Premix charge, compression ignition combustion system optimization

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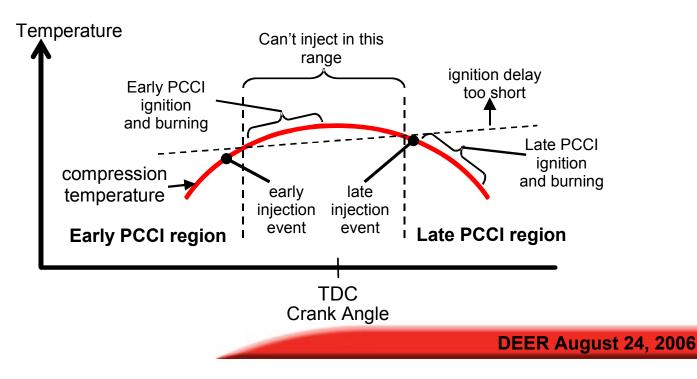




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Project Goals

 Utilize PCCI combustion technology to optimize fuel economy while meeting EPA 2010 emission targets and customer requirements for noise and drivability



Critical Parameters

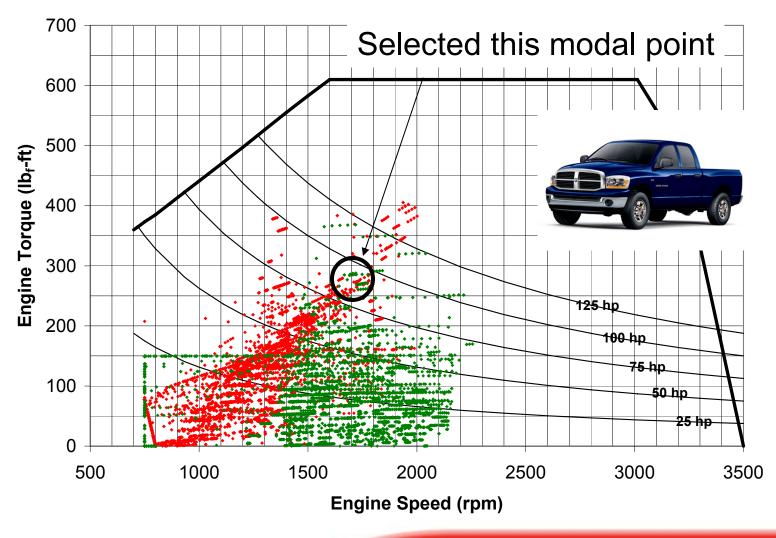




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Narrowing Domain ...





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Narrowing Domain ...

Fresh A/F (λ)

Residual

. . . .

Piston Bowl

Geometric

• Bowl shape

compression ratio

Intake O₂ fraction



- Speed
- IMT (effective)
- Swirl
- Nozzle
 - # holes
 - Angle
 - Flow
 - AFM (hydro-grind)
 - L/D K factor

Injection

- Rail P
- Shape
- Pilots
- Post
- Main

Piston bowl and nozzle characteristics recommended by KIVA computational analysis



Bowl 20



Experimental Method

- Utilized Cummins single cylinder 6.7L test engine
- Used a space filling test plan
 - Rail pressure
 - Two pilot injections
 - Main injection
 - Post injection
 - O₂ intake fraction
 - Fresh A/F ratio

Analysis with response surface quadratic fits (reduced models)



Experimental Results

- fsNOx
- fsPM via smoke (FSN)
- HC
- Fuel consumption
- Combustion noise

Extremely important parameter for the pickup truck and SUV market – difficult technical hurdle for PCCI combustion



Noise Measurement, Calculation ...

