

# Evaluating $^{99}\text{Tc}$ Release from Intact Saltstone Monoliths

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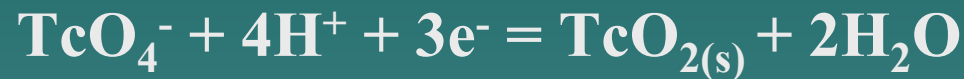
**The University of Georgia**

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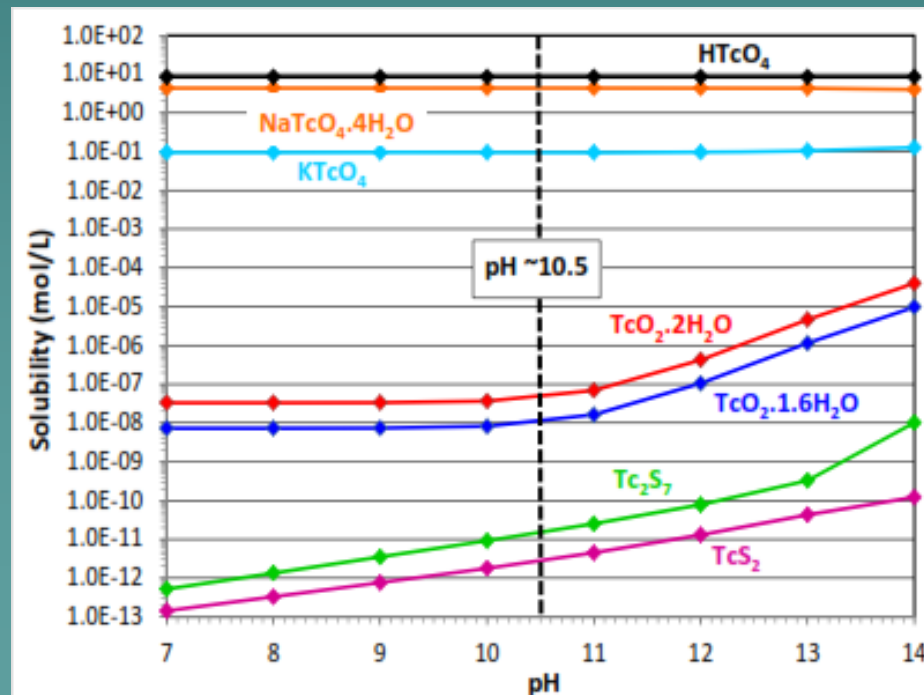


# Technetium (Tc) Characteristics

- ◆ Reduced form Tc(IV) is less soluble/mobile
- ◆ Tc(VII) reduced to Tc(IV) which precipitates as  $\text{TcO}_2 \cdot n\text{H}_2\text{O}_{(s)}$  or with  $\text{S}^{2-}$

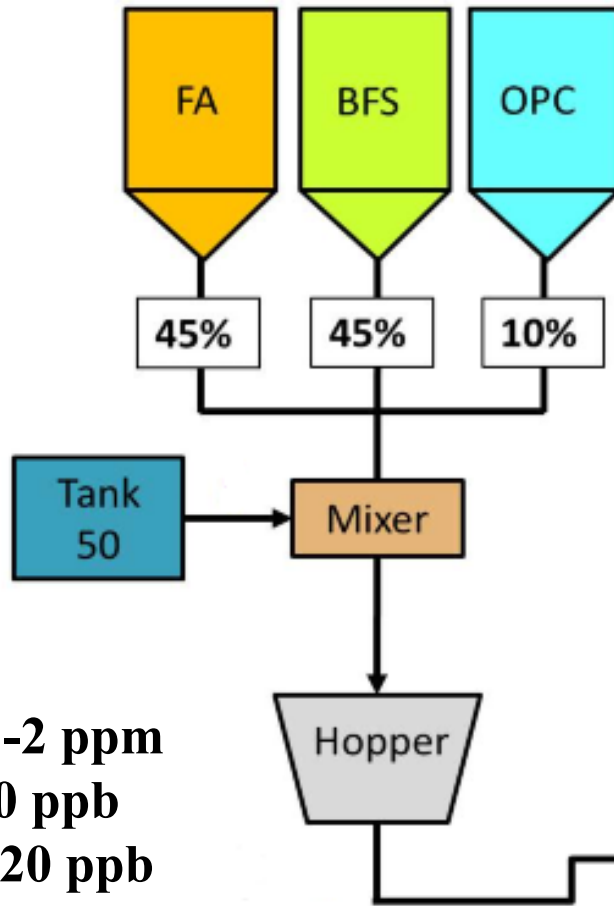


- ◆ Tc(IV) may be oxidized with moderate  $\text{O}_2$  exposure
  - dependence on physical and chemical integrity of the waste form



# SRS LAW Strategy

## Tank 50 Composition



Rads		pCi/mL
$^3\text{H}$		607
$^{14}\text{C}$		4,700
$^{90}\text{Sr}$		1,930
$^{99}\text{Tc}$		19,300
$^{129}\text{I}$		14
$^{137}\text{Cs}$		1,210,000
		mg/L
$\text{NO}_3$		1.36E+05
$\text{NO}_2$		2.13E+04

$^{99}\text{Tc}$  – 1-2 ppm  
 $^{129}\text{I}$  - 60 ppb  
 $^{137}\text{Cs}$  – 20 ppb

$^{99}\text{Tc}$  Drinking Water Standard is 900 pCi/L  
 $^{129}\text{I}$  Drinking Water Standard is 1 pCi/L

# Saltstone Experiments

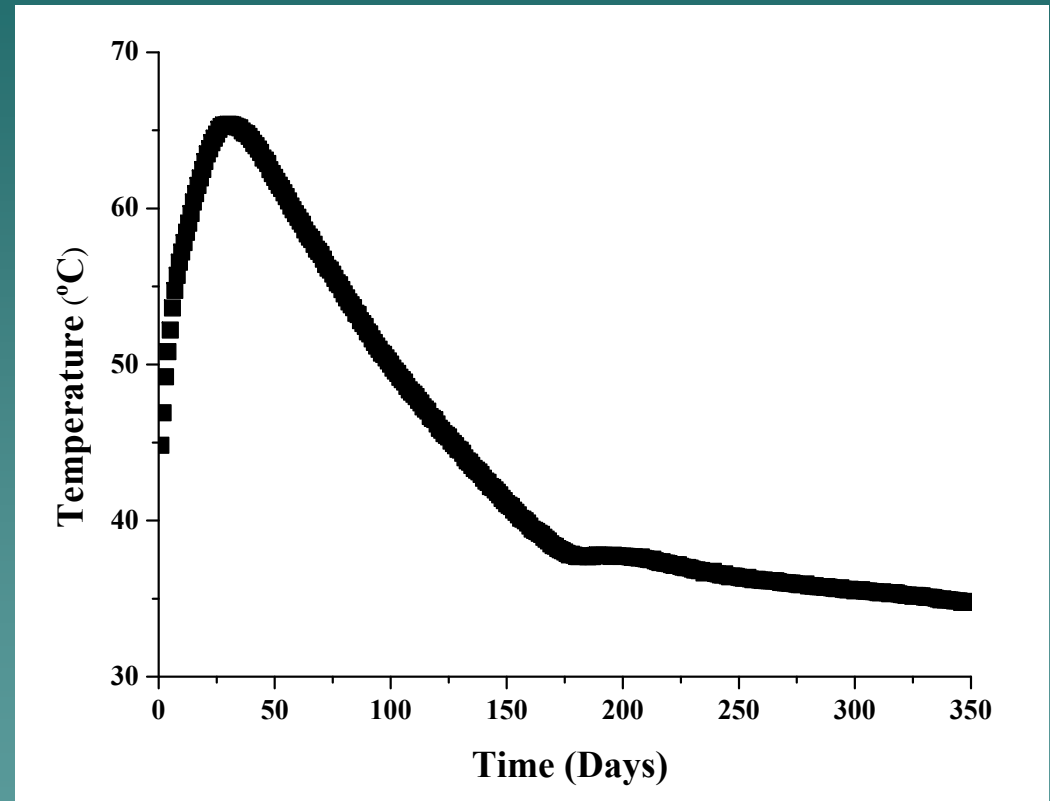
- ◆ Saltstone Simulants - spiked with  $^{127}\text{I}$ , Re or  $^{99}\text{Tc}$
- ◆ Multiple BFS Sources, i.e., inherent reductive capacity
- ◆ Curing 6+ months – Temperature regime to matches vaults
- ◆ Saltstone core samples from SDU2A
- ◆ EPA 1315: *Mass transfer rates of constituents in Monolithic or Compacted Granular Materials using a Semi-Dynamic Tank Leaching Procedure (ANS 16.1)*
- ◆ Dynamic Leaching Method (DLM)
- ◆ Monitor:  $^{99}\text{Tc}$ ,  $^{137}\text{Cs}$ ,  $^{127}\text{I}$ ,  $^{129}\text{I}$  (pending),  $\text{NO}_3^-$  and Re (when added)

# Saltwaste/Saltstone Simulants

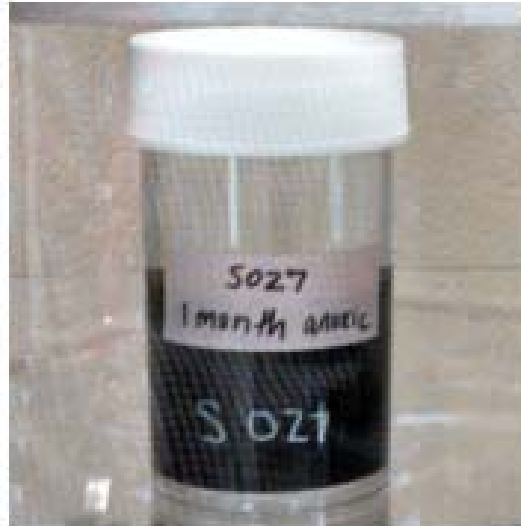
Material	ARP/MCU Salt Simulant	
	Molarity (moles/L)	Mass (g/L)
Sodium Hydroxide, NaOH (50 wt.% by weight)	1.594	127.50
Sodium Nitrate, NaNO <sub>3</sub>	3.159	268.48
Sodium Nitrite, NaNO <sub>2</sub>	0.368	25.39
Sodium Carbonate, Na <sub>2</sub> CO <sub>3</sub>	0.176	18.65
Sodium Sulfate, Na <sub>2</sub> SO <sub>4</sub>	0.059	8.37
Aluminum Nitrate, Al(NO <sub>3</sub> ) <sub>3</sub> ·9H <sub>2</sub> O	0.054	20.33
Sodium Phosphate, Na <sub>3</sub> PO <sub>4</sub> ·12H <sub>2</sub> O	0.012	4.67



