

# Permeation, Diffusion, Solubility Measurements: Results and Issues

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# Presentation Outline

- **Project Objectives**
- **ORNL Activities**
- **SRNL Activities**
- **UIUC Activities**
- **Plan for FY08 and future**
- **Conclusion**

# Research Objectives

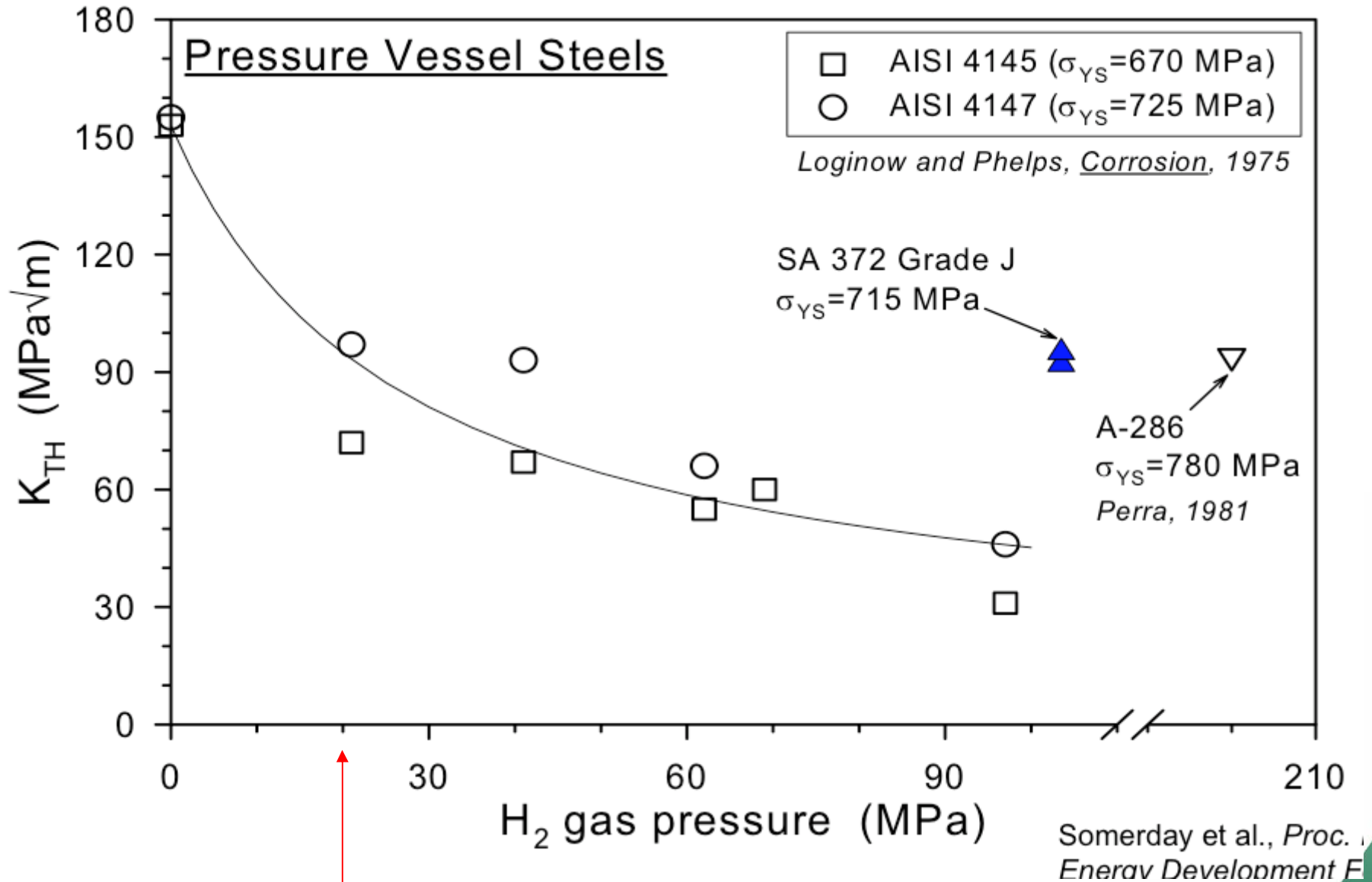
- **To understand the hydrogen transport behavior**
  - How does gaseous hydrogen enter material (absorption)?
  - How fast does hydrogen move inside material (diffusion)?
  - How much hydrogen is there in material (solubility)?
- **Under conditions relevant to hydrogen delivery infrastructure**
  - Gaseous hydrogen: composition and purity level
  - Pressure range: up to 10,000psi H<sub>2</sub>
  - Temperature range: -40 to 150C
  - Service life: 50 years and beyond
  - **Material**
    - Pipeline steels and their weld
    - Polymer/composite pipeline
  - **Surface condition**
    - Naturally formed surface oxide layer
    - Surface coating/modification
    - Others
  - Others



# Needs for Hydrogen Transport R&D

- **Steel pipeline infrastructure**
  - Mechanical property degradation due to hydrogen embrittlement
- **Polymer/composite pipeline infrastructure**
  - Permeation rate/leak resistance

# Degradation of Fracture Toughness as Function of H<sub>2</sub> Pressure



3000psi



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# Hydrogen Embrittlement

- **The degree of HE depends on hydrogen pressure (hydrogen concentration) for many metallic materials (including high-strength steels).**
- **Successful application of steels for hydrogen storage relies on systematic engineering design so that the system operates under the threshold with a safety margin**
  - **Need to quantify the degree of mechanical property degradation as function of hydrogen pressure (concentration), microstructure and temperature**

# So We Need to Learn the Following from Hydrogen Transport Study

- **Hydrogen solubility/concentration in steel**
  - Influences the degree of mechanical property degradation
- **Hydrogen diffusivity**
  - Influences crack propagation rate - the kinetics
- **Hydrogen absorption/surface effect**
  - Influences amount and rate of hydrogen entering steel
- **Hydrogen transport knowledge will be needed for**
  - Safe operation of hydrogen pipeline infrastructure
  - Laboratory mechanical property testing



# Prior R&D on Hydrogen Transport

- **Abundant data under electrochemical charging and at low pressure (< 1atm)**
- **Very limited data exists for high-pressure gaseous hydrogen in “real-world” pipeline environment**
  - **Surface absorption kinetics**
  - **Diffusivity**
  - **Solubility**
  - **Others**



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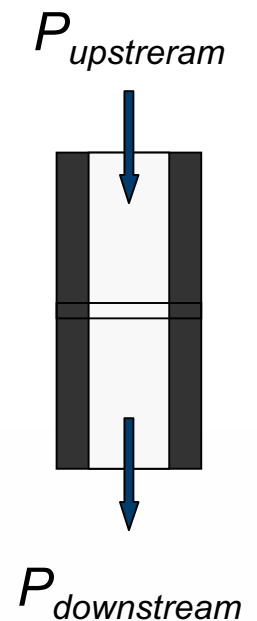


# How do We Study Hydrogen Transport Behavior?

- **Primary method**
  - Hydrogen gas permeation experiment
- **Other techniques**
  - Hydrogen traps: thermal desorption spectroscopy
  - Diffusible hydrogen concentration
    - Gas chromatography
    - Fluid displacement methods (glycerin, silicon oil, mercury)
  - Total hydrogen concentration:
    - Thermal extraction
    - Gas chromatography
- **Microstructure characterization**
- **Surface analysis**
- **Isotopic exchange with depth profiling**

# Permeation Test Principle

- Gaseous hydrogen on the upstream side (charging side) is maintained at pre-determined pressure
- Hydrogen atoms/protons diffuse through the test sample, and are collected in the downstream side to determine the permeation rate
- Determination of hydrogen permeated through the sample
  - Record H<sub>2</sub> pressure increase in a constant volume chamber recorded as function of time (ORNL)
  - Ion pump and gas chromatography (SRNL, UIUC)



# What really happens in a permeation test

- Involves several major steps

- On entrance surface:

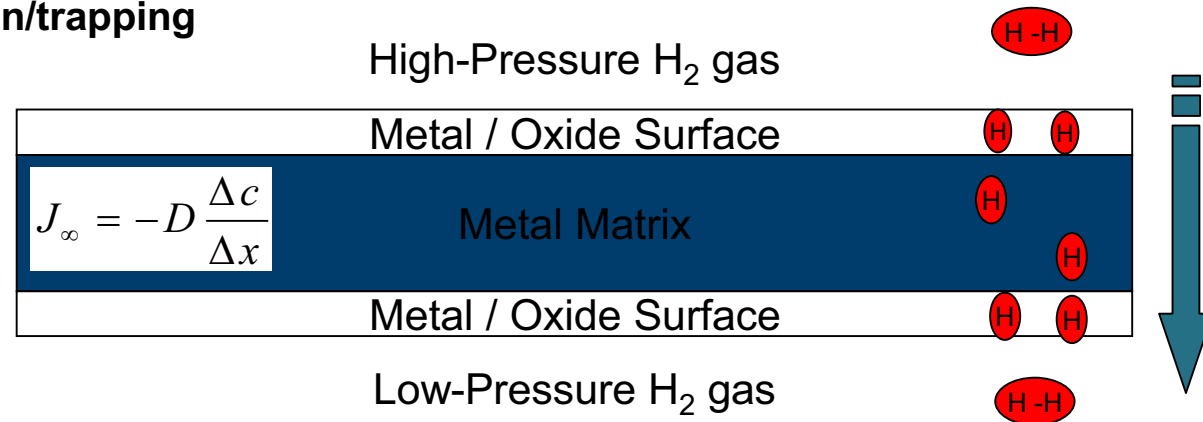
- Hydrogen molecule adsorption/trapping
    - Hydrogen dissociation
    - Hydrogen dissolution

- Within metal

- Hydrogen diffusion
    - Hydrogen trapping

- On exit surface

- Hydrogen recombination
    - Hydrogen desorption



$$J_{\infty} = -D \frac{\Delta c}{\Delta x}$$

- In order to determine hydrogen diffusion in bulk metal, the surface processes must be controlled and their influence on the kinetics (rate of permeation) must be minimized or separated

- If  $J_{\text{surface}} \ll J_{\text{bulk}}$  (i.e. rate at surface dominate), then  $J_{\text{measure}} = J_{\text{surface}}$  and diffusivity of metal cannot be determined reliably

- Once the bulk diffusivity is understood, separate tests can be performed to specifically study the surface effects on hydrogen transport in metal.



# Permeability

- **Permeability: the rate of hydrogen flux passing through the material**

$$J = P \frac{\sqrt{\Delta p_{H_2}}}{l}$$

- **In this study, permeability is determined after the flux reaches steady-state**

$$P = J_{ss} \frac{l}{\sqrt{\Delta p_{H_2}}} \quad \left( \frac{\text{mole}}{\text{cm sec psi}^{1/2}} \right)$$



# Determination of “Effective” Diffusivity and Solubility from Permeation Test

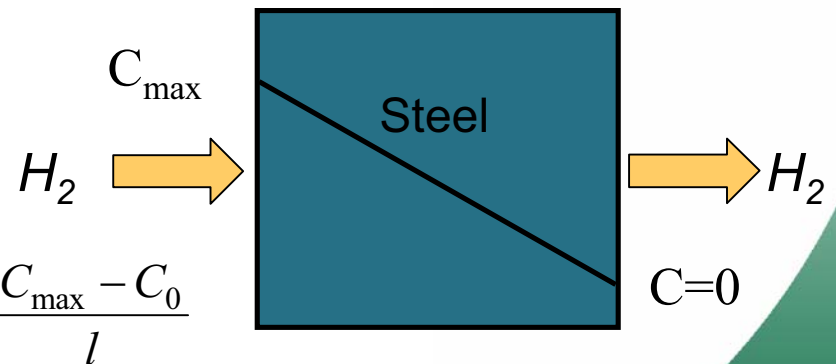
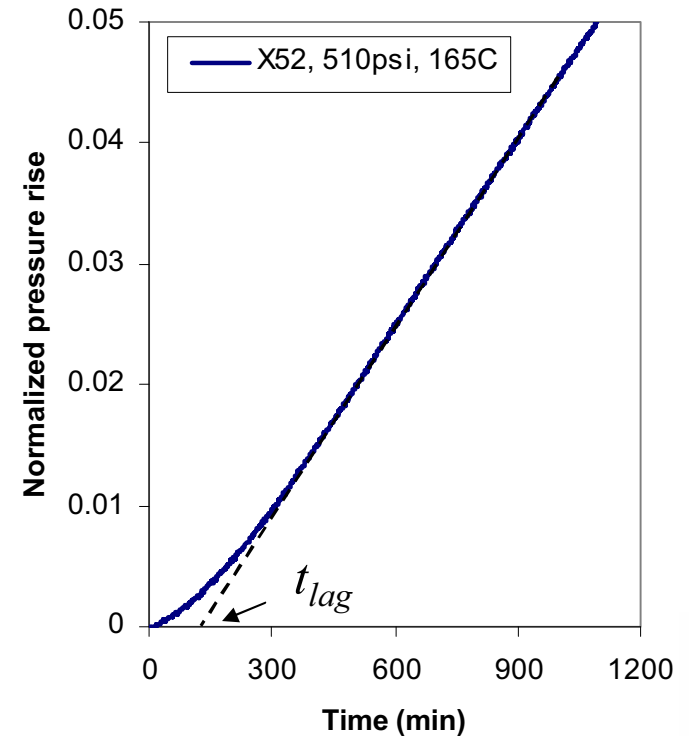
- ASTM G148-97 (for electrochemical charging)
- Basic assumptions:
  - Diffusivity is independent of H concentration
  - Surface processes are so fast that the permeation rate is control by the bulk diffusion process in metal
- “Effective” diffusivity is determined from the accumulated pressure vs time curve using the asymptotic slope method

$$D_{eff} = l^2 / 6t_{lag}$$

- Atomic hydrogen concentration on the upstream surface (max concentration or solubility) is determined from the steady state permeation rate and diffusivity:

