

# **Materials Compatibility of Power Electronics**

**B. L. Armstrong, D. F. Wilson, C. W. Ayers, S. L. Campbell**

**And**

**S. J. Pawel**

**Oak Ridge National Laboratory**

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**This presentation does not contain any proprietary or confidential information.**

# Overview—Technical Work Has Been Ongoing For Approximately Two Years

## Timeline

- Start – March 2008
- End – Sep 2010
- Percent complete – 70%

## Budget

- Total project funding
  - DOE – \$493K
- Funding in FY08 -- \$200K
- Funding in FY09 -- \$175K
- Funding for FY10 -- \$118K

## Barriers

- Barriers addressed
  - A. Cost of high temperature integrated power electronic (HTIPE) systems
  - D. Abuse tolerance and ruggedness of HTIPE systems
  - E. Weight, volume and thermal control of HTIPE systems

# **Objectives Addresses Needs Within the Propulsion Materials Program**

- **Develop and validate a laboratory methodology to evaluate the degradation of power electronics materials/components by evaporative cooling liquids**
  - **Direct cooling of components will allow for reduction of weight and volume of systems**
  - **Methodology will allow for expression of abuse tolerance and ruggedness of HTIPE**

# Milestones—Are Focused On Addressing Performance

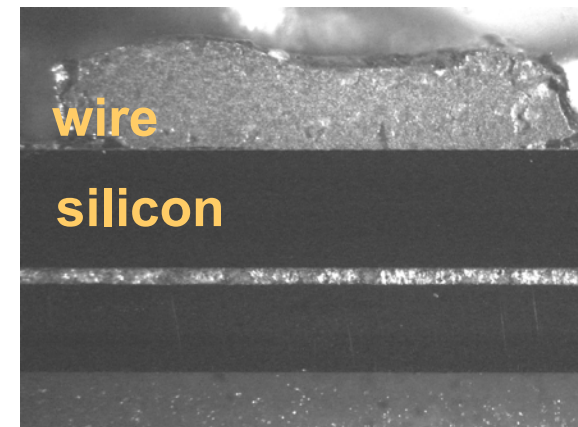
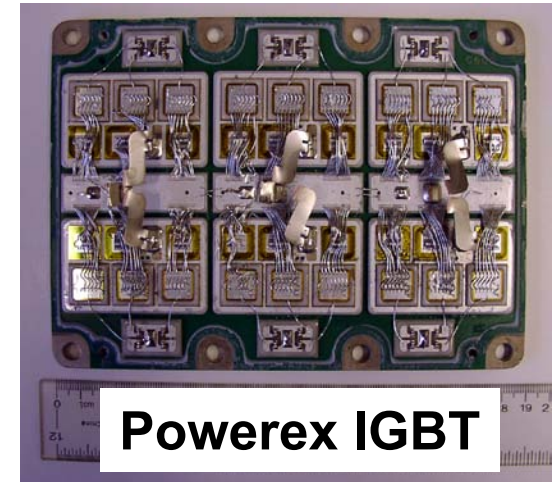
- Develop methodology to evaluate the interaction of the power electronic components with the fluids used in the evaporative cooling systems. Initiate testing of methodology (09/08) *Achieved*
  - Built test system and acquired commercially produced test specimens
  - Initiated testing
- Validate the proposed methodology for examining the interaction of the electrical components with evaporative coolant. (09/09) *Achieved*
  - Collected and evaluated test data
  - Modified test parameter
  - Related data to material/component performance
  - Define “go/no-go” of failure as related to materials/component performance *Material Failure Demonstrated*

# Milestones—Are Focused On Addressing Performance

- **Initiate mapping of materials compatibility space of power electronics with appropriate evaporative coolant. (09/10)** *On track*
  - One coolant
    - No consensus on what will replace R134a
  - Two configurations (circular and rectangular cross-sections) of wires
    - Does similar material failure mode occur
  - Refine “go/no-go” criteria of failure
    - Separate effects due to methodology from that due to coolant
      - Variables include coolant, current, cycle time
  - Confirm feasibility of cooling approach and develop minimum test data that allows for a meaningful dialogue with system designers

