

### Performance, Market and Manufacturing Constraints relevant to the Industrialization of Thermoelectric Devices

**2011 Thermoelectrics Applications Workshop** 

Andrew Miner, Ph.D. Founder and CEO Romny Scientific, Inc.



#### **Romny Scientific**

Founded 2006

**Mission**: Driving down thermoelectric module costs to reach broad deployment in new markets.

Integrated Module and Materials Technology Company

Based in Richmond, California





### Industrialization of Thermoelectrics

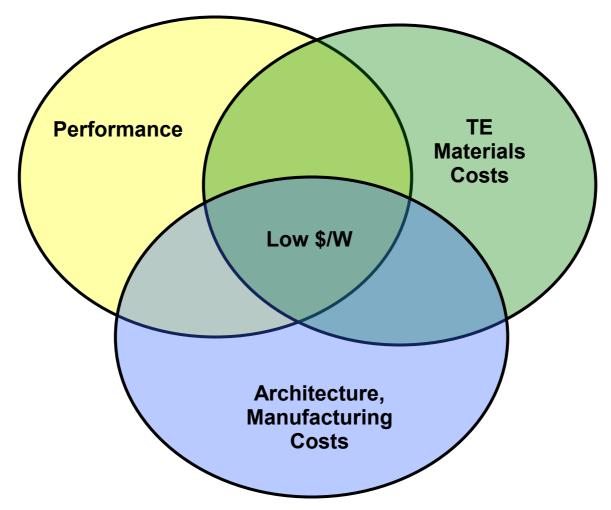
What are the metrics used by the decision makers in volume power generation markets?

Market	Primary Metric	Secondary Metrics
Transportation	\$/Watt	Mass/Watt, Vol./Watt
Portable Power (Military)	Mass/Watt, Vol./Watt, Mass/Watt-Hr	\$/Watt
Portable Power (Commercial)	\$/Watt	Mass/Watt, Vol./Watt
Aerospace	Mass/Watt, Vol./Watt	\$/Watt



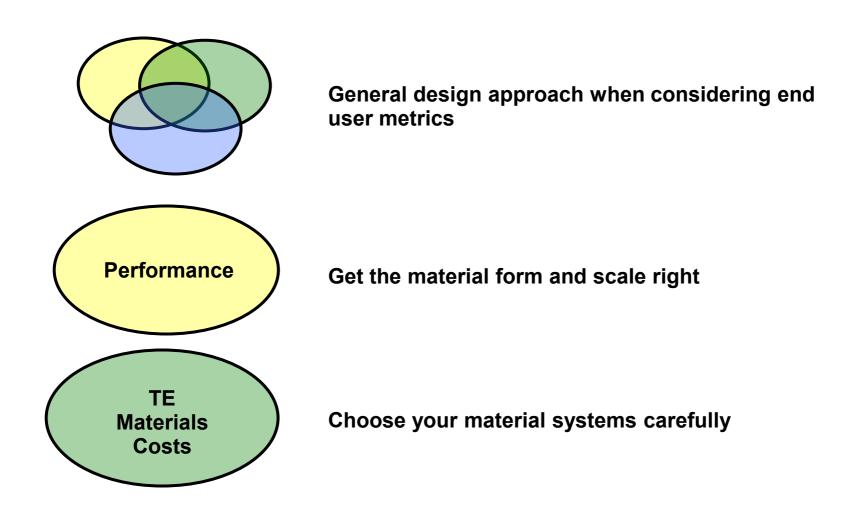
#### Industrialization of Thermoelectrics

Is there overlap that enables high volume industrialization?





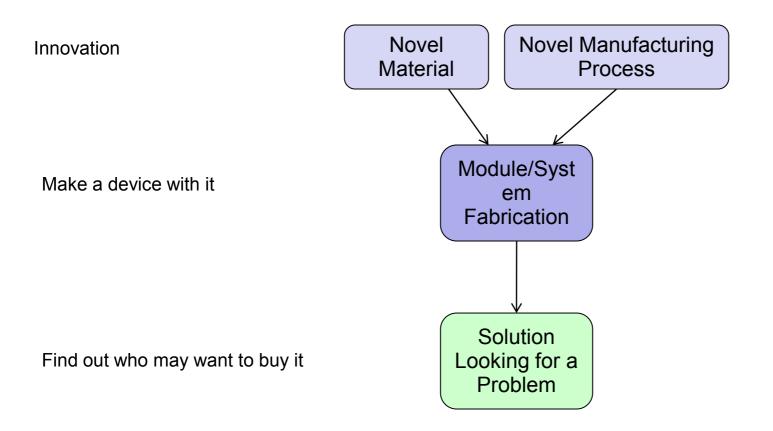
### **Important Factors for Industrialization**



