CAA.

**Cascade:** The process system that is used to separate the isotopic streams of uranium-235 and uranium-238 in gaseous diffusion plants.

**Cask:** A heavily shielded, typically robust container for shipping or storing spent nuclear fuel. Spent nuclear fuel casks are usually cylindrical containers with radiation shielding provided by steel, lead, concrete, or depleted uranium.

**Census tract:** An area usually containing between 2,500 and 8,000 persons that is used for organizing and monitoring census data. The geographic dimensions of census tracts vary widely, depending on population settlement density. Census tracts do not cross county borders.

**Clean Air Act (CAA):** The Act that mandates the issuance and enforcement of air pollution

control standards for stationary sources and motor vehicles.

**Clean Air Act Amendments of 1990:** An Act that expanded the enforcement powers of the EPA and added restrictions on air toxins, ozone-depleting chemicals, stationary and mobile emissions sources, and emissions implicated in acid rain and global warming.

**Clean Water Act of 1972, 1987:** The Act that regulates the discharge of pollutants from a point source into navigable waters of the United States in compliance with a National Pollution Discharge Elimination System permit. Also regulates discharges to or dredging of wetlands.

**Code of Federal Regulations (CFR):** The codified form in which all federal regulations in force are published.

**Collective dose:** Summation of individual radiation doses received by all those exposed to the source or event being considered. The collective radiation dose received by a population group is usually measured in units of person-rem.

**Collective population risk:** A measure of possible loss in a group of people that takes into account the probability that the hazard will cause harm and the consequences of that event. The collective population risk does not express the risk to specific individual members of the population.

**Committed effective dose equivalent:** The sum of the committed dose equivalents to various tissues of the body, each multiplied by its weighting factor. It does not include contributions from external doses. Committed effective dose equivalent is expressed in units of rem and provides an estimate of the lifetime radiation dose to an individual from

radioactive material taken into the body through either inhalation or ingestion.

**Convection:** Process by which heat is transferred between a surface and a moving fluid when they are at different temperatures.

**Criteria pollutants:** Six air pollutants for which national ambient air quality standards are established by the EPA under Title I of the CAA. The six pollutants are sulfur dioxide (SO<sub>2</sub>), nitrogen oxides (NO<sub>x</sub>), carbon monoxide (CO), ozone (O<sub>3</sub>), particulate matter (PM<sub>10</sub>, particles with a mean diameter of 10 micrometers [ $\mu\text{m}$ ] or less), and lead (Pb).

**Critical habitat:** Air, land, or water area and constituent elements, the loss of which would appreciably decrease the likelihood of survival and recovery of a species listed as threatened or endangered or a distinct segment of the population of that species.

**Cultural resources:** Archaeological sites, architectural structures or features, traditional use areas, and Native American sacred sites or special use areas.

**Cumulative impacts:** The impacts assessed in an environmental impact statement that could potentially result from the incremental impact of the action when added to other past, present, and reasonably foreseeable future actions regardless of what agency (federal or nonfederal), private industry, or individual undertakes such other actions. Cumulative impacts can result from individually minor but collectively significant actions taking place over a period of time.

**Curie (Ci):** A measure of the radioactivity of a material, equal to  $3.7 \times 10^{10}$  disintegrations per second.

**Cylinder:** As defined for this EIS, a large steel container used to store depleted uranium hexafluoride (DUF<sub>6</sub>). Cylinders are typically about 12 ft long by 4 ft in diameter and weigh about 9 to 13 t (10 to 14 tons) when full of DUF<sub>6</sub>.

**Cylinder preparation:** The activities required to prepare DUF<sub>6</sub> cylinders for transportation. Cylinder preparation would be required if cylinders were transported to a conversion facility.

**Decay:** see also *radioactive decay*.

**Decay products:** see also *radioactive decay products*.

**Decommissioning:** The process of removing a facility from operation, followed by decontamination, entombment, dismantlement, or conversion to another use.

**Defluorination:** The conversion of uranium hexafluoride to triuranium octaoxide (U<sub>3</sub>O<sub>8</sub> [uranyl uranate]) accomplished by using steam. UF<sub>6</sub> is chemically decomposed with steam and heat to produce U<sub>3</sub>O<sub>8</sub> and HF, with concentrated HF as the direct by-product.

**Depleted uranium hexafluoride (DUF<sub>6</sub>):** A compound of uranium and fluorine from which most of the uranium-235 isotope has been removed. Isotope separation results in two product “streams.” The stream containing the additional uranium-235 is said to be “enriched” and is collected for further processing into other forms of enriched uranium. The remaining UF<sub>6</sub> stream is said to be “depleted” and is now stored at the Paducah, Portsmouth, and ETTP sites.