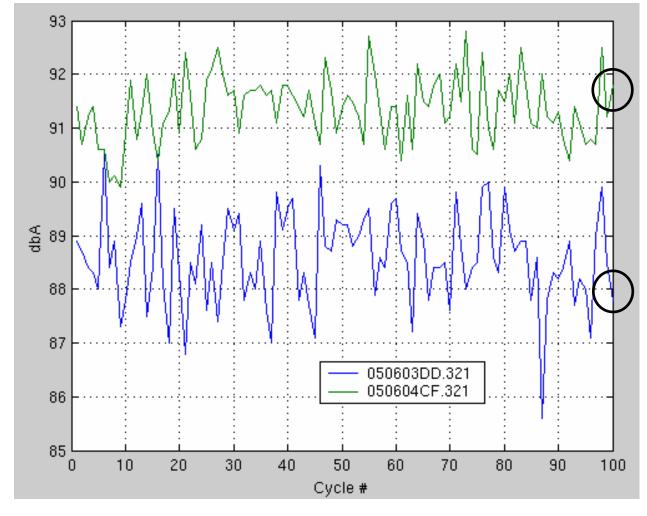
- Simulation of noise meter analyzes each of 100 total cycles per data point, results are tabulated as average of these noise calculations plus deviation
- Method: FFT of cylinder pressure → filtered gains applied → inverse FFT → RMS noise power calc → customer acceptance criteria

Sound Pressure Level:

$$SPL = 10\log\left(\frac{p_{RMS}}{p_{ref}^2}\right) \quad OR \quad SPL = 20\log\left(\frac{p_{RMS}}{p_{ref}}\right) \qquad p_{ref} = 2 \times 10^{-5} \text{ Pa}$$