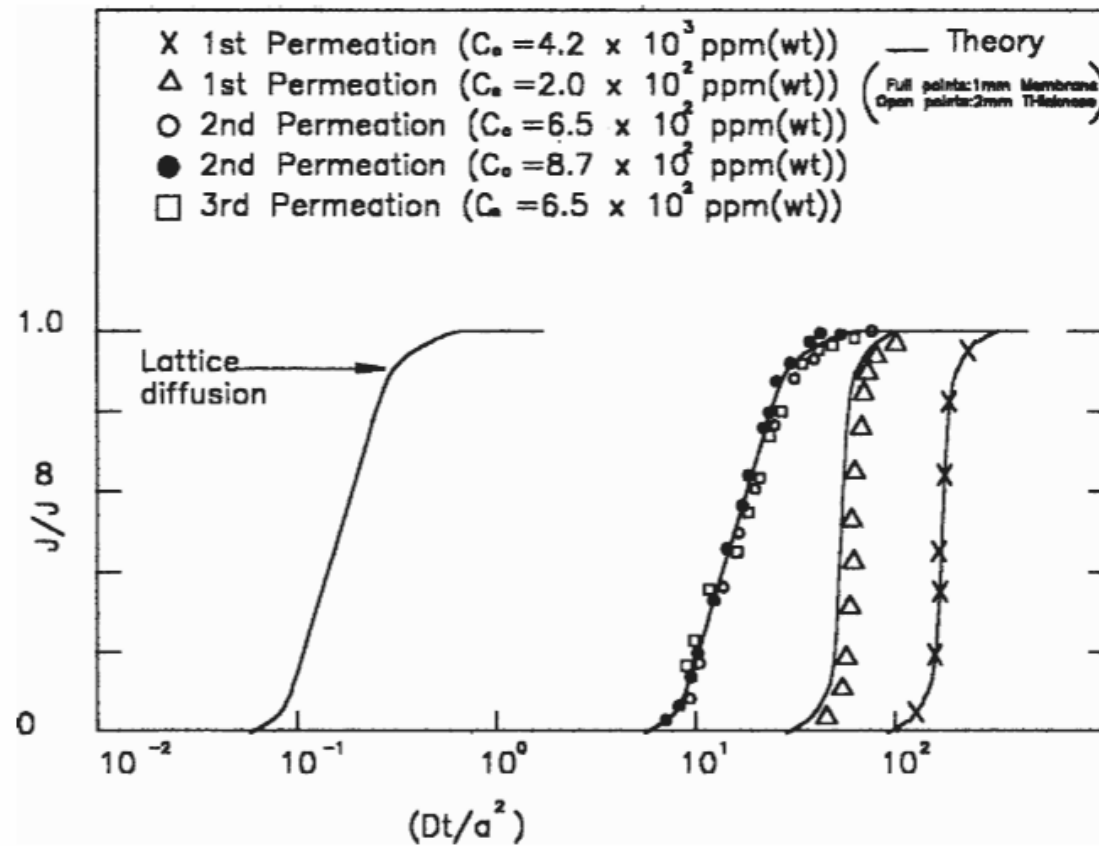
$$C_{max} = J_{ss} \frac{l}{D_{eff}}$$

$$J_{ss} = D_{eff} \frac{C_{max} - C_0}{l}$$



# Effect of Hydrogen Traps on Permeation Measurement (ATMS G148-97)

ASTM G 148 - 97 (2003)

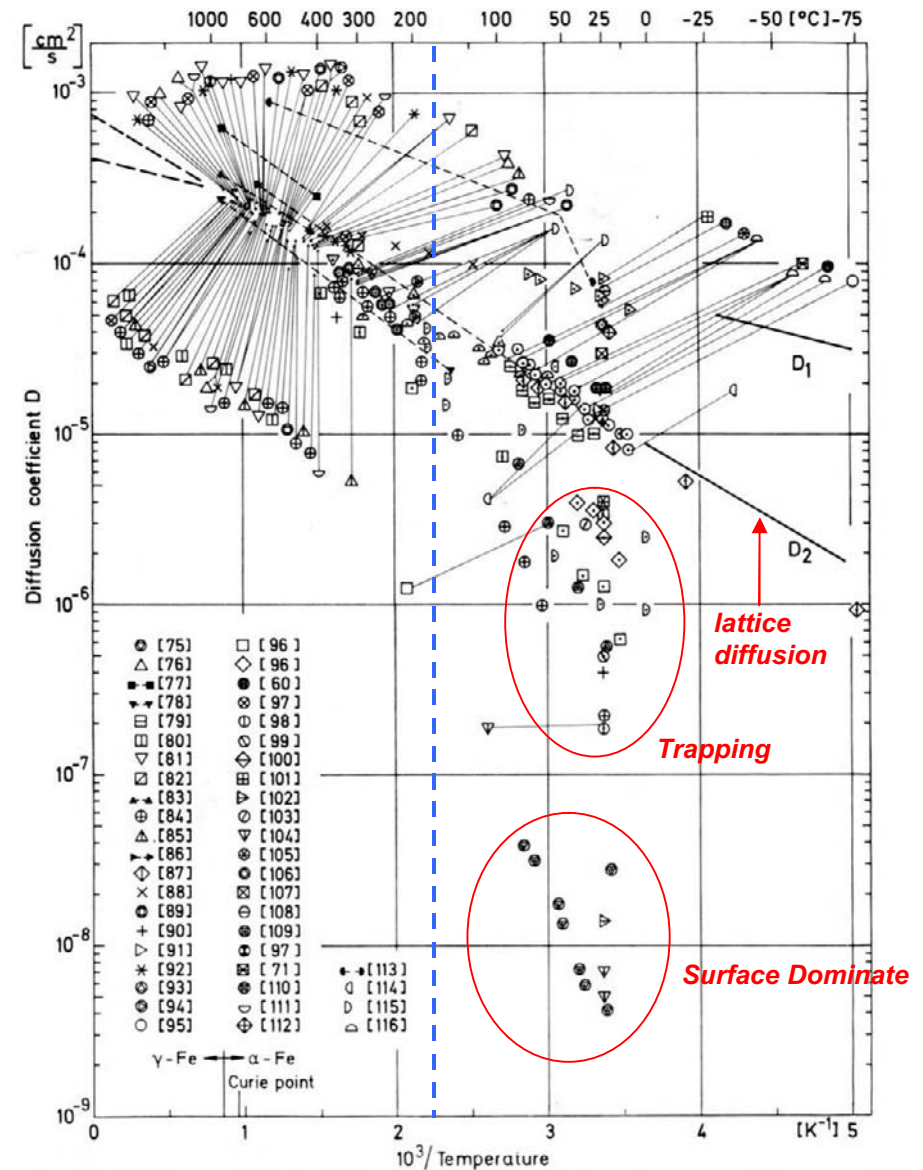


NOTE 1—Rising permeation transients for BS 970 410S21 stainless steel in acidified NaCl at 77°C. Results show irreversible trapping (1<sup>st</sup> transient) and dependency on charging conditions ( $C_0$  value). Note the time of delay and steepening of the curves relative to lattice diffusion (Fick's law), the similarity of second and third transients and the independence of thickness.

FIG. 3 Permeation Transients

# Diffusivity Data in the Open Literature

- High temperature (>100C):
  - low pressure (< 1atm) gas permeation measurement
- Low temperature (<100C):
  - Low pressure gas permeation
  - Electrochemical charging permeation
  - Permeation from acid
- Mostly under “controlled” laboratory surface conditions
  - Clean, polished surface
  - Surface coating (Pd) to eliminate surface effects (per ASTM G148)
- Hydrogen will permeate through pipeline steel during long-term (>20 years) service





# Hydrogen Diffusivity of Micro-Alloyed Steels and Low-Carbon Steels

(Boellinghaus et al., "A scatterband for hydrogen diffusion coefficients in micro-alloyed and low-carbon structure steels" *Welding in the World* v.35n2 83-96)

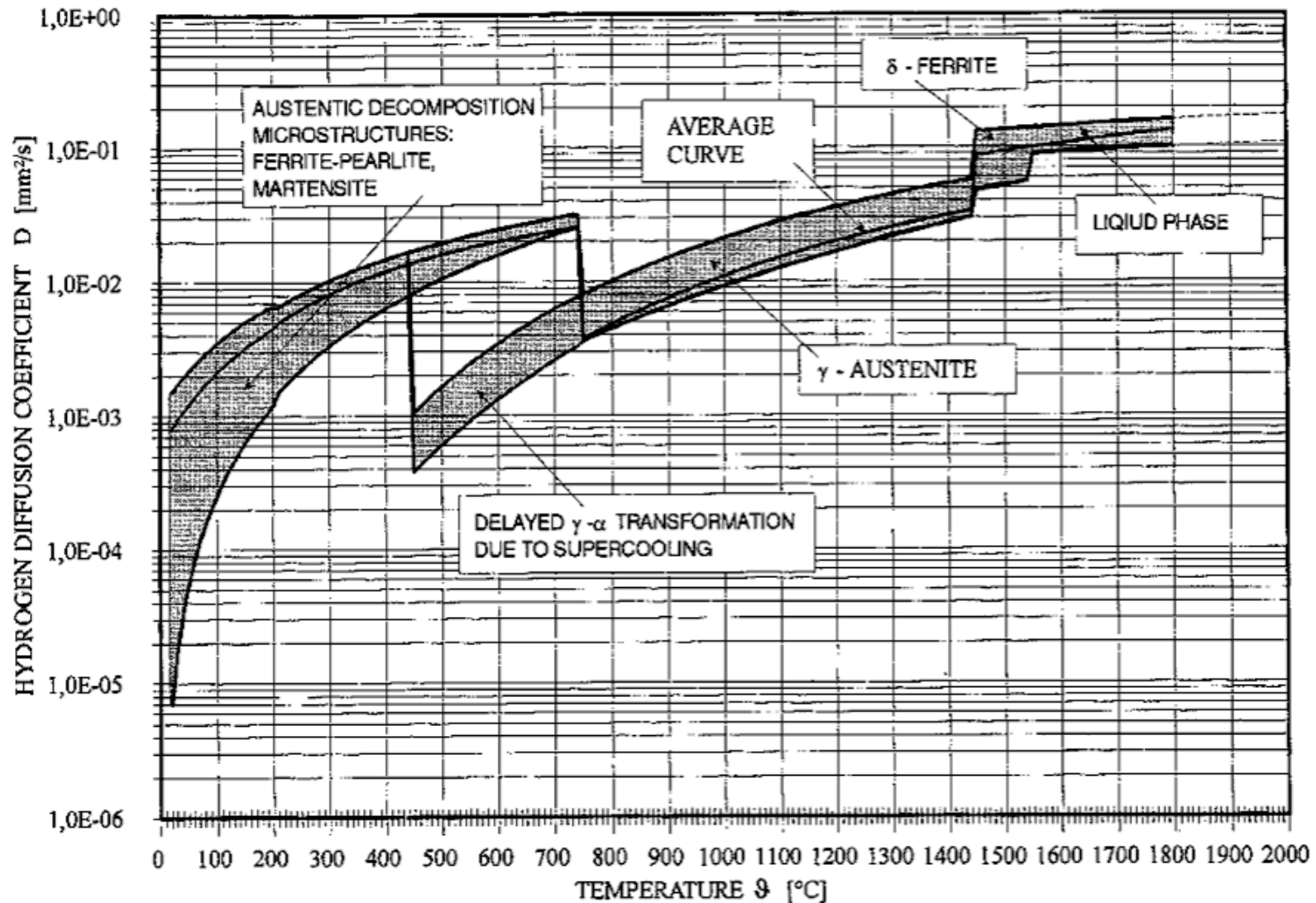


Fig. 13. Scatterband for hydrogen diffusion coefficients in micro-alloyed and low carbon structural steels



# ORNL Progress and Status

- **High-pressure hydrogen permeation test**
  - System upgrade
  - System verification test with Pd
    - Confirm high-pressure hydrogen permeation measurement system and testing procedure
  - Baseline permeation tests with pure Iron
    - Test procedure development
    - Temperature effect
    - Pressure effect
    - Surface effect
    - Data reduction procedure
  - Permeation measurement for polymers
  - Interactions with other permeation test groups

# System Upgrade

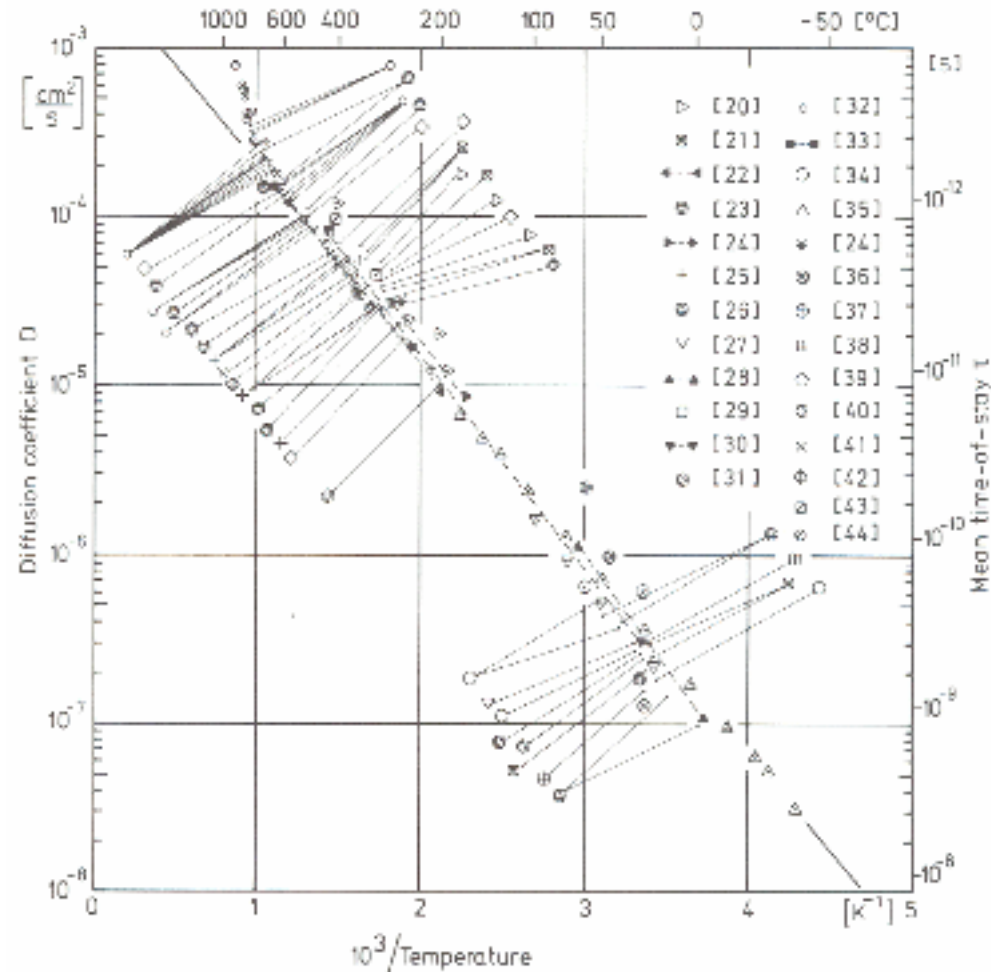
- **Improved temperature control below 300°C**
  - Low temperature control was essential for HE in steel and polymer composites
  - Verified long-term stability/accuracy: 0.2-0.3°C
- **Improvement on low pressure measurement sensitivity and accuracy to 0.1 torr (0.002psi)**
  - Essential for detection of break-through time and determination of diffusivity