# Saltstone Curing Temperature SDU 2A



# Contaminant Release: EPA 1315

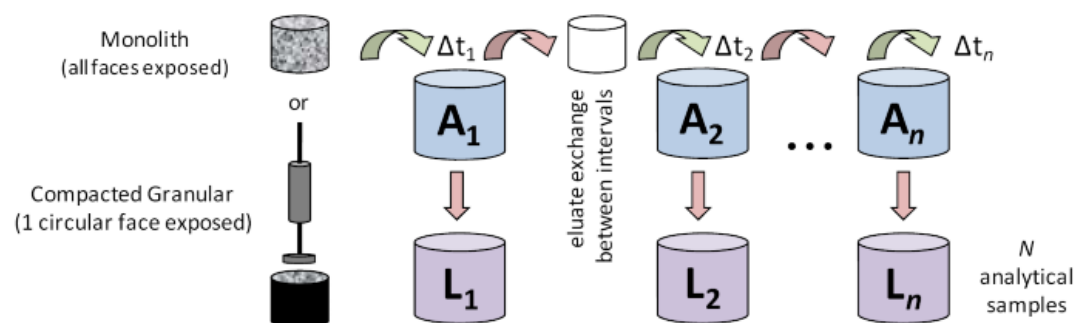


- Tc/Re-spiked samples
- Test Monolith Dimensions
  - 5.1 cm diameter
  - 5.0 cm length
- $\geq 5$ cm liquid above exposed surface
- Tested with leachates equilibrated with air, UHP  $N_2$ , and  $N_2$ -2% $H_2$ .

- SDU2A cores and Tc-spiked samples
- $\geq 5$ cm liquid around sample all exposed surfaces
- Test Monolith Dimensions
  - 5.1 cm diameter
  - 8.0 to 10.5 cm length
- Tested only with leachates equilibrated with air

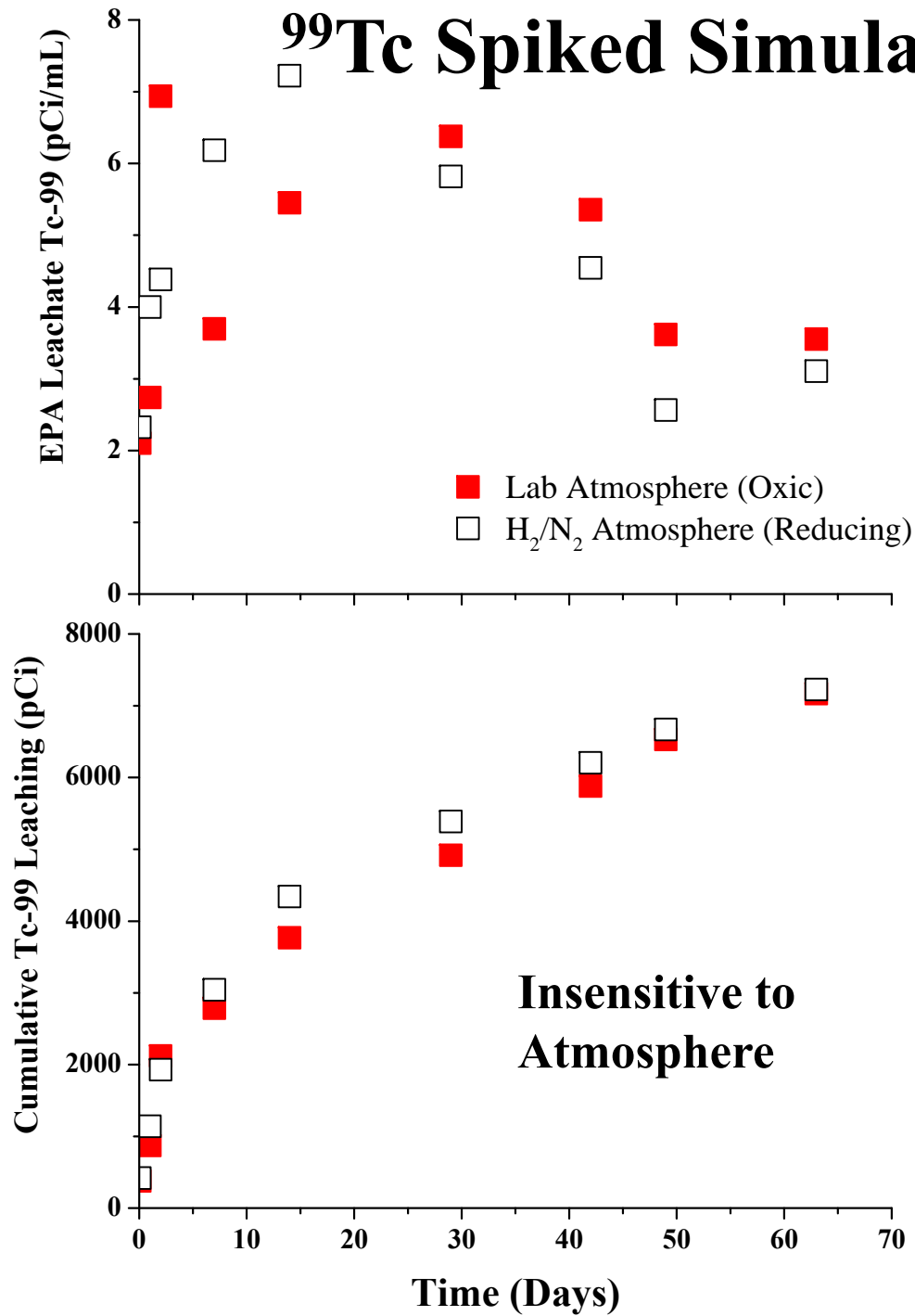
# Contaminant Release: EPA 1315

Interval Label	Interval Duration (h)	Interval Duration (d)	Cumulative Leaching Time (d)
T01	$2.0 \pm 0.25$		0.08
T02	$23.0 \pm 0.5$		1
T03	$23.0 \pm 0.5$		2
T04		$5.0 \pm 0.1$	7
T05		$7.0 \pm 0.1$	14
T06		$14.0 \pm 0.1$	28
T07		$14.0 \pm 0.1$	42
T08		$7.0 \pm 0.1$	49
T09		$14.0 \pm 0.1$	63





# <sup>99</sup>Tc Spiked Simulant



# Leaching Data Analysis

## Effective Diffusivity

$$D_e = \pi \left[ \frac{a_n/A_o}{\Delta t_n} \right] \left[ \frac{V}{S} \right]^2 T$$

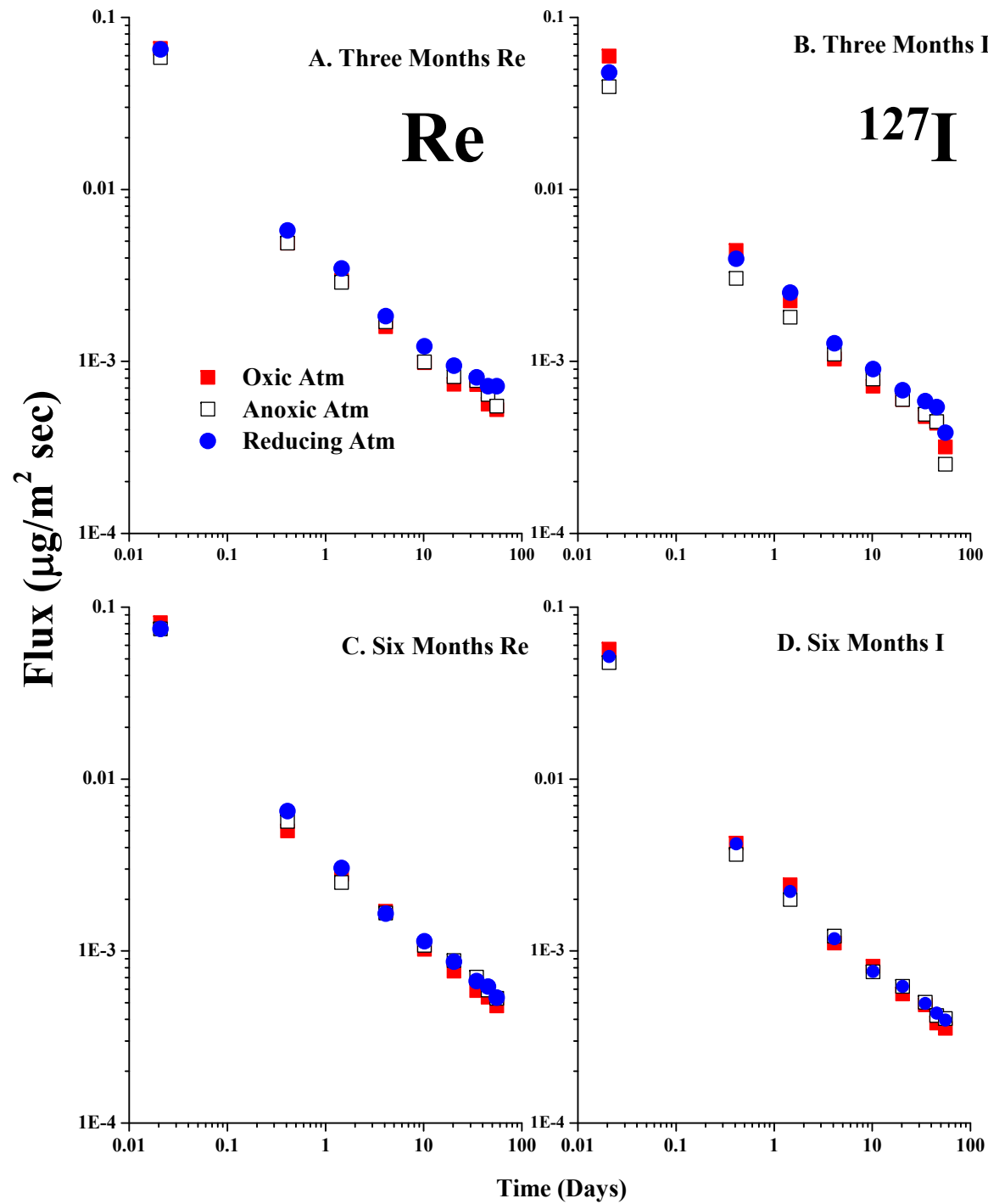
## Generalized Mean Square Root of Leaching Time