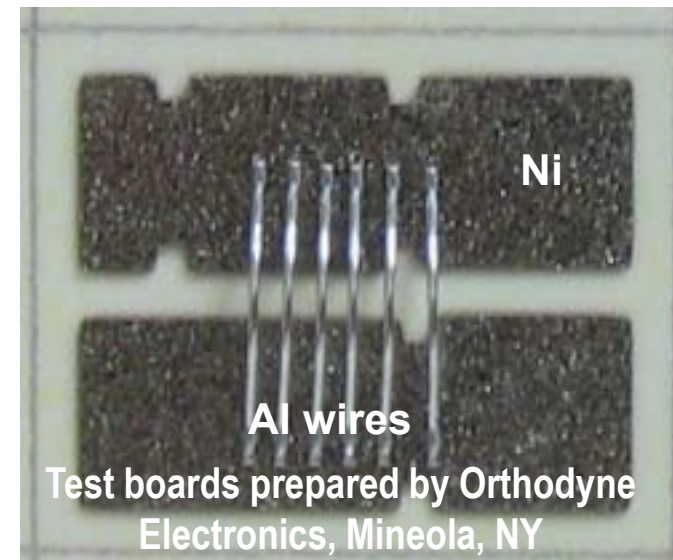
# Compatibility Addresses Barriers/Design Criteria of Automotive Industry

- Barriers to deployment of power electronics (PEs) are:
  - Weight, size, reliability and cost
- Approach to decrease weight, size, and cost of PEs is to use:
  - Direct cooling of PEs by side-stream cooling from existing air-conditioner (A/C) systems using R134a refrigerant
    - Reduces weight of PEs
    - Eliminates secondary cooling system
- Direct side-stream cooling necessitates evaluation of PEs compatibility with and reliability in the coolant



# **In Addition, Because of the Anticipated Low Reaction Rates in R134a, An Accelerated Test Was Sought**

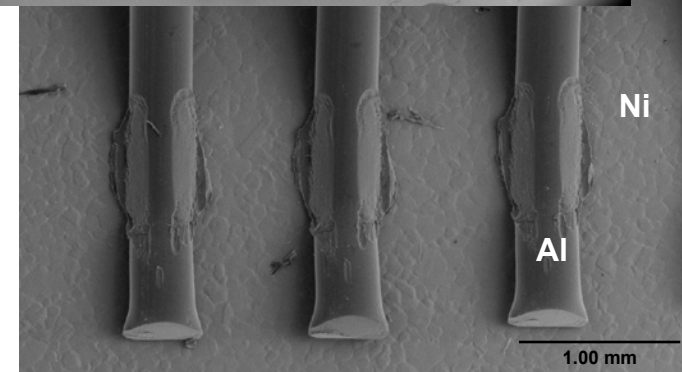
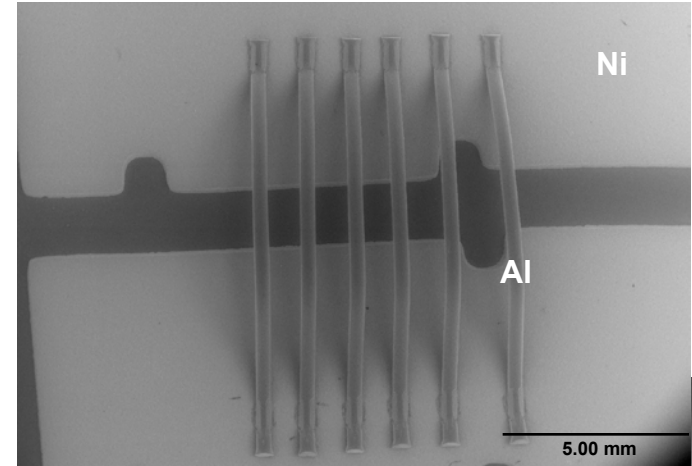
- **Mimic in service use**
- **Exacerbate nucleate boiling effects**
- **Maximize effect of impurities**
- **Aggravate thermal mechanical stress**
- **But does not change the in-service failure mechanisms**