**Disposal:** The emplacement of material in a manner designed to ensure isolation for the foreseeable future. Disposal is considered to

be permanent, with no intent to retrieve the material for future use.

***Disposal facility:*** A facility or part of a facility into which hazardous, radioactive, or solid waste is intentionally placed and at which waste is intended to permanently remain after closure of the facility.

***Disproportionately high and adverse environmental impact:*** An adverse environmental impact determined to be unacceptable or above generally accepted norms. A disproportionately high impact refers to an environmental hazard with a risk or rate of exposure for a low-income or minority population that exceeds the risk or rate of exposure for the general population.

***Disproportionately high and adverse human health effect:*** Any effect on human health from exposure to environmental hazards that exceeds generally accepted levels of risk and affects low-income and minority populations at a rate that appreciably exceeds the rate for the general population. Adverse health effects are measured in risks and rates that could result in latent cancer fatalities, as well as other fatal or nonfatal adverse impacts to human health.

***Dose:*** The amount of energy deposited in body tissue due to radiation exposure. Various technical terms — such as dose equivalent, effective dose equivalent, and collective dose — are used to evaluate the amount of radiation received by an exposed individual or population.

***Dose rate:*** Radiation dose delivered per unit of time and measured in rem per hour.

***Drain:*** A device (e.g., a channel or pipe) used to carry away or to empty liquid from a liquid source.

***Effective dose equivalent:*** The sum of the products of the dose equivalent to various organs or tissues and the weighting factors applicable to each of the body organs or tissues that are irradiated. The effective dose equivalent includes the dose from radiation sources internal and/or external to the body and is expressed in units of rem.

***Emergency Planning and Community Right-to-Know Act of 1986:*** The Act that established programs to provide the public with important information on the hazardous and toxic chemicals in their communities and established emergency planning and notification requirements to protect the public in the event of a release of hazardous substances.

***Emergency Response Planning Guideline (ERPG):*** A hazardous-material personnel exposure level or range which, when exceeded by a short-term or acute exposure, will cause adverse reproductive, developmental, or carcinogenic effects in humans. ERPGs are approved by a committee of the American Industrial Hygiene Association.

***Endangered species:*** Any species that is in danger of extinction throughout all or a significant portion of its geographic range.

***Endangered Species Act, as amended:*** The Act intended to prevent the further decline of endangered and threatened species and to restore these species and their habitats. Consultation with the USFWS is necessary to determine whether endangered and threatened species or their critical habitats are known to be in the vicinity of the proposed action.

***Engineering analysis:*** A comprehensive technical analysis of DUF<sub>6</sub> technology options, including conversion, use, transportation, storage, and disposal.

**Enrichment:** An isotopic separation process that increases the portion of the uranium-235 isotope in relation to uranium-238 in natural uranium. In addition to the enriched uranium, this process also produces uranium depleted in uranium-235. Enrichment is accomplished in the United States through a process called gaseous diffusion.

**Environmental impact statement (EIS):** A document prepared in accordance with the requirements of the National Environmental Policy Act (NEPA).

**Environmental justice:** The fair treatment of people of all races, cultures, incomes, and educational levels with respect to the development, implementation, and enforcement of environmental laws, regulations, and policies. Fair treatment implies that no population of people should be forced to shoulder a disproportionate share of the negative environmental impacts of pollution or environmental hazards as a result of their lack of political or economic strength.

**Evapotranspiration:** Loss of water from the soil by both evaporation and transpiration from plants growing in the soil.

**Exposure:** The condition of being made subject to the action of radiation, chemicals, or physical hazards. Exposure is sometimes used as a generic term to refer to the dose of radiation or chemicals absorbed by an individual or population.

**External exposure:** Exposure to radiation, principally gamma radiation, that originates from sources outside of the body.

**Farmland Protection Policy Act of 1981:** An Act that requires federal agencies to take steps to ensure that federal actions do not contribute to the unnecessary and irreversible conversion

of farmland to nonagricultural uses in cases in which other national interests do not override the importance of protecting the farmland resources.

**Fault:** A fracture in the earth's crust accompanied by displacement of one side of the fracture with respect to the other and in a direction parallel to the fracture.

**Federal Facilities Compliance Act of 1992:** An Act that amended the Resource Conservation and Recovery Act (RCRA) with the objectives of bringing all federal facilities into compliance with applicable federal and state hazardous waste laws, of waiving federal sovereign immunity under those laws, and of allowing the imposition of fines and penalties. The law also requires the U.S. Department of Energy (DOE) to submit an inventory of all its mixed waste and to develop a treatment plan for mixed waste.

