NOx Abatement Research and Development CRADA with Navistar Incorporated

(successor to International Truck and Engine Corporation)

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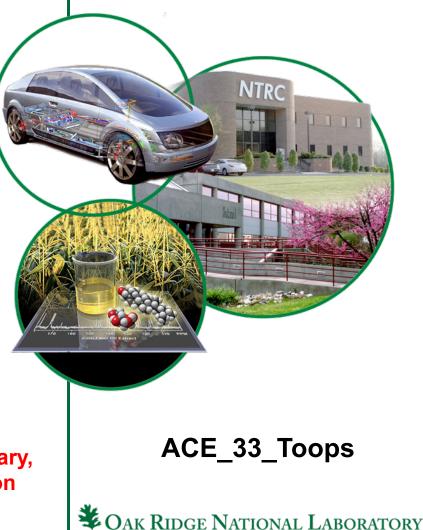
Vadim Strots and Ed Derybowski Navistar/ITEC

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May 21, 2009

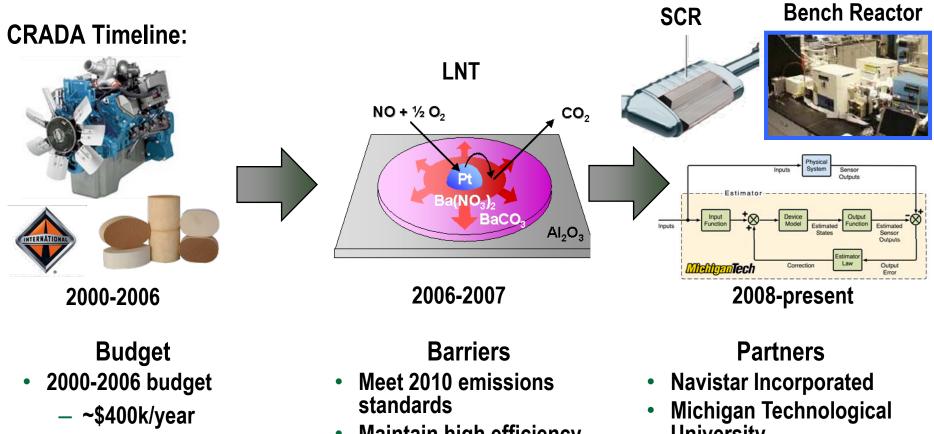
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NOx Abatement R&D – Navistar CRADA **Project Overview**



- **Funding for FY08** •
 - \$125k
- Funding for FY09 – \$125k

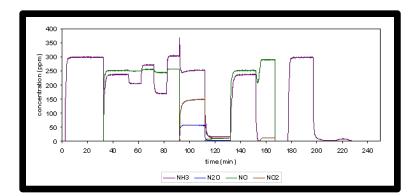
- Maintain high efficiency
- **Control SCR performance** •
 - Minimize NOx and NH₃ emissions

University



NOx Abatement R&D – Navistar CRADA Objectives

- Enable maximum fuel economy while meeting emissions regulations
 - Modeling and understanding emissions control devices critical to efficient operation
- Obtain accurate temperature dependent data under transient operation
 - Performance data and rate parameters
 - Define key catalyst characteristics and storage capacity



 Evaluate sensors for on-board diagnostic (OBD)