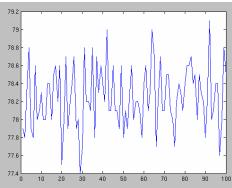
100 Cycle Noise PCCI Combustion

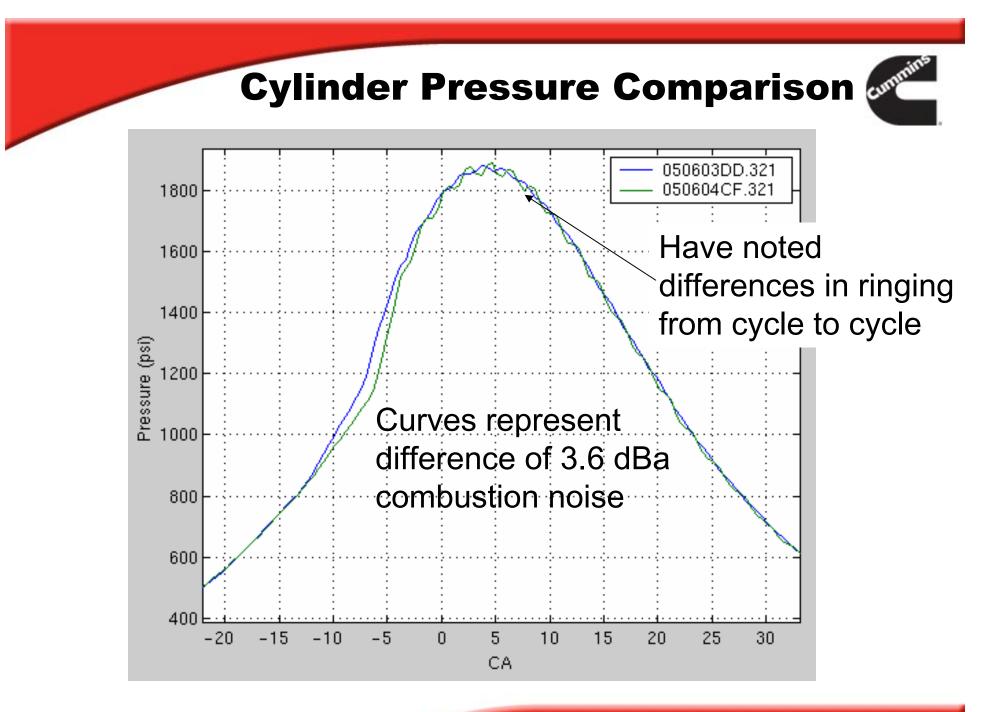




More detailed analysis of these last two cycles

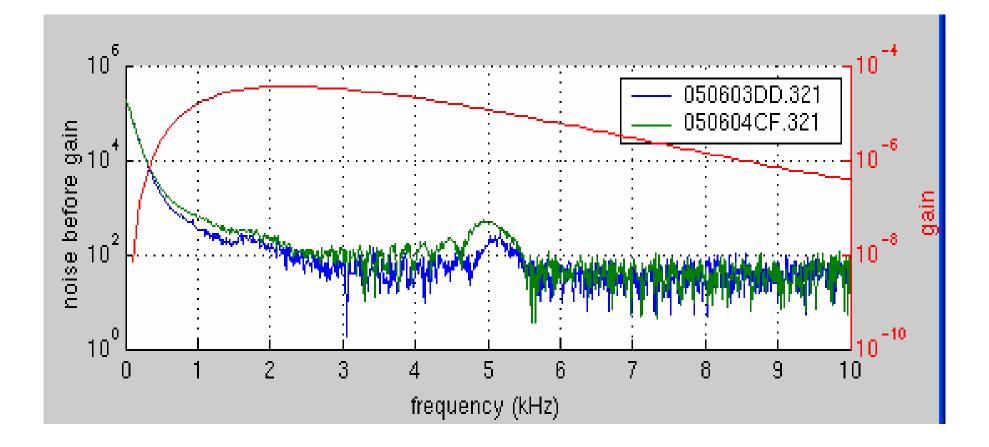
Motoring noise is ~78 dBa





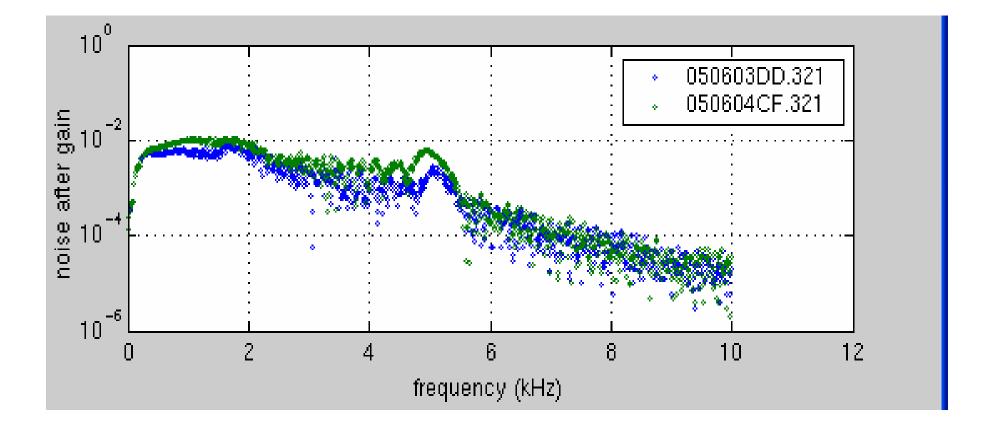
cummins