**Federal listed species:** see also *threatened*, *endangered*, and *candidate species*.

**Fission:** The splitting of a heavy atomic nucleus into two nuclei of lighter elements, accompanied by the release of energy and generally one or more neutrons. Fission can occur spontaneously or be induced by neutron bombardment.

**Floodplain:** The lowlands adjoining inland and coastal waters and relatively flat areas, including at a minimum that area inundated by a 1% or greater chance flood in any given year. The base floodplain is defined as the 100-year (1%) floodplain. The critical action floodplain is defined as the 500-year (0.2%) floodplain.

**Food chain:** The scheme of feeding relationships between trophic levels that unites the member species of a biological community.

**Fugitive dust:** The dust released from activities associated with construction, manufacturing, or transportation.

**Fugitive emissions:** Uncontrolled emissions to the atmosphere from pumps, valves, flanges, seals, and other process points not vented through a stack. Also includes emissions from area sources such as ponds, lagoons, landfills, and piles of stored material.

**Gamma radiation ( $\gamma$ ):** High-energy, short-wavelength electromagnetic radiation (a packet of energy) emitted from a radioactive nucleus during decay. Gamma radiation frequently accompanies alpha and beta emissions and always accompanies fission. Gamma rays are very penetrating and are best stopped or shielded against by dense materials such as lead or uranium. Gamma rays are similar to X-rays, but are usually more energetic.

**Gaseous diffusion:** The uranium enrichment process first developed in the 1940s as part of the Manhattan Project. In gaseous diffusion, gaseous UF<sub>6</sub> is allowed to flow irreversibly through a membrane or diffusion barrier. With holes just large enough to allow the passage of individual molecules without passage of the bulk gas through the membrane or diffusion barrier, more of the lighter molecules (i.e., those containing uranium-235 atoms) will flow through the barrier than the heavier molecules (i.e., those containing uranium-238 atoms), thus effecting partial separation. Gaseous diffusion results in two streams of UF<sub>6</sub>: one enriched in the uranium-235 isotope and one depleted in the uranium-235 isotope.

**General public:** For purposes of analyses in this EIS, anyone outside the boundary of a site at the time of an accident or during normal facility operations, as well as people

along transportation routes used to ship hazardous chemicals or radioactive materials.

**Glove box:** An airtight box used to work with hazardous material, vented to a closed filtering system, having gloves attached inside the box to protect the worker.

**Greater-than-Class-C waste:** Low-level radioactive waste generated by the commercial sector that exceeds U.S. Nuclear Regulatory Commission (NRC) concentration limits for Class-C low-level waste, as specified in Title 10, Part 61, *Code of Federal Regulations* (10 CFR Part 61).

**Green salt:** see *uranium tetrafluoride*.

**Groundshine:** Gamma radiation emitted from radioactive materials deposited on the ground.

**Groundwater:** Generally, all water contained in the ground; water held below the water table available to freely enter wells.

**Grout:** A cementing or sealing mixture of cement and water to which sand, sawdust, or other fillers (additives — e.g., waste) may be added.

**Grouted waste:** Refers to the solid material obtained by mixing waste material with cement and repackaging it in drums. Grouting is intended to reduce the mobility of the waste material.

**Habitat:** Area where a plant or animal lives.

**Hazard index:** A summation of the hazard quotients for all chemicals to which an individual is exposed. A hazard index value of 1.0 or less than 1.0 indicates that no adverse human health effects (noncancer) are expected to occur.

**Hazard quotient:** A comparison of an estimated chemical intake (dose) with a reference dose level below which adverse health effects are unlikely. The hazard quotient is expressed as the ratio of the estimated intake to the reference dose. The value is used to evaluate the potential for noncancer health effects, such as organ damage, from chemical exposures.

**Hazardous air pollutants:** The 189 chemicals and chemical classes — such as asbestos, beryllium, mercury, benzene, and radionuclides — whose emissions are specially regulated by the CAA.

**Hazardous material:** A material that poses a potential risk to health, safety, and property when transported or handled.

**Hazardous waste:** Under RCRA, a solid waste, or combination of solid waste, which — because of its quantity, concentration, or physical, chemical, or infectious characteristics — may (a) cause or significantly contribute to an increase in mortality or an increase in serious irreversible, or incapacitating reversible, illness or (b) pose a substantial present or potential hazard to human health or the environment when improperly treated, stored, transported, or disposed of, or otherwise managed. Source material (including UF<sub>6</sub>), special nuclear material, and by-product material, as defined by the AEA, are specifically excluded from the definition of solid waste.

