MODULAR CONNECTION TECHNOLOGIES FOR SC WALLS OF SMRs

Sep 29, 2015

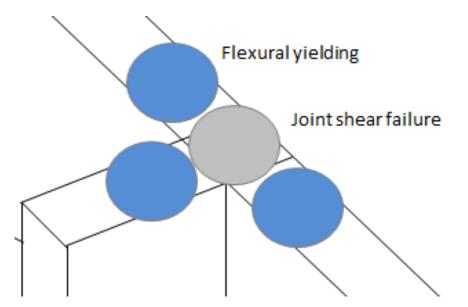
Amit H. Varma, Jungil Seo, Tom Bradt Purdue University

OUTLINE

- SC Wall-to-Wall T Connection
- SC Wall-to-Wall L Connection
- Benchmarking Analysis
- SC Slab-to-Wall Connection
- Findings

SC WALL-TO-WALL T CONNECTION *DESIGN PHILOSOPHY*

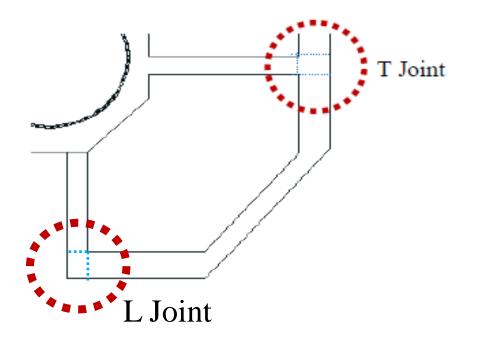
- Full-strength connection design philosophy
 - Develops the expected strength
- Implementation of full-strength design
 - Two parts in SC wall joints
 SC wall and SC wall joints
 - Desired failure mode
 - Flexural yielding (ductile) plastic hinges



SC WALL-TO-WALL T CONNECTION *DESIGN PHILOSOPHY*

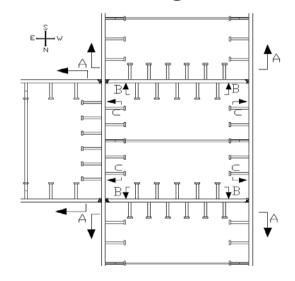
- SC wall-to-wall joints in the CIS
 - Common joint configurations (T and L)
- Implementation of full-strength design
 - The required joint shear strength
 Based on the force transfer mechanism
 - Calculation of the available joint shear strength
 - ACI 349-06 equation
 γ = 12 for SC wall T-joints
 γ = 8 for SC wall L-joints
 Verification is required

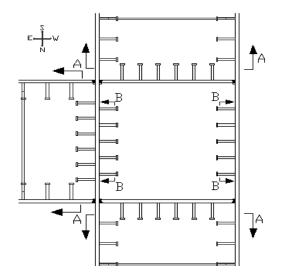
$$V_n = \gamma \sqrt{f_c'} A_j$$



- Four full-scale SC wall T-joint shear specimens
 - T = 30 in.
 - To evaluate the influence of (i) the shear reinforcement ratio and (ii) The steel headed stud layout
 - Designed to undergo joint shear failure

SpecimenSteel faceplate thickness, t_p (in.)		Steel tie plate dimension		No. of tie	Shear
		Continuous SC wall	Discontinuous SC wall	plates in the Joint	Stud Layout
JS-T1-F	0.75	$3^{3}/_{4} \ge 5/_{16}$ in.	$3^{3}/_{4} \times 1^{1}/_{2}$ in.	1	F
JS-T0-F	0.75	$3^{3}/_{4} \ge 5/_{16}$ in.	$3^{3}/_{4} \times 1^{1}/_{2}$ in.	0	F
JS-T0-P	0.75	$3^{3}/_{4} \ge 5/_{16}$ in.	$3^{3}/_{4} \times 1^{1}/_{2}$ in.	0	Р
JS-T2-F	0.75	$3^{3}/_{4} \ge 5/_{16}$ in.	$3^{3}/_{4} \times 1^{1}/_{2}$ in.	2	F