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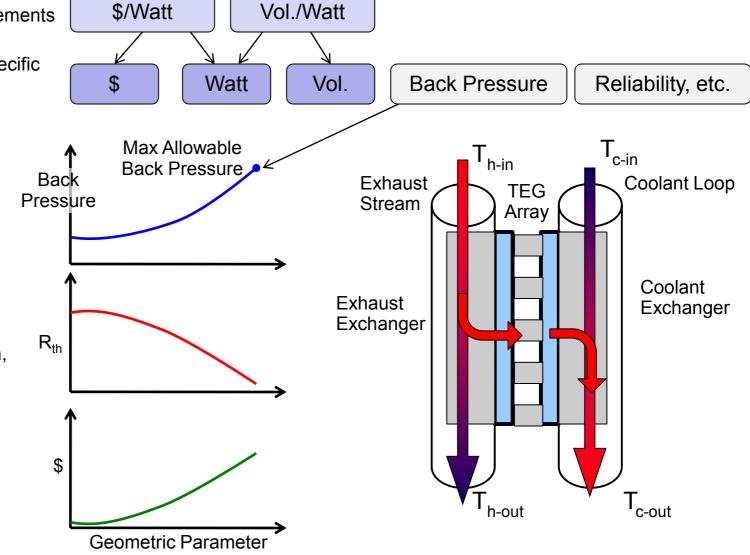
## General design approach (Undesirable Approach)



High Level Customer Requirements

Platform Definition allows Specific Targets to be Defined

Exhaust Side and Coolant Side Exchanger Modeling •Performance characterized by many possible geometric parameters, materials, and constructions •Back Pressure, Rth, and \$ are key to the model •Without \$ as a consideration, optimum design typically seeks min Rth and at Max Back Pressure



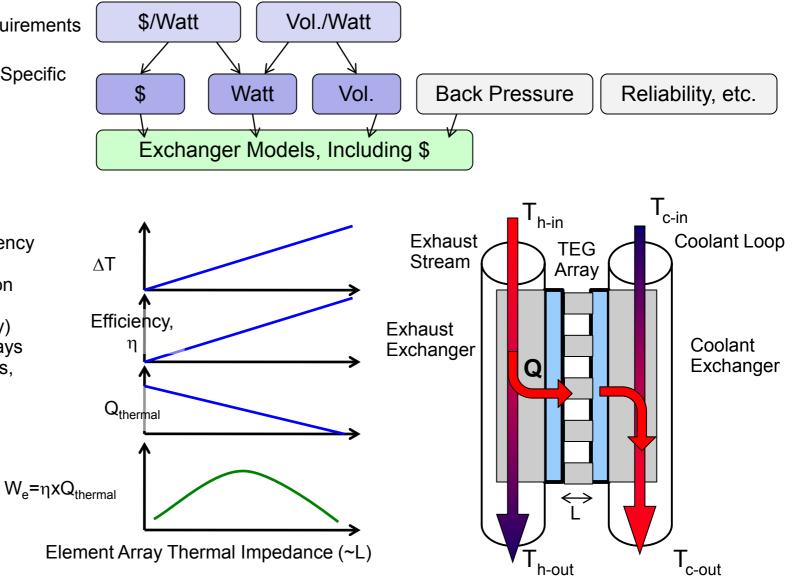
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High Level Customer Requirements

Platform Definition allows Specific Targets to be Defined

**Exchanger Modeling** 

TEG Array Design Optimization •Maximizing DT and efficiency is undesirable (no Q<sub>thermal</sub>) •Maximizing heat extraction from exhaust stream is undesirable (low efficiency) •Low impedance TEG arrays (thin films, nanowire arrays, etc.) generally poor W