$$T = \left[ \frac{\sqrt{t_n} + \sqrt{t_{n-1}}}{2} \right]^2$$

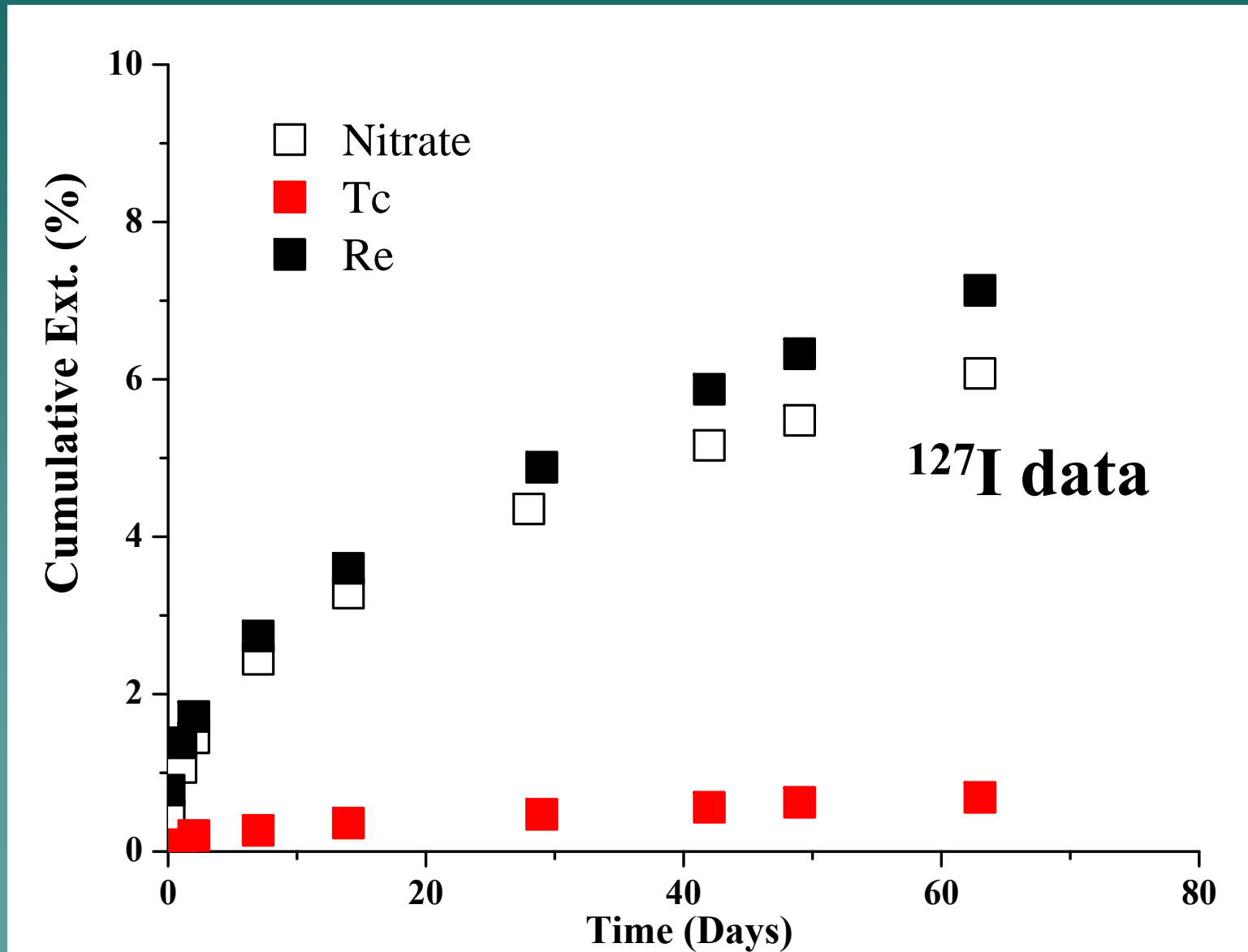
## Leaching Index

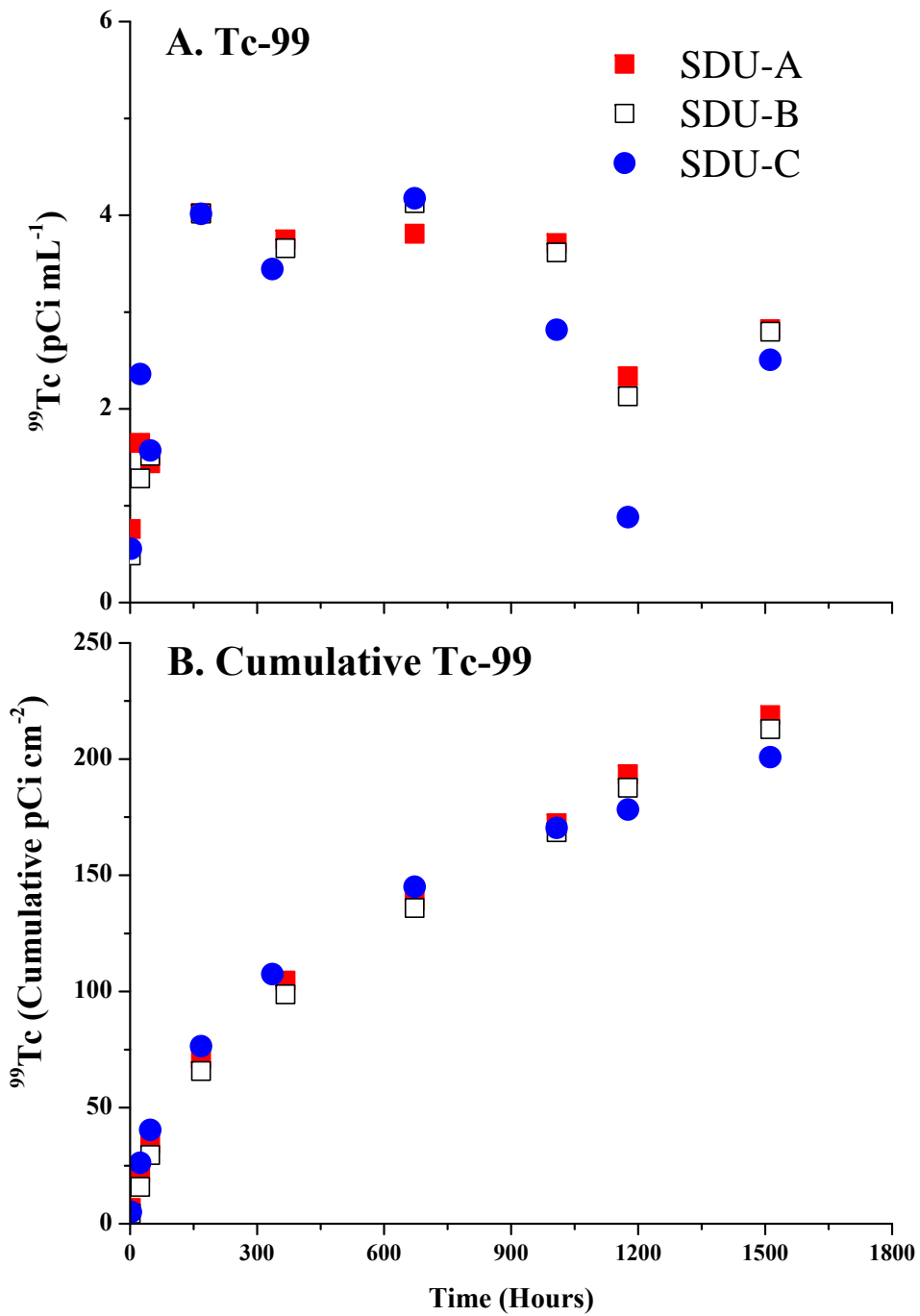
$$LI_n = -\log[D_e]$$

↑  $LI$  = slower leaching  
↓  $LI$  = faster leaching

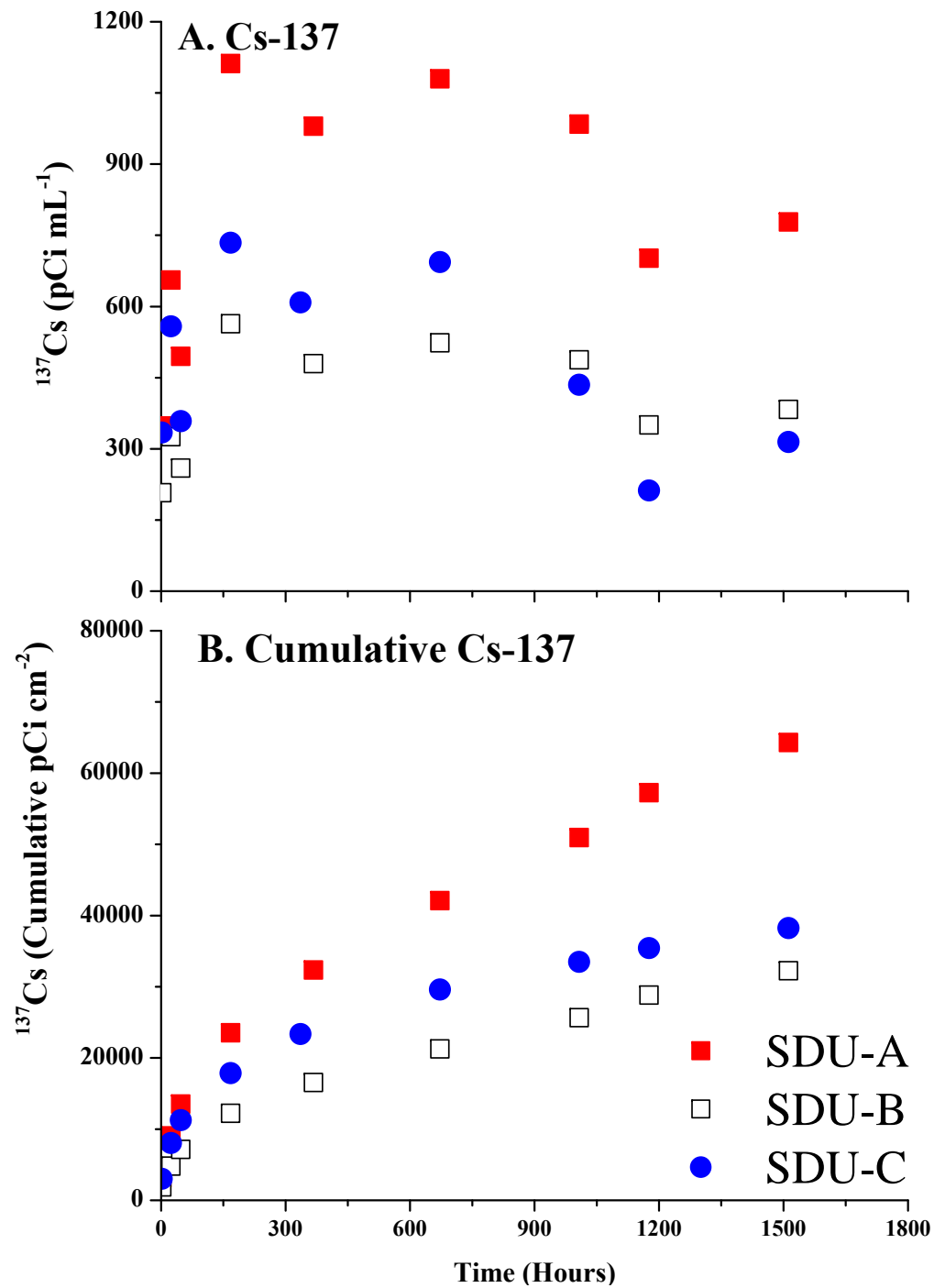


# Cumulative % Extracted (1D Test): <sup>99</sup>Tc and Re Spiked Simulant Grouts





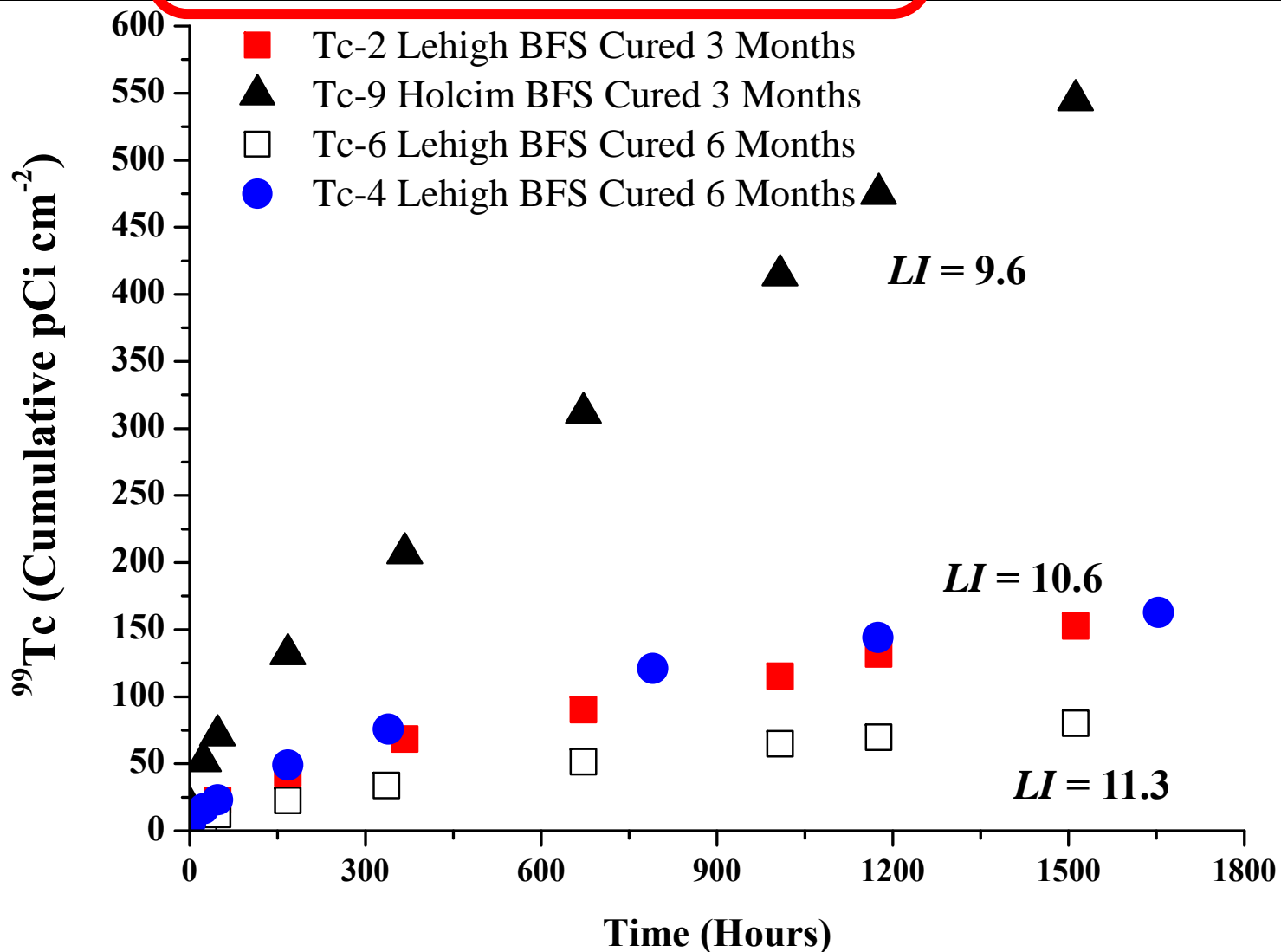
# Three SDU Grout Samples



## Three SDU Grout Samples

# <sup>99</sup>Tc-Spiked Grout Samples: Impact of BFS Source

SAMPLE	Reductive Capacity	Fe	S	Ca	Al
	$\mu\text{eq gm}^{-1}$	mg/kg	mg/kg	mg/kg	mg/kg
Holcim BFS (FY15)	713	1,685	13,934	234,566	18,324
Lehigh BFS (Batch 1)	1600	3,504	23,620	285,232	39,933

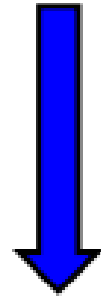


# EPA 1315 Data Summary: Leachability Indices

		<sup>99</sup> Tc	Re	<sup>137</sup> Cs	NO <sub>3</sub>	<sup>127</sup> I