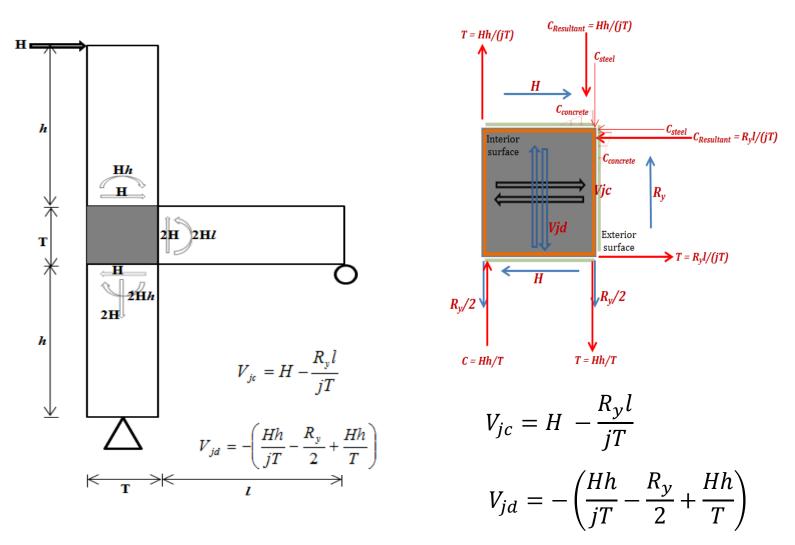




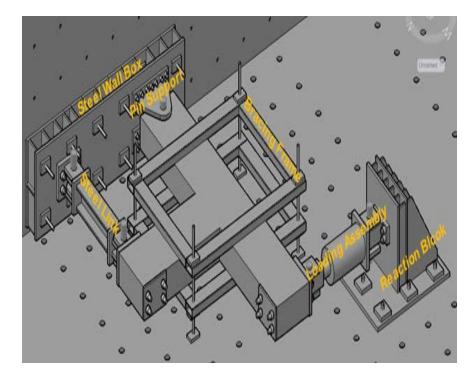
o Material properties

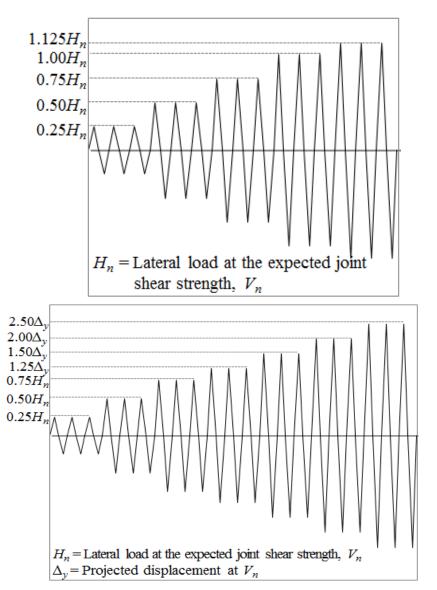
Cassimon	Faceplates		Tie plates		Studs	Concrete, psi
Specimen	F _y , ksi	F _u , ksi	F _y , ksi	F _u , ksi	F _u , ksi	
JS-T1-F	58.6	83.9	60.4	69.1	74.0	6,473
JS-T0-F	58.0	77.0	62.7	73.5	80.9	6,402
JS-T0-P	58.0	77.0	62.7	73.5	80.9	6,502
JS-T2-F	58.5	78.6	62.7	73.5	80.9	6,504
						Avg = 6,502