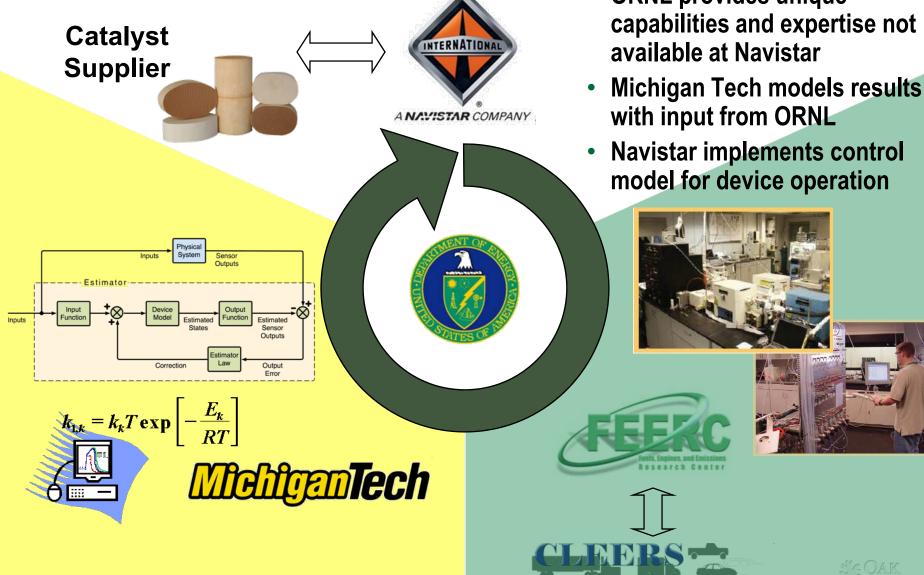


NOx Abatement R&D – Navistar CRADA Milestones

- FY 08 (<u>Completed</u> September 30, 2008)
 - Evaluate at least two LNT samples in bench flow reactor to establish relationship between space velocity, temperature, and product selectivity
 - FY 09 (<u>On Target</u> for September 30, 2009 completion)
 - Evaluate NH₃ storage and reactivity on fresh and aged fully-formulated urea SCR catalysts



NOx Abatement R&D – Navistar CRADA Approach · ORNL provides unique



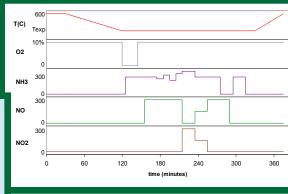
2009-03 ACE 33 toops



NOx Abatement R&D – Navistar CRADA Technical Accomplishments

- Established SCR test protocol that provides critical transient and steady-state conditions for a given temperature
- Evaluated fresh zeolite-based SCR catalyst using protocol at nine temperatures and two space velocities as of March 2009
- Evaluated NOx sensor while operating protocol
- Automated bench reactor to allow unattended operation
 - Meets ORNL's stringent safety regulations



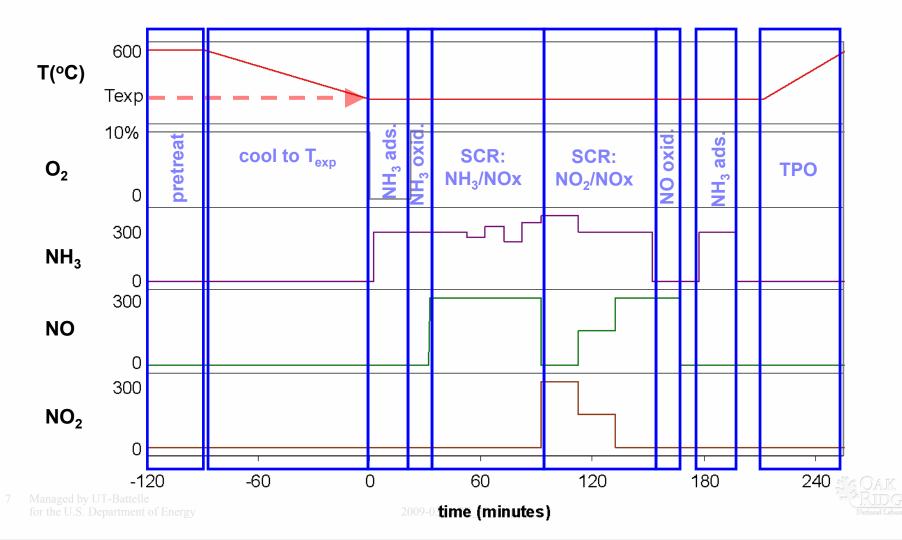






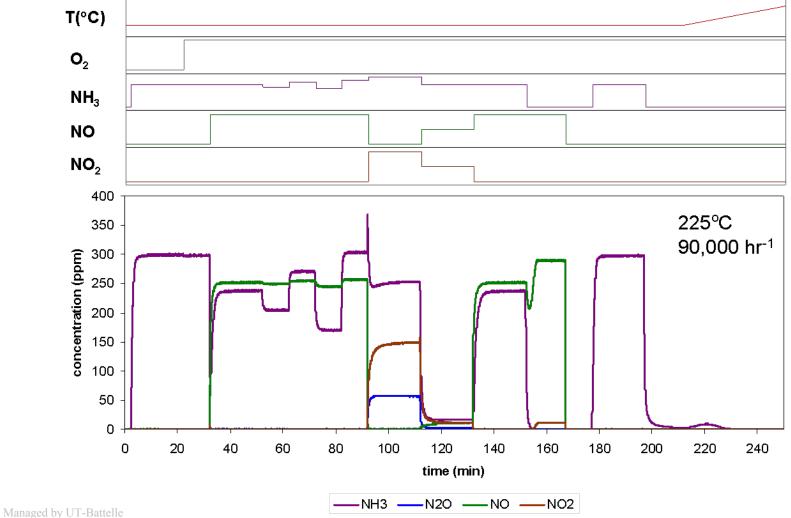
Evaluation Protocol Developed for SCR

- CLEERS SCR focus-group has developed a <u>steady-state</u> SCR protocol
- Accurate models also require transient data; especially for system control
- CRADA-developed protocol provides both transient & steady-state model parameters