# An Integrated Approach to Compatibility Issues Has Been Developed

- Effect of coolant on the PEs materials
  - Aluminum, nickel (general corrosion)
  - Bonds of aluminum and nickel (galvanic corrosion)
  - Polymeric materials
- Effect of nucleate boiling on the surface of the metals
- Effect of impurities in the coolant
  - Off-the-shelf or a result of interaction with containment materials
- Effect of thermal stress on the PEs materials
- Evaluation of synergistic effects

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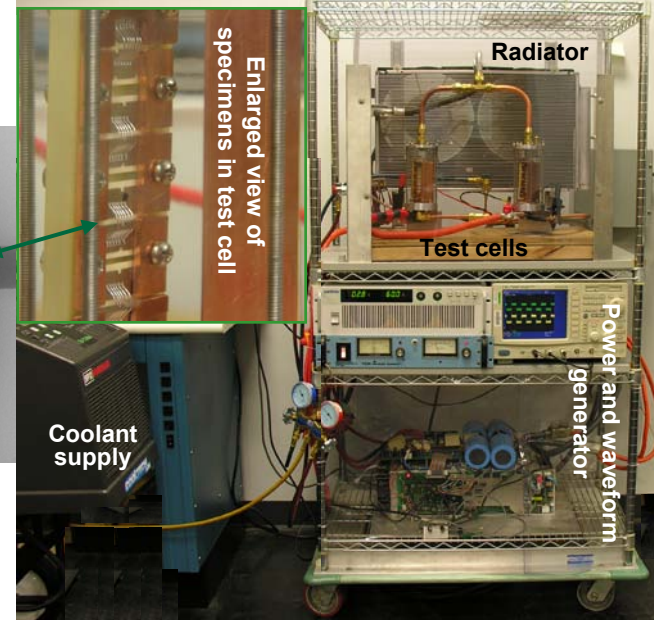
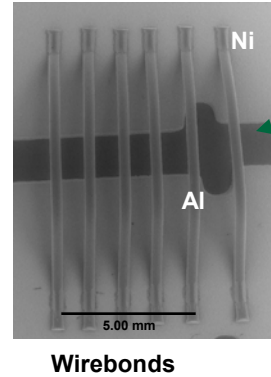
- Bonds all show uniform contact area and deformation associated with the bonding process



# A Test System Was Designed and Built for Accelerated Evaluations

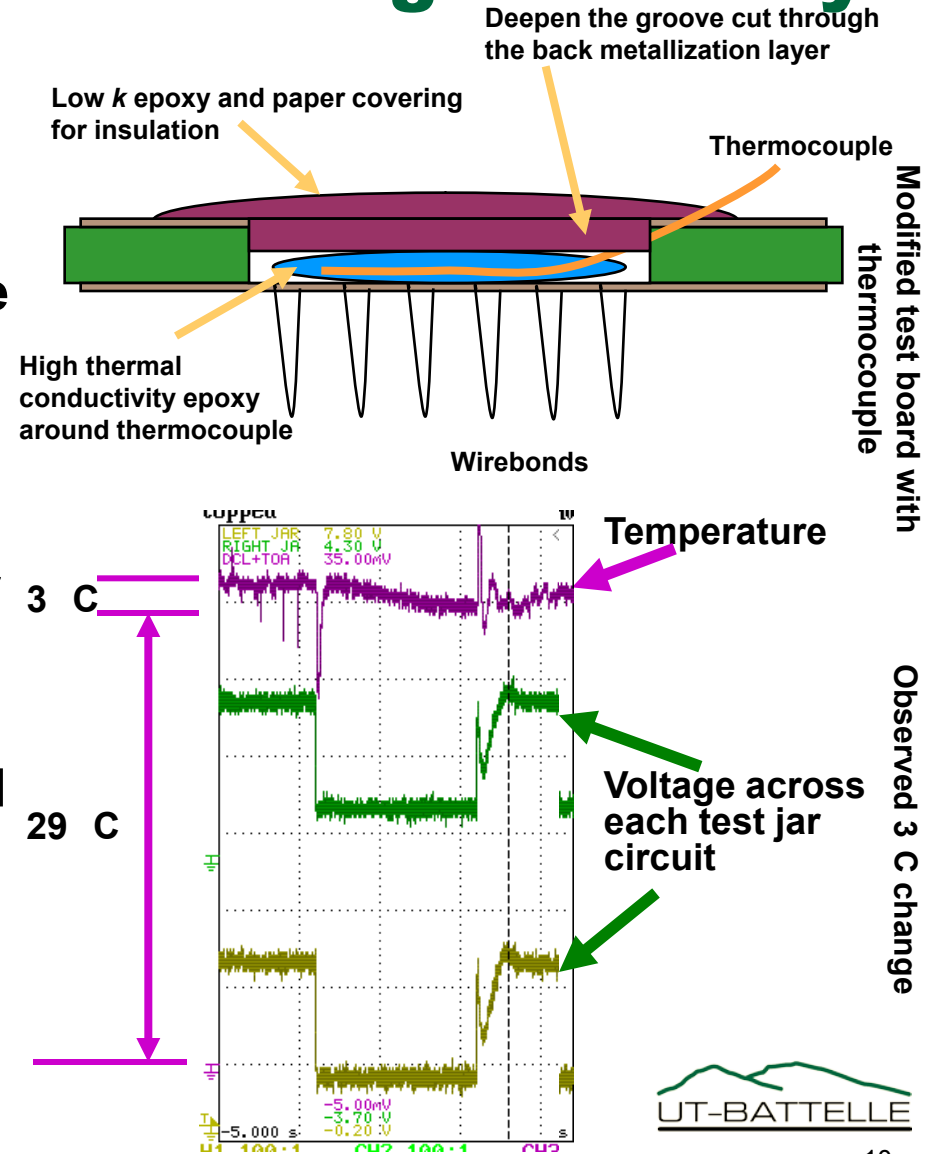
- Allows for high current flow and shaping of the current wave form
  - A square wave of one second on and one second off is driving 10 amperes through each 0.4 mm (400 microns) diameter aluminum wire
- Data recording
- Visual observation of the boards
- Post exposure evaluation of effects of resulting nucleate boiling on the aluminum bonds