o Boundary conditions and joint shear force terms





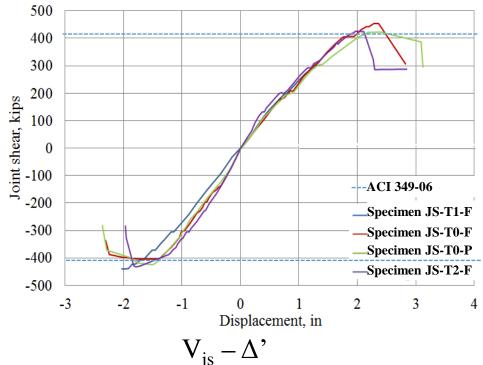




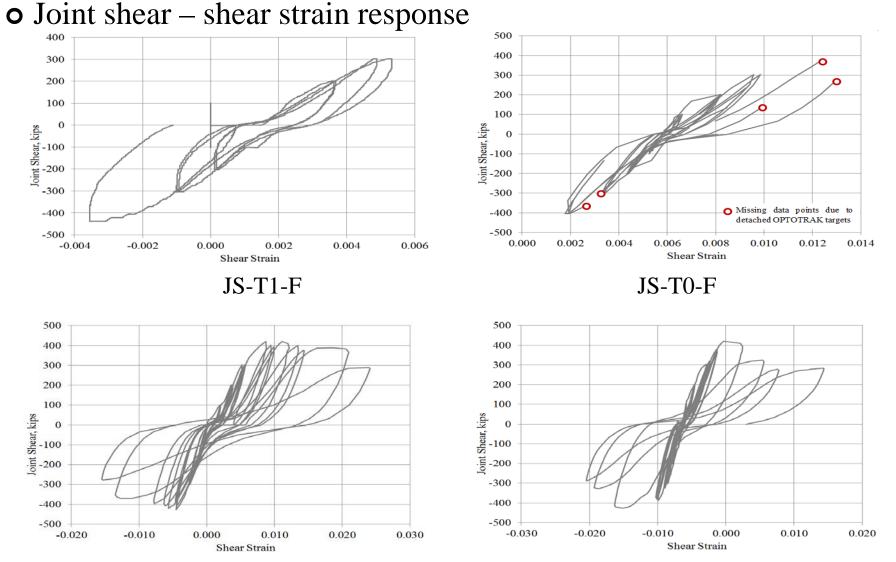
• Summary of experimental results

Specimen	Ultimate joint shear, kips	Shear strain at the ultimate joint shear	Governing failure mode	Event order in the Joint region
JS-T1-F	438.4	0.0049	Joint shear	Concrete crack ↓ Yielding of steel tie plate ↓ Extensive concrete cracking
JS-T0-F	455.5	0.0070	Joint shear	Concrete crack ↓ Extensive concrete cracking
JS-T0-P	427.8	0.0069	Joint shear	Concrete crack ↓ Extensive concrete cracking
JS-T2-F	431.6	0.0060	Joint shear	Concrete crack ↓ Yielding of steel tie plates ↓ Extensive concrete cracking

o Joint shear – displacement response



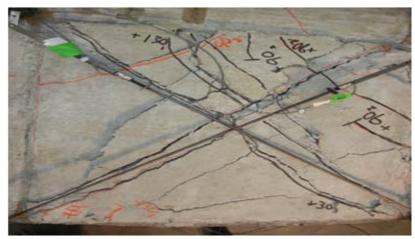
- V_{njs}^{TEST} within the range of 426.7 454 kips
- Greater than $V_{njs}^{ACI-exp}$ (413 kips) by 3.1 10.3%.



