

# Upset Protrusion Joining Techniques for Joining Dissimilar Metals

Stephen D. Logan – Principle Investigator FCA US LLC June 12, 2015

Project ID #LM100

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#### <u>Timeline</u>

- Start date: September 30, 2013
- End date: December 31, 2016
- Percent complete: ~40%

## <u>Budget</u>

- Total project funding
  - DOE share: \$587,248
  - Contractor share: \$251,678
- Funding received in FY14:
  - \$81,591
- Funding for FY15:
  - \$361,437

#### <u>Barriers</u>

- F- "High-volume, high-yield joining technologies for lightweight and dissimilar materials needs further development"
  - Develop and demonstrate robust, cost effective, and versatile process to join Mg die castings to Al and steel sheet

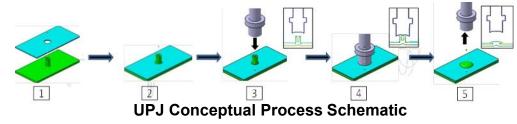
#### Partners

- FCA US LLC Project Lead
- AET Integration, Inc.
- Meridian Lightweight Technologies



#### **Overall Objectives**

• Develop and demonstrate a robust, cost effective, and versatile joining technique, known as Upset Protrusion Joining (UPJ), for joining challenging dissimilar metal combinations, especially those where one of the metals is a die cast magnesium (Mg) component, and develop variations for unique requirements, such as oval boss UPJ for narrow flanges and upset cast riveting (UCR) for dissimilar metal joints where neither metal is a casting.



#### **Objectives** (September 2013 to March 2015):

- Characterize thermo-mechanical behavior of Mg alloys to support computer process
  modeling to assist in optimizing UPJ joining process.
- Optimize UPJ protrusion and electrode geometries, and process parameters, to provide robust, repeatable joining performance for each configuration being considered.
- For benchmark self pierce riveting (SPR), and round boss and oval joint UPJ, produce test coupons to support mechanical and corrosion performance evaluations.
- Conduct pre-corrosion mechanical testing for SPR and round boss UPJ assemblies.

#### Impact on barriers

• All objectives are aimed at addressing the VTO barrier "High-volume, high-yield joining technologies for lightweight and dissimilar materials needs further development".

Date	Milestones and Go/No-Go Decisions	Status
September, 2013	<u>Milestone</u> Project kick-off	Complete
January, 2015	Milestone Complete process development preparation	Complete
January, 2015	Go/No-Go Decision SPR and round boss UPJ joints assembled and coated	Complete
December, 2015	Milestone Evaluate first set of UPJ and UCR Joints for pre- corrosion mechanical/structural performance	On track
December, 2015	Go/No-Go Decision Complete initial (pre-corrosion) mechanical/structural evaluations for all joints	On track

## Approach

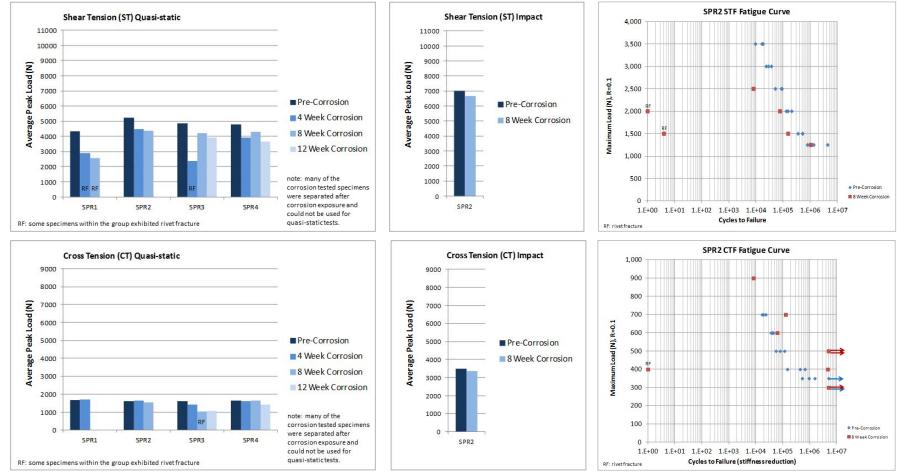
- Establish *benchmark* performance of Mg to Al joints produced through Self Pierce Riveting (SPR) *for comparison purposes <u>only</u>* using the following "evaluation procedure":
  - Subject all joints to mechanical tests including microstructure / defect evaluation, shear tension and cross tension quasi-static, impact, and fatigue testing.
  - Subject all joints to accelerated corrosion tests, reviewing visually every two weeks and removing three samples of each configuration at four week intervals for quasi-static testing.
  - Subject select configurations to post-corrosion fatigue and impact testing for comparison to pre-corrosion performance.
- Characterize thermo-mechanical behavior of Mg alloys through Gleeble<sup>®</sup> testing being conducted in Canada at no cost to the U.S. Department of Energy (DOE).
- Optimize protrusion and electrode geometries and process parameters to reduce electrical current requirements and provide robust, repeatable forming performance for each of the joint configurations being considered.
- For each joint type/material/coating configuration, produce tensile shear and cross tension test coupons to support mechanical/structural and corrosion evaluations using the "evaluation procedure" described above for SPR.