**SRNL**



# System Verification: Palladium



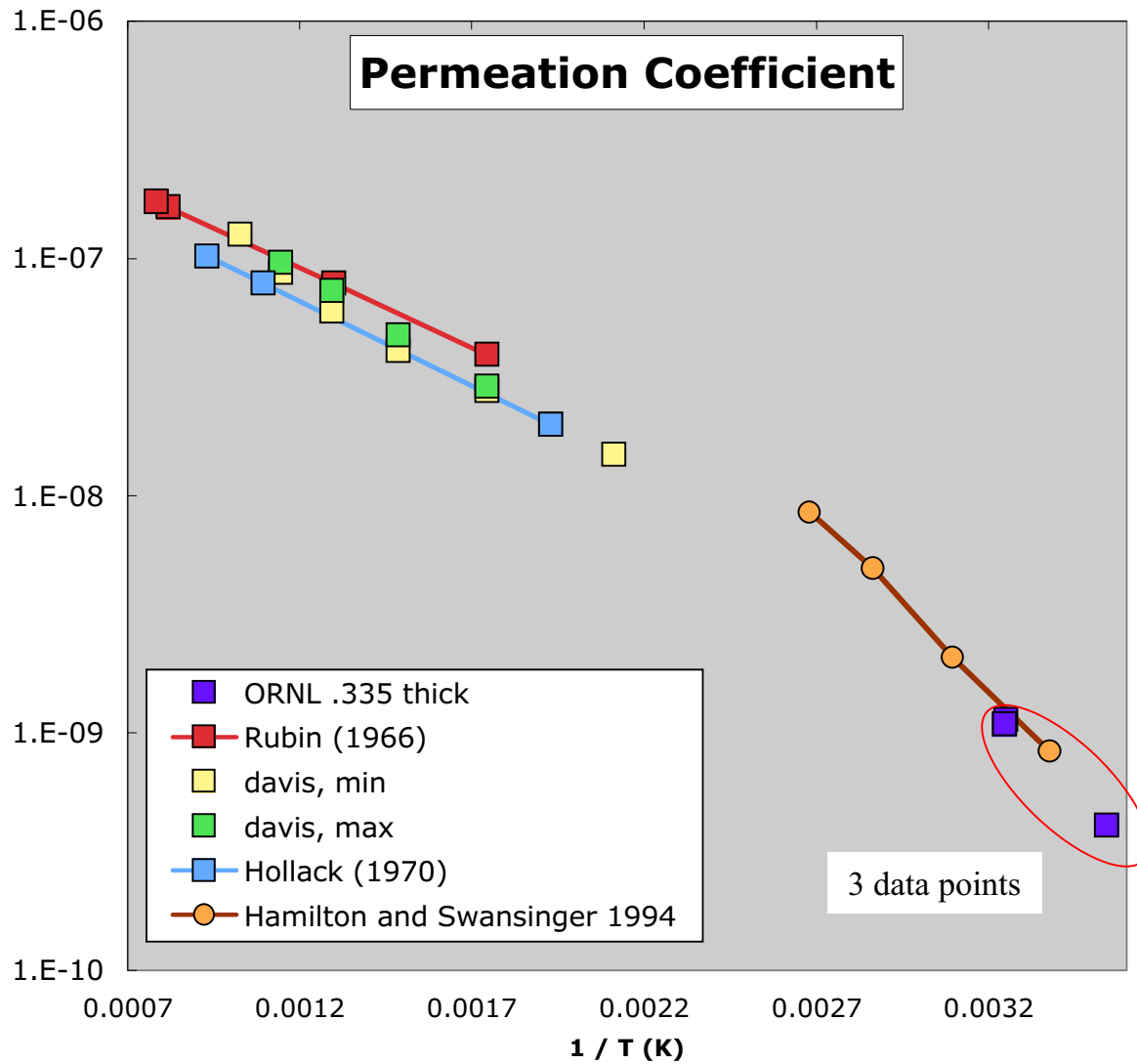
- Diffusion data for palladium are fast and relatively consistent (Alefeld & Volkl, 1978 p324)
- A good system test - do our data agree ?

# Caveats

- **Lower temperature palladium experiments measured permeability and calculated diffusivity from published PCT (solubility) data.**
- **Data are corrected from measured (Fickian) diffusion coefficients to (Einstein) diffusion coefficients that correct for variable concentration as a function of pressure and temperature, and a 'site-blocking' factor**
- **Many of the data sets were measured at low-pressure conditions - P dependence not evaluated**

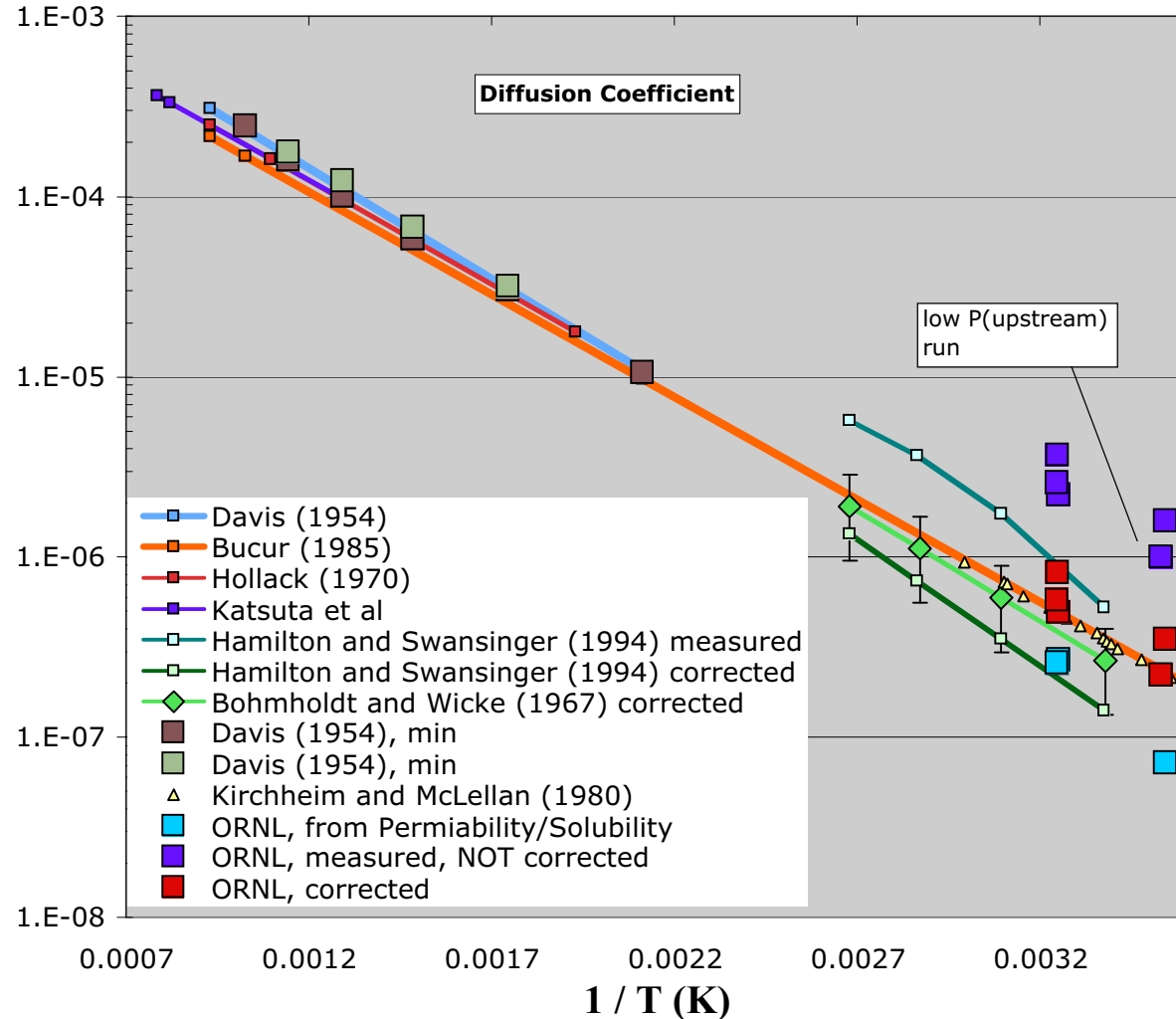


# Permeation Data



- Our data at 10 and 35°C agree well with published results
- Samples annealed at 850C for 90min
- Multiple runs very consistent

# Diffusion Data



- Our measured D values (P ~ 23 bars) are similar to, but a bit faster than the uncorrected Hamilton and Swansinger (1994) data (P ~ 1200 torr)
- D values calculated from P and measured (T extrapolated) solubility data also agree with corrected literature values and are very consistent
- Suggests PCT dependence to D

# Conclusions from Palladium Test

- **High-pressure permeation system works - replicates literature data**

# Baseline Measurement with Pure Iron

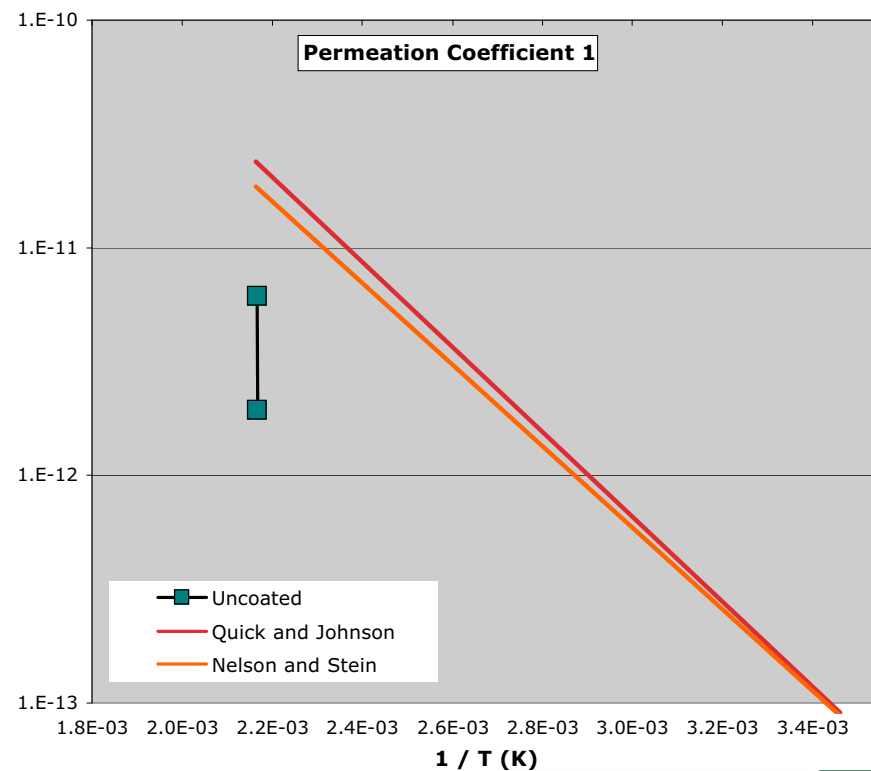
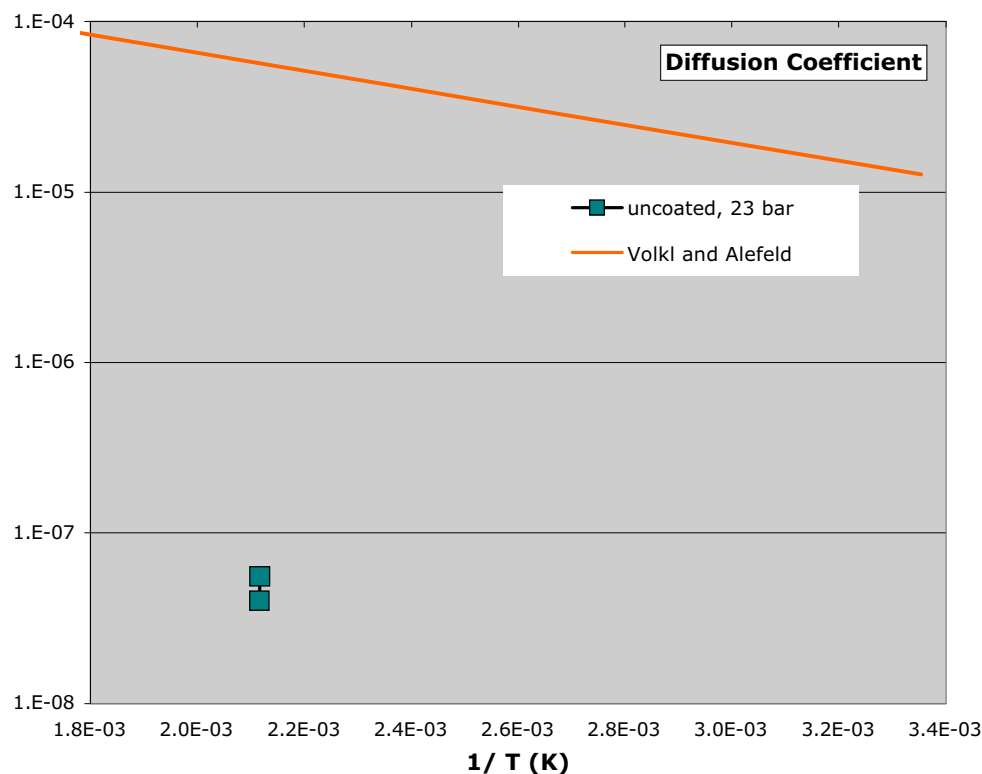
- **A “clean” material to develop baseline information for pipeline steel**
  - Well annealed pure iron minimizes hydrogen trap effect
  - Further develop testing and data analysis procedure
  - Study surface effect (alloy system dependent)
- **Sample preparation**
  - 99.995% pure, 0.25 to 2 mm thick
  - Annealed at 1000°C for 2 hrs before testing
  - Hydrogen purity: 99.9995% (research grade)