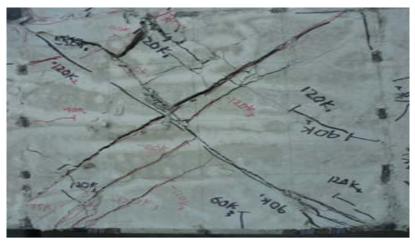
JS-T0-P

JS-T2-F

• Crack pattern at the ultimate joint shear : all specimens

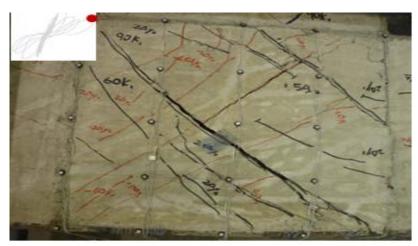


JS-T1-F



JS-T0-F





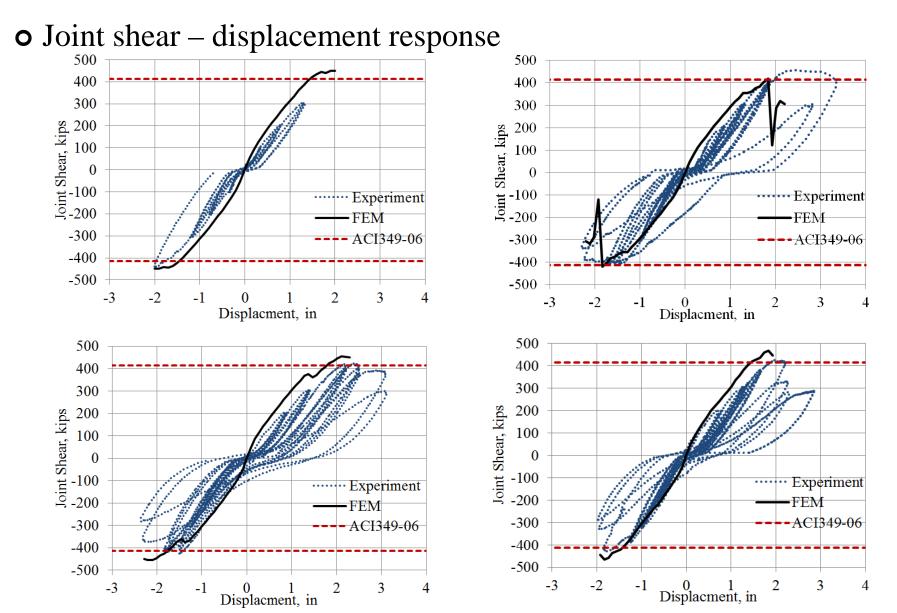
JS-T2-F

JS-TO-P

SC WALL-TO-WALL T CONNECTION *Benchmarking Analysis*

- 3-D FE analysis for additional insights
- Comparison with experimental results
- ABAQUS explicit
 - The quasi static analysis
 - Shell (S4R) elements for steel, solid (C3D8R) elements for concrete, and Timoshenko beam elements (B32) for stud
 - Connector elements (CONN3D2)
- CEF concrete model
 - Elastic in compression, Uniaxial tension strength and post-peak behavior defined in CEB-FIP mc 90 (1993)
 - Element deletion to prevent excessive deformation
- Steel material model
 - Multi-axial plasticity theory
 - Idealized uniaxial stress-strain curve