Protocol reveals characteristic transient chemistry of catalyst

• Planned protocol evaluated at 150-600°C, 30k-120k h⁻¹, inlet NOx: 150-500 ppm



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Steady-State Results

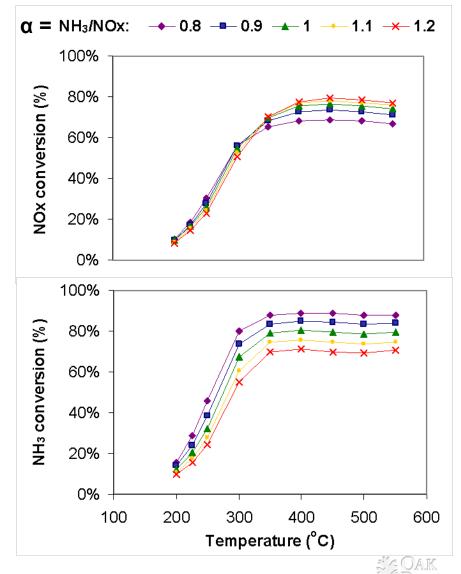


Varying NH₃/NOx (α-ratio) and T demonstrate operating range of catalyst

- Generally, expected trends observed
 - With increasing temperature:
 - NOx and NH₃ conversion increase
 - With increasing NH_3 dose (α-ratio):
 - NOx conversion increases
 - NH₃ conversion decreases

Experiment conditions:

- SV = 90,000 hr⁻¹
- $NO_2/NOx = 0$
- α = NH₃/NOx = 0.8, 0.9, 1.0, 1.1, 1.2
- Total NOx = 300 ppm
- $10\% O_2, 5\% CO_2, 5\% H_2O$

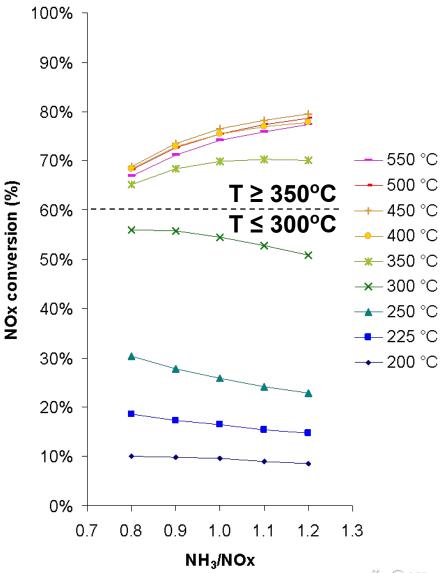


NH₃ inhibits **NO-SCR** reaction at low **T**

- Re-plotting data as a function of NH₃/NOx ratio reveals NH₃ inhibition
- For T ≤ 300°C, increasing NH₃ decreases NOx conversion
 - Indicates inhibition of NO-SCR reaction by excess NH₃ at low T
- Trend previously reported for zeolite-SCR
 - M. Wallin et al., J. Catal. 218 (2003) 354
 - A. Grossale et al., Catal. Today 136 (2008) 18
- Temperature of inhibition is catalyst dependent

Experiment conditions:

- SV = 90,000 hr⁻¹
- $NO_2/NOx = 0$
- $\text{ NH}_{3}/\text{NOx} = 0.8, 0.9, 1.0, 1.1, 1.2$
- Total NOx = 300 ppm
- $10\% O_2, 5\% CO_2, 5\% H_2O$





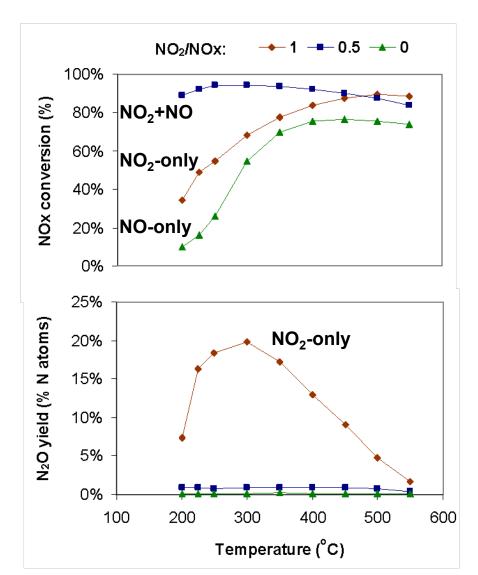
NO₂ more reactive than NO at all T

- As expected, 1:1 mixture of NO+NO₂ gives best performance
 - "Fast SCR" reaction
- However, NO₂ more reactive than NO at all temperatures
 - "Slow SCR" reaction not observed with NO₂
 - NO-only is "slowest" reaction
 - Characteristic of zeolite catalyst
 - A. Grossale et al. Catal. Today 136 (2008) 18
- NO₂-SCR reaction only contributor to N₂O formation