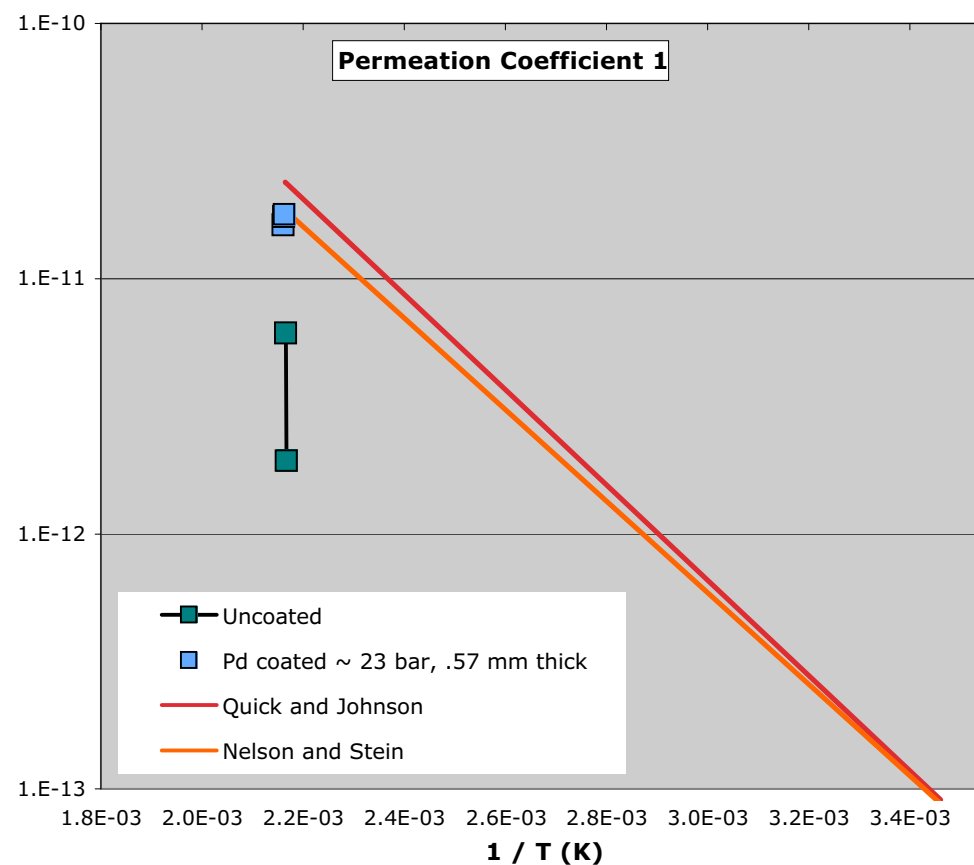
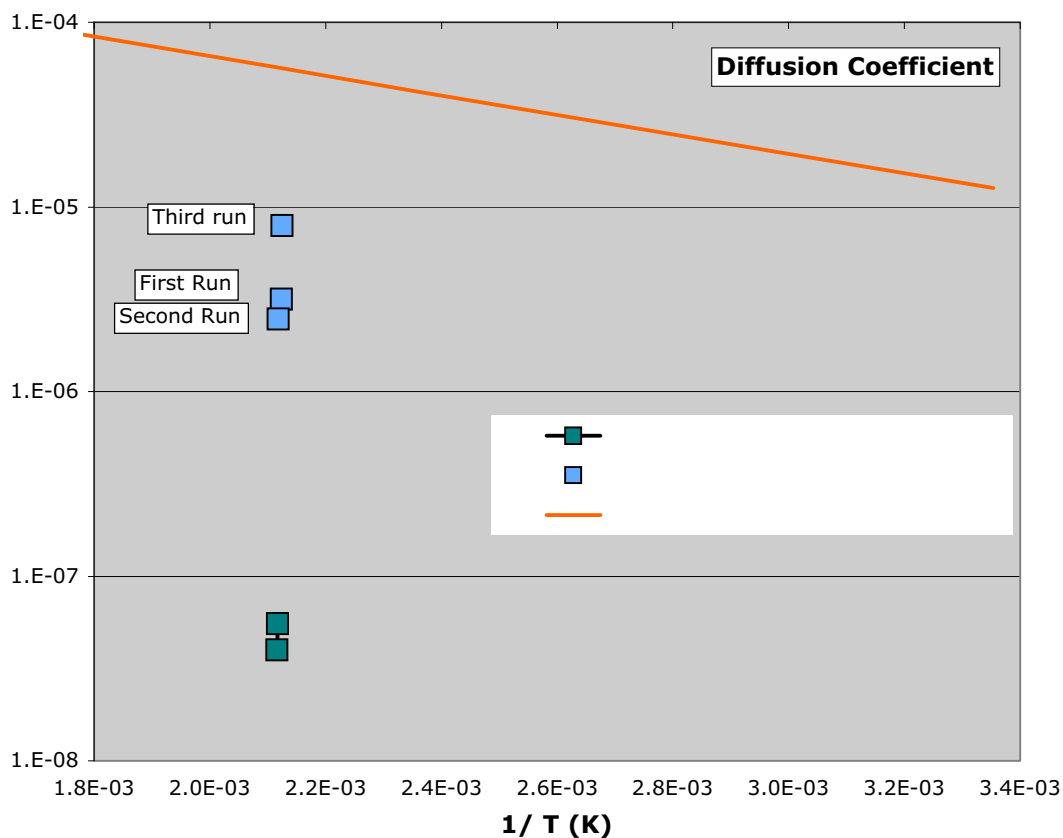
# Pure Iron with Bare, Clean Surface

- Sample surfaces were mechanically ground and acetone cleaned
- Tested at 200°C to reduce trapping effects
- Pressure: 330psi
- Diffusivity is three orders of magnitude too low
- Permeability is also low
- Suggest surface effect dominating

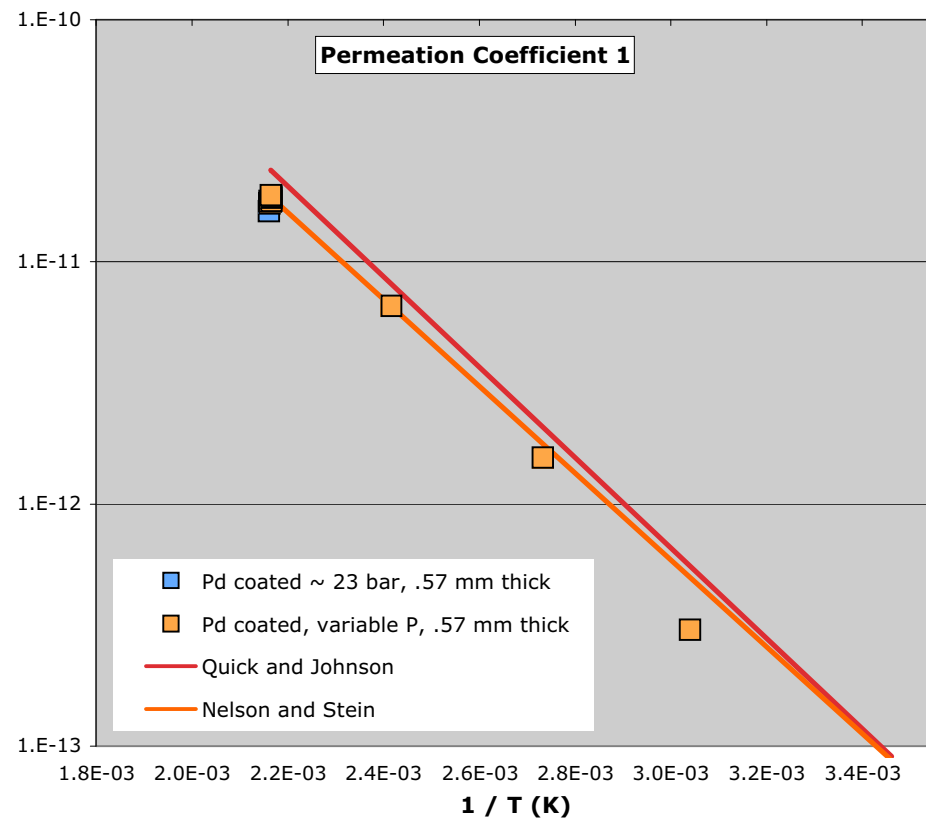
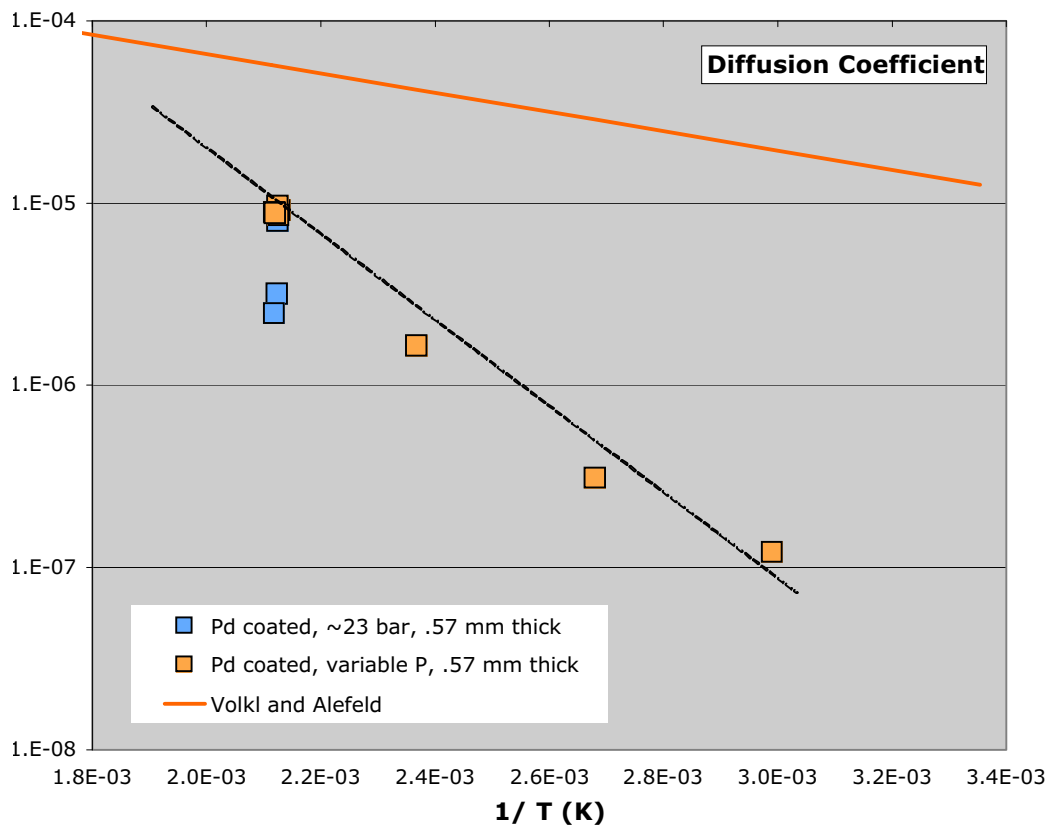


# Pure Iron with Pd Coating

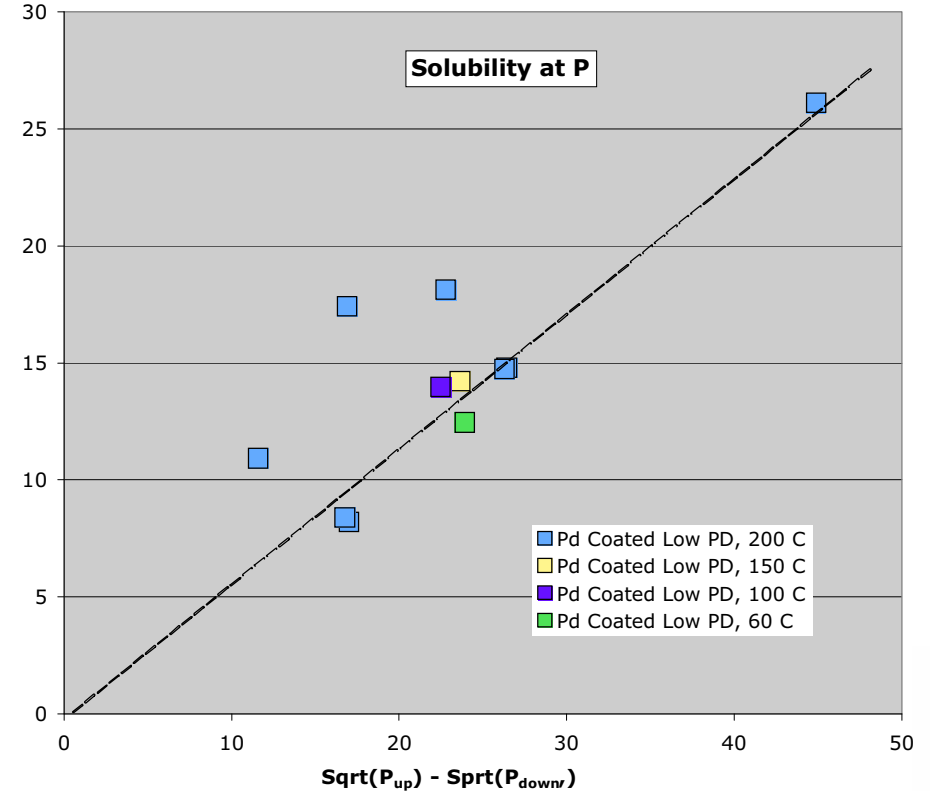
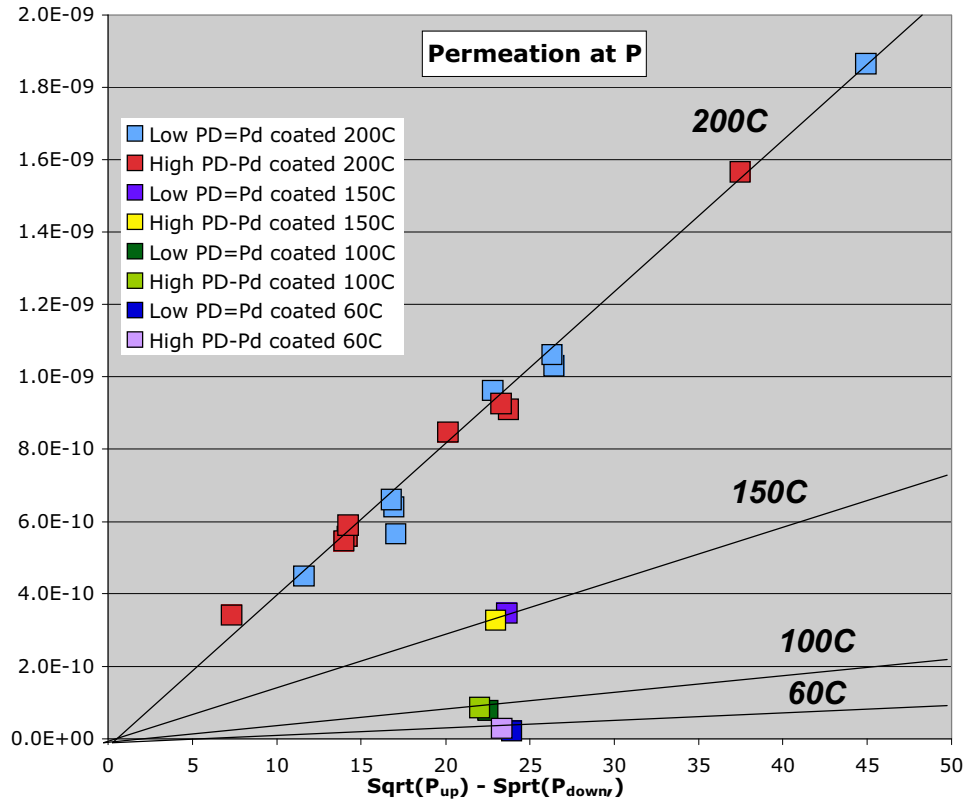
- 20 nm Pd coating on both sides