SC WALL-TO-WALL T CONNECTION *Analysis Results*



SC WALL-TO-WALL T CONNECTION *Benchmarking Analysis*

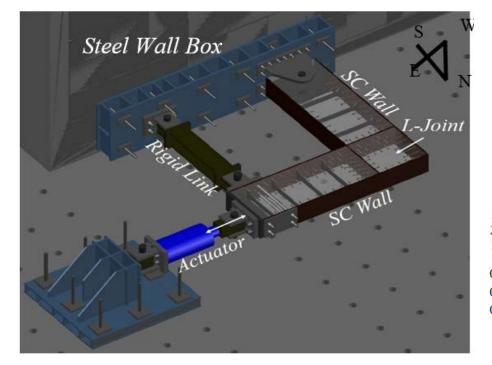
o Summary

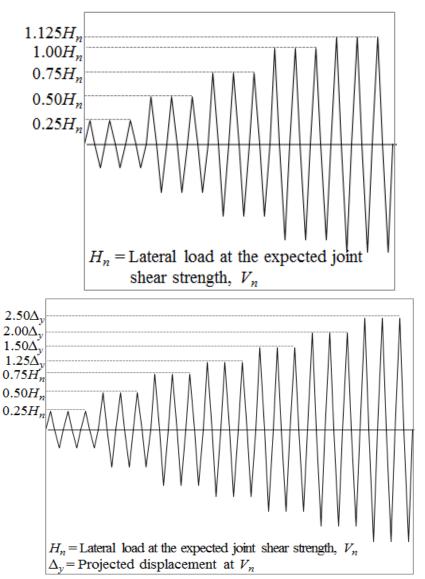
Specimen	Ultimate joint shear, kips	Shear strain at the ultimate joint shear	Governing failure mode	Event Order in the Joint region
JS-T1-F	450.0	0.0157	Joint shear	Concrete crack ↓ Yielding of steel tie plate ↓ Extensive concrete cracking
JS-T0-F	418	0.0142	Joint shear	Concrete crack ↓ Extensive concrete cracking
JS-T0-P	455.4	0.0164	Joint shear	Concrete crack ↓ Extensive concrete cracking
JS-T2-F	465.6	0.0147	Joint shear	Concrete crack ↓ Yielding of steel tie plates ↓ Extensive concrete cracking

- One full-scale SC wall L-joint shear specimens
 - T = 30 in.
 - To experimentally investigate the joint shear behavior of SC wall-towall L joint
 - The same specimen design approach and test procedure from SC wall-to-wall T joint specimens

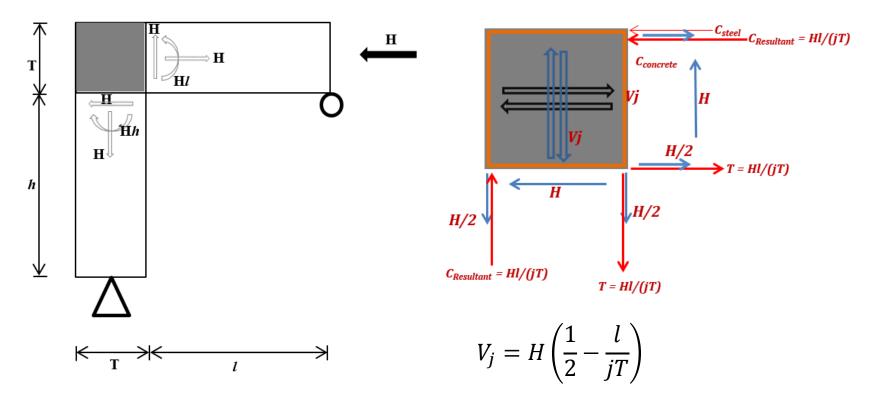
		Steel tie plat	te dimension	No. of tie	Shear
Specimen	Steel faceplate thickness, t _p (in.)	Continuous SC wall	Discontinuous SC wall	plates in the Joint	Stud Layout
JS-L-T0-F	0.75	$3^{3}/_{4} \ge 5/_{16}$ in.	$3^{3}/_{4} \times 1^{1}/_{2}$ in.	0	F