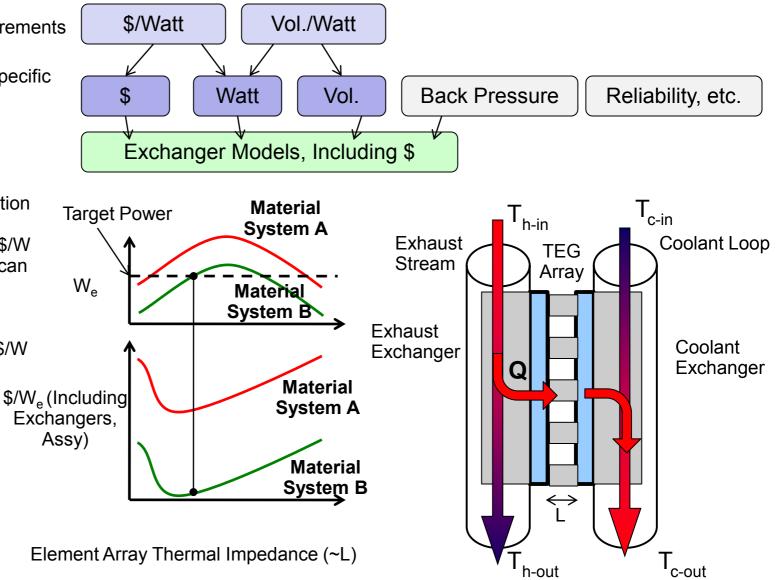
High Level Customer Requirements

Platform Definition allows Specific Targets to be Defined

**Exchanger Modeling** 

TEG Array Design Optimization •Thinner Array = lower \$/W •Low Cost Material = lower \$/W •A minimum acceptable ZT can be determined

•Meets the Design Target Power, and potentially at a \$/W that enables wide market adoption \$/W

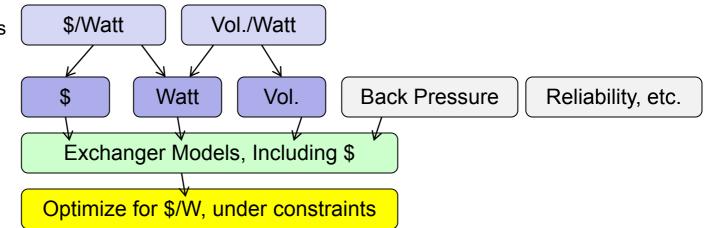


High Level Customer Requirements

Platform Definition allows Specific Targets to be Defined

**Exchanger Modeling** 

**TEG Array Design Optimization** 



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When using end-user metrics for Design Optimization:

Allows one to specify a minimum acceptable ZT for material system
Best design may not be the highest ZT material system
Best design may not be the most efficient heat exchange design
Best material quite likely not a thin film



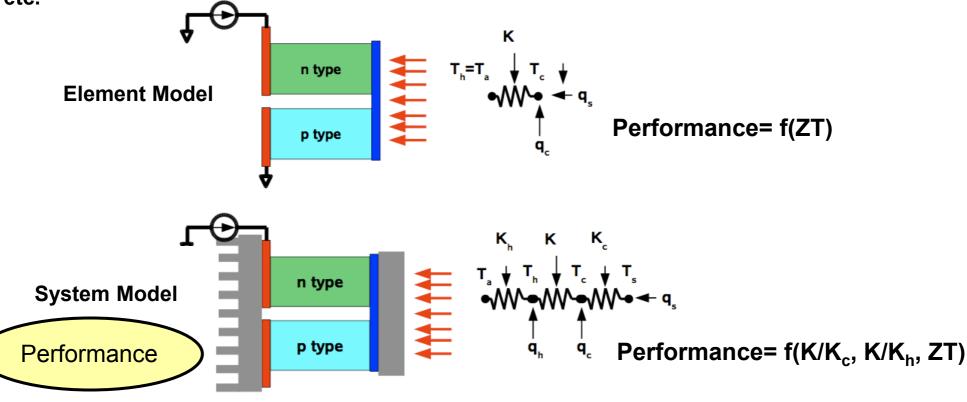
## Get the material form and scale right (Cooling)

A TE Cooler is only as good as its heat sink

#### Thermoelectric System Performance Depends Principally on:

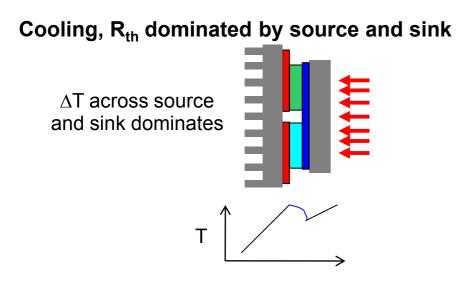
1. The Ratio of the element array conductance to the entry and exit thermal conductance 2. ZT

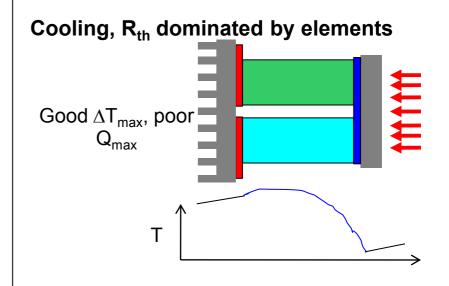
Secondarily, it depends on thermal bypass, interface resistances, compatibility factor, etc.