**Health risk conversion factors:** Estimates of the expected number of health effects (i.e., cancer cases, cancer fatalities, or genetic effects) caused by exposure to a given amount of radiation. Health risk conversion factors are multiplied by the estimated radiation dose received by a given population (such as workers or members of the public) in order to

estimate the number of health effects expected to occur as a result of the exposure. Health risk conversion factors are derived from data collected from Japanese atomic bomb survivors, historical medical and industrial exposures, and animal experimentation.

**Heels:** Residual amounts of nonvolatile material left in a cylinder following the removal of DUF<sub>6</sub>.

**High-efficiency particulate air (HEPA) filter:** A filter with an efficiency of at least 99.95% used to separate particles from air exhaust streams prior to releasing that air into the atmosphere.

**Hydrocarbons:** Chemical compounds containing carbon and hydrogen as the principal elements.

**Hydrogen fluoride (HF):** A colorless, toxic, fuming, corrosive liquid or gas miscible with cold water and very soluble in hot water. HF is produced when UF<sub>6</sub> comes in contact with water, such as humidity in the air, and is often a by-product produced when UF<sub>6</sub> is converted to another chemical form.

**Hygroscopic:** A chemical substance with an affinity for water; one that will absorb moisture, usually from the air.

**Inconel:** A metal alloy containing nickel, chromium, and iron, which exhibits good resistance to corrosion in aqueous environments.

**Internal exposure:** The ingestion or inhalation of radioactive contaminants in air, water, food, or soil, and the subsequent radiation dose to internal organs and tissues of the body.

**Involved worker:** A worker directly involved in the handling or processing of radioactive or hazardous materials.

**Ion:** An atom, molecule, or molecular fragment carrying a positive or negative electrical charge.

**Ionizing radiation:** Radiation that has enough energy to remove electrons from substances that it passes through, forming ions.

**Isotope:** One of two or more species of an element that have the same atomic number but different masses. The difference in mass is due to the presence of one or more extra neutrons in the nucleus. The number of protons for different isotopes of the same element is the same. Uranium-235 and uranium-238 are examples of isotopes of the element uranium.

**Land disposal restrictions:** Restrictions on the disposal of waste that is hazardous under RCRA. The land disposal restrictions include technology-based or performance-based treatment standards that must be met before hazardous waste can be disposed of on land.

**Latent cancer fatality (LCF):** Term used to indicate the estimated number of cancer fatalities that may result from exposure to a cancer-causing element. Latent cancer fatalities are similar to naturally occurring cancers and may be expressed at any time after the initial exposure.

**Lead (Pb):** A toxic metal element with atomic number 82. Overexposure to this metal in air, food, water, and soil can cause damage to the circulatory, digestive, and central nervous systems. Lead is one of six criteria air pollutants specified under Title I of the CAA.

**Long-term storage:** The containment of a material for a period of years, in such a

manner as not to constitute disposal of such material. Long-term storage would preserve access to the material until a future use is identified or until a decision is made to dispose of the material.

**Low-income population:** Persons of low-income status. This status is based on U.S. Bureau of the Census definitions of individuals living below the poverty line, as defined by a statistical threshold that considers family size and income. For 1990, the poverty line threshold for a family unit of four individuals was \$12,674 (based on 1989 income). In this EIS, low-income population was defined as consisting of any census tract located within a 50-mi (80-km) radius of a site that has a proportion of low-income population that is greater than the respective state average.

**Low-level mixed waste (LLMW):** Waste that contains both hazardous waste under RCRA and radioactive material, including source, special nuclear, or by-product material subject to the AEA. Such waste has to be handled, processed, and disposed of in a manner that considers its chemical as well as its radioactive components.

**Low-level radioactive waste (LLW):** Waste that contains radioactivity but is not classified as high-level waste, transuranic waste, spent nuclear fuel, or "11e(2) by-product material" as defined by DOE Order 5820.2A. Low-level waste is typically disposed of by using shallow land burial.

**Low-Level Radioactive Waste Policy Act:** The Act, as amended, that established procedures for the implementation of compacts providing for the establishment and operation of regional disposal facilities for LLW that made the federal government responsible for ultimate disposal of commercially generated waste with a

classification of greater-than-Class-C (see also *greater-than-Class-C waste*).

**Maximally exposed individual (MEI):** A hypothetical individual who — because of proximity, activities, or living habits — could potentially receive the maximum possible dose of radiation or of a hazardous chemical from a given event or process.

