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## Effect of Various Impurities on the Hydrogen Absorption on SAES ST198

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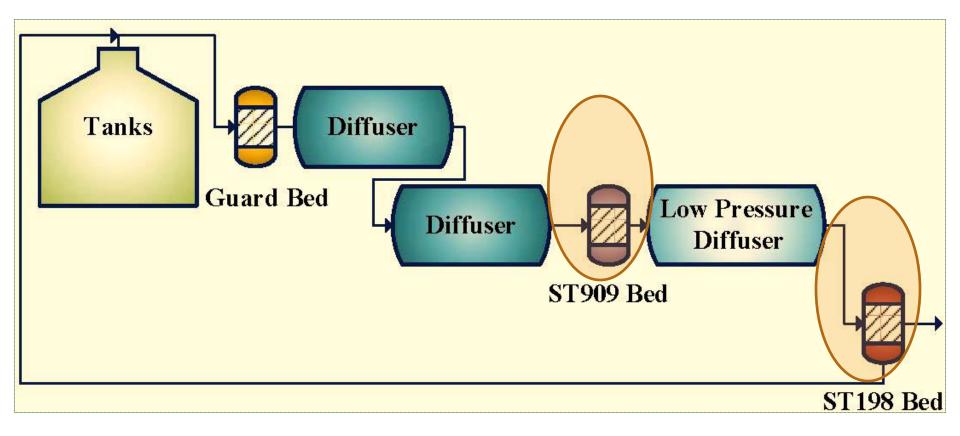
SRNL-STI-2015-00592



- Tritium Purification System
- ST909
- ST198
- Results of ST198 Impurity Testing
- Conclusions/Summary



#### **TPS Overview**



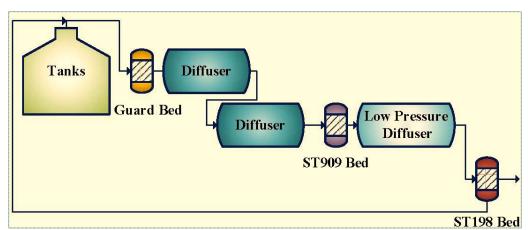
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- Zr(Mn<sub>0.5</sub>Fe<sub>0.5</sub>)<sub>2</sub> or Zr-Mn-Fe (40.5% Zr, 24.5% Mn, 25.0% Fe, 10% AI)
- Manganese and iron catalytic active sites for decomposition
  - $-CH_4$
  - $-NH_3$
  - CO
  - $CO_{2}$
  - $Q_2 O$
- Zirconium active sites for the gettering of elements
  - 0
  - N
  - C

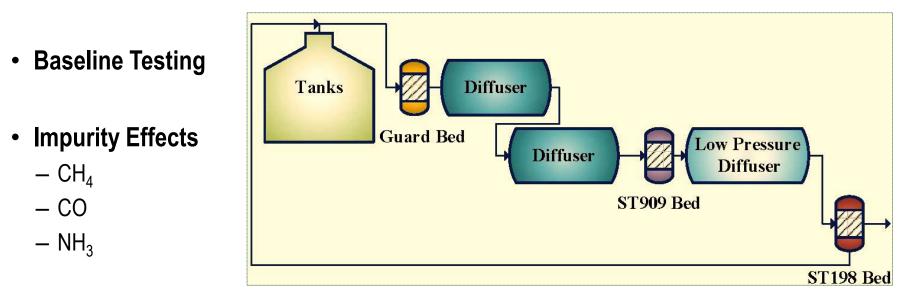
#### Literature tells us

- Other getter materials, may have better methane cracking performance than ST909,
- No other single material was best for use in helium, hydrogen, or nitrogen carrier gas streams

- SAES ST909 is expensive
  - (~\$4200-5300/kg, depending on the quantity of the material requested)
- Consumable material
- Foreign sole source supplier
- Difficult to Obtain Special Order