• Test-setup and loading protocol

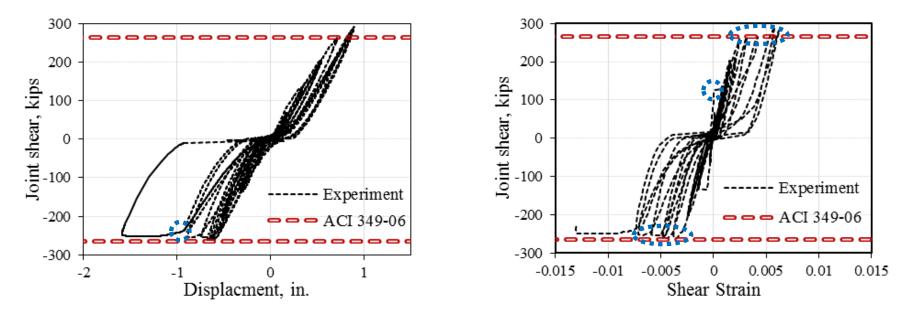




o Boundary conditions and joint shear force terms



o Joint shear – displacement response



Ultimate	Shear strain	Governing	Event order in the Joint region
joint shear, kips	at the ultimate joint shear	failure mode	
261.7 (-) 290.3 (+)	- 0.0071 (-) 0.0089 (+)	Joint Shear Failure	$\begin{array}{c} \text{Concrete crack} \\ \downarrow \\ \text{Extensive concrete cracking} \\ \downarrow \\ \text{Yielding of diaphragm plates} \end{array}$

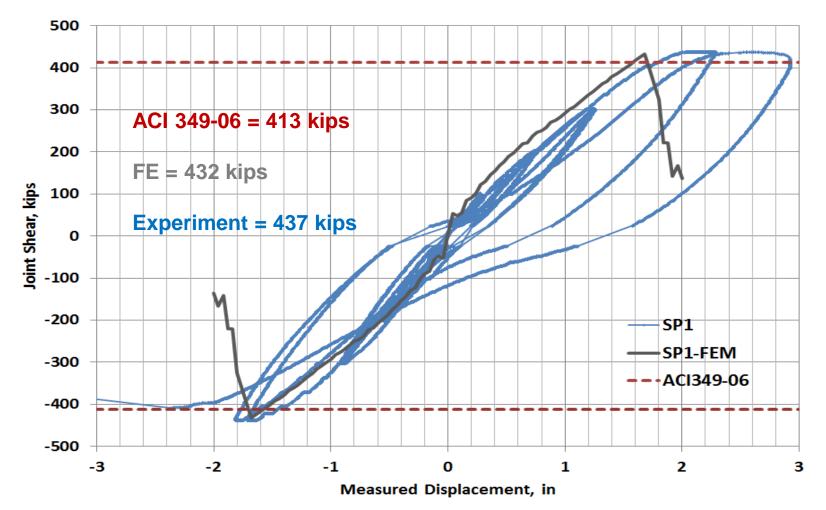
 $V_{njs}^{TEST} = 276 \text{ kips}$ $V_{njs}^{ACI-exp} (262.7 \text{ kips})$