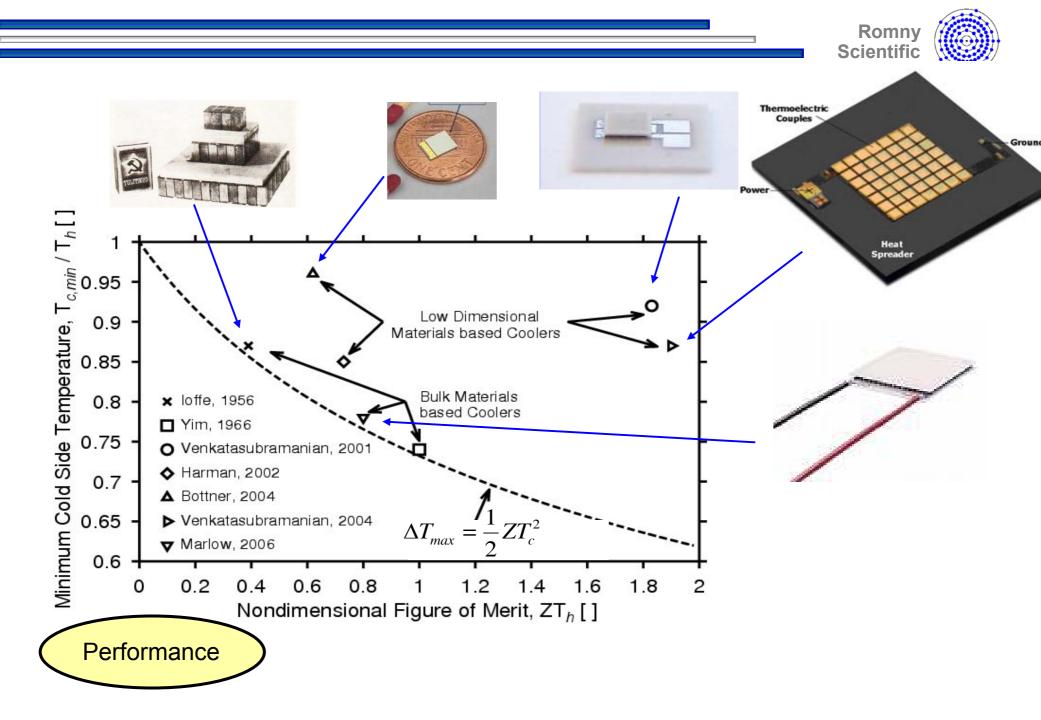




### Get the material form and scale right



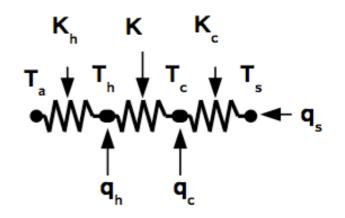




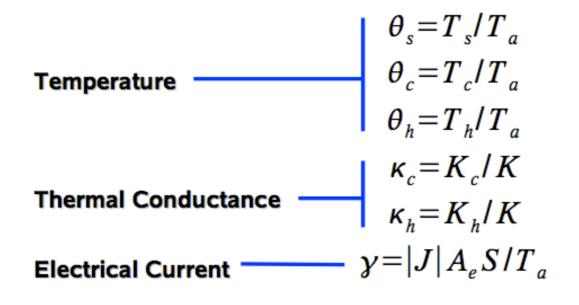


#### Doing the Math System Model: Find Governing Equations

Energy balance at  $T_h$  and  $T_c$ 



Nondimensionalize







### **Non-dimensionalized Cooling Performance**

- Performance ≠ f(ZT)
- Performance =  $f(ZT, \kappa_c, \kappa_h)$ 
  - **Junction Temperatures**