Experiment conditions

- SV = 90,000 hr⁻¹
- NO₂/NOx = 0, 0.5, 1.0
- $NH_3/NOx = stoichiometric$
- Total NOx = 300 ppm
- $\quad 10\% \ O_2, \ 5\% \ CO_2, \ 5\% \ H_2O$

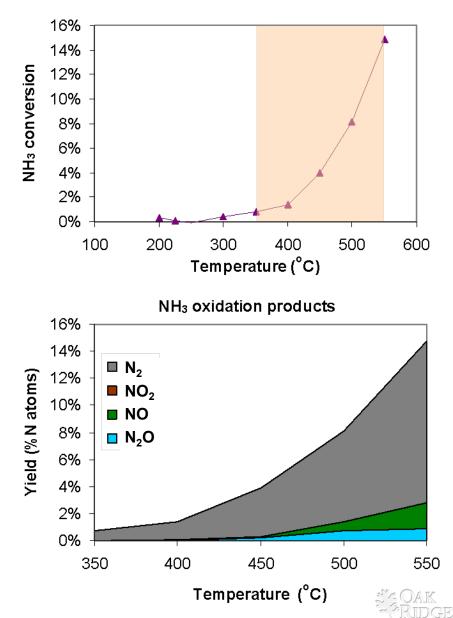
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NH₃ oxidation observed above 350°C

- NH₃ oxidation increases rapidly above 350°C
- Catalyst selective for N₂ production from NH₃ oxidation
 - Typically oxidized to NO over precious metals
- Model must account for losses of NH₃ to direct oxidation
 - but not for additional NO formation

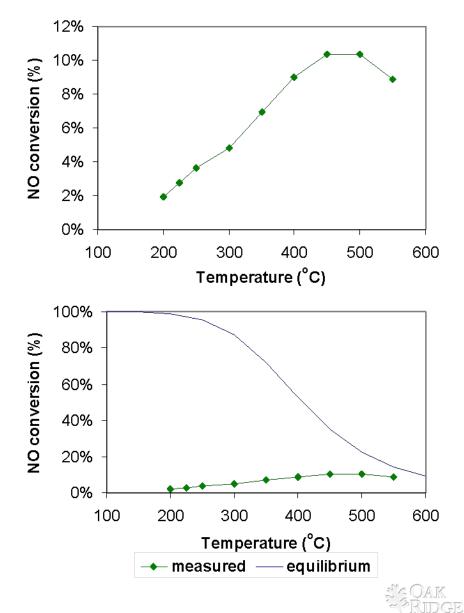


Experiment conditions

- SV = 90,000 hr⁻¹
- 300 ppm NH₃, 10% O₂, 5% CO₂, 5% H₂O

NO-oxidation peaks at 450-500°C

- NO oxidation increases with temperature up to 450°C
- Conversion decreases above 500°C
 - NOx concentrations approach equilibrium values ∴ reaction slows



Experiment conditions

- SV = 90,000 hr⁻¹
- 300 ppm NO, 10% O₂, 5% CO₂, 5% H₂O

Transient Results

All surface NH₃ oxidizes or desorbs at temperatures above 400°C

- NH₃ storage capacity probed at two points:
 - 1. NH₃ uptake during step change at inlet
 - Absence of O₂
 - NH₃ stored at all temperatures
 - Storage decreases as T increases
 - 2. Temperature Programmed Oxidation (TPO) performed after lean NH₃ storage
 - Single <u>desorption</u> peak centered near 300°C
 - All NH₃ released/oxidized by 400°C
- All NH₃ stored at T ≥ 400°C oxidized by O₂ or desorbed when NH₃ flow stops

Experiment conditions

- SV = 90,000 hr⁻¹
- NH₃ Ads: 300 ppm NH₃, 0-10% O₂, 5% CO₂, 5% H₂O
- TPO: 10% O₂, 5% CO₂, 5% H₂O, 5°C/min ramp