# Temperature Dependency (Pd Coated Pure Iron)

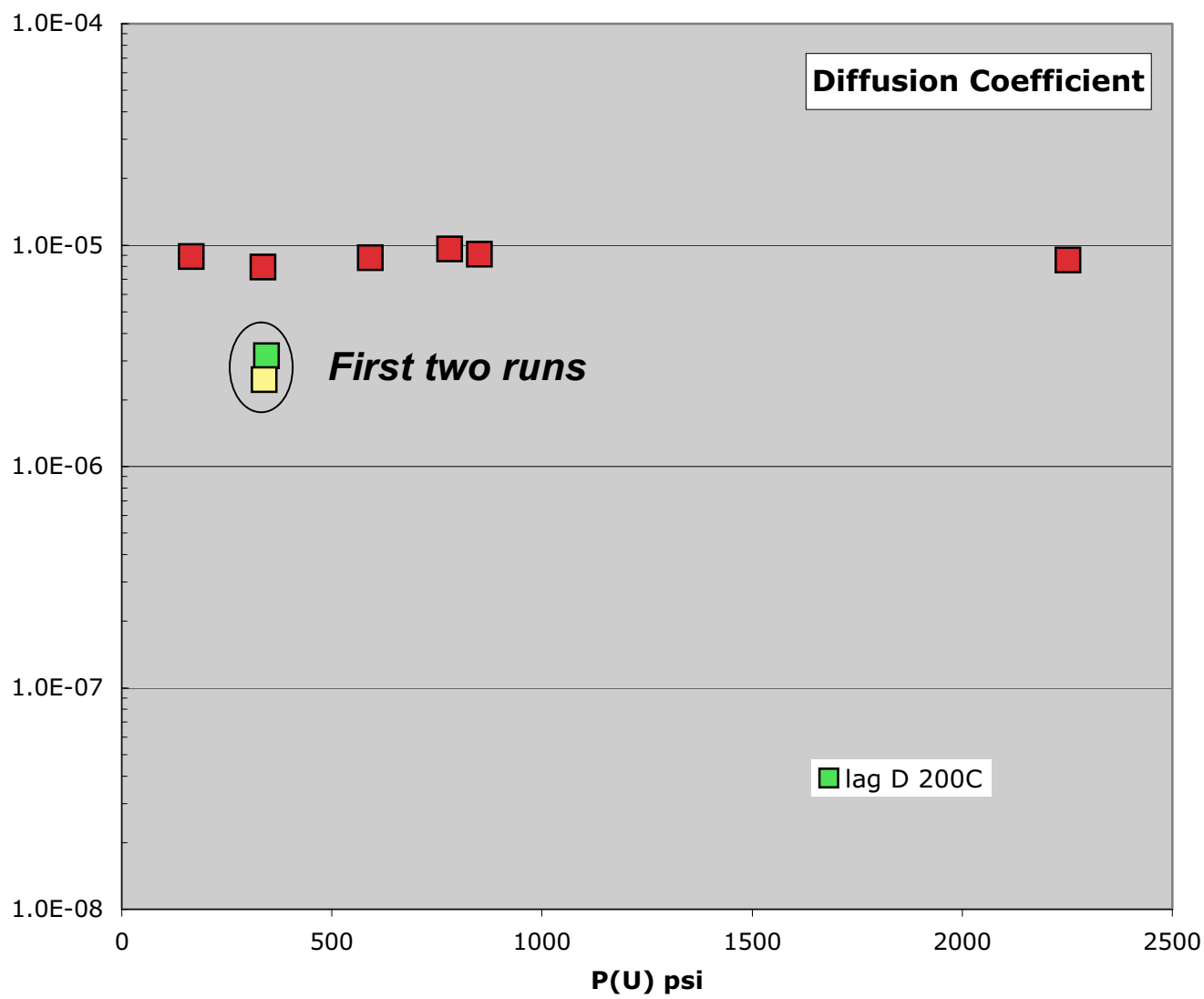


# Pressure Dependency (Pd Coated Pure Iron)



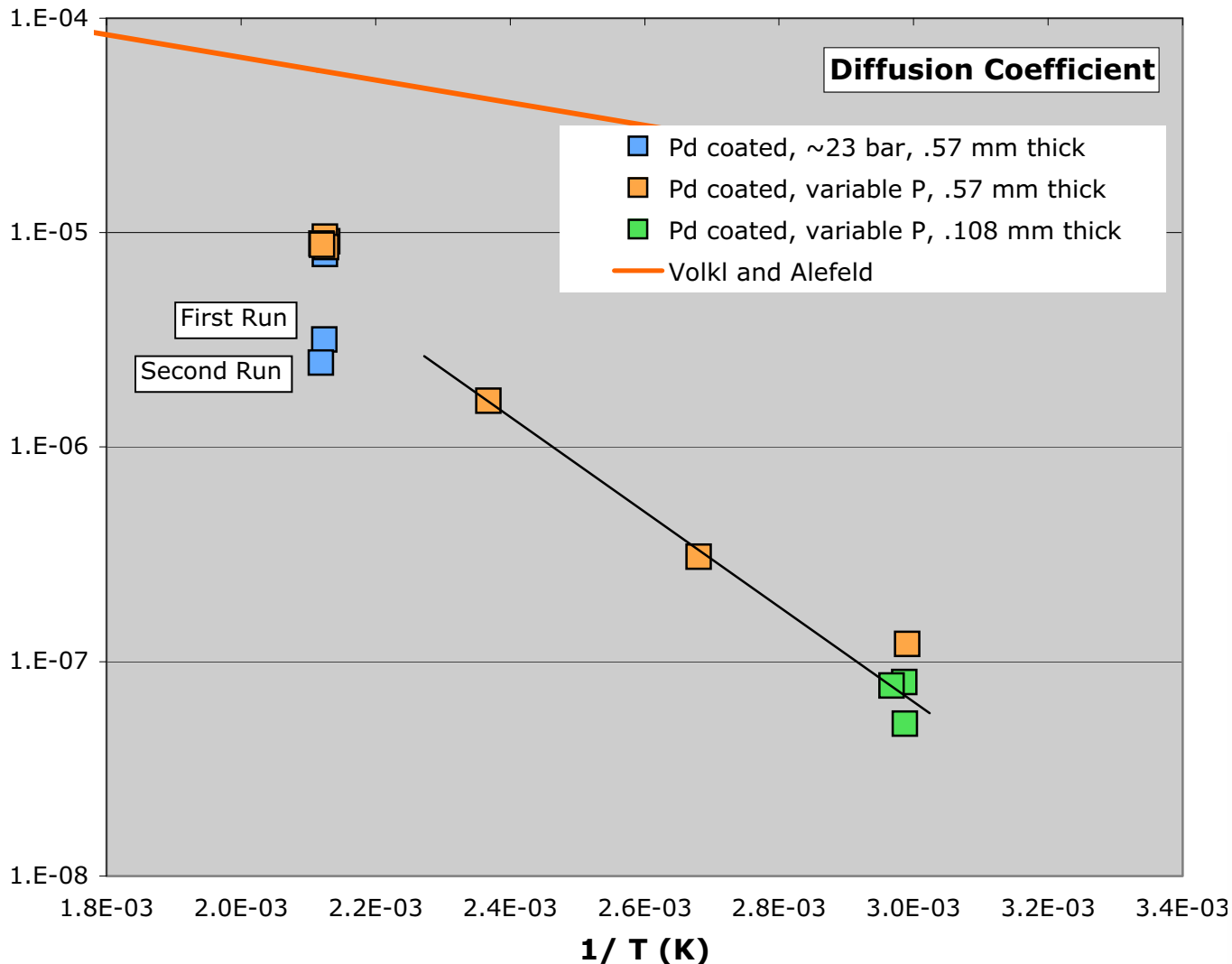
- Solubility increases as charging pressure increases
- Permeation rate has square root dependency on pressure, at given temperature

# Pressure Dependency of Diffusivity (Pd Coated Pure Iron) (@200C)



# Effect of Sample Thickness

- Pd coating may not completely eliminate surface effects
- Refined data reduction procedure is being worked to separate bulk diffusion from surface effect



# Summary of ORNL Task

- **High-pressure measurement system has been verified**
- **Measurements on pure iron provide baseline data to study steels and welds**
- **More rigorous data reduction procedure is being developed**
- **Complete measurements on pure iron and then move to steels**



**SRNL**

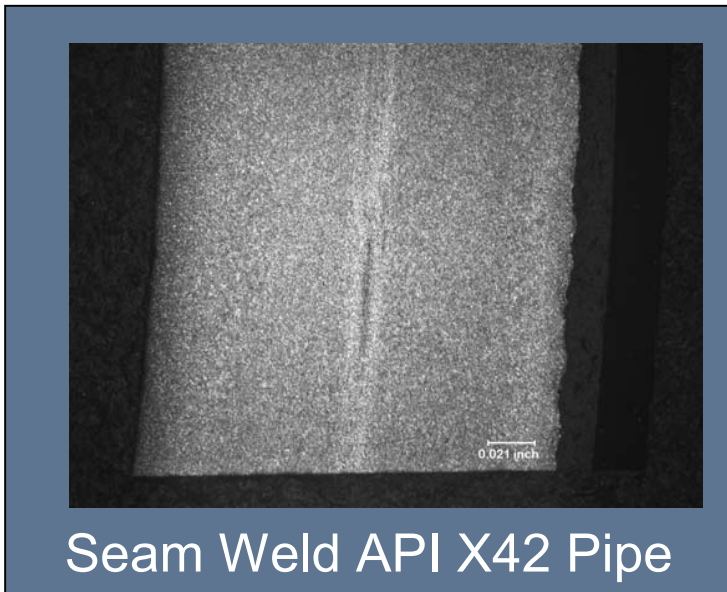


# SRNL Progress and Status



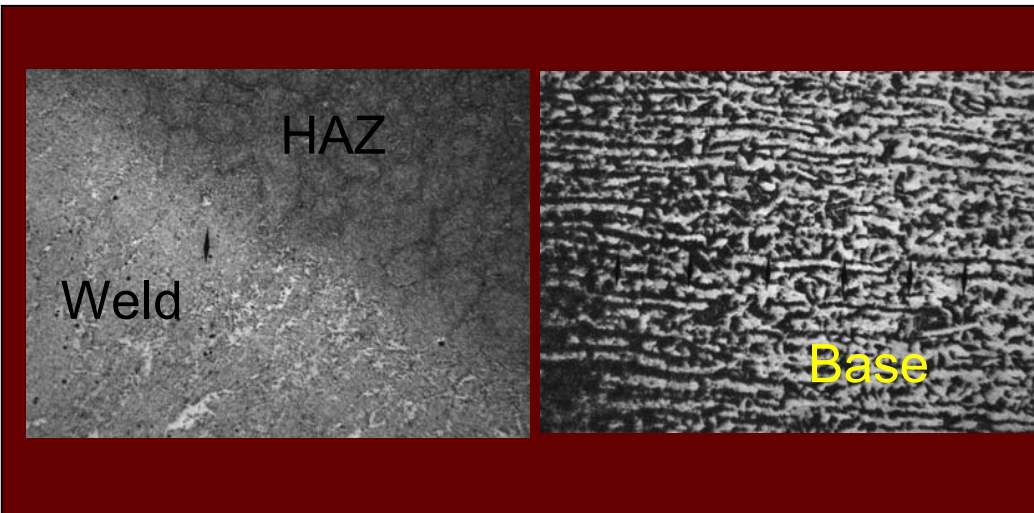
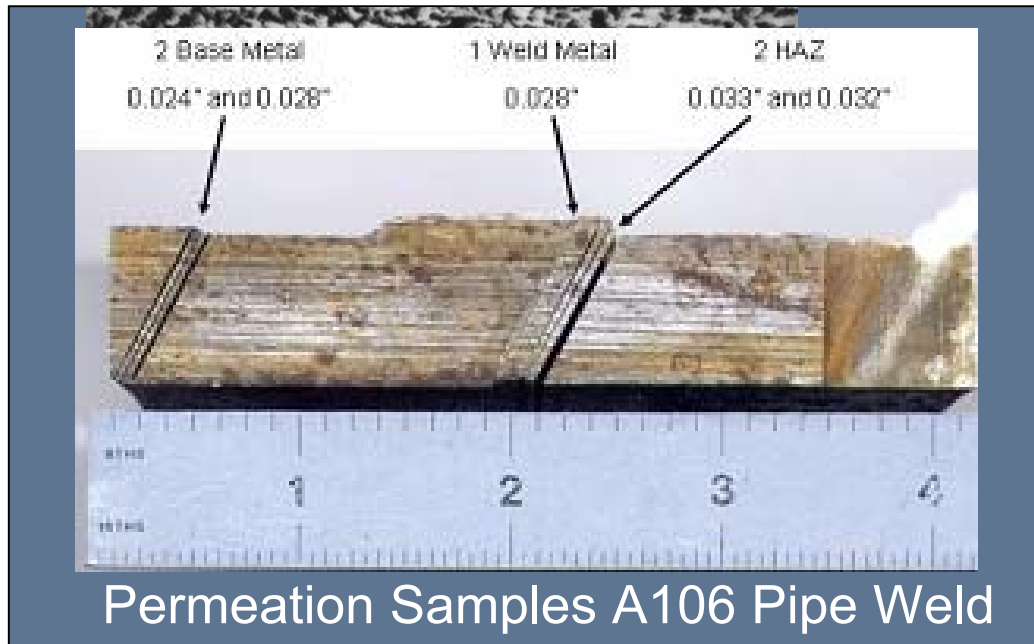
# SRNL Weld/HAZ Permeation & Embrittlement