$$\theta_{c}(\boldsymbol{\gamma}) = \frac{(\kappa_{h} + 1 - \boldsymbol{\gamma})(\boldsymbol{\gamma}^{2}/2\mathbf{Z}\mathbf{T}_{a} + \kappa_{c}\theta_{s}) + \boldsymbol{\gamma}^{2}/2\mathbf{Z}\mathbf{T}_{a} + \kappa_{h}}{(\kappa_{h} + 1 - \boldsymbol{\gamma})(\kappa_{c} + 1 + \boldsymbol{\gamma}) - 1}$$
$$\theta_{h}(\boldsymbol{\gamma}) = \frac{(\kappa_{c} + 1 + \boldsymbol{\gamma})(\boldsymbol{\gamma}^{2}/2\mathbf{Z}\mathbf{T}_{a} + \kappa_{h}) + \boldsymbol{\gamma}^{2}/2\mathbf{Z}\mathbf{T}_{a} + \kappa_{c}\theta_{s}}{(\kappa_{h} + 1 - \boldsymbol{\gamma})(\kappa_{c} + 1 + \boldsymbol{\gamma}) - 1}$$

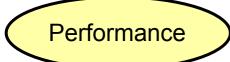
#### **Minimum Cold Side Temperature**

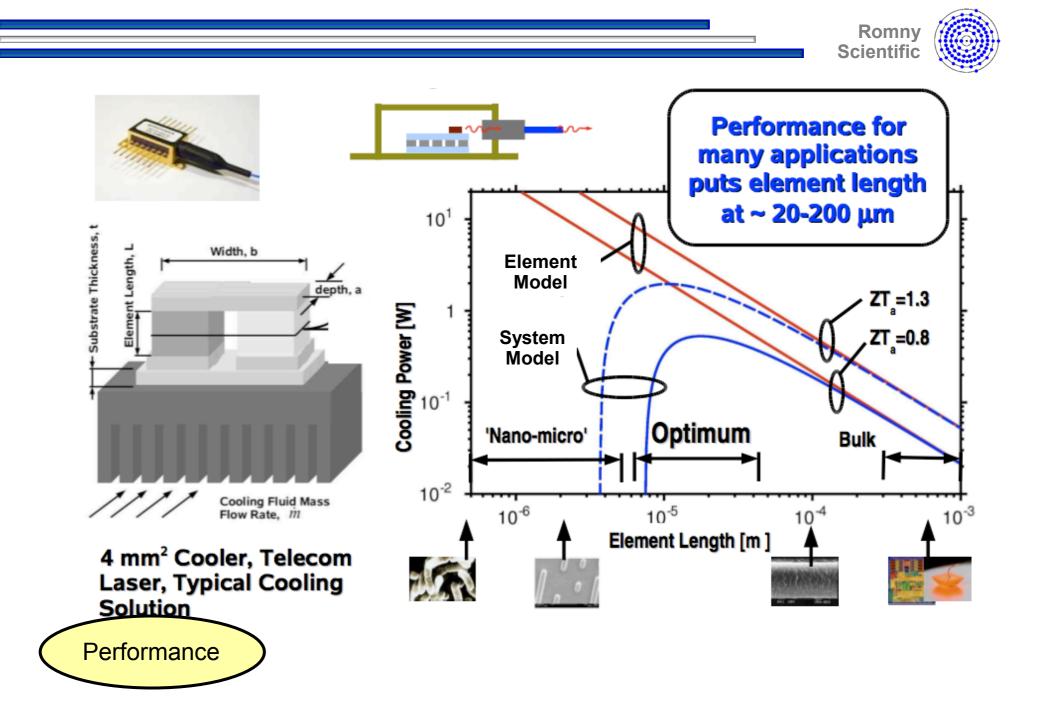
q=0  $\theta_s=\theta_c$ 

$$\theta_{(c,min)} = \frac{(\kappa_h + 2 - \gamma_0)\gamma_0^2/2ZT_a + \kappa_h}{(\kappa_h + 1 - \gamma_0)(\gamma_0 + 1) - 1}$$

**Maximum Cooling Power** 

$$q_{max}/KT_a = (\theta_s - \theta_{c,q_{max}})\kappa_c$$







## **Material Choice for Performance**

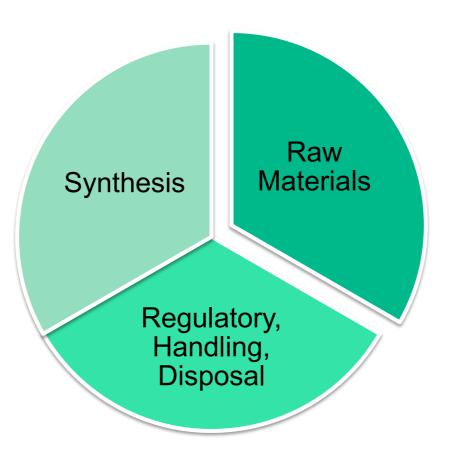
All ZTs are not created equal

Must choose material system capable of being formed at appropriate length scales (thin films face challenges)