NH₃ uptake - inert conditions 200°C 350 NH₃ concentration (ppm) -225°C 300 -250°C 250 300°C 200 ·350°C Increasing 150 400°C 450°C 100 500°C 50 550°C 0 bypass 2 3 Time (min) **TPO after lean NH**₃ uptake $\mathsf{T}_{\mathsf{ads}}$ 20 -200°C NH₃ concentration (ppm) -225°C NH₃ 15 –250°C desorption -300°C 350°C 10 400°C 450°C 5 500°C 550°C 0 3°C OAK 100 200 400 500 300 600 Temperature (°C)

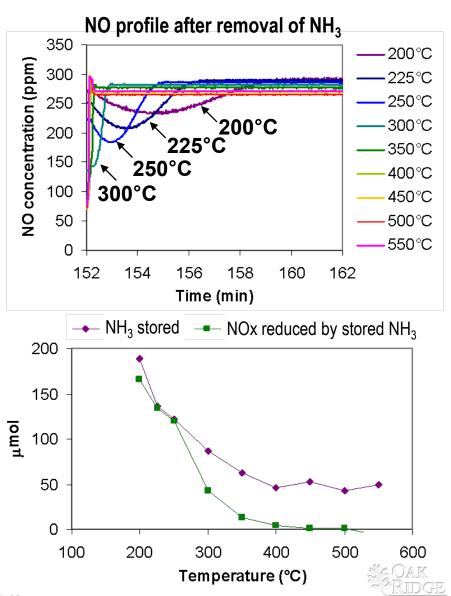


Stored NH_3 not available for subsequent NO_x reduction above 350°C

- NO oxidation step provides another measure of NH₃ storage capacity
 - NO feed constant at 300 ppm after NH₃ turned off
 - Dips in NO concentration due to conversion by stored NH₃
 - Rate of stored NH₃ consumption (depth of dip in NO) increases with T
- Comparison to NOx uptake under inert conditions confirms oxidation or desorption of previously stored NH₃

Experiment conditions

- SV = 90,000 hr⁻¹
- $\quad 300 \text{ ppm NO, } 10\% \text{ O}_2\text{, } 5\% \text{ CO}_2\text{, } 5\% \text{ H}_2\text{O}$



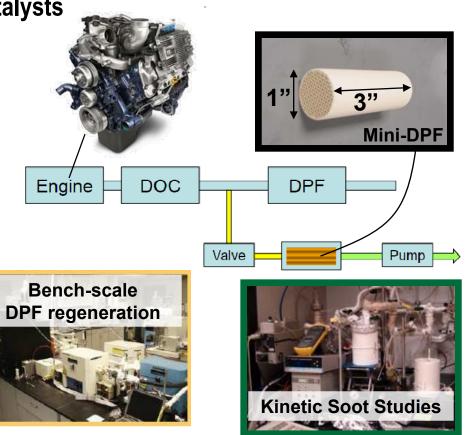
Optimization of protocol necessary

- Current research plan requires ~300 hours of catalyst evaluation
 - Planned protocol evaluated at 150-600°C, 30k-120k h⁻¹, inlet NOx: 150-500 ppm
 - Eight weeks of normal workday operation
- Protocol must be optimized to aid new catalyst transitions
 - Identify most critical experiments through model parameter sensitivity analysis
 - Experiments with low sensitivity are removed from the matrix
- Work through CLEERS to relate complete and optimized protocol



NOx Abatement R&D – Navistar CRADA Future Plans

- Fully execute protocol under all conditions and space velocities
 - Vary total NOx level and increase space velocity up to 120k h⁻¹
- Complete model development and protocol optimization
- Evaluate model parameters with aged catalysts
- New direction for FY10: DOC and DPF regeneration kinetics
 - DPF regeneration has large impact on fuel economy
 - Soot to be collected on production or production-intent Navistar engines
 - Explore effects of advanced combustion modes
 - Hydrocarbons generated and effect on soot oxidation



NOx Abatement R&D – Navistar CRADA Summary

- Established evaluation protocol providing both steady-state and transient chemistry
 - Benefits experimental and modeling community in addition to Navistar
 - Optimized protocol will economize experiments
 - Starting point for validated CLEERS SCR protocol for transient behavior
- Several key SCR-chemistry findings
 - Stored NH₃ reactivity identified specifically for reactivity to NOx reduction
 - NH₃ identified as an inhibiting species at low temperatures
 - Temperature dependent NH₃ storage identified
- Detailed transient and steady-state data generated for CRADA partner and model
 - Additionally benefits systems level modeling efforts (PSAT)
 - Current plans are to publish model and data

