

Engine and Reactor Evaluations of HC-SCR for Diesel NOx Reduction

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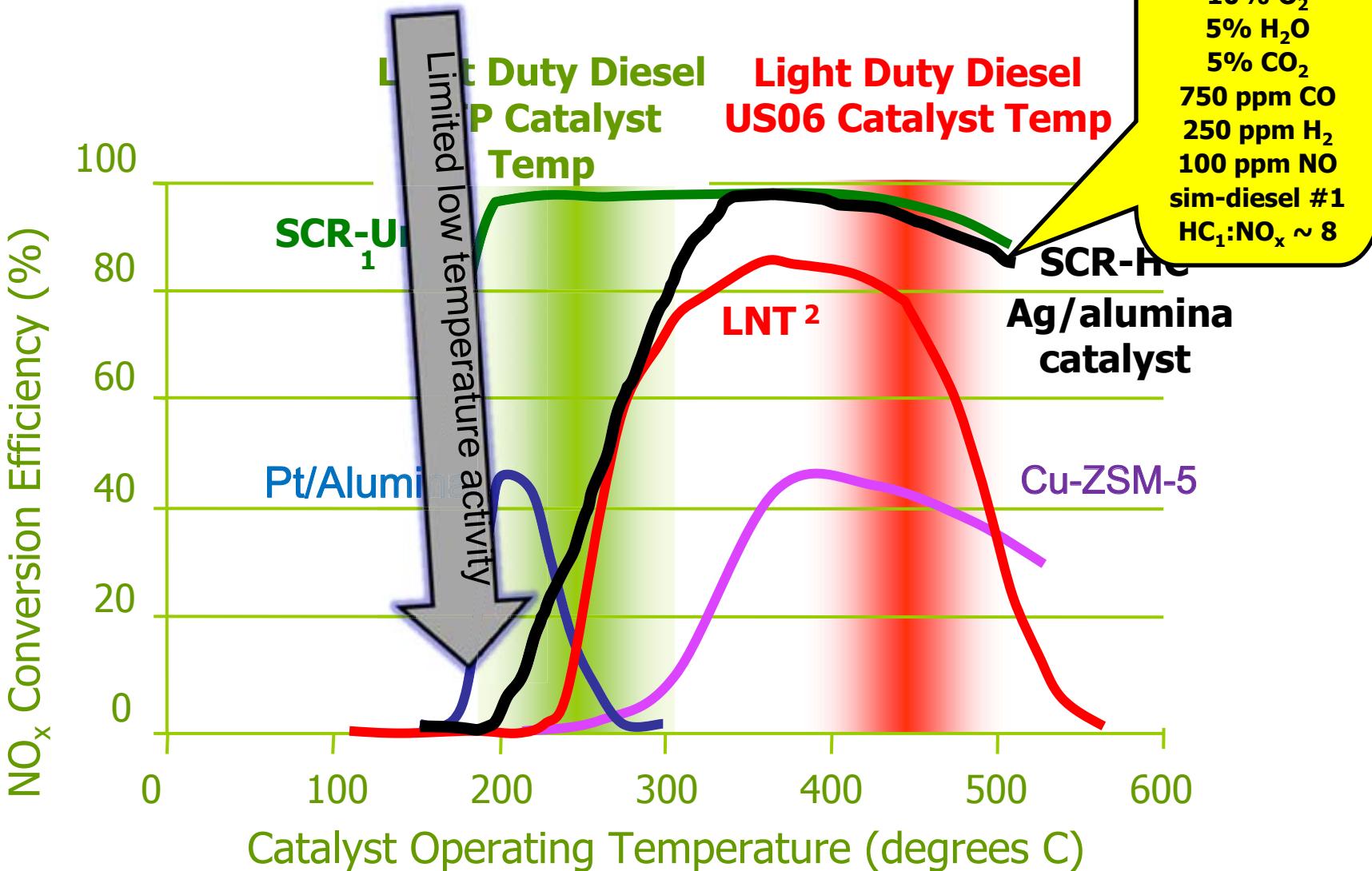
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Background:

Hydrocarbon assisted NOx SCR for automotive catalysis

- Copper zeolites late 80's early 90's
 - Held, et al, SAE 900496, 1990
 - Iwamoto, et al, Proc. Catalytic Technology for the Removal of NO, Tokyo, 1990
- Supported catalysts (PGMs and base metals) early 90's
 - Hamada, et al., Applied Catalysis, 1991
 - Bethke, Alt and Kung, Catalysis Letters, 1994
- Ag/alumina
 - Burch and Millington, Catalysis Today, 1996.
 - Shimizu et al., Applied Catalysis B: Environmental, 2000.
- DOE NOx Discovery Project
 - Initiated in August of 2002, completed end of 2007
 - Over 16,000 materials synthesized and evaluated
 - **Ag/alumina selected as optimum material**

Lean NO_x Aftertreatment

¹ Aged 120 k mi² Aged 120 k mi

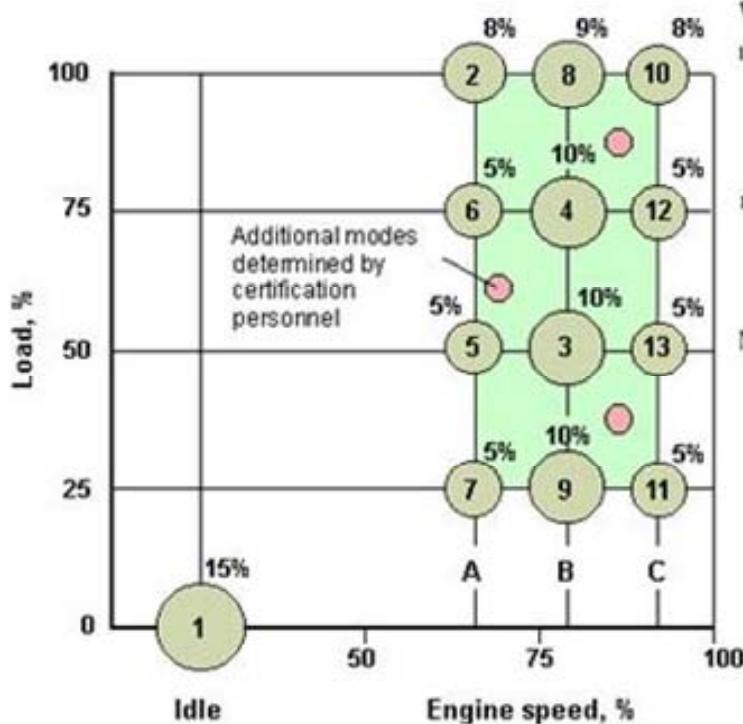
Engine Results

Focus is the heavy duty, US dynamometer certification using the Duramax 6.6 liter diesel

- Catalyst volume:
 - Four, 5.0 liter bricks (20.0L total vol.)
 - emission measurements are after brick 3 and brick 4
- Reductant by in-exhaust injection:
 - diesel fuel
 - ethanol
- Federal test cycles:
 - Heavy duty FTP (HDFTP),
 - Cold-start HDFTP (CHDFTP)
 - Set 13 (Supplemental Emission Test)

Supplemental Emission Test (SET)

(aka Steady State Test / 13 Mode Test, Euro III - European Stationary Cycle / ESC)



- rpm/load changes complete within first 20 sec of each mode
- 2 minutes at each non-idle mode, 4 minutes at idle
- 1 PM filter for over 13 modes

Where:

n_{hi} = High speed as determined by calculating 70% of the maximum power. The highest engine speed where this power value occurs on the power curve is defined as n_{hi} .

n_{lo} = Low speed as determined by calculating 50% of the maximum power. The lowest engine speed where this power value occurs on the power curve is defined as n_{lo} . Maximum power = the maximum observed power calculated according to the engine mapping procedures defined in § 86.1332.

$$\text{Speed A} = n_{lo} + 0.25 \times (n_{hi} - n_{lo})$$

$$\text{Speed B} = n_{lo} + 0.50 \times (n_{hi} - n_{lo})$$

$$\text{Speed C} = n_{lo} + 0.75 \times (n_{hi} - n_{lo})$$

$$A_{WA} = \frac{\sum_{i=1}^n [A_{Mi} \times WF_i]}{\sum_{i=2}^n [A_{Pi} \times WF_i]}$$

Where:

A_{WA} = Weighted average emissions for each regulated gaseous pollutant, in grams per brake horse-power hour.

A_M = Modal average mass emissions level, in grams per hour. Mass emissions must be calculated as described in § 86.1342.