• Crack pattern at the ultimate joint shear

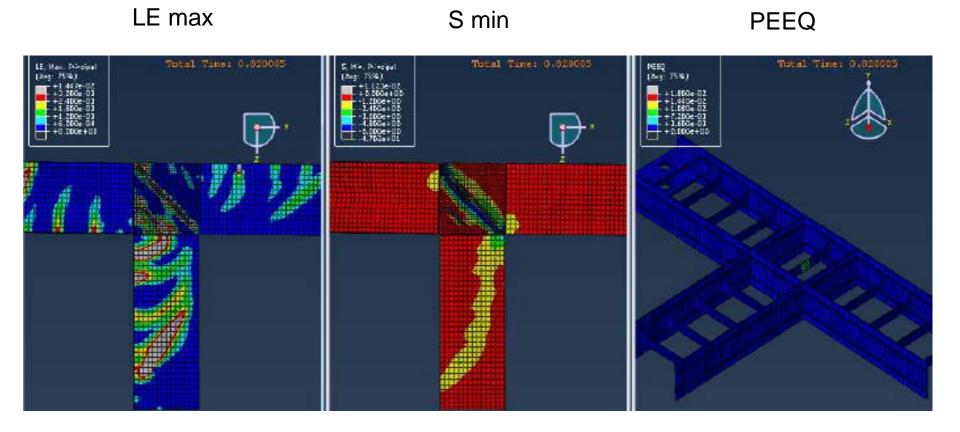


JS-L-T0-F

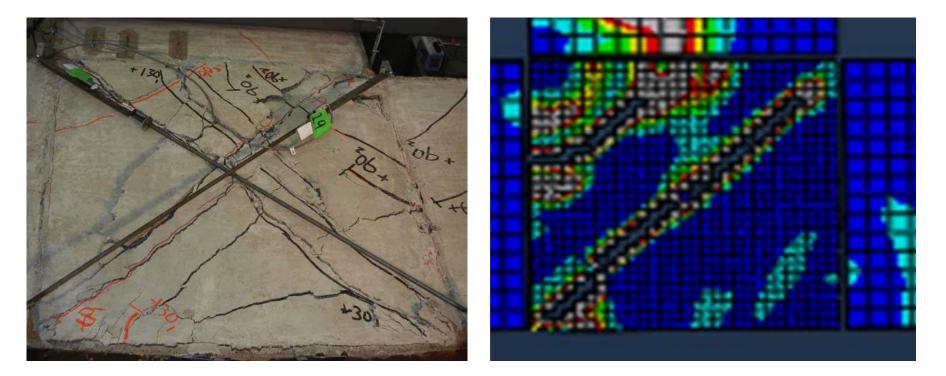
- Analysis results Specimen JS-T1-F
 - Joint shear displacement response



- Analysis results Specimen JS-T1-F
 - Stress and strain distribution

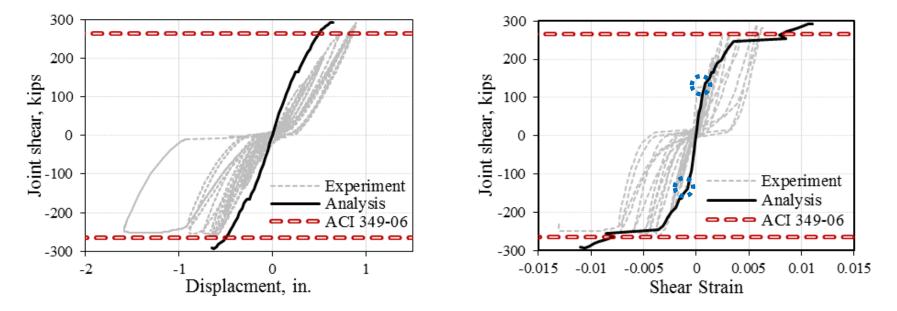


- Analysis results Specimen JS-T1-F
 - Crack pattern



• Analysis results – Specimen JS-L-TO-F Joint shear – displacement response Join

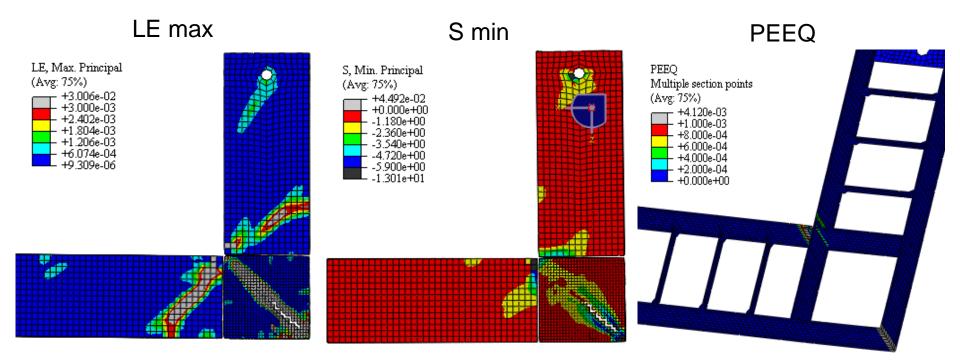
Joint shear – shear strain response



• $V_{js}^{ACI349-06} = 262.7 \text{ Kips (1.17MN)}$ • $V_{js}^{FEM} = 292.3 \text{ Kips (1.3 MN) (+ 29.6 kips)}$ • $V_{js}^{Exp} = 276 \text{ Kips (1.22 MN) (+ 13.3 kips)}$ • Joint shear failure