FFT and Meter Gains

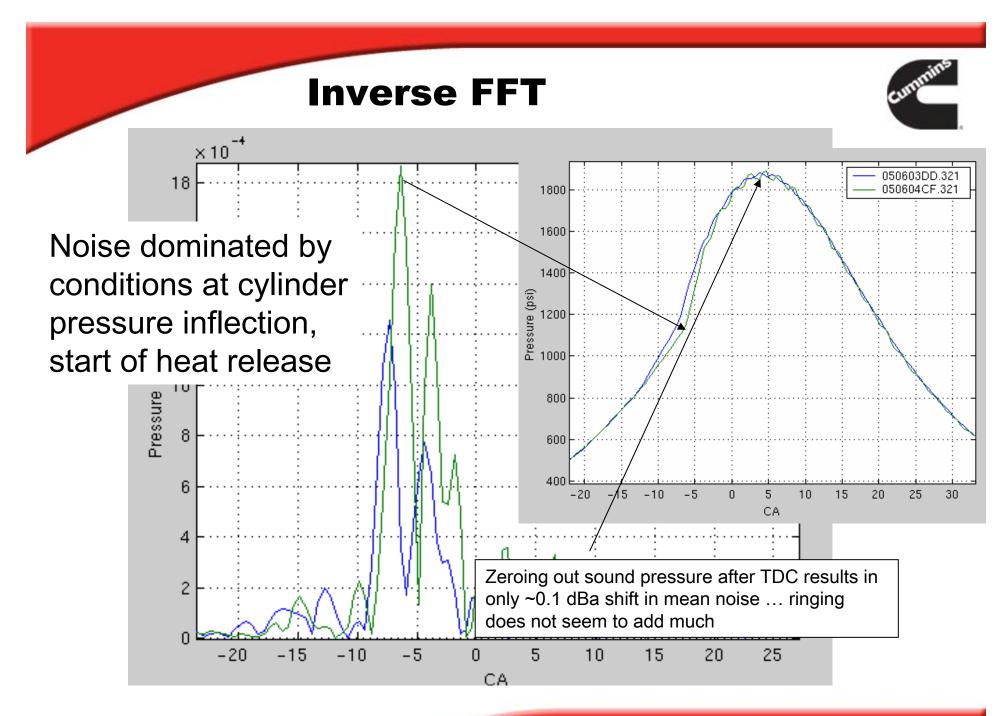




Sound Pressure (after gains)

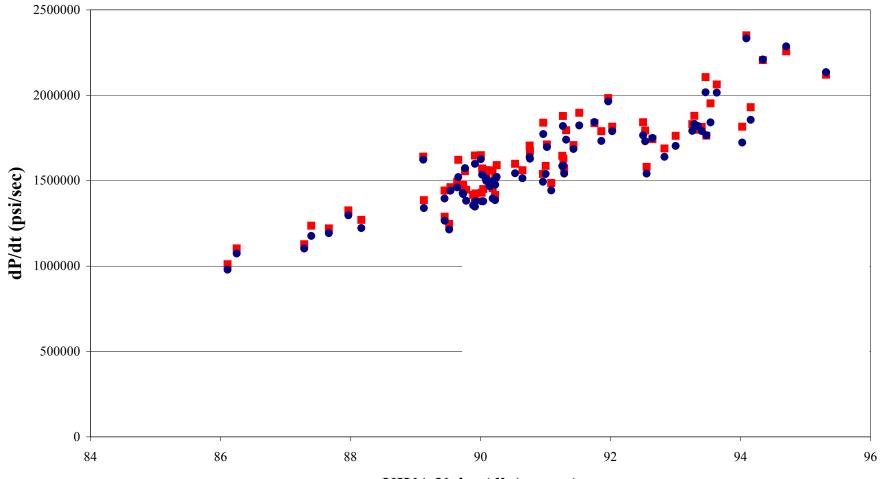






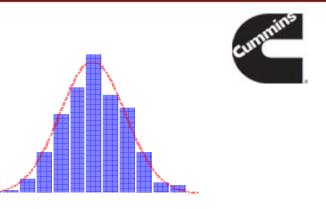
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Rate of Pressure Change



KIVA Noise (dbA mean)