Sample		LI	LI	LI	LI	LI
<b>FY15 Spiked Saltstone</b>						
	<b>Old BFS (Holcim)</b>	<b>9.7-9.9</b>	<b>7.5-7.7</b>	<b>NA</b>	<b>7.5-7.9</b>	<b>7.6-7.8</b>
<b>FY16 Spiked Saltstone</b>						
	<b>New BFS (Lehigh)</b>	<b>10.6-11.3</b>	<b>NA</b>	<b>NA</b>	<b>6.7-7.5</b>	<b><sup>129</sup>I</b> <b>NA</b>
	<b>Old BFS (Holcim)</b>	<b>9.6</b>	<b>NA</b>	<b>NA</b>	<b>7.5</b>	<b>NA</b>
<b>Three SDU Cores</b>						
	<b>Old BFS (Holcim)</b>	<b>10.2-10.3</b>	<b>NA</b>	<b>9.4-10.0</b>	<b>6.6-8.5</b>	<b>pending</b>



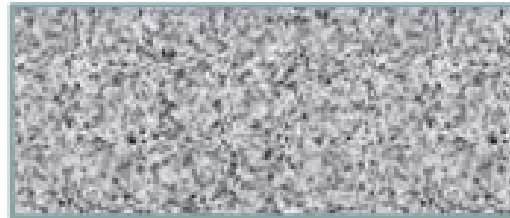
# Dynamic Leaching Method Based on $K_{sat}$ FWP



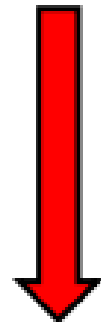
AGW

pH ~6-7;  $E_h$  ~600 mV

Variables: (1) DO (0 or 8 ppm)  
(2) Added  $^{99}\text{Tc}$  as  $(\text{TcO}_4)^-$



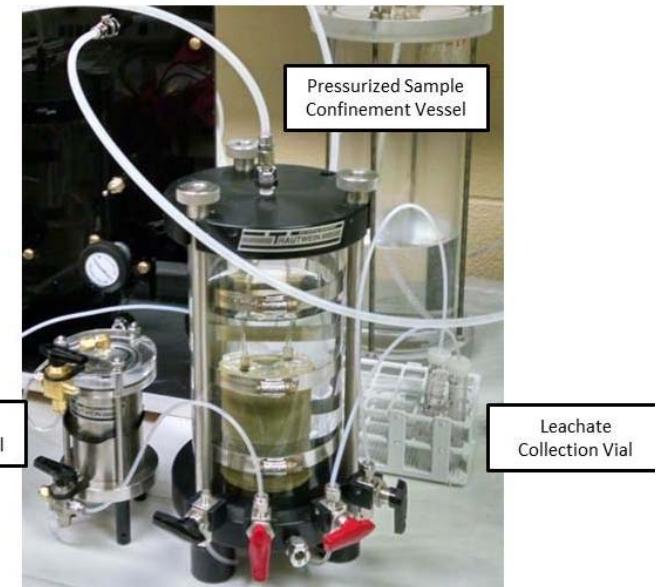
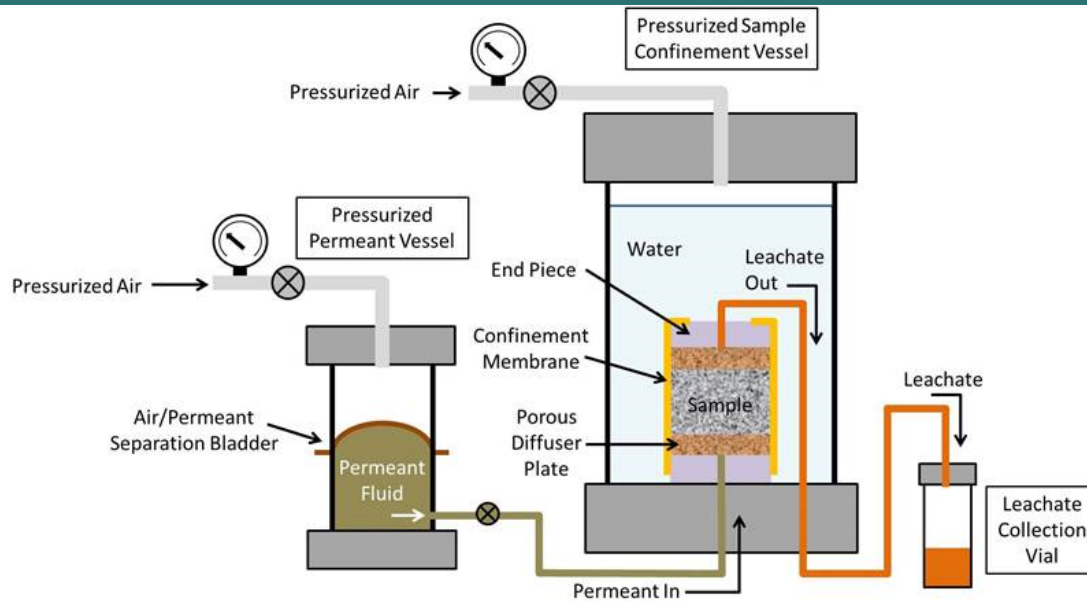
10-20 psi pressure differential