- Established *benchmark* performance of magnesium to aluminum joints produced through SPR:
  - Optimized joining process to produce high quality 2.0 mm Mg AM60B to 2.2 mm Al6013-T4 dissimilar metal joints by down-selecting the most promising (best rivet engagement, least cracking, etc.) from17 different rivet and die combinations.
  - Produced over 200 shear and cross tension assemblies to support evaluation of mechanical/structural and corrosion performance.
  - Evaluated *pre-corrosion* structural/mechanical performance of 105 samples and *post corrosion* performance of 122 joints subjected to ASTM G85-A2 accelerated corrosion procedure.

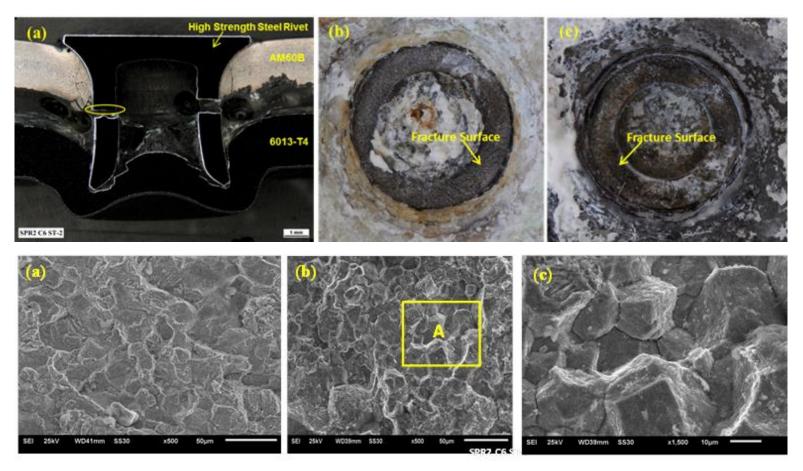
Self-Pierce Riveting - Round Rivet AM60B 2t																									
Base I	Plate Config	uration	Joir	ning Plat	te		Preliminary Evaluations (Prior to Corrosion Exposure)								On-Going Accelerated Corrosion Exposure Evaluation										
Material						Coated	Micro- structure	Qua	asi-					4 v	vks	8 v	wks			12	wks				
	Test Type Configu- ration	Surface Condition	Material	Thick- ness (mm)	Surface Condition	Assem- bly?	Charac- terization and Defect	Sta		Fati	gue	Imp	oact	Qu Sta	asi- atic		asi- atic	Qu Sta		Fati	gue	Imp	npact		
							Evaluation	ST	ст	ST	ст	ST	СТ	SТ	ст	ST	ст	ST	ст	ST	ст	ST	СТ		
		Bare	AI 6013 T4	2.2	Bare	No	5	5						3		3		3							
	Shear				Pre-treat	Yes		5		20		5		3		3		3		20		5			
	Tension	Pre-Treat	AI 6013 T4	2.2	Coated	No		5						3		3		3							
Mg					Coated	Yes		5						3		3		3							
AM60B		Bare	AI 6013 T4	2.2	Bare	No			5						3		3		3						
	Cross Tension				Pre-treat	Yes	5		5		20		5		3		3		3		20		5		
		Pre-Treat	AI 6013 T4	2.2	Coated	No			5						3		3		3						
					Coated	Yes	5		5		1				3		3		3						