**Migratory Bird Treaty Act, as amended:** Act intended to protect birds that have common migration patterns between the United States and Canada, Mexico, Japan, and Russia.

**Millirem:** A unit of radiation exposure equal to one-thousandth of a rem.

**Minority population:** Persons classified by the U.S. Bureau of the Census as Negro/Black/African-American, Hispanic, Asian and Pacific Islander, American Indian, Eskimo, Aleut, or other nonwhite; based on self-classification by individuals according to the race with which they most closely identify. For this EIS, a minority population was defined as any census tract located within a 50-mi (80-km) radius of a site that has a proportion of minority population that is greater than the respective state average.

**Mixed waste:** see also *low-level mixed waste*.

**Model:** A conceptual, mathematical, or physical system obeying certain specified conditions, whose behavior is used to understand the physical system to which it is analogous. Models are often used to predict the behavior or outcome of future events.

**Modified Mercalli Intensity:** A level on the Modified Mercalli scale. A measure of the perceived intensity of earthquake ground-shaking with 12 divisions, from I (not felt by people) to XII (damage nearly total).

**Monel:** Trade name for a white copper-nickel alloy that is acid- and corrosion-resistant.

**National Ambient Air Quality Standards (NAAQS):** Air quality standards established by the CAA, as amended. The primary NAAQS are intended to protect the public health with an adequate margin of safety; the secondary NAAQS are intended to protect the public welfare from any known or anticipated adverse effects of a pollutant.

**National Emission Standards for Hazardous Air Pollutants (NESHAPs):** A set of national emission standards for listed hazardous pollutants emitted from specific classes or categories of new and existing sources. These standards were implemented in the CAA Amendments of 1977.

**National Environmental Policy Act (NEPA) of 1969:** The Act that established the national policy to protect humans and the environment, requiring environmental reviews of federal actions that have the potential for significant impact on the environment. It also established the Council on Environmental Quality (CEQ).

**National Historic Preservation Act of 1966, as amended:** The Act directing federal agencies to consider the effects of their programs and projects on properties listed on or eligible for the National Register of Historic Places. It does not require any permits, but pursuant to federal code, if a proposed action might impact any archaeological, historical, or architectural resource, this Act mandates consultation with the proper agencies.

**National Pollutant Discharge Elimination System (NPDES):** Federal permitting system required for hazardous effluents regulated through the CWA, as amended.

**National Register of Historic Places:** A list maintained by the Secretary of the Interior as the official list of historic properties (districts, sites, buildings, structures, and objects) deserving preservation because of their local, state, or national significance in American history, architecture, archaeology, engineering, and culture. Properties listed on or eligible for the National Register are protected by the National Historic Preservation Act of 1966, as amended.

**NEPA document:** A document prepared pursuant to requirements of the National Environmental Policy Act or CEQ regulations, including the following: environmental assessment, environmental impact statement, Notice of Intent, Record of Decision, and Finding of No Significant Impact.

**Nitrogen oxides (NO<sub>x</sub>):** The oxides of nitrogen, primarily nitrogen oxide (NO) and nitrogen dioxide (NO<sub>2</sub>), that are produced in the combustion of fossil fuels and can constitute an air pollution problem. When NO<sub>2</sub> combines with volatile organic

compounds in sunlight, ozone is produced. Nitrogen oxides are one of six criteria air pollutants specified under Title I of the CAA.

**Nonattainment area:** An AQCR (or a portion thereof) for which the EPA has determined that ambient air concentrations exceed NAAQS for one or more criteria pollutants (see also *attainment area* and *criteria pollutants*).

**Nonhazardous waste:** Routinely generated waste, including general facility refuse such as paper, cardboard, glass, wood, plastics, scrap, metal containers, dirt, and rubble. Nonhazardous waste is segregated and recycled whenever possible.

**Noninvolved worker:** A worker employed at a site who is not directly involved in the handling of radioactive or hazardous materials.

**Normal operations:** Conditions during which facilities and processes operate as expected or designed. In general, the evaluation of normal operations includes the occurrence of some infrequent events that, although not considered routine, are not classified as accidents. For example, the identification and repair of breached cylinders, expected to occur infrequently, was considered to be normal operations.

**Nuclear weapon:** The general name given to any weapon in which the explosion results from energy released by reactions involving atomic nuclei — either fission or fusion, or both.

**Occupational Safety and Health Administration (OSHA):** The agency that oversees and regulates workplace health and safety, created by the Occupational Safety and Health Act of 1970.