Effluent measurements include:

1. pH,  $E_h$
2.  $^{99}\text{Tc}$ ,  $(\text{NO}_3)^{2-}$  (+  $^{129}\text{I}$ ,  $^{137}\text{Cs}$  for SDU2A cores)
3. DO

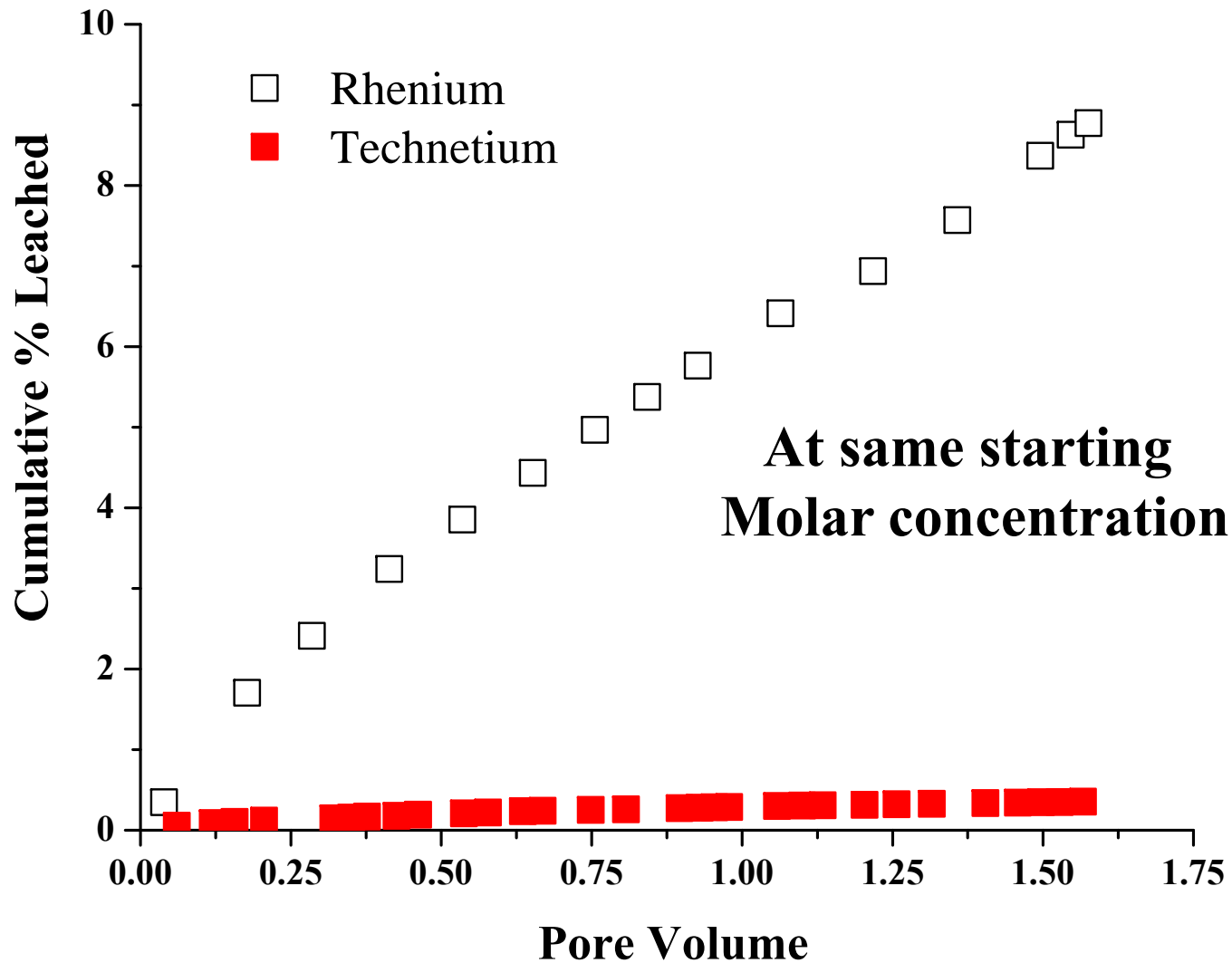
# SREL DLM System

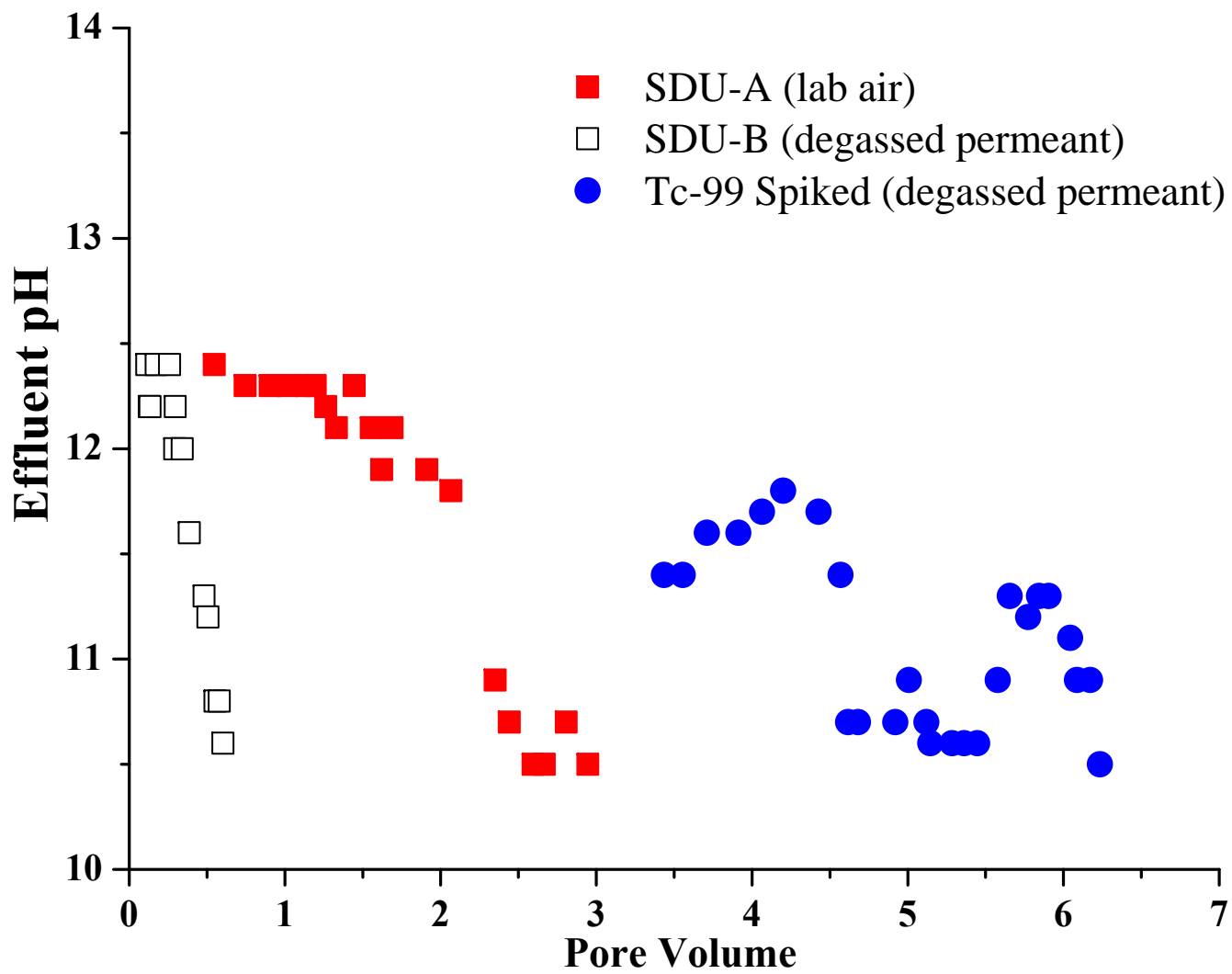