Full SPR test matrix – Green squares indicate testing completed, red squares indicate parts had to be removed early (after 8 wks) from testing due to numerous premature failures

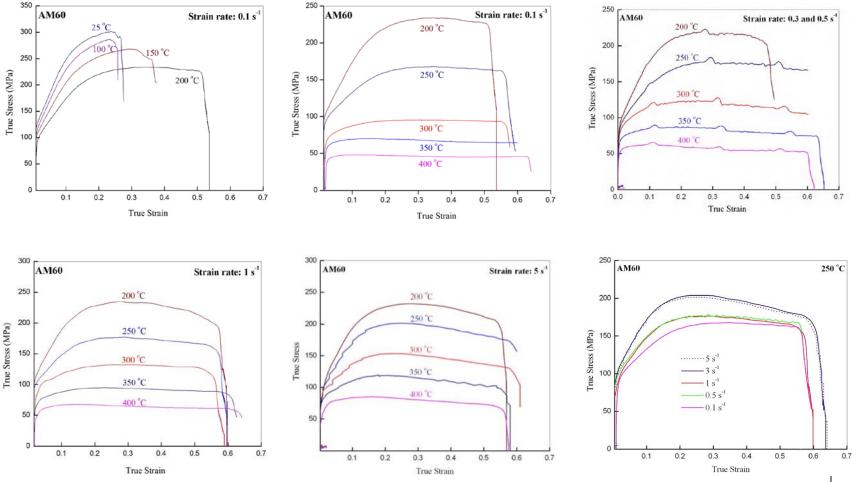
- Established *benchmark* performance of magnesium to aluminum joints produced through SPR.
  - Conducted structural/mechanical testing/evaluation throughout accelerated corrosion testing and fatigue and impact testing at the end of accelerated corrosion testing.



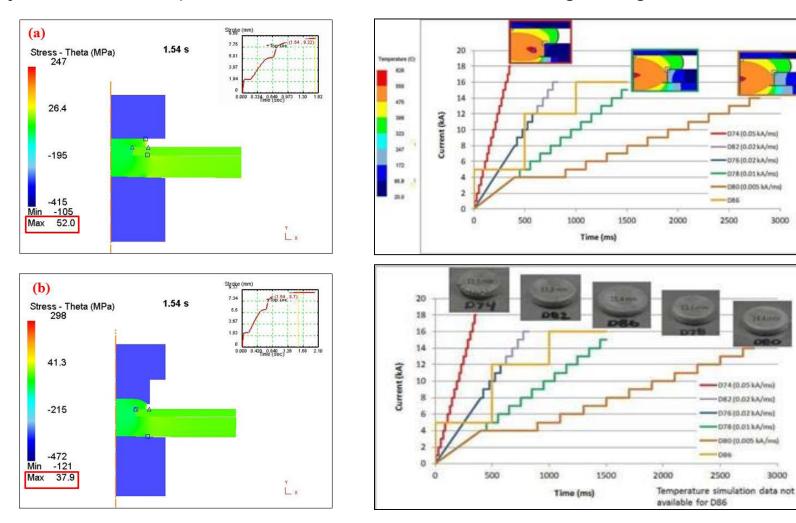
- Established *benchmark* performance of magnesium to aluminum joints produced through SPR.
  - Evaluated reason for premature joint failures of numerous samples during corrosion exposure to be hydrogen embrittlement of the steel rivet.



- Characterized thermo-mechanical behavior for Mg AM60B at several strain rates between 0.1 and 5.0 s<sup>-1</sup> and temperatures from 25°C to 400°C, through a Canadian Government Automotive Partnership Canada (APC) funded project with McMaster University, to support modeling predictions of UPJ process. Examples are shown below:



Conducted extensive process modeling and simulation development work as ٠ well as additional experimental work to support production of robust, repeatable joints for 11 unique round boss UPJ material / coating configurations.