## Introduction



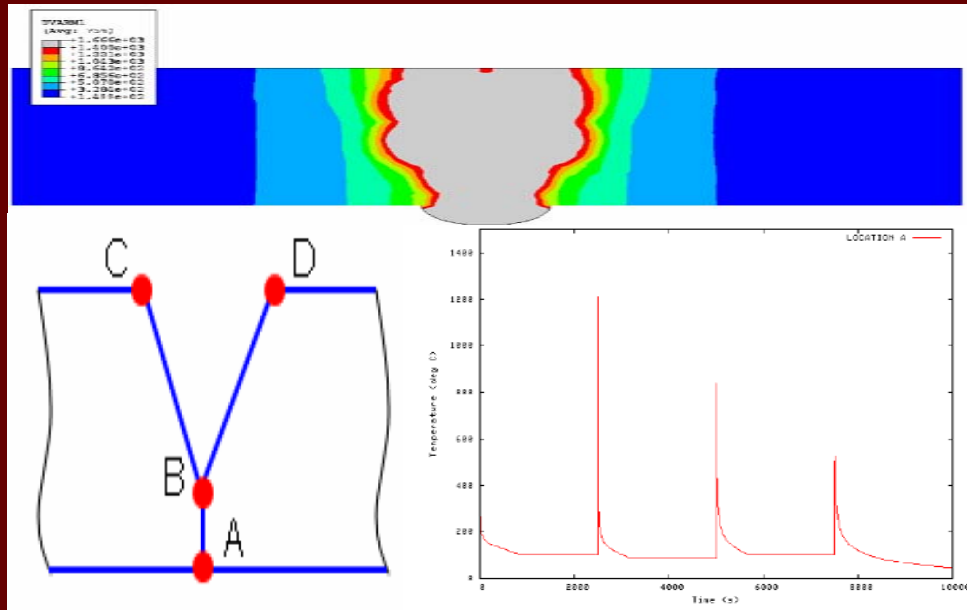
- Main Project Focus to Determine the Relationship Between Hydrogen Transport--Permeation Diffusivity, Solubility in Weld/HAZ Microstructures in Steel Pipeline Materials and the Link to Susceptibility to Hydrogen Embrittlement
- Collaborations with ORNL, EWI, and Praxair in FY07
  - Samples from Welded Pipe Sections
    - Permeation Measurements at Pressures up to 700Torr and Temperature to 200°C
  - GLEEBLE Simulations of HAZ
    - Permeation Testing of Simulated Microstructures

# SRNL Weld/HAZ Permeation & Embrittlement Progress

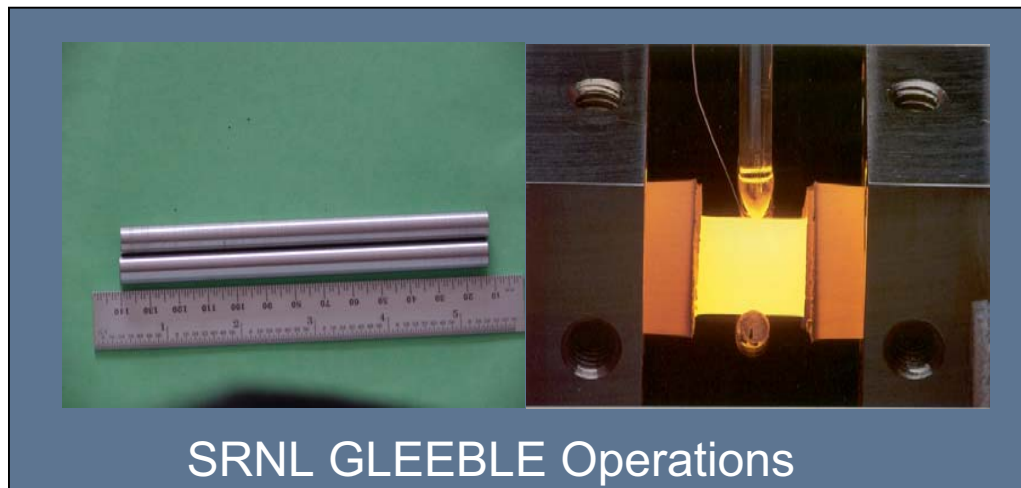


- Received Welded Pipe Materials—Praxair—API 5L Grade B/A106 Grade B—SMAW Girth Weld w/ TIG Root Pass
- Sectioned Weld and Identified Base, HAZ, and Weld Regions
  - Harvested Permeation Disk Samples from Three Regions
  - Approx. 0.030" thickness
- Low Pressure Permeation Testing in SRNL
  - E-beam Weld into 2 1/8" Flange
  - Pressure up to 700 Torr
  - Temperature up to 200°C
- Measure Hydrogen Permeability and Diffusivity
- Solubility Determined from Permeation Test Data

# SRNL Weld/HAZ Permeation & Embrittlement Progress



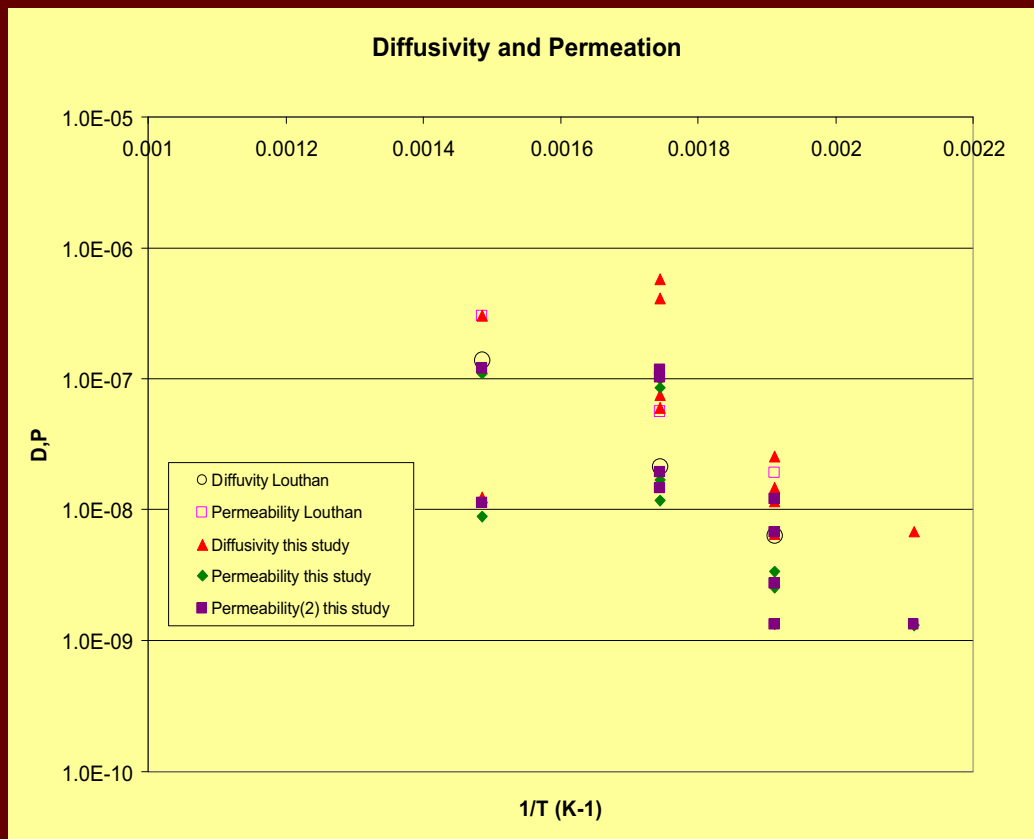
Weld Modeling with EWI



SRNL GLEEBLE Operations

- Simulations of Weld HAZ Microstructures
  - Collaborated with EWI on Weld Simulations Modeling to Develop Input for GLEEBLE Thermal Simulation
    - V-Groove Joint Design
    - TIG Root Pass
    - Multi-Pass SMAW Fill
- Designed GLEEBLE Samples from A106 Grade B Pipe Stock for Thermal Treatment
  - 0.375" Diameter Cylinders Harvested from Pipe Wall
  - GLEEBLE Control Software Program Developed
  - GLEEBLE Treatments Initiated

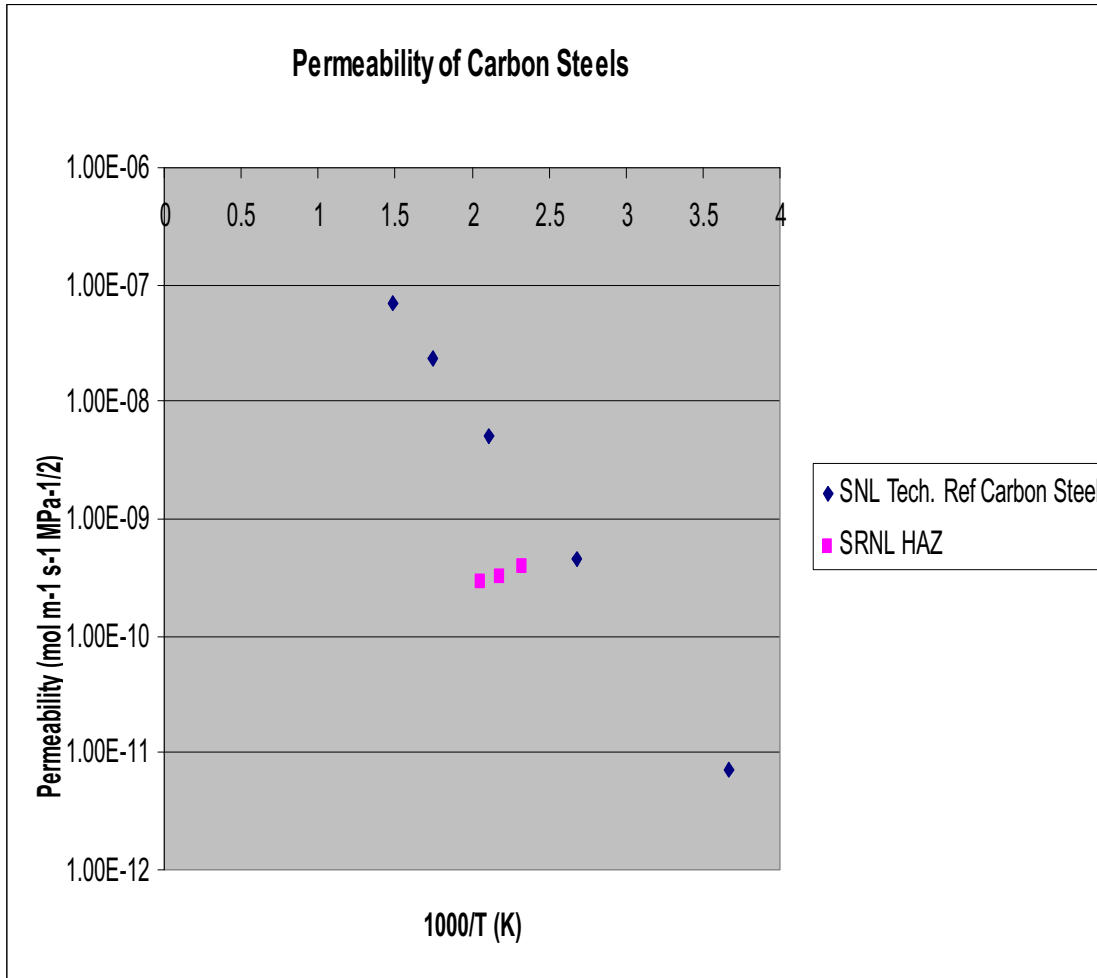
# SRNL Weld/HAZ Permeation & Embrittlement Progress



Proofing SRNL System & Test Methodology

- Questions Concerning Low-Pressure H<sub>2</sub> Permeability Measurements
  - SRNL Conducted Previous Studies of 304L SS Alloy
- SRNL Data in Comparison to Previously Published Literature Shows Good Agreement
- Agreement Between Published Data and Collected Data Demonstrates feasibility of using Low Pressure Permeation Measurements
- Current SRNL Testing Methodology and System is Proofed—Testing of HAZ Materials from A106 Gr. B Pipe Weld Initiated.
- Testing Conducted at 700T H<sub>2</sub> Pressure @ 150°C, 175°C, and 200°C