**Overpack:** Container used for transporting cylinders not meeting U.S. Department of Transportation (DOT) requirements. An overpack is a container into which a cylinder would be placed for shipment. The overpack would be designed, tested, and certified to meet all DOT shipping requirements and would be suitable to contain, transport, and store the cylinder contents regardless of cylinder condition.

**Ozone (O<sub>3</sub>):** The triatomic form of oxygen. In the stratosphere, ozone protects the earth from the sun's ultraviolet rays, but in lower levels of the atmosphere, ozone is considered an air pollutant and can cause irritation of the eyes and respiratory tract. Ozone is one of six

criteria air pollutants specified under Title I of the CAA.

***Palustrine:*** Nontidal wetlands dominated by trees, shrubs, or persistent emergent vegetation or small shallow wetlands.

***Particulate matter, particulates:*** Particles in an aerosol stream, the larger of which usually can be removed by filtration.

***Pasquill stability categories:*** Classification scheme that describes the degree of atmospheric turbulence. Categories range from extremely unstable (A) to extremely stable (F). Unstable conditions promote the rapid dispersion of atmospheric contaminants and result in lower air concentrations compared with stable conditions.

***Pathway:*** A route or sequence of processes by which radioactive or hazardous material may move through the environment to humans or other organisms. For example, one potential exposure pathway involves the contamination and subsequent use of surface water or groundwater.

***Permeability:*** In hydrology, the capacity of a medium (rock, sediment, or soil) to transmit groundwater. Permeability depends on the size and shape of the pores in the medium and how they are interconnected.

***Permissible exposure limits (PELs):*** Occupational exposure limits established for worker exposures to various chemicals, endorsed by the OSHA. Permissible exposure limits are defined so as to protect worker health and may be for short-term or 8-hour duration exposure.

***Plume:*** The spatial distribution of a release of airborne or waterborne material as it disperses in the environment.

***Plutonium (Pu):*** A heavy, radioactive, metallic element with the atomic number 94. Plutonium is produced artificially in a reactor by bombardment of uranium with neutrons and is used primarily in the production of nuclear weapons.

***PM<sub>10</sub>:*** Particulate matter with a mean aerodynamic diameter of 10 micrometers (µm) or less. PM<sub>10</sub> is one of six criteria air pollutants specified under Title I of the CAA.

***Pollution Prevention Act of 1990:*** The Act establishing the national policy that pollution should be prevented or reduced at the source or recycled in an environmentally safe manner and that pollution that cannot be prevented or recycled should be, as a last resort, treated and disposed of in an environmentally safe manner.

***Polychlorinated biphenyls (PCBs):*** A class of chemical substances formerly manufactured as an insulating fluid in electrical equipment. PCBs are highly toxic to aquatic life and, in the environment, exhibit many of the characteristics of dichloro diphenyl trichloroethane (DDT). PCBs persist in the environment for a long time and accumulate in animals.

***Polycyclic aromatic hydrocarbons (PAHs):*** A group of organic compounds, some of which are known to be potent human carcinogens.

***Population dose:*** see also *collective dose*.

***Programmatic environmental impact statement (PEIS):*** A type of EIS that deals with broad strategies and decisions, such as those that are regional or national in scope.

**Proposed action:** The term used in an EIS to refer to the activity planned by a federal agency that generates the need to prepare an EIS.

**Public:** see also *general public*.

**Radiation:** The particles (alpha and beta particles) or photons (gamma rays) emitted from the nuclei of radioactive atoms. Some elements are naturally radioactive; others are induced to become radioactive by bombardment in a reactor. Naturally occurring radiation, such as that from uranium, is indistinguishable from induced radiation.

**Radiation absorbed dose (rad):** The basic unit of absorbed dose equal to the absorption of 0.01 joule per kilogram (J/kg) of absorbing material.

**Radioactivity:** The spontaneous decay or disintegration of unstable atomic nuclei, accompanied by the emission of radiation.

**Radioactive decay:** Natural process by which a radioactive atom is physically transformed into another form by the release of energy in the form of subatomic particles such as alpha or beta particles, or electromagnetic radiation such as gamma rays.

**Radioactive decay products:** The isotopes produced when another isotope undergoes radioactive decay. The decay products are also typically radioactive.

**Radionuclide:** An atom that exhibits radioactive properties. Standard practice for naming a radionuclide is to use the name or atomic symbol of the element followed by its atomic weight (e.g., cobalt-60 [Co-60], a radionuclide of cobalt with an atomic weight of 60).