3000

3000

 Produced over 650 round boss UPJ joints from 11 unique material/coating configurations and conducted pre-corrosion mechanical tests of over 300 joints from those same configurations. Evaluations included microstructure evaluations, joining induced defect characterization, and quasi-static, impact, and fatigue tests of shear and cross tension joint configurations.

							Upset Protrusion Joining - Roun	d Boss AN	/160B 2t																	
Base Plate Configuration					Joining Plate				Preliminary Evaluations (Prior to Corrosion Exposure)								On-Going Accelerated Corrosion Exposure Evaluation									
	Riv	ret						Coated Assem-	Microstructure	0	asi-					4 v	wks	8 v	vks			12 wks				
	guration configu- ration		Material	Thick- ness	Surface Condition		Characterization and Defect	Static		Fatigue		Impact		Qu Sta		Quasi- Static		Quasi- Static		Fatigue	e Im	pact				
	Shape	Size							Evaluation	ST	СТ	ST	СТ	ST	СТ	ST	СТ	ST	СТ	ST	СТ	sт ст	ST	СТ		
				Bare	Al 6016	1.0 mm	Bare	No		5		Ī		5		3		3		3			5			
			Shear	Alodine	Al 6016	1.0 mm	Pre-treat	Yes	5	5						3		3		3						
Mg AM60B		7 mm	Tension	5200	Al 6016	1.0 mm	Powder-coated	No Yes		5 5						3 3		3 3		3 3	_		5	mpact T CT 5 2 5 2 5 2 5 2 5 2 5 2 5 2 5 2		
	Round	Diam		Bare	Al 6016	1.0 mm	Bare	No	5		5				5		3		3		3			5		
			Cross	Alodine	Al 6016	1.0 mm	Pre-treat	Yes			5						3		3		3					
			Tension	5200	AL C01C	Al 6016 1.0 mm	Powder-coated	No	5		5						3		3		3					
				5200	A1 0010	1.0 1111	Fowder-coaled	Yes			5					3	3		3			5				
				Dave	AM60B	2.0 mm	Bare	No		5		20		5												
				Bare	Al 6013	2.2 mm	Bare	No		5						3		3		3		20	5			
			Shear				Pre-treat	Yes	5	5						3		3		3						
			Tension	Alodine	Al 6013	2.2 mm	Powder-coated	No		5						3		3		3						
			rension	5200				Yes		5		20		5		3		3		3		20	5			
					HSS DP-590		Armorgalv, zinc-phosphate, Tritop, Universal	No		5						3		3		3						
Mg	Round	8 mm			HSS DP-590	2.0 mm	Armorgalv, zinc-phosphate, E-Coat w/ sealed edges	Yes	5	5		20		5		3		3		3	_	20	5			
AM60B		Diam		Bare	AM60B	2.0 mm	Bare	No	3		5	20		5												
					Al 6013	2.2 mm	Bare	No	5		5						3		3		3	20	)	5		
			Cross				Pre-treat	No			5				_		3		3		3					
			Tension	Alodine	Al 6013	2.2 mm	Powder-coated	No Yes	-		5		20		5		3		3		3	20	,	5		
				5200	HSS DP-590	2.0 mm	Armorgalv, zinc-phosphate, Tritop, Universal	No	5		5						3		3		3					
					HSS DP-590	2.0 mm	Armorgalv, zinc-phosphate, E-Coat w/ sealed edges	Yes			5		20		5		3		3		3	20		5		

Full test matrix for round boss UPJ joints - green squares indicate that work has been completed



 Produced "good" joints (i.e., good head formation, no visible cracks, no observable damage to coatings on joined materials, etc.) from 11 unique material/coating configurations to support mechanical and corrosion performance evaluations. Six examples are shown below:



UPJ8-1 2.0 mm (Armorgalv) DP590 (Bare) AM60



2.2 mm (Pre-treated) Al 6013-T4 (Pre-treated) AM60 Powdercoated Assembly



UPJ8-6 2.2 mm (Powdercoated) Al 6013-T4 (Pre-treated) AM60 Powdercoated Assembly



UPJ8-2 2.2 mm (Bare) Al 6013-T4 (Bare) AM60



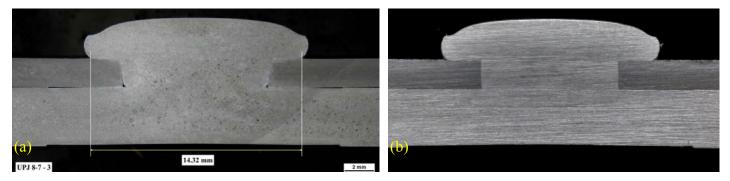
UPJ8-5 2.2 mm (Powdercoated) Al 6013-T4 (Pre-treated) AM60



UPJ8-7 2.0 mm (Bare) AM60 (Bare) AM60



• Evaluated microstructures of round boss UPJ samples.



#### Magnesium Upper Sheet

14.09 mm

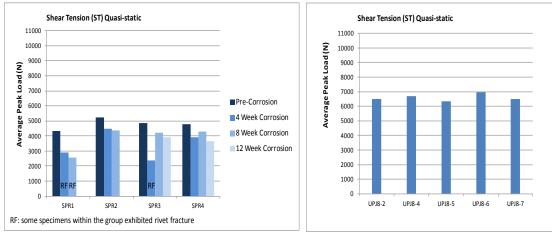
Aluminum Al6013 Upper Sheet

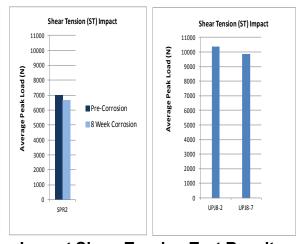
**Steel Upper Sheet** 

• Evaluated pre-corrosion *quasi-static* structural / mechanical performance of round boss UPJ joints and compared to similar performance of SPR joints.

UPJ8-6

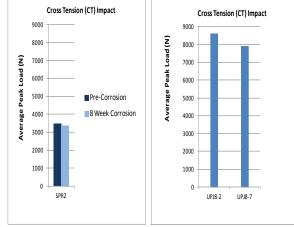
UPJ8-7





#### Quasi-Static Shear Tension Test Results of SPR (before, during, and after corrosion) and UPJ (pre-corrosion only)

Cross Tension (CT) Quasi-static Cross Tension (CT) Quasi-static 9000 9000 Load (N) 8000 8000 Load (N) 7000 7000 Peak 6000 6000 Peak Average 5000 Pre-Corrosion 5000 age 4 Week Corrosion 4000 4000 Aver 8 Week Corrosion 3000 3000 12 Week Corrosion 2000 2000 1000 1000 0 SPR1 SPR2 SPR3 SPR4 UPJ8-2 UPJ8-4 UP18-5 RF: some specimens within the group exhibited rivet fracture



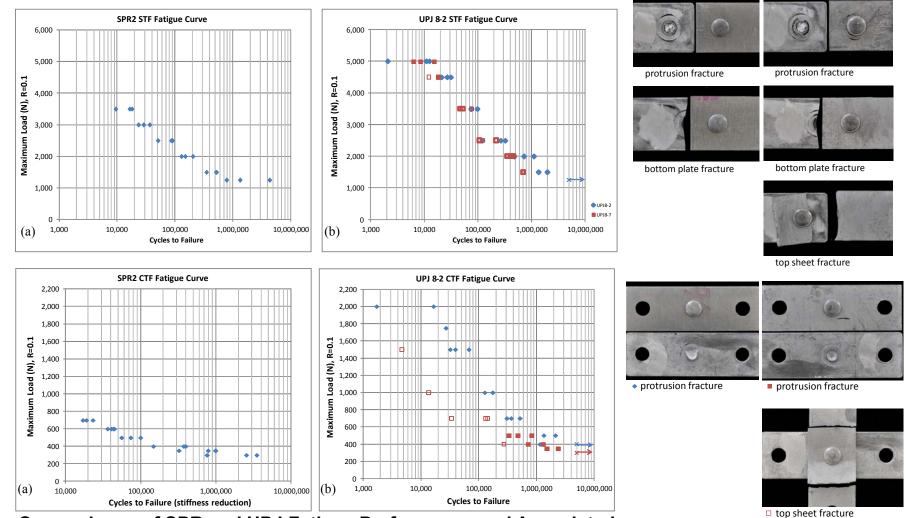
#### Impact Cross Tension Test Results of SPR and UPU