- Downstream effects if ST909 did not perform
- ST198 Impurity Testing



• Effect of Temperature in relationship to Impurities

- ST198 is a metal alloy getter manufactured by SAES
  - Nominal composition of 76.5% Zr and 23.5% Fe
  - Primary phase is  $Zr_2Fe$

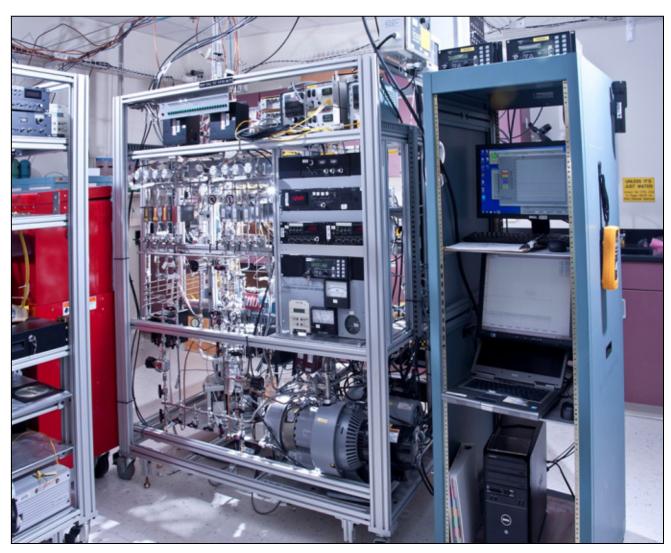
### • ST198 reacts with:

- hydrogen isotopes, oxygen, water, and other gases
- unreactive towards nitrogen.
- Each pellet is roughly 0.6 grams with a density of 5.3 g/cm<sub>3</sub>
- Useful for tritium removal from process gas streams with low tritium concentrations.
  - Removes tritium without the formation of tritiated water
  - Tritium is unrecoverable



#### **Experimental Test System**

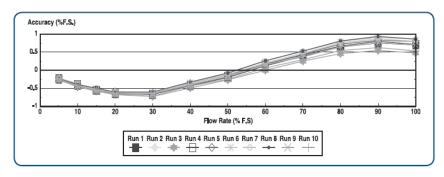
- Pressure transducers
- MKS Flow Controllers
- Gas supplies of Ar,  $N_2$ , and  $H_2$
- 2 Residual Gas Analyzers
- 1 Inficon micro GC
- Flow through testing