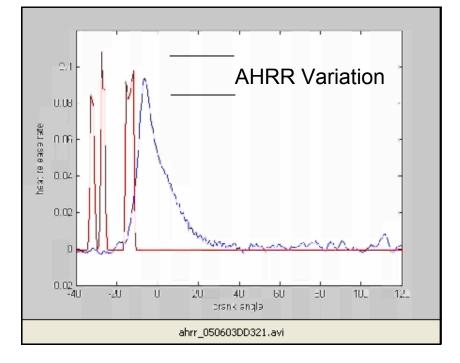
Repeatability of Noise

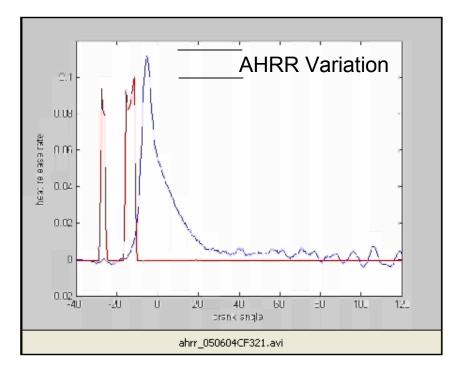


- Engine test repeat points also showed substantial variation of *mean* noise levels ~ 1 dBa, cycle/cycle variation was also of this order
- Analysis of fuel system and air charge conditions did not account for observed noise variation



Noise Variations and Apparent Heat Release ...



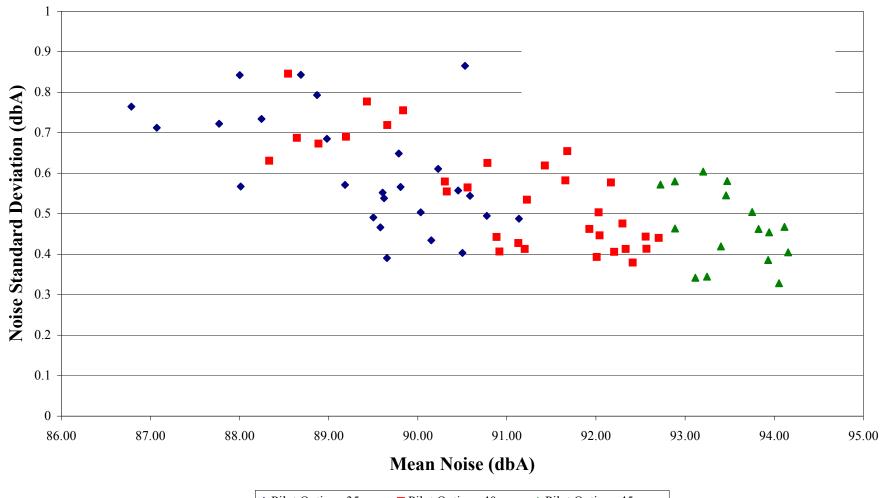


Mean noise = 88.6 dBa Std Dev = 0.9 dBa Mean noise = 91.4 dBa Std Dev = 0.6 dBa Cycle to Cycle σ



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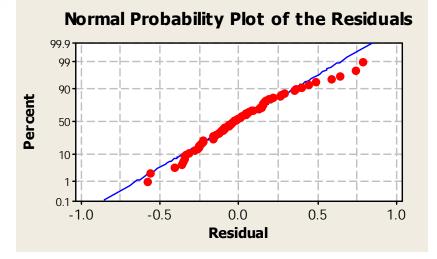
◆ Pilot Ontime .35 msec ■ Pilot Ontime .40 msec ▲ Pilot Ontime .45 msec

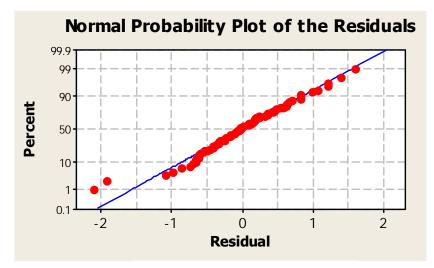


Combustion Noise Conclusions

- Substantial cycle to cycle and mean variation was noted for early PCCI combustion with multi-pulse injection
- Analysis of fuel system and air charge inputs did not account for variation
- Analysis technique appears to be capturing fundamental noise phenomena
- Early PCCI heat release process <u>may</u> have inherently higher variation causing observed noise variation ...
 longer ignition delay has more variation in subsequent heat release ... more investigation required