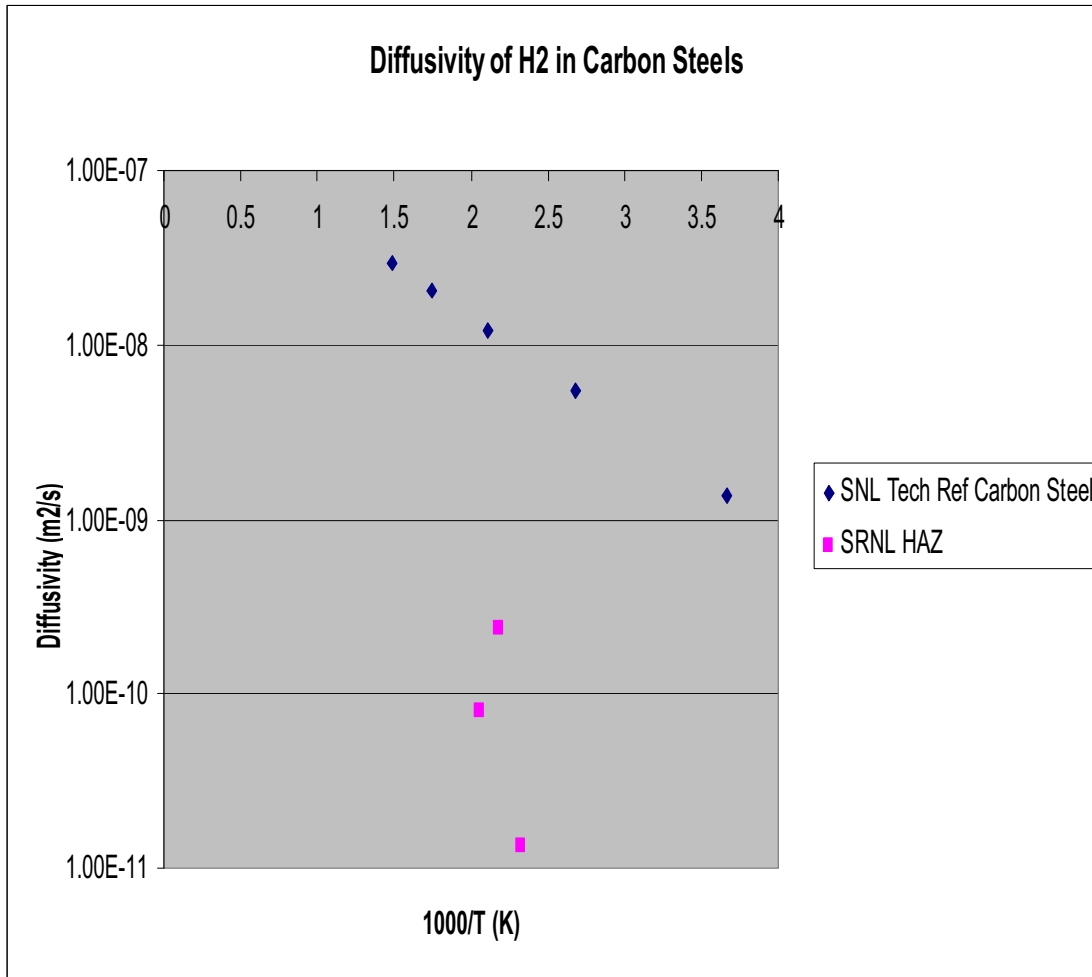
# SRNL Weld/HAZ Permeation & Embrittlement Progress



- Permeability Measurements of HAZ—700T @150, 175, and 200°C
- SNL Technical Reference on Carbon Steels Provides an Expression for Permeability ( $\Phi$ ) for Several CS Alloys (normalized, spherodized, and Q&T)—SRNL HAZ Data Compared to 1020 Alloy
  - $\Phi = 3.77E-05 \exp(-35.07/RT)$
- SRNL Measured Permeability Data for A106 Grade B.—C-content =0.185
  - 150°C = 3.92 E-10 mol/m s MPa<sup>1/2</sup>
  - 175°C = 3.23 E-10 mol/m s MPa<sup>1/2</sup>
  - 200°C = 2.87 E-10 mol/m s MPa<sup>1/2</sup>

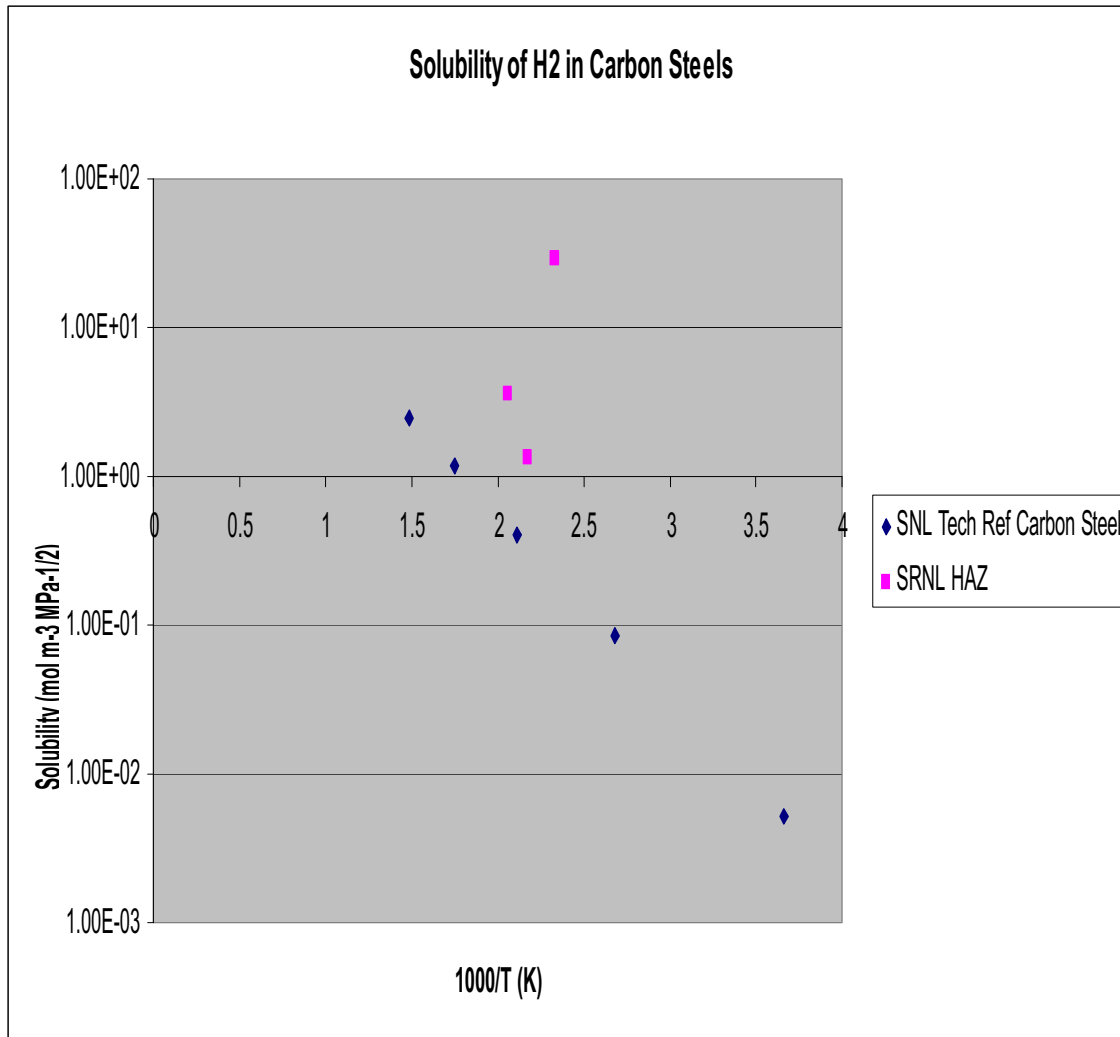


# SRNL Weld/HAZ Permeation & Embrittlement Progress



- Diffusivity Determined from Permeation Tests of HAZ—700T @150, 175, and 200°C
- SNL Technical Reference on Carbon Steels Provides an Expression for Permeability ( $\Phi$  and Solubility (S) for Several CS Alloys (normalized, spheroidized, and Q&T)—SRNL HAZ Data Compared to 1020 Alloy
  - $D = \Phi S$ —Plot Data Calculated Using SNL Tech Reference
- SRNL Measured Diffusivity Data for A106 Grade B.—C-content =0.185
  - 150°C = 1.34 E-11 m<sup>2</sup>/s
  - 175°C = 2.36 E-10 m<sup>2</sup>/s
  - 200°C = 7.87E-11 m<sup>2</sup>/s

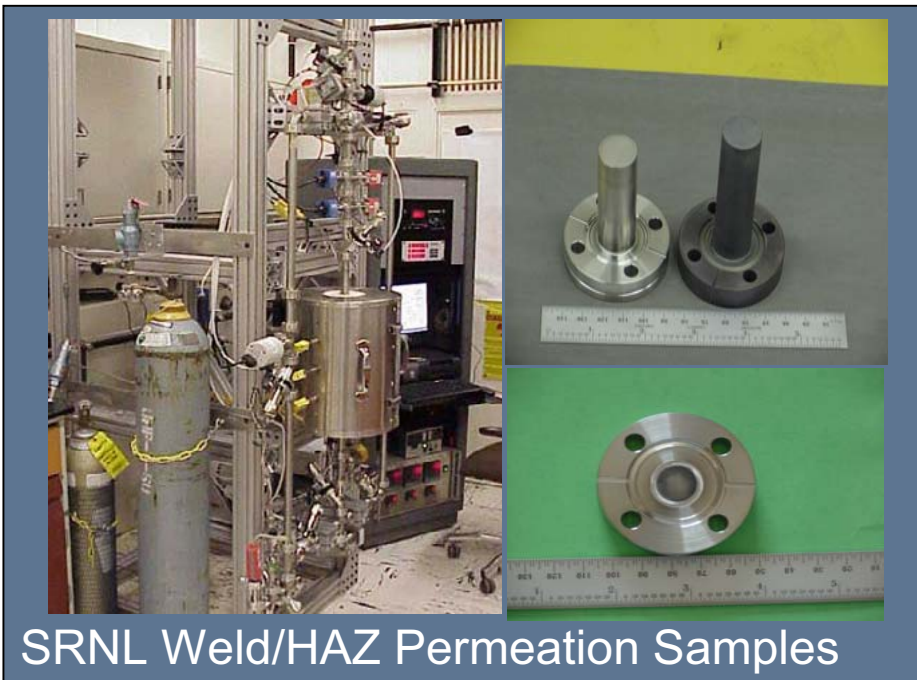
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- SNL Technical Reference on Carbon Steels Provides an Expression for Solubility (S) for Several CS Alloys ( normalized, spherodized, and Q&T)—SRNL HAZ Data Compared to 1020 Alloy
  - $S = 159 \exp(-23.54/RT)$
- SRNL Calculated Solubility Data for A106 Grade B.—C-content =0.185
  - 150°C = 29.25 mols/m<sup>3</sup> MPa<sup>1/2</sup>
  - 175°C = 1.36 mols/m<sup>3</sup> MPa<sup>1/2</sup>
  - 200°C = 3.64 mols/m<sup>3</sup> MPa<sup>1/2</sup>

# SRNL Weld/HAZ Permeation & Embrittlement

## Path Forward FY08



- **FY08 AOP Plan**
  - Closer Collaboration with ORNL, Univ. of Illinois Test Programs
  - Focus on Understanding Link Between HAZ Microstructure and Hydrogen Diffusivity/Solubility and Connection to Susceptibility to Hydrogen Embrittlement
  - Focus on HAZ Materials via GLEEBLE Simulation
    - HAZ Thermal Simulations
    - Microstructure Characterization
  - Permeation/Diffusivity/Solubility Measurements
  - Focus Testing on A106 Gr. B/X42 and X52 Alloys
  - SRNL to Prepare GLEEBLE Samples for Testing and to Provide Companion Samples to ORNL/Illinois for Low-Pressure vs High Pressure Comparisons
  - Initiate Basic Tensile Property Data of GLEEBLE HAZ Materials
    - ASTM G142—Notched/Unnotched Tensile
    - Demonstrate Increased Susceptibility in HAZ



**SRNL**



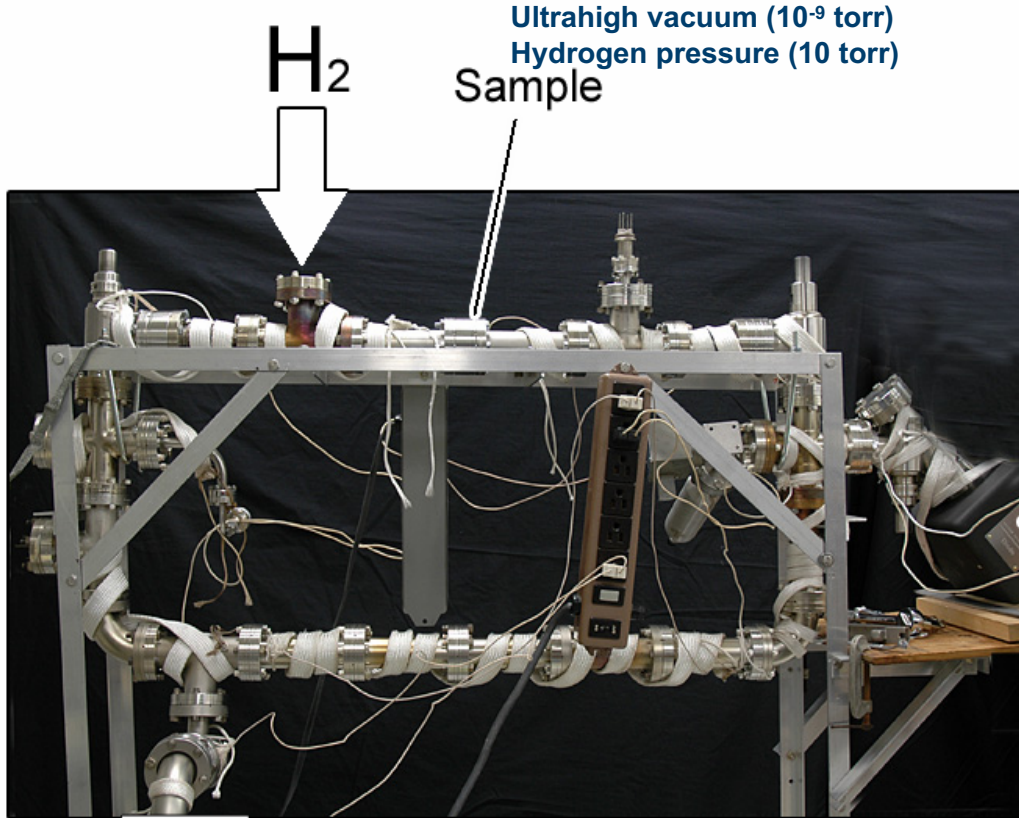
# University of Illinois Progress and Status