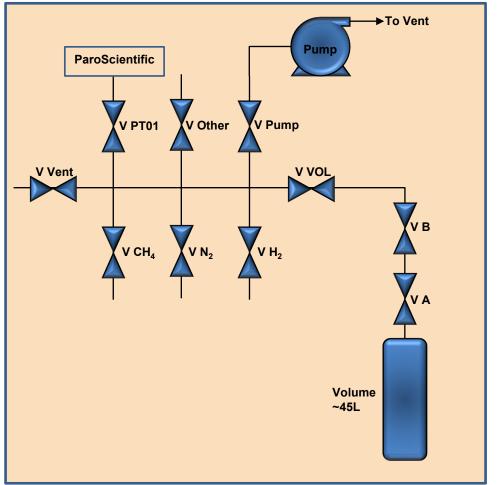
#### ST198 Test Matrix

ST198 Test	Gas Constituents (percent by volume)	Test Cell Temperature (°C)
1	1% H <sub>2</sub> , 99% N <sub>2</sub>	350
2	1% H <sub>2</sub> , 99% N <sub>2</sub>	24
3	0.1% H <sub>2</sub> , 99.9% N <sub>2</sub>	350
4	0.1% H <sub>2</sub> , 99.9% N <sub>2</sub>	24
5	0.1% H <sub>2</sub> , 0.1% CH <sub>4</sub> , 99.8% N <sub>2</sub>	350
6	$0.13\%~{ m H_2}, 0.1\%~{ m CH_{4,}}~0.1\%~{ m NH_3}, 99.67\%~{ m N_2}$	350
7	$0.13\%~{ m H_2}, 0.1\%~{ m CH_{4,}}~0.1\%~{ m NH_3}, 99.67\%~{ m N_2}$	350
8	$0.13\%~{ m H_2}, 0.1\%~{ m CH_{4,}}~0.1\%~{ m NH_3}, 99.67\%~{ m N_2}$	24
9	$0.1\%~{ m H_2}, 0.1\%~{ m CH_{4_{,}}}~0.05\%~{ m NH_{3}}, 99.75\%~{ m N_2}$	350
10	$0.1\%~{ m H_2}, 0.1\%~{ m CH_{4_{,}}}~0.05\%~{ m NH_{3}}, 99.75\%~{ m N_2}$	24
11	0.1% H <sub>2</sub> , 0.1% CO, 99.8% N <sub>2</sub>	350
12	0.1% H <sub>2</sub> , 0.1% CO, 99.8% N <sub>2</sub>	24
13	0.1% H <sub>2</sub> , 0.1% CO, 99.8% N <sub>2</sub>	24
14	0.1% H <sub>2</sub> , 0.1% CO, 99.8% N <sub>2</sub>	350
15	0.1% H <sub>2</sub> , 0.1% CH <sub>4</sub> , 99.8% N <sub>2</sub>	24

 Low concentration of impurities could not be reliably controlled with flow controllers at low flow rates

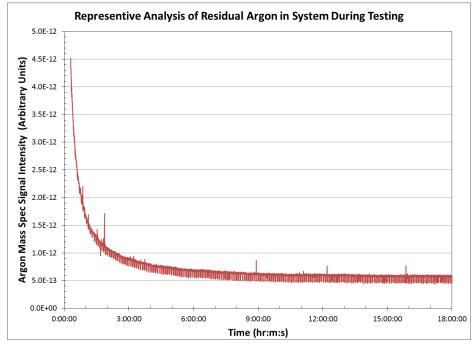


 Assembled a gas mixing manifold to prepare gas mixtures with low levels of H<sub>2</sub> and various impurities.





- Argon purge at ambient temperature to displace the residual air after activation
  - 30 sccm and ~1875 torr
- Nominal temperature ramp to 450°C for 4 hours
- Evacuation of the system for 1-2 hours to remove the residual argon



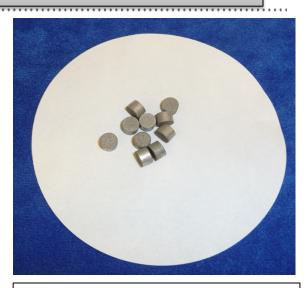
• Upon completion of the activation the sample temperature was lowered to 350°C or 24°C depending on the test protocol.

#### **Test Cell Configuration**



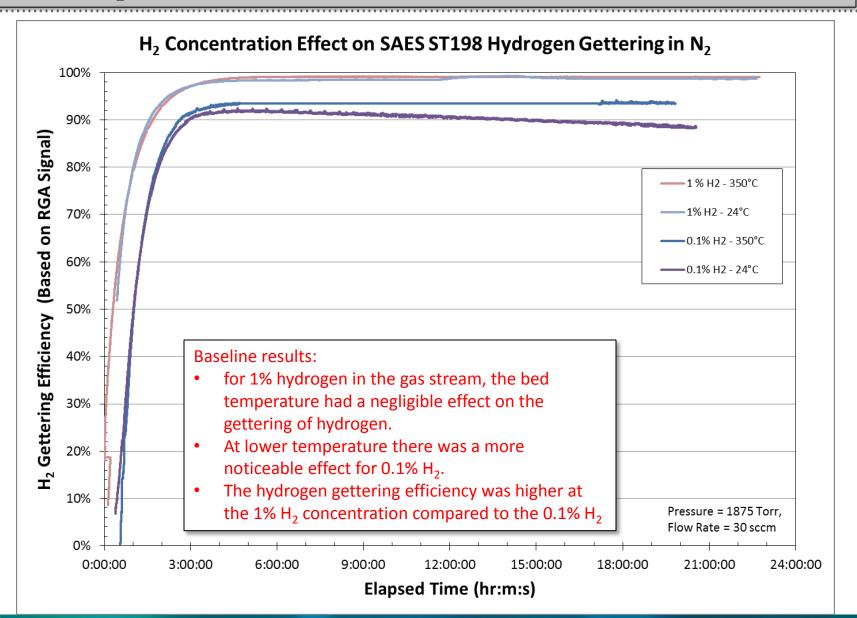
- 1/4" diameter tubing 9" long
- VCR #8 fittings
- Welded Fritted Disk up about 1/3 of the way
- Vertical Configuration