# DLM Manifold (3 Sample Capacity)

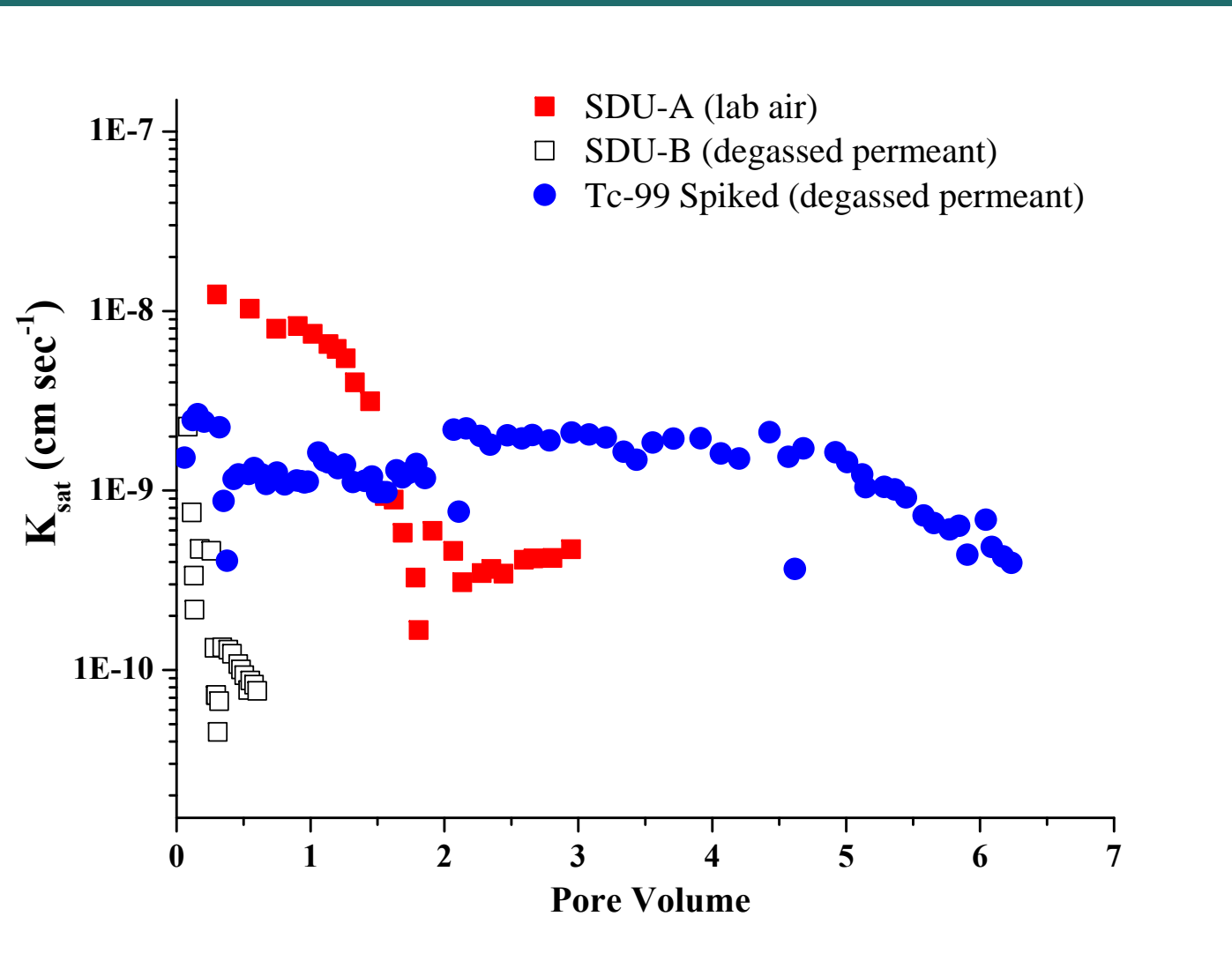


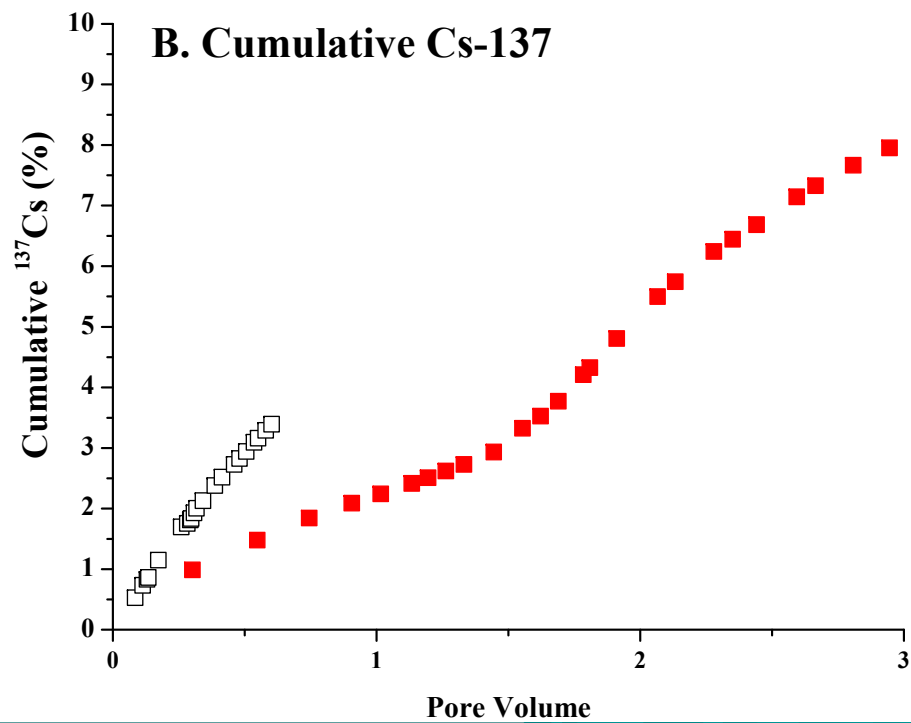
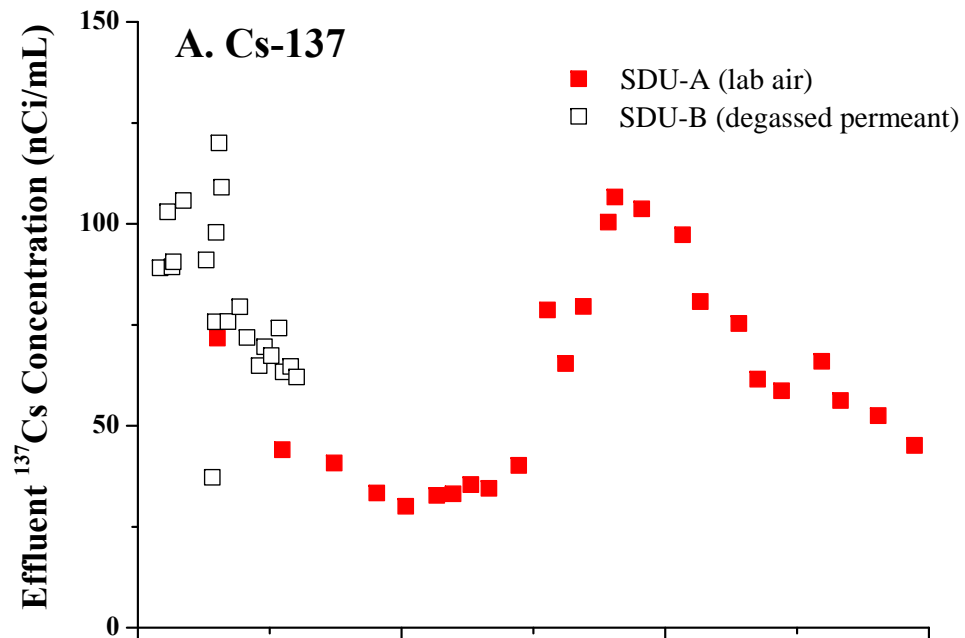
# Dynamic Leaching Spiked Grouts: Re vs $^{99}\text{Tc}$

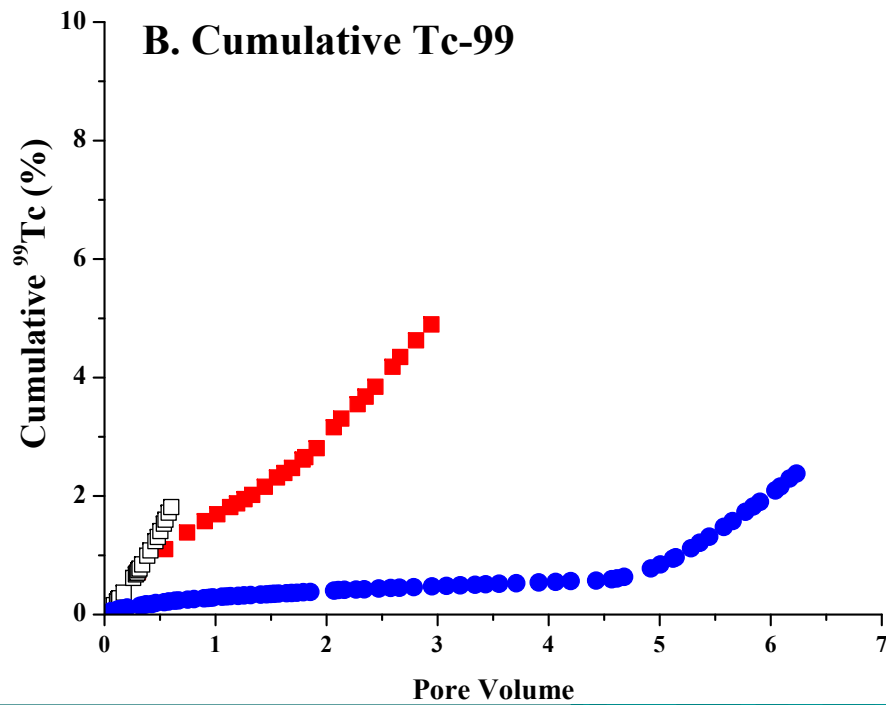
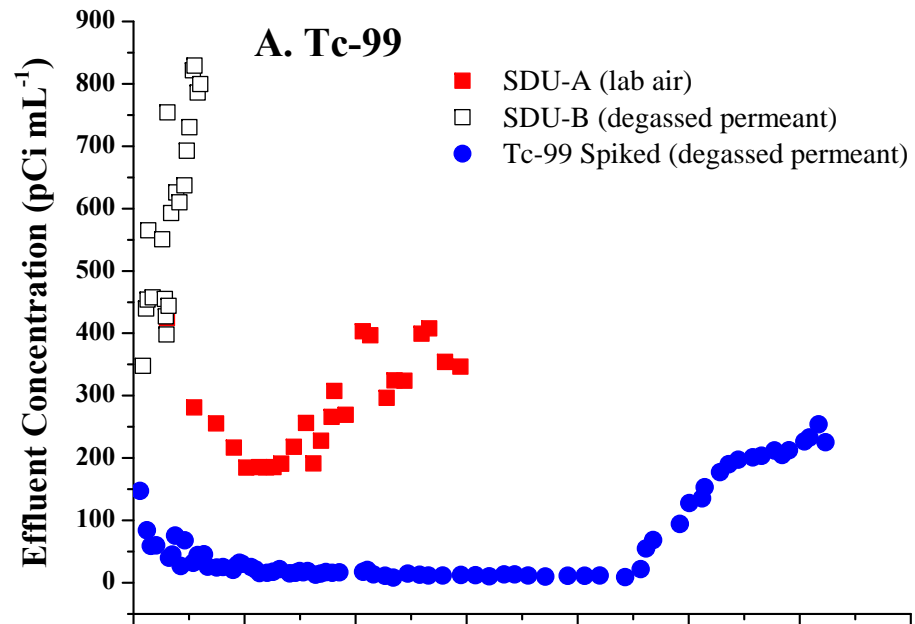