• Analysis results – Specimen JS-L-T0-F

• Stress and strain distribution

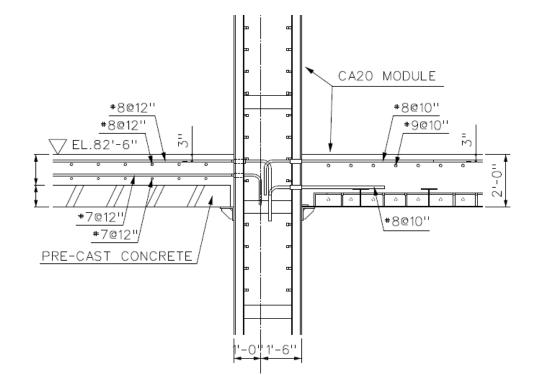


- Background
 - Existing design recommendations and aids for RC slab (column) to slab connections
 - No existing design recommendation for SC slab-to-wall connection
 - The applicability of existing code provisions for RC slab (column) to slab connection on SC slab-to-wall connection

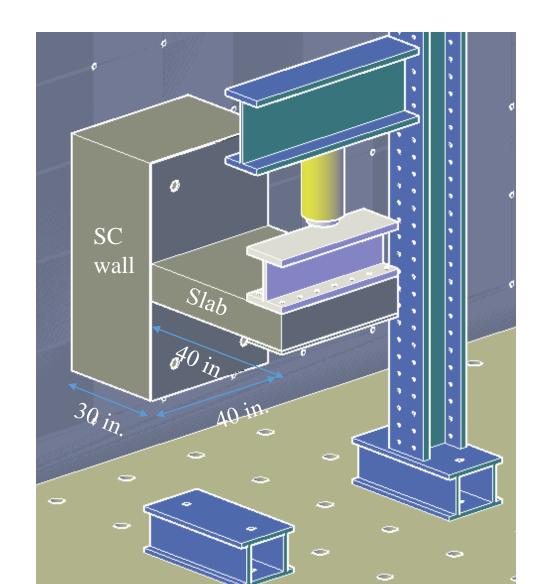
o Design philosophy

- The full strength connection design philosophy
- The connection region should not be the weakest point
- Capability of transferring both shear and flexural demand

- Test parameters
 - Slab type : RC or half SC (HSC)
 - Rebar : rebar type (Hooked bar or T headed rebar), Reinforcement ratio, Embedded length, and Rebar location in the SC wall portion



o Test setup



FINDINGS

o SC wall-to-wall T connection test

- The joint shear failure mode for all test specimens
- No significant effects of the shear reinforcement ratio and the steel headed stud layout
- V_{njs}^{TEST} within the range of 426.7 kips 454 kips Greater than $V_{njs}^{ACI-exp}$ (413 kips) by 3.1% 10.6%
- The ACI 349-06 (2006) code equation is applicable and conservative for estimating the joint shear strength of SC wall-to-wall T joints with γ of 12
- SC wall-to-wall L connection test
 - The joint shear failure mode
 - V_{njs}^{TEST} of 261.7 kips close to $V_{njs}^{ACI-exp}$ (262.7 kips)
 - The ACI 349-06 (2006) code equation is applicable for estimating the joint shear strength of SC wall-to-wall L joints with γ of 8

Publications

 Seo, J., Varma, A.H., and Winkler, D. (2013). "Preliminary Investigations of the Joint Shear Strength of SC Wall-to-Wall T-Joints." Transactions of SMiRT 22, IASMIRT, NCSU, Raleigh, NC, pp. 1-10.

http://www.iasmirt.org/transactions/22/Pap_863_ver_3.pdf

 Seo, J., and Varma, A.H. (2015). "Behaviour and Design of Corner or L-Joints in SC Walls." Transactions of SMiRT 23 in Manchester, UK, Paper ID 695, IASMIRT, North Carolina State University, Raleigh, NC, pp. 1-10, <u>http://smirt23.uk/attachments/SMiRT-23_Paper_695.pdf</u>