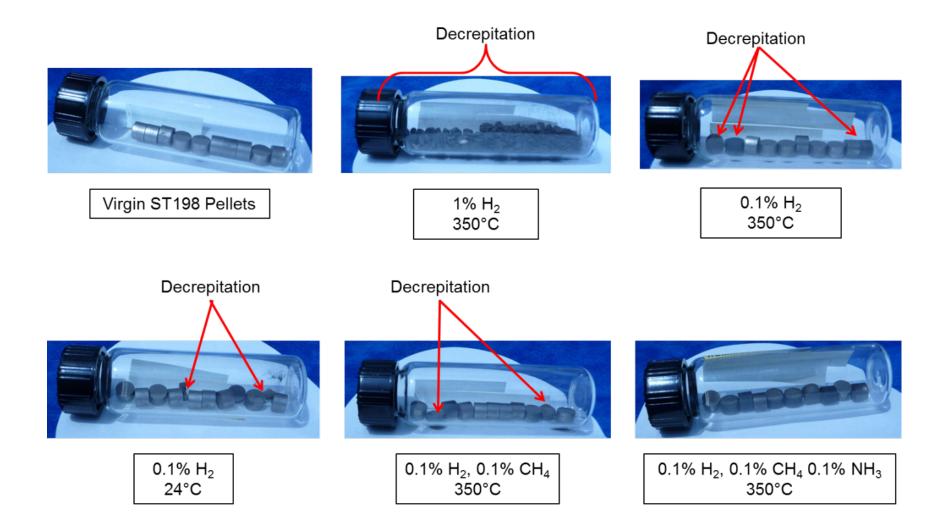


- Approximately 6 grams total
- 10 Pellets
  - Right cylinder pellets
  - 6 mm diameter x 4 mm tall
- Stacked configuration