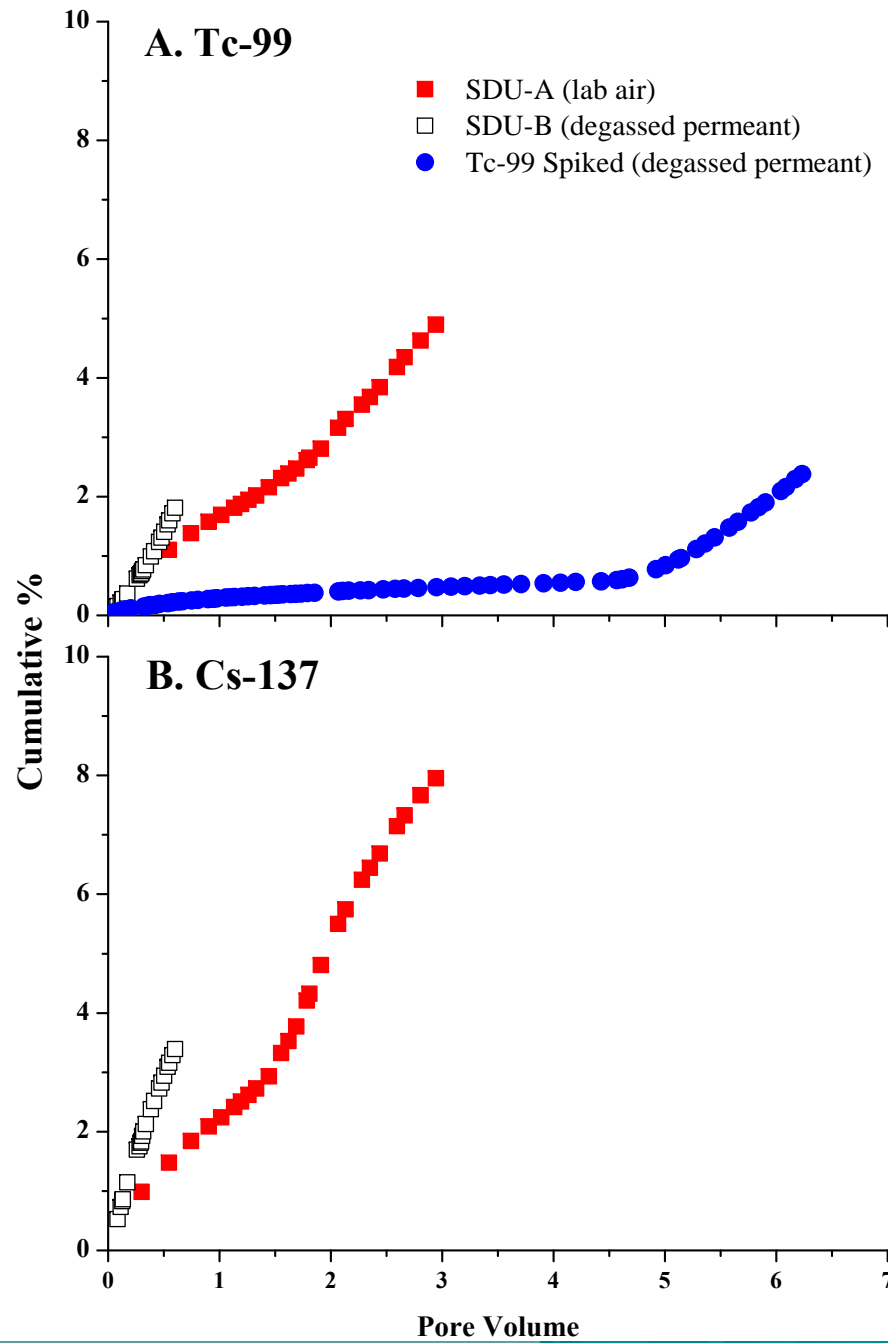
# Hydraulic Conductivity ( $K_{sat}$ )

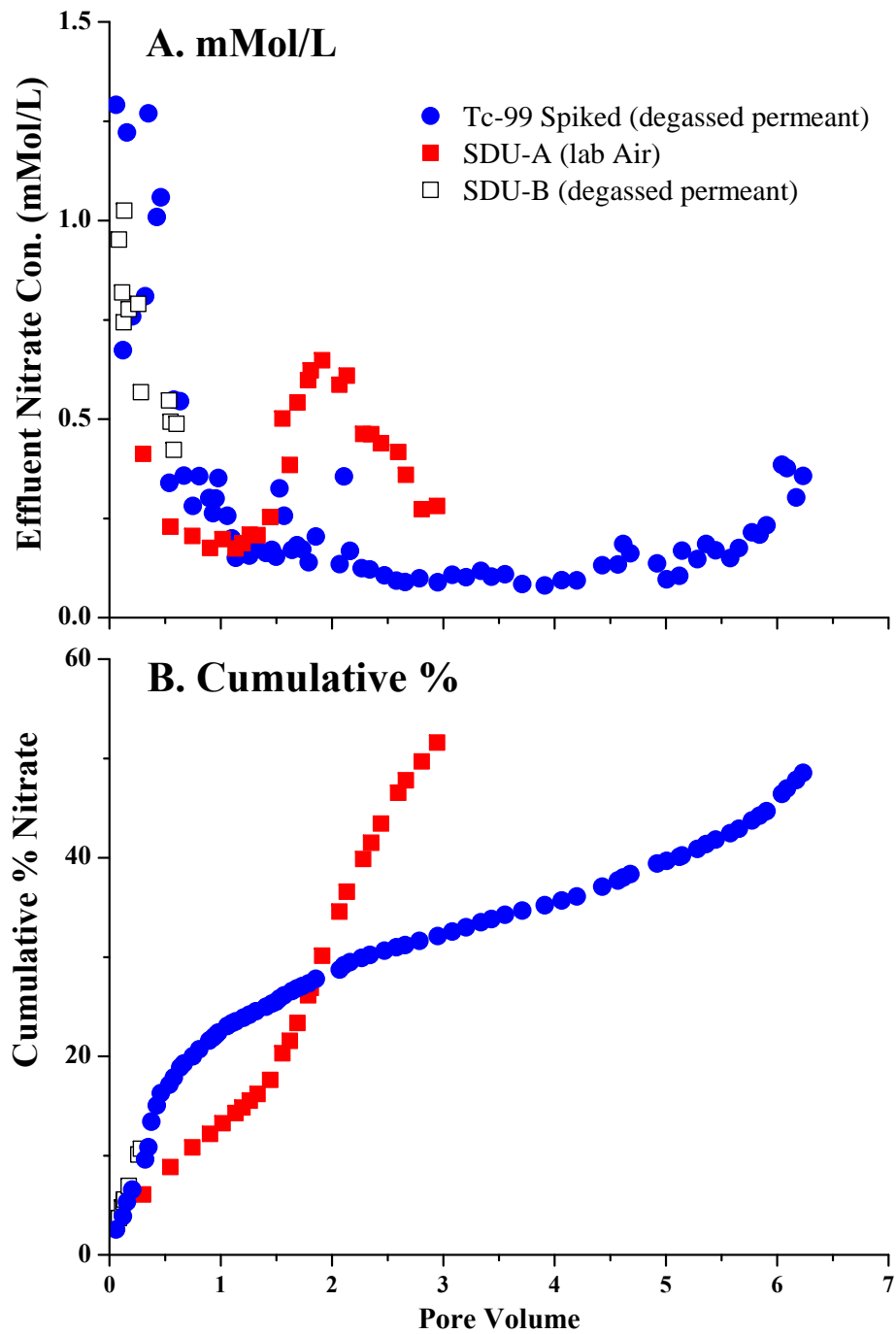












# Conclusions I: Spiked Samples

- ◆ Re,  $^{127}\text{I}$ , and  $\text{NO}_3^-$  leach at similar rates, i.e., non-reactive (*LI 7.5-7.9*)
- ◆  $^{99}\text{Tc}$  leaches at much slower rate than Re (*LI 9.7-11.3*)
- ◆  $^{99}\text{Tc}$  results consistent with Hanford Cast Stone results (Westik et al., 2013; Serne et al., 2015)
- ◆ Extraction atmosphere didn't impact Re, Tc, or  $^{127}\text{I}$  leaching
  - Re mobile/oxidized (redox potential or Re(IV) solubility)
  - Tc immobilized/reduced
  - $^{129}\text{I}$  tests ongoing

# Conclusions II: SDU Cores

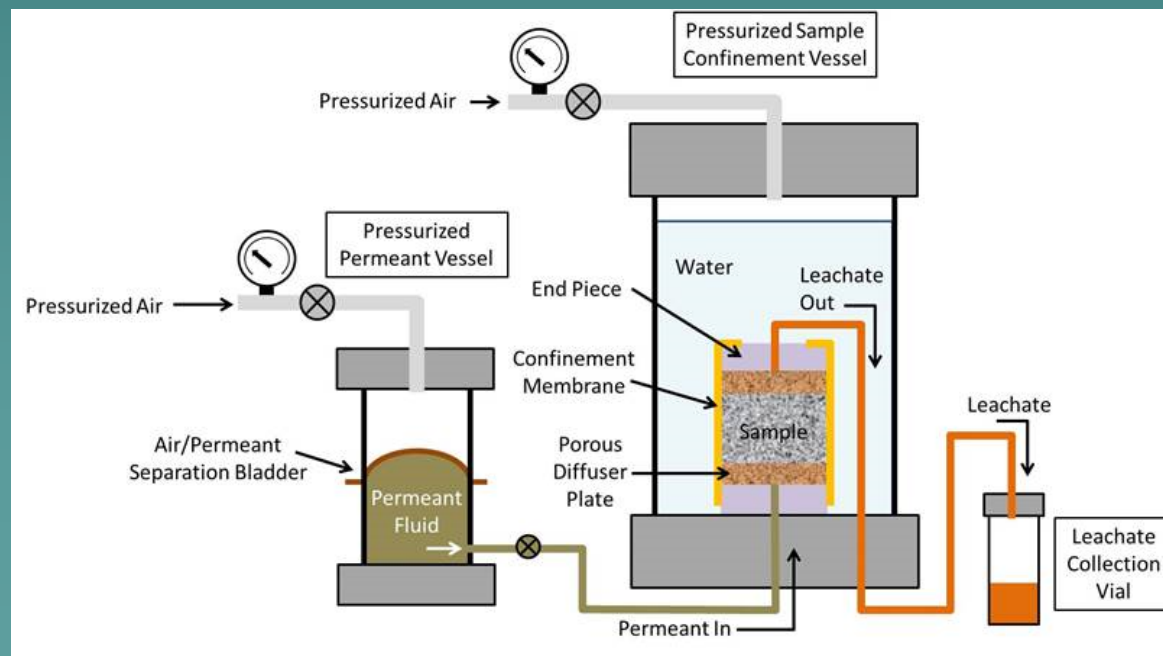
- ◆ Similar  $^{99}\text{Tc}$  leachability observed for SDU and simulant materials (*LI 9.6 to 11.3*)
- ◆  $^{99}\text{Tc}$  leachability dependent on BFS source (reductive capacity) and curing time
  - (*LI 9.6 vs 11.3*)
- ◆  $^{137}\text{Cs}$  leaching slower than predicted
  - (*LI 9.4-9.9*)

# Conclusions III: DLM Tests

- ◆ Variable residence times make comparisons difficult
- ◆  $K_{sat}$  Lab Simulants > SDU Cores (i.e.,  $10^{-9}$  vs  $10^{-10}$  to  $10^{-11}$  cm s<sup>-1</sup>)
- ◆ Rate of leaching:  $\text{NO}_3^- \gg \text{}^{137}\text{Cs} > \text{}^{99}\text{Tc}$
- ◆ Tc leaching generally consistent with  $\text{TcO}_2$  nH<sub>2</sub>O

# Modified DLM System

- ◆ Constant inlet flow rate with monitored backpressure
  - Target  $\approx 1+$  mL/day
- ◆ Automated control of confining pressure (i.e., inlet + 4 PSI)
- ◆ Low-volume (50  $\mu$ L) flow-through sensors (pH, ORP, DO)
  - Reduce leachate exposure to atmosphere
- ◆ Controlled backpressure at the outlet (1-2 PSI)
  - Minimize leachate degassing before collection