**Recharge:** Replenishment of water to an aquifer.

**Record of Decision (ROD):** A document prepared in accordance with the requirements of 40 CFR 1505.2 that provides a concise public record of the DOE's decision on a proposed action for which an EIS was prepared. A ROD identifies the alternatives considered in reaching the decision, the environmentally preferable alternative(s), and the factors balanced by the DOE in making the decision. The ROD also identifies whether all practicable means of avoiding or minimizing environmental harm have been adopted and, if not, why they were not.

**Region of influence (ROI):** The physical area that bounds the environmental, sociological, economic, or cultural feature of interest for the purpose of analysis.

**Rem:** The dosage of an ionizing radiation that will cause the same biological effect as one roentgen of X-ray or gamma-ray exposure.

**Resource Conservation and Recovery Act (RCRA), as amended:** An act that provides a "cradle-to-grave" regulatory program for hazardous waste that established, among other things, a system for managing hazardous waste from its generation until its ultimate disposal.

**Retardation:** The process by which dissolved material moves more slowly through the soil than the velocity of the bulk fluid (i.e., water).

**Risk:** A quantitative or qualitative expression of possible loss that considers both the probability that a hazard will cause harm and the consequences of that event.

**Safe Drinking Water Act, as amended:** An act that protects the quality of public water supplies and all sources of drinking water.

**Sanitary waste:** Waste generated by normal housekeeping activities, liquid or solid

(includes sludge), that is not hazardous or radioactive.

**Scope:** The range of actions, alternatives, and impacts to be considered in a document prepared pursuant to NEPA of 1969.

**Scoping:** The process of inviting public comment on what should be considered prior to preparation of an EIS.

**Severe accident:** An accident with a frequency of less than 1 in 1 million ( $10^{-6}$ ) per year that would have more severe consequences than a design-basis accident in terms of damage to the facility, off-site consequences, or both.

**Shielding:** Any material that is placed between a source of radiation and people, equipment, or other objects, in order to absorb the radiation and thereby reduce radiation exposure. Common shielding materials include concrete, steel, water, and lead. In general, for shielding gamma radiation sources, the denser a material is, the more effective it is as a shield.

**Sinter:** To form a homogenous mass by heating without melting.

**Socioeconomic analysis:** Analysis of those parts of the human environment in a particular location that are related to existing and potential future economic and social conditions.

**Socioeconomic impacts:** For this EIS, impacts expressed in terms of regional economic impacts (notably changes in local employment, income, and economic output [sales]), impacts to public services and finance in local jurisdictions, and impacts to local housing markets.

**Soil and Water Conservation Act of 1977:** An Act to establish a program administered by the Secretary of Agriculture to further the conservation of soil, water, and related resources consistent with the roles and responsibilities of other federal agencies and state and local governments.

**Solid Waste Disposal Act:** An Act that regulates the treatment, storage, or disposal of solid, both nonhazardous and hazardous, waste, as amended by RCRA and the Hazardous and Solid Waste Amendments of 1984.

**Source:** Any physical entity that may cause radiation exposure, for example, by emitting ionizing radiation or releasing radioactive material. Examples of radiation sources include X-ray machines and radionuclides such as uranium.

**Source term:** The amount of radioactive or hazardous material released to the environment following an accident.

**Stability class:** see *Pasquill stability categories*.

**Stakeholder:** Any person or organization interested in or potentially affected by activities and decisions of the DOE.

**Storage:** The temporary holding of material in a controlled and monitored facility.

**Sulfur dioxide (SO<sub>2</sub>):** A compound of sulfur produced by burning sulfur-containing compounds. It is considered a major air pollutant and is one of six criteria air pollutants specified under Title I of the CAA.

**Sulfur oxides (SO<sub>x</sub>):** A general term used to describe the oxides of sulfur — pungent, colorless gases formed primarily by the

combustion of fossil fuels. Sulfur oxides, which are considered major air pollutants, may damage the respiratory tract as well as vegetation.

***Technetium:*** A radioactive element with the atomic number 43. Its isotope, Tc-99 is generated in nuclear reactors during uranium and plutonium fission.

***Terrestrial:*** Pertaining to plants or animals living on land rather than in the water.

***Threatened species:*** Any species that is likely to become an endangered species within the foreseeable future throughout all or a significant portion of its range.

***Throughput:*** A general term that refers to the amount of material handled or processed by a facility in a year.

***Tiering:*** The process of first addressing general (programmatic) matters in a broad PEIS, followed by more narrowly focused (project-level) environmental documentation that incorporates by reference the more general document.