# Permeation Measurements at Illinois

- **Currently conducting permeation tests with high purity iron to set the baseline. Permeation tests for C-Type steel microstructure (X60/70) from Oregon Steel Mills have been done.**
- **Materials analyzed**
  - Oregon Steel Mills (A,B, C, D microstructures)
  - SECAT (sample with Schott North America coating on)
  - Pipelines in service
    - AirLequide pipeline
    - Air-Products pipeline
    - Kinder Morgan pipeline
- **Coupling permeation measurements with finite element simulations to extract the trap density and binding energy**
  - In conjunction with Thermal Desorption Spectroscopy

# UIUC Permeation



Ultrahigh vacuum ( $10^{-9}$  torr)  
Hydrogen pressure (10 torr)

H<sub>2</sub>

Sample

Hydrogen  
Detector

- Hydrogen is introduced on one side of the sample
- Permeates through sample
- Detected by ion pump

Turbo  
pump

- 4.75 cm disks
- 100 micron thickness
- Palladium coating on exit side
- Testing coatings on hydrogen side



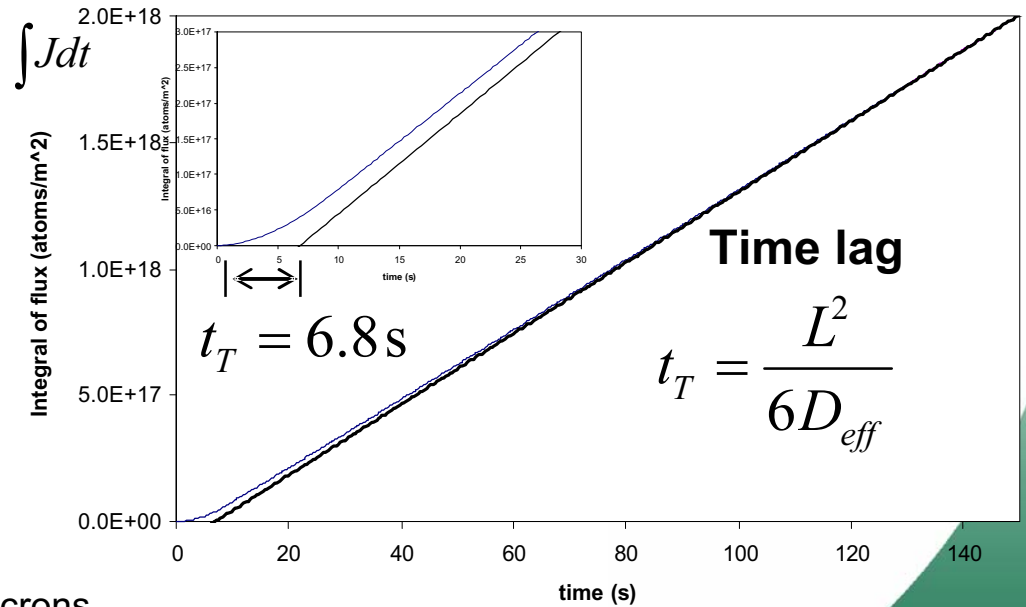
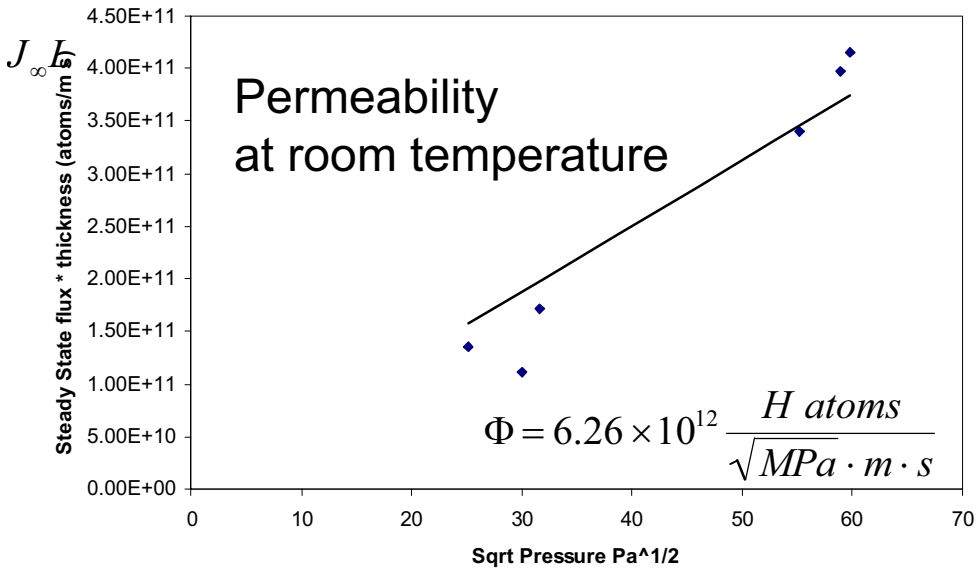
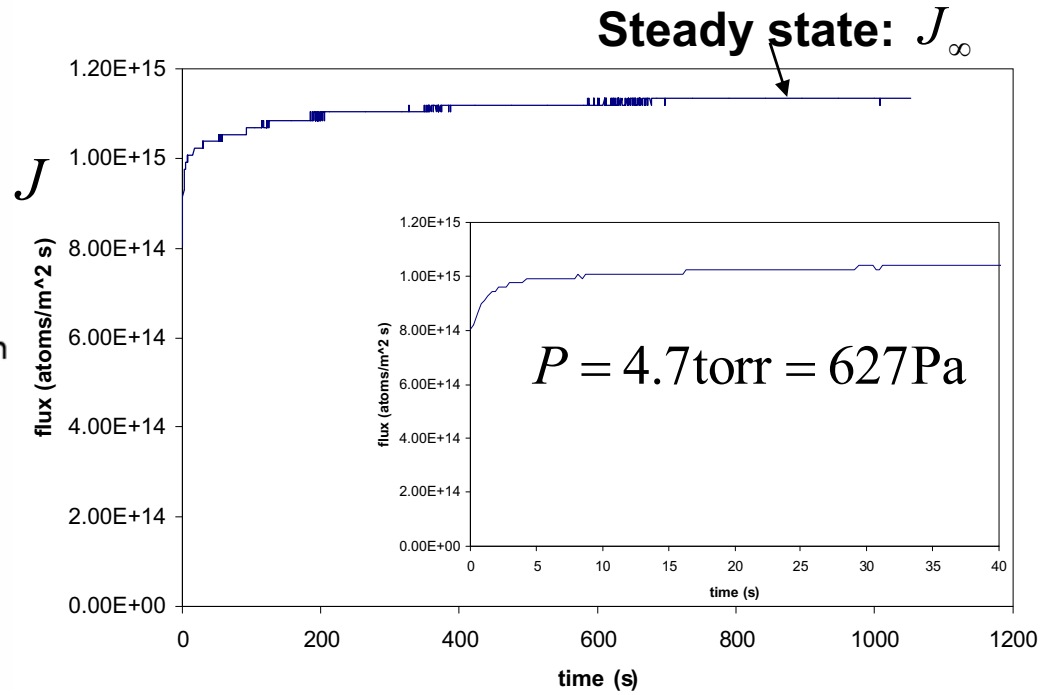
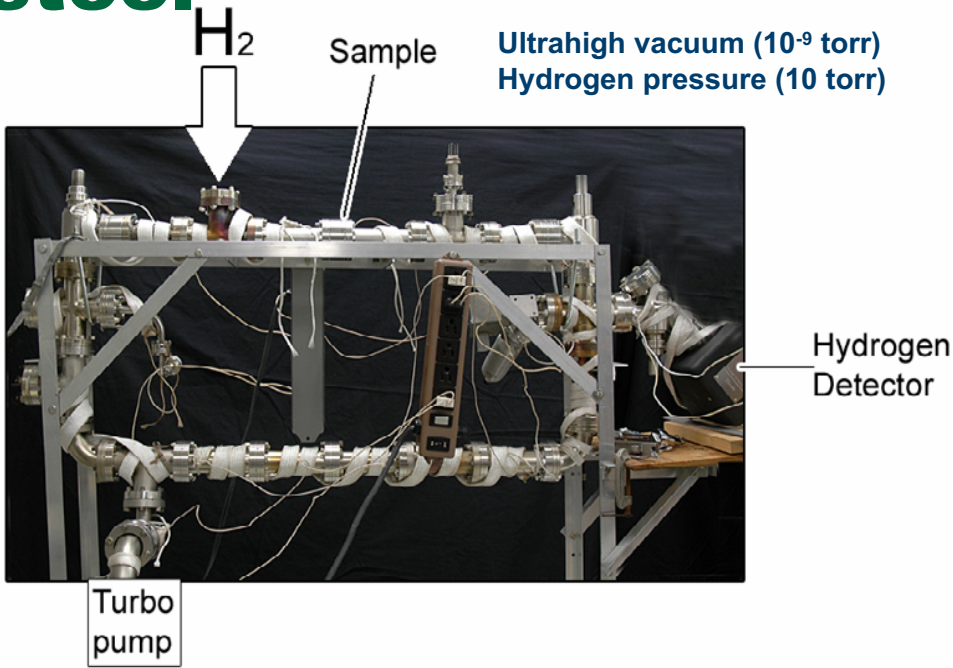
Real-world pipeline specimens are in our possession for testing  
Air Liquide and Air Products provided the coupons



SRNL

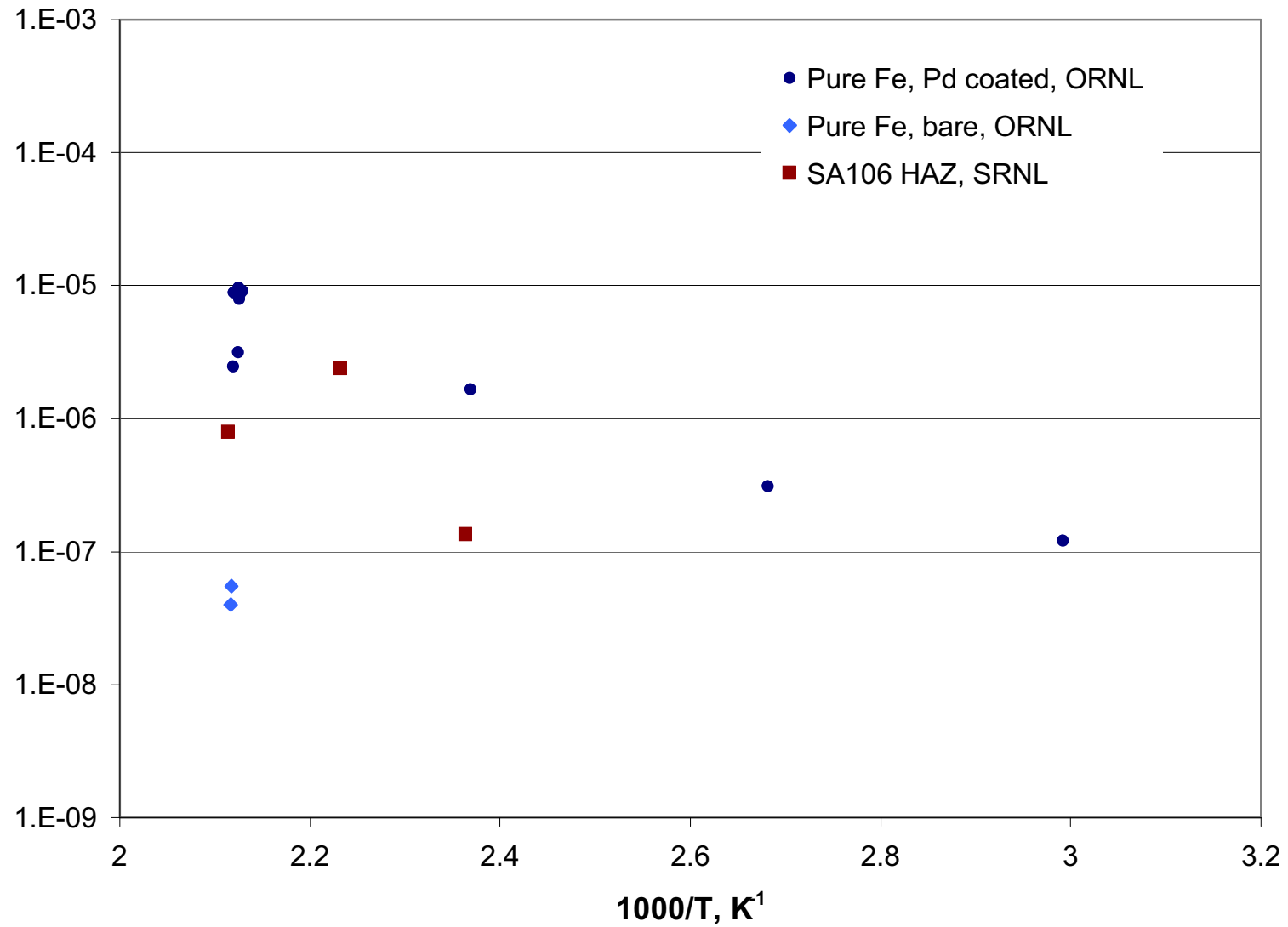


# UIUC Hydrogen Permeation Measurements: C-steel



- Oregon Steel Mills sample: thickness 120 microns
- room temperature

# Comparison of Data (ORNL, SRNL, UIUC)



# FY08 Plan

- **Close coordination among ORNL, SRNL and UIUC (ORNL lead)**
  - Sample preparation procedure
  - Testing procedure
  - Data analysis and reduction procedure
  - Round-robin test on selected steels
  - Testing matrix (steels, welds, surface conditions)
- **Focus on generating reliable data for pipeline steels and welds**
  - Effect of microstructure
  - Effect of temperature
  - Effect of pressure
- **ORNL:**
  - High pressure permeation
- **SRNL:**
  - Low pressure permeation
- **UIUC:**
  - Modeling and hydrogen trap study
  - Low pressure permeation



# Questions?