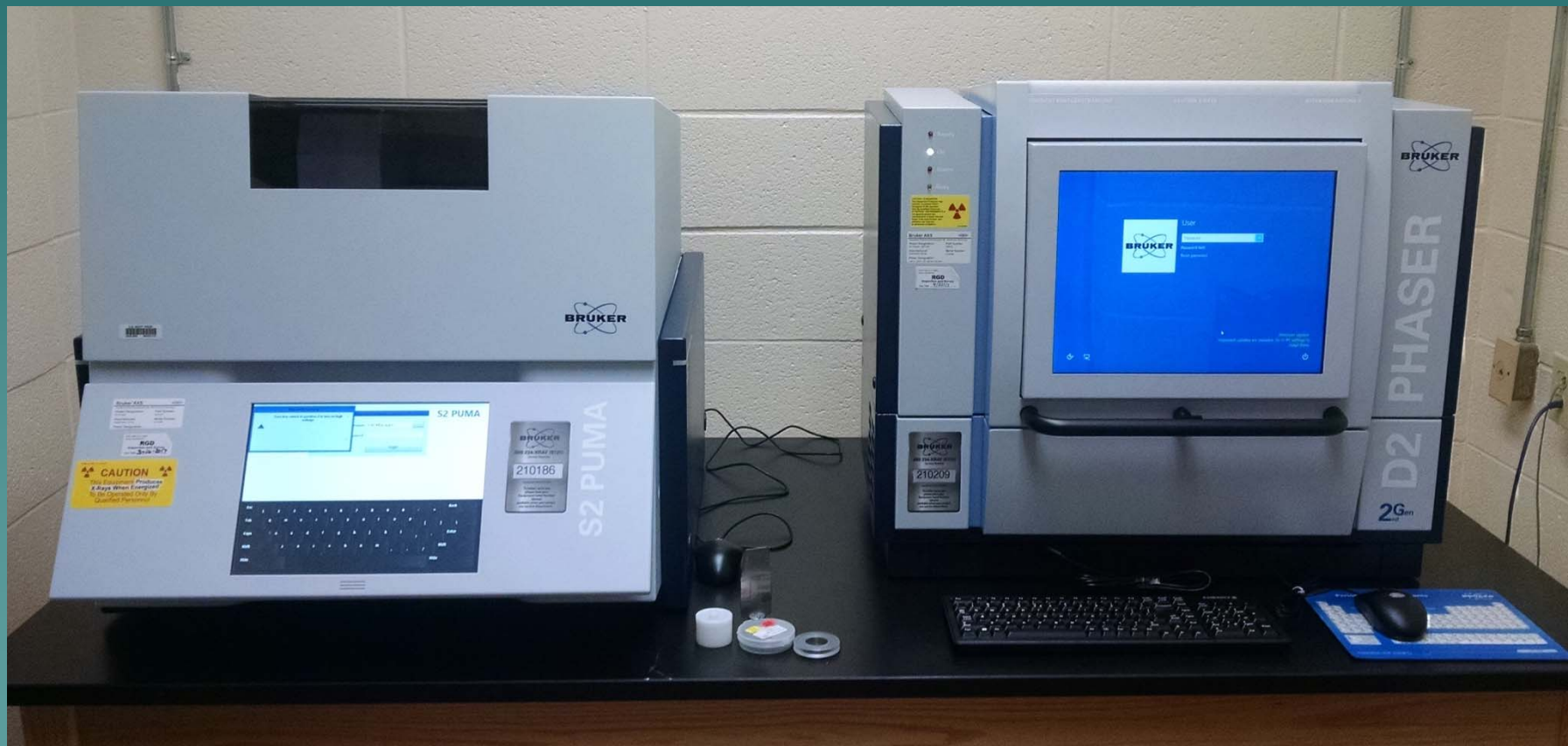
# FY17 Testing

- ◆ EPA1315 and DLM tests with  $^{129}\text{I}$ -spiked saltstone, BFS source materials
- ◆ Expanded DLM testing with controlled flow rates (solubility vs kinetic controls)
- ◆ Non-reactive tracer ( $^3\text{H}_2\text{O}$ ) to estimate conductive porosity

◆ Solid phase characterization during curing and leaching tests (XRF, XRD, TGA)

XRF

XRD

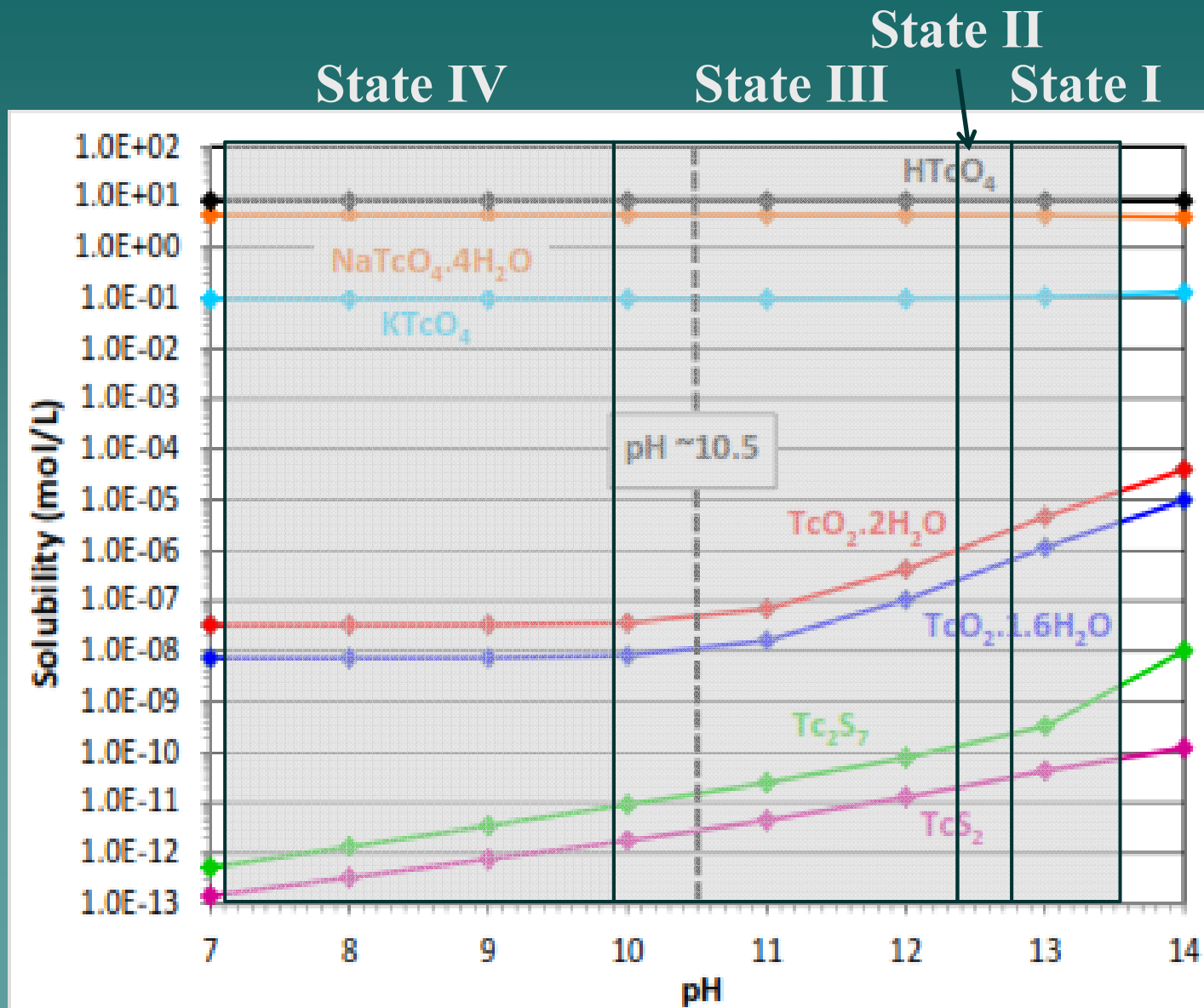




# FY17 Testing

- ◆ **Geochemical Modeling – EPA and DLM data**
  - CSH transformations
  - Residual reductive capacity
  - $^{99}\text{Tc}$  phase identification
  - Carbonation
- ◆ **Calorimetry – Heat Capacity, Heat of Hydration**
  - Processing - Curing rates
  - Durability

# $^{99}\text{Tc}$ Solubility vs Cement Weathering



# Important Redox Reactions

Reaction	$E^\circ, \text{Volt}$
1. $\text{ReO}_4^- + 4\text{H}^+ + 3\text{e}^- \leftrightarrow \text{ReO}_2 + 2\text{H}_2\text{O}$	-0.55
2. $\text{TcO}_4^- + 4\text{H}^+ + 3\text{e}^- \leftrightarrow \text{TcO}_2 + 2\text{H}_2\text{O}$	-0.36
3. $\text{Fe}^{2+} + 2\text{e}^- \leftrightarrow \text{Fe}$	-0.44
4. $\text{CrO}_4^{2-} + 4\text{H}_2\text{O} + 3\text{e}^- \leftrightarrow \text{Cr}(\text{OH})_3 + 5\text{OH}^-$	-0.13
5. $2\text{H}^+ + 2\text{e}^- \leftrightarrow \text{H}_2$	0.00
6. $\text{Fe}^{3+} + \text{e}^- \leftrightarrow \text{Fe}^{2+}$	+0.77
7. $\frac{1}{8}\text{NO}_3^- + \frac{5}{4}\text{H}^+ + \text{e}^- \leftrightarrow \frac{1}{8}\text{NH}_4^+ + \frac{3}{8}\text{H}_2\text{O}$	+0.88
8. $\text{Fe}(\text{OH})_3 + 3\text{H}^+ + \text{e}^- \leftrightarrow \text{Fe}^{2+} + 3\text{H}_2\text{O}$	+0.98
9. $\frac{1}{6}\text{NO}_2^- + \frac{4}{3}\text{H}^+ + \text{e}^- \leftrightarrow \frac{1}{6}\text{NH}_4^+ + \frac{1}{3}\text{H}_2\text{O}$	+1.12
10. $\text{O}_2 + 4\text{H}^+ + 4\text{e}^- \leftrightarrow 2\text{H}_2\text{O}$	+1.23
11. $\text{NO}_3^- + 6\text{H}^+ + 5\text{e}^- \leftrightarrow \frac{1}{2}\text{N}_2 + 2\text{H}_2\text{O}$	+1.26

# $^{99}\text{Tc}$ Analysis by ICP-MS