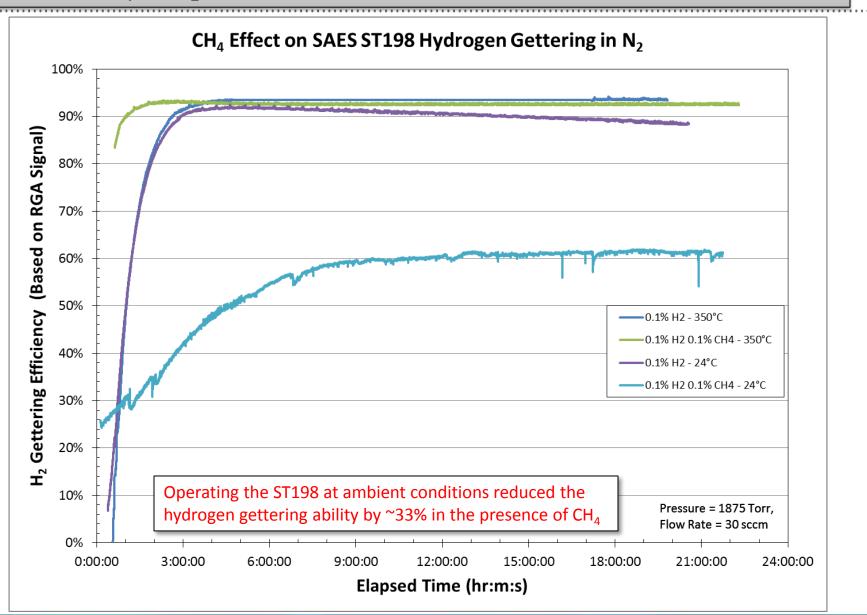




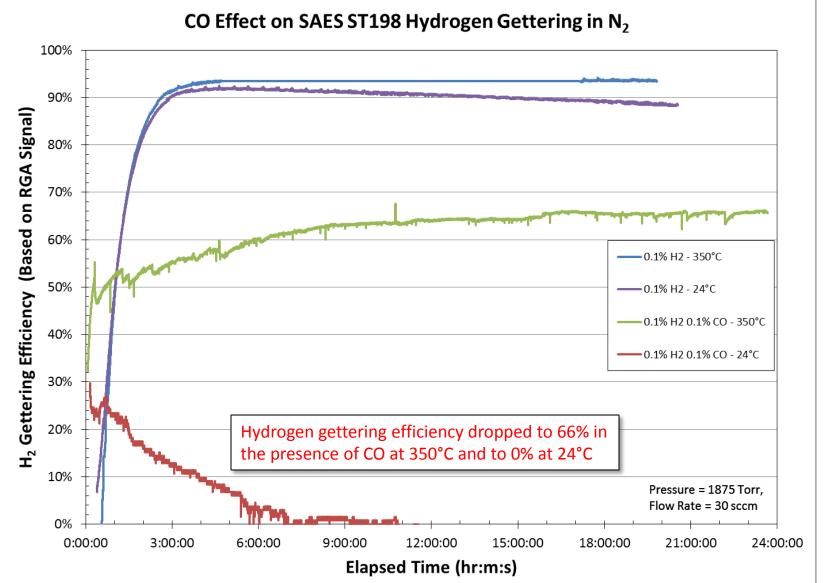
#### **ST198** Decrepitation



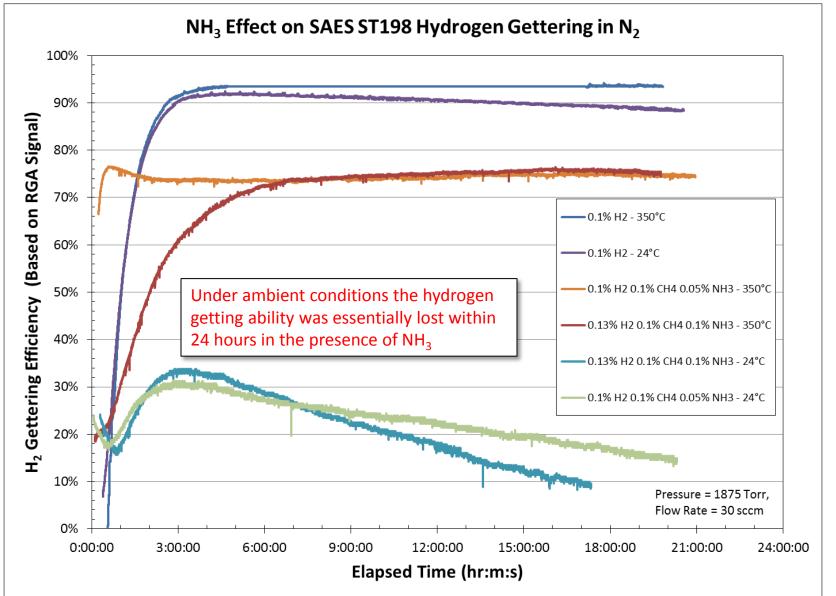
#### Effect of CH<sub>4</sub> on H<sub>2</sub> Gettering Ability of ST198