## Quasi-Static Cross Tension Test Results of SPR (before, during, and after corrosion) and UPJ (pre-corrosion only)

Impact Shear Tension Test Results of SPR and UPJ



 Evaluated *fatigue* performance of round boss UPJ joints and compared to performance of benchmark SPR joints.



Comparisons of SPR and UPJ Fatigue Performance and Associated UPJ Failure Modes (Shown on the Right)



#### **Responses to Previous Year Reviewers' Comments**

This project was not reviewed last year.



#### Within the VT Program

- AET Integration, Inc. Industry Primary subcontractor to FCA US
  - Provided weld process development, machining services, joint evaluations, and metallurgical services throughout the project as well as overseeing additional subcontractors, joining SPR coupons, overseeing process modeling simulation efforts, and providing testing and evaluation services for all testing except corrosion.
- Meridian Lightweight Technologies Industry subcontractor to FCA US
  - Provided die cast UPJ test coupons.
- Almond Products Industry subcontractor to AET
  - Provided pretreated and coated magnesium, aluminum, and steel test coupons.

#### **Outside the VT Program**

- McMaster University University collaboration
  - Worked with Canmet to develop magnesium alloy thermo-mechanical compression and electrical resistivity data, and constitutive equations, to support process modeling efforts.
- Canmet Materials (CMAT) Canadian federal laboratory collaboration
  - Provided use of their Gleeble<sup>®</sup> test machines as well as technical assistance to McMaster University researchers in order to obtain thermo-mechanical evaluation and characterization data from cylindrical compression test coupons.

## **Remaining Challenges and Barriers**



- Corrosion performance of UPJ joints for joining dissimilar metals must be validated.
  - Even when coating the cathode before joining, this is <u>not</u> a trivial issue, especially when joining Mg to steel.
- Unique oval boss UPJ joint geometry must be developed to support use of UPJ process on narrow flanges.
- Neither round boss or oval boss UPJ is amenable to joining surfaces where the casting die direction is not perpendicular to the material surface.
- Neither round boss or oval boss UPJ is feasible in joint combinations where neither metal is a casting.



#### FY2015

- Conduct accelerated corrosion evaluation and post-corrosion evaluation of round boss UPJ joints.
- Finish optimizing oval boss UPJ joining processes, produce oval boss UPJ joints, and conduct structural / mechanical evaluation of these joints.
  - These joints will not be exposed to accelerated corrosion aging as there is no reason to expect them to perform differently from the round boss UPJ samples.
- Finish optimizing round boss UCR process for joints that do not include a casting or where the joint surface is not perpendicular to die direction; produce joint evaluation samples, and conduct structural / mechanical evaluation of these joints.

#### FY2016

 Conduct accelerated corrosion evaluation, and conduct post corrosion evaluation of round boss UCR joints.

## Summary



- During the past fiscal year, over 200 Mg to AI SPR joints were produced and evaluated for mechanical and corrosion performance to serve as a benchmark for UPJ performance evaluations.
  - Many benchmark SPR joints were unable to pass the full test exposure prescribed by FCA US Corrosion Engineering without losing joint integrity.
  - Several joints failed as a result of hydrogen embrittlement of the steel rivet.
- Extensive thermo-mechanical material characterization, computer modeling and physical experimentation were used to optimize round boss UPJ process parameters to support production of over 650 assemblies in 11 unique configurations, over 300 of which have been subjected to pre-corrosion mechanical evaluation, and compared to SPR performance.
  - Quasi-static and impact performance substantially improved over SPR.
  - Low cycle fatigue performance substantially improved over SPR while high cycle fatigue performance is similar to SPR.
  - Corrosion performance of round boss UPJ joints yet to be evaluated in FY2015.
- Process simulation and optimization were conducted on oval boss UPJ and round boss UCR to support joining and evaluation work in FY2015.