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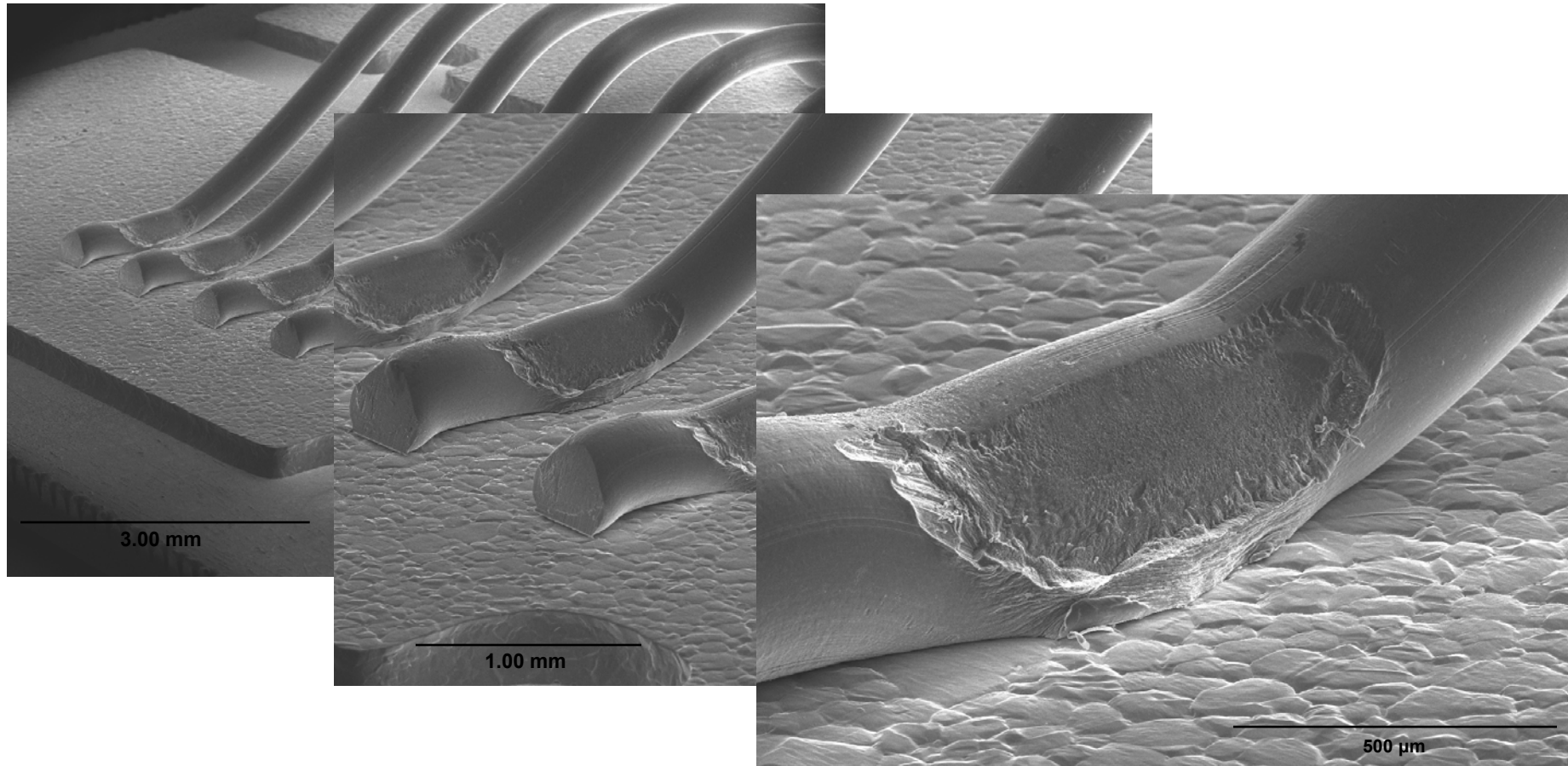