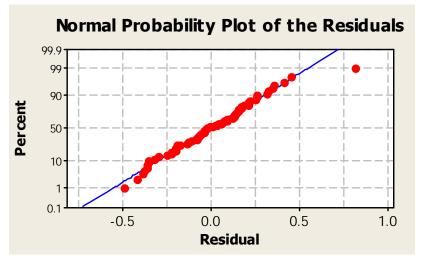
Design of Experiment Fits





Noise, dBa

fsNOx, g/kg



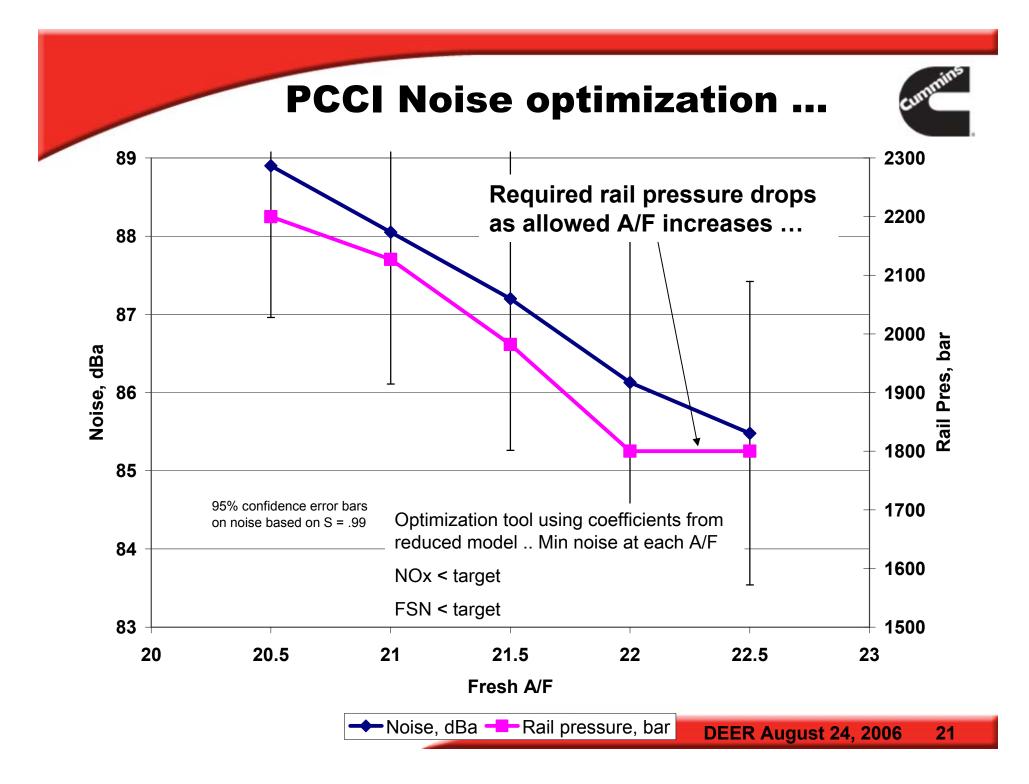
Smoke, FSN

cummin

Optimization ...



- The correlation of experimental results were adequate with noted variation in combustion noise
 - Rail pressure
 - Two pilot injections
 - Main injection
 - Post injection
 - O₂ intake fraction
 - Fresh A/F ratio
- Resulting reduced quadratic models were incorporated in an optimizing software code
- Results for minimum combustion noise meeting emission constraints were obtained for various A/F ratio limits …





Summary

- Experiments indicate that high A/F and EGR rates are critical for meeting emission and noise targets
- Injection pressure requirements are reduced with higher A/F
- Noise targets are difficult to obtain with early PCCI combustion, significant variation noted with multi-pulse pilot with early main injection