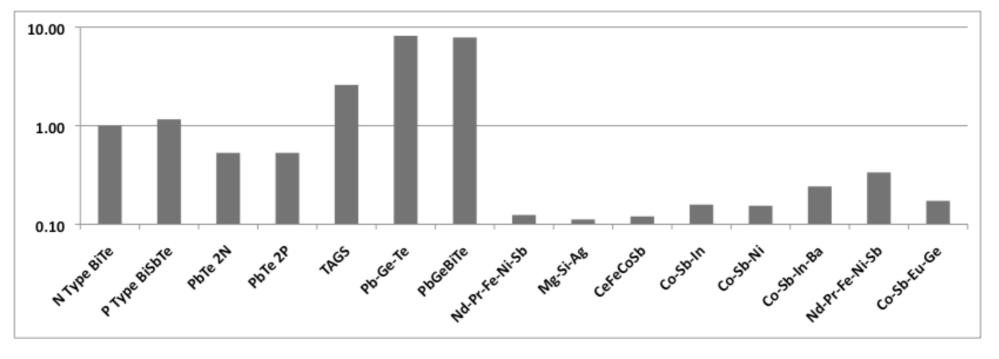
### **Materials Costs**





#### **Materials Costs**

#### **Relative Raw Material Costs (n-BiTe = 1.0)**



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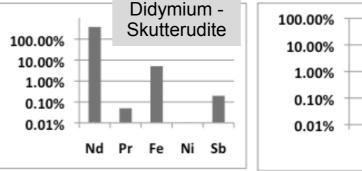
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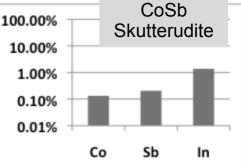


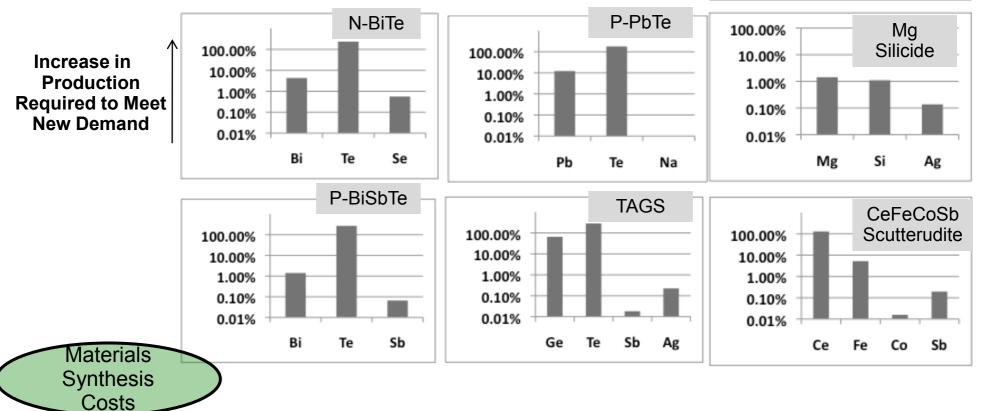
### **Materials Costs**

#### Impact of Thermoelectric Device Ramp on Today's Production Levels

- Assume 500K Unit Production of Automotive TEG Systems
- ~130cc of TE Material per Vehicle





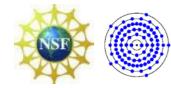


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## **Performance per Cost**

#### Romny's current NSF Funded work on Skutterudites

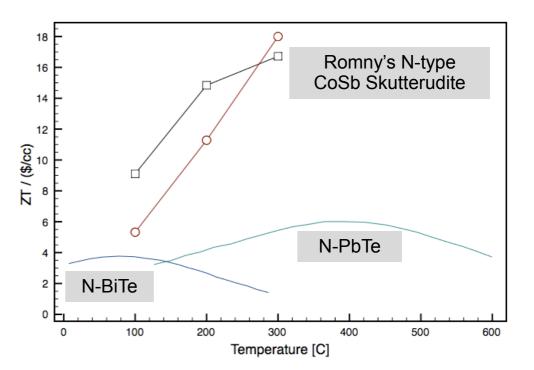
- High Performance per Price
- Integrated into Novel Module MFG process



#### Focus of Current DOE/NSF Funded effort with VT (Huxtable, et. al.)

Mg-Si based alloys







#### Industrialization of Thermoelectrics

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