# Temperature Measurements Allow For Correlating Current Changes To Temperature Swings And Testing Flexibility

- Measure temperature change
  - Actual temperature measurements in evaporative cooling is inherently difficult
- Increase test current
  - Testing at 50% greater peak current per wire reported for available hybrid auto inverter
- Increase current on time of waveform
  - A square wave of two second on and two second off is driving 30 amperes through each 0.4 mm (400 microns) diameter Al wire



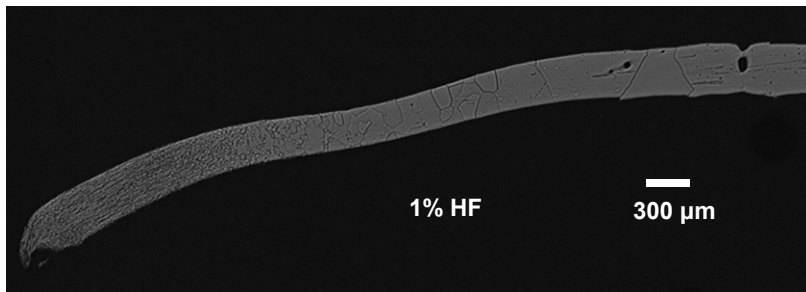
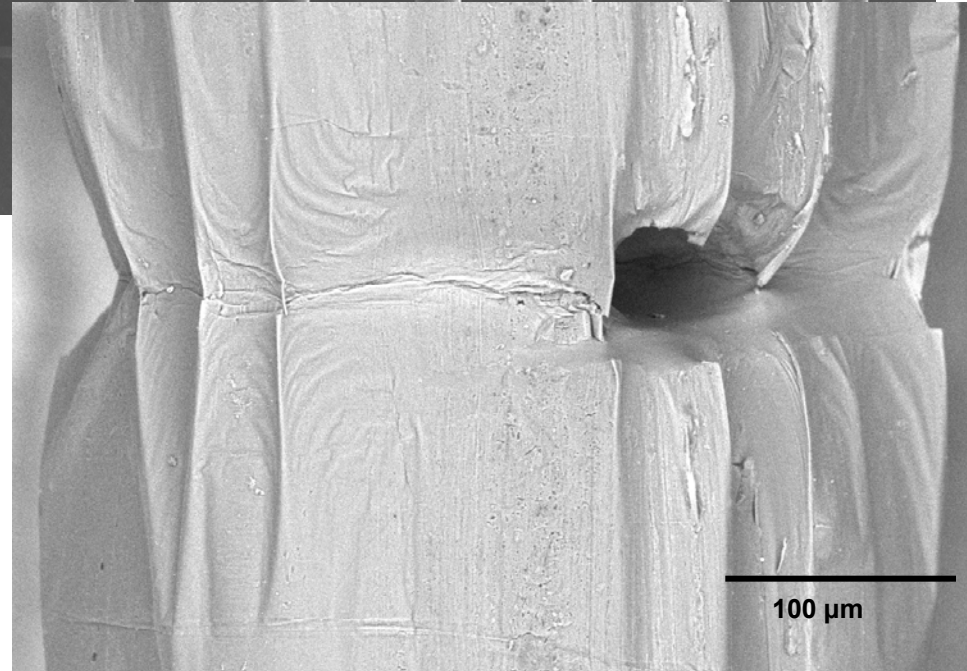
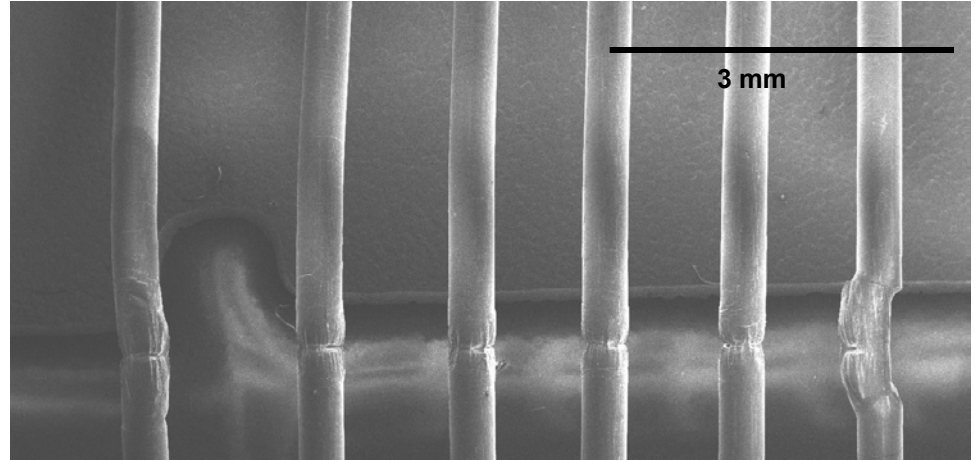
# **There Were No Observable Environmental Effects On Wires Or Board After 690,570 Test Cycles Of One Second On (10 Amperes) And One Second Off**





# However, Changes Were Observed After 932,770 Cycles Of 2 Seconds On (40 Amperes) And 2 Seconds Off

- Deformation of wires
  - Especially at crown
  - Possible pore formation
- Recrystallization and grain growth
  - Few grains across diameter of Al wire at the crown



# **Recently, Testing Up To 933,400 Cycles Of 2 Seconds On (39 Amperes) And 2 Seconds Off Have Been Completed**

- **Evaluate significance of current value**
  - Initial optical evaluation did not reveal the massive deformation seen at 40 amperes
  - Detailed microstructural evaluation will be performed
- **Modifications for testing of rectangular cross-section wires is being pursued**
  - Current density limitations

# **The Evolving Methodology Allowed For Expression Of Failure & Accelerated Testing**

- **Work continues to determine the relationships between the morphological changes**
  - **Changes in grain size and structure, and the failure at the crown of the wires**
- **Final failure occurs as a result of the wires achieving a critical heat flux (CHF) at the crown**
  - **Under CHF conditions, the vapor filled bubbles cannot transport themselves away fast enough to allow for cooling in the region**
  - **Insulation provided by the vapor reduces the cooling at this site and the crown melts**
- **Basis of “Go/no go” criteria is changes in microstructure which then leads to the critical heat flux situation**

# **Future Work—Continue As Needed Enhancements**

- **Use more prototypic boards**
  - Refine “go/no-go” criteria of failure
- **Develop minimum test data that allows for a meaningful dialogue with system designers**

# Successful Demonstration of Compatibility of Direct Side-Stream A/C Cooling With Power Electronics Allows For:

- PEs concepts that reduce the component count and integrate functionality to decrease size, weight, and cost