***Topography:*** Physical shape of the ground surface.

***Total effective dose equivalent:*** The sum of the effective dose equivalent from external exposure and the 50-year committed effective dose equivalent from internal exposure.

***Toxic Substances Control Act of 1976 (TSCA):*** The act authorizing the EPA to secure information on all new and existing chemical substances and to control any of these substances determined to cause an unreasonable risk to public health or the environment. This law requires that the health and environmental effects of all new chemicals be reviewed by the EPA before

they are manufactured for commercial purposes.

***Transuranic (TRU) waste:*** Waste contaminated by alpha-emitting transuranic radionuclides (i.e., radionuclides with atomic numbers greater than 92) with half-lives of more than 20 years and concentrations higher than 100 nanocuries per gram (nCi/g) at the time of assay.

***Triuranium octaoxide (U<sub>3</sub>O<sub>8</sub>):*** An oxide form of uranium that is the most common chemical form found in nature. U<sub>3</sub>O<sub>8</sub> is very stable and has a low solubility in water.

***Uranium:*** A heavy, silvery white, naturally radioactive, metallic element (atomic number 92). Its two principally occurring isotopes are uranium-235 and uranium-238. Uranium-235 is indispensable to the nuclear industry because it is the only isotope existing in nature to any appreciable extent that is fissionable by thermal neutrons. Uranium-238 is also important because it absorbs neutrons to produce a radioactive isotope that subsequently decays to plutonium-239, an isotope that also is fissionable by thermal neutrons.

***Uranium dioxide (UO<sub>2</sub>):*** A black crystalline powder that is widely used in the manufacture of fuel pellets for nuclear reactors. Pressed and sintered, it is stable when exposed to water or air below 300°C (572°F).

***Uranium hexafluoride (UF<sub>6</sub>):*** A chemical composed of one atom of uranium combined with six atoms of fluorine. UF<sub>6</sub> is a volatile white crystalline solid at ambient conditions. This form of uranium is used as feed for gaseous diffusion enrichment plants.

***Uranium metal:*** A heavy, silvery white, malleable, ductile, softer-than-steel metallic element. One of the densest materials known,

it is 1.6 times more dense than lead and slightly less toxic. Uranium metal is not as stable as U<sub>3</sub>O<sub>8</sub> or UF<sub>4</sub> because it is subject to surface oxidation. It tarnishes in air, with the oxide film preventing further oxidation of massive metal at room temperature.

**Uranium tetrafluoride (UF<sub>4</sub>):** A green crystalline solid that melts at about 960°C (1,652°F) and has an insignificant vapor pressure. It is very slightly soluble in water; generally an intermediate in the conversion of UF<sub>6</sub> to either uranium oxide (U<sub>3</sub>O<sub>8</sub> or UO<sub>2</sub>) or uranium metal. Also known as green salt.

**Uranyl fluoride (UO<sub>2</sub>F<sub>2</sub>):** A yellow hygroscopic (i.e., moisture-retaining) solid that is very soluble in water. In accidental releases of UF<sub>6</sub>, UO<sub>2</sub>F<sub>2</sub> is a solid particulate compound that may deposit on the ground over a large area.

**Vacuum:** A pressure less than atmospheric. Depleted uranium hexafluoride (DUF<sub>6</sub>) is stored in a vacuum in cylinders.

**Volatile organic compounds (VOCs):** A broad range of organic compounds (such as benzene, chloroform, and methyl alcohol), often halogenated, that vaporize at ambient or relatively low temperatures.

**Waste management:** The planning, coordination, and direction of those functions related to generation, handling, treatment, storage, transportation, and disposal of waste, as well as associated pollution prevention and surveillance and maintenance activities.

**Waste minimization:** An action that economically avoids or reduces the generation of waste via source reduction, reducing the toxicity of hazardous waste, improving energy usage, or recycling.

**Wastewater:** Water that typically contains less than a 1% concentration of organic hazardous waste materials.

**Water Quality Act of 1987:** An act amending the Federal Water Pollution Control Act to make NPDES requirements applicable to storm water discharges.

**Web site:** A collection of information — possibly including text, figures, pictures, audio, and video — that can be accessed by computer through the Internet computer network. These sites are intended to communicate and distribute information to anyone having access to the Internet.

**Wetlands:** Lands or areas exhibiting hydric soils, saturated or inundated soil during some portion of the plant growing season, and plant species tolerant of such conditions (include swamps, marshes, and bogs).

**Wild and Scenic Rivers Act:** An Act providing for protection of the free-flowing, scenic, and natural values of rivers designated as components or potential components of the National Wild and Scenic Rivers System.

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