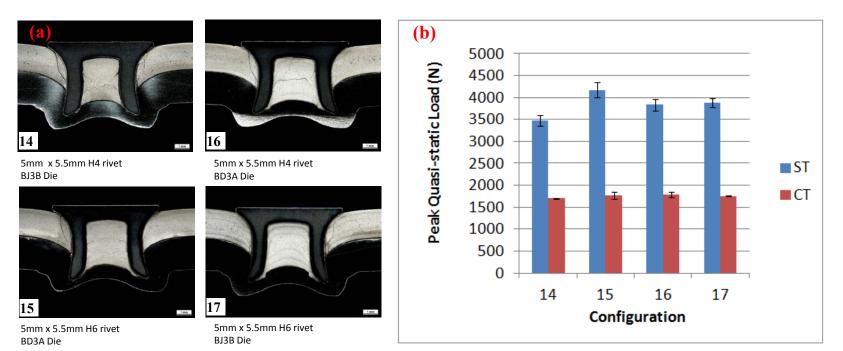
# Acknowledgement of Federal support and Disclaimer

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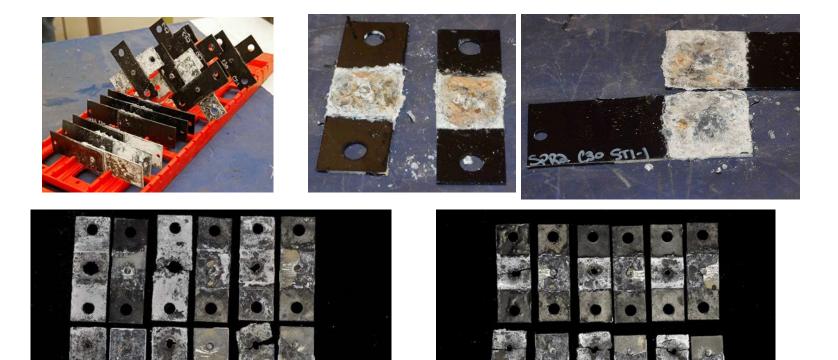
## **Technical Back-Up Slides**

- Established *benchmark* performance of magnesium to aluminum joints produced through SPR.
  - Optimized SPR joining process to produce high quality 2.0 mm Mg AM60B to 2.2 mm Al6013-T4 dissimilar metal joints by evaluating 17 different rivet and die combinations, and down-selecting four that looked most promising (best rivet engagement, least cracking, etc.).

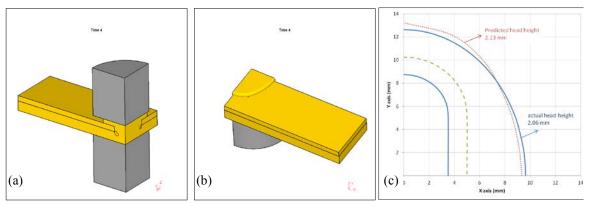


 Configuration 17 was selected to continue development work due to least material cracking and most repeatable results.

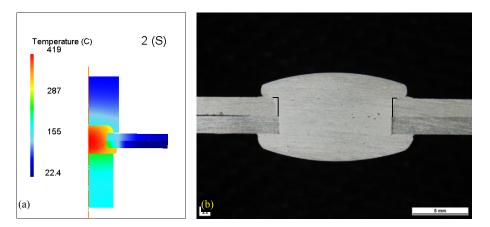
- Established *benchmark* performance of magnesium to aluminum joints produced through SPR.
  - Subjected 122 shear and cross tension assemblies to ASTM G85-A2 accelerated corrosion procedure.



 Conducted initial simulation work and some physical experimentation to develop optimized electrode shapes for *oval joint UPJ* and *round boss UCR* joints for evaluation in the next fiscal year.



Oval Joint Forming Simulation and Head Shape Outline Comparison to Physical Experimental Part



Round Boss UCR Process Simulation and Section Through Actual Experimental Joint



Experimental Oval Boss Head Shape with Hole Shape Superimposed