#### Effect of CO on H<sub>2</sub> Gettering Ability of ST198



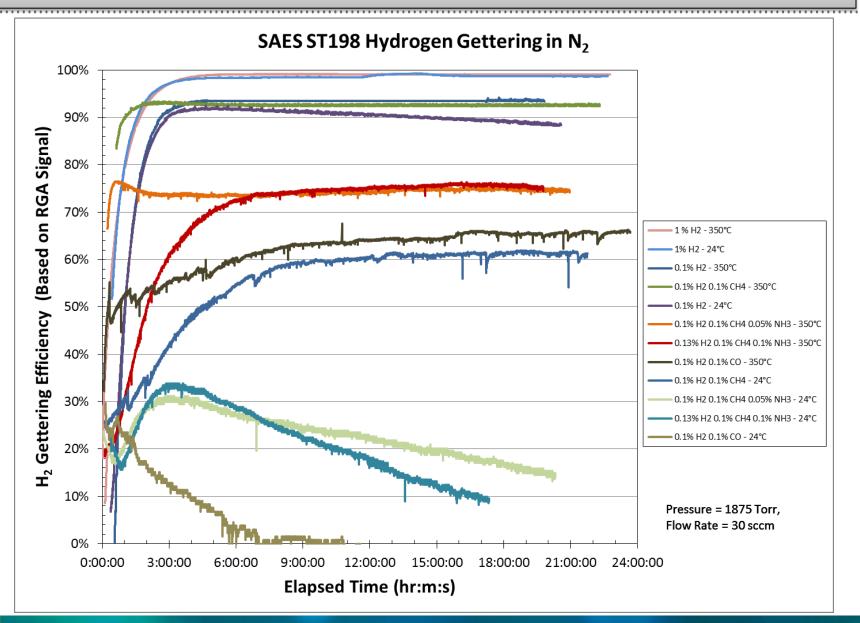
#### Effect of NH<sub>3</sub> on H<sub>2</sub> Gettering Ability of ST198



#### Effect of NH<sub>3</sub> on H<sub>2</sub> Gettering Ability of ST198

Argon Effect on SAES ST198 Hydrogen Gettering in N<sub>2</sub> 100% 5.00E-12 0.13% H2 0.1% CH4 0.1% NH3 90% 4.50E-12 0.1% H2 0.1%CH4 0.05% NH3 Argon Mass Spec Signal Intensity (arbitrary Units) Ar in 0.1% NH3 mix Test 4.00E-12 Ar in 0.05% NH3 mix Test 3.50E-12 Pressure = 1875 Torr Flow rate = 30 sccm Temp = 24°C 3.00E-12 2.50E-12 The presence of residual Ar in the test system caused a slight delay in the deactivation of the 2.00E-12 ST198 by NH<sub>3</sub> 1.50E-12 1.00E-12 10% 5.00E-13 0% 0.00E+00 0:00:00 3:00:00 6:00:00 9:00:00 12:00:00 15:00:00 21:00:00 24:00:00 18:00:00 Time (hr:m:s)

#### **Alternative Getter Materials - Summary**



- 1% hydrogen in the gas stream bed temperature negligible effect
- At ambient conditions impurities compromised ST198 hydrogen gettering ability to a greater extent than at higher temperatures.
- Experiments showed only a slight reduction of gettering ability with the addition of methane (CH<sub>4</sub>) at 350°C.
- At ambient temperature conditions, the hydrogen gettering efficiency was reduced by 33% in the presence of CH<sub>4</sub>.
- Reduction of hydrogen gettering with carbon monoxide at both temperatures.
  - Reduction of hydrogen gettering capability dropped ~29% for the tests at 350°C (compared to baseline capabilities as related to the reduction of the RGA signal from the mass spectrometer).
  - At ambient conditions, the hydrogen gettering effectiveness was reduced to zero within 10 hours upon contact with CO.
- At ambient temperature, ammonia also reduced the hydrogen gettering efficiency but to a lesser extent than the CO.



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# Thanks for your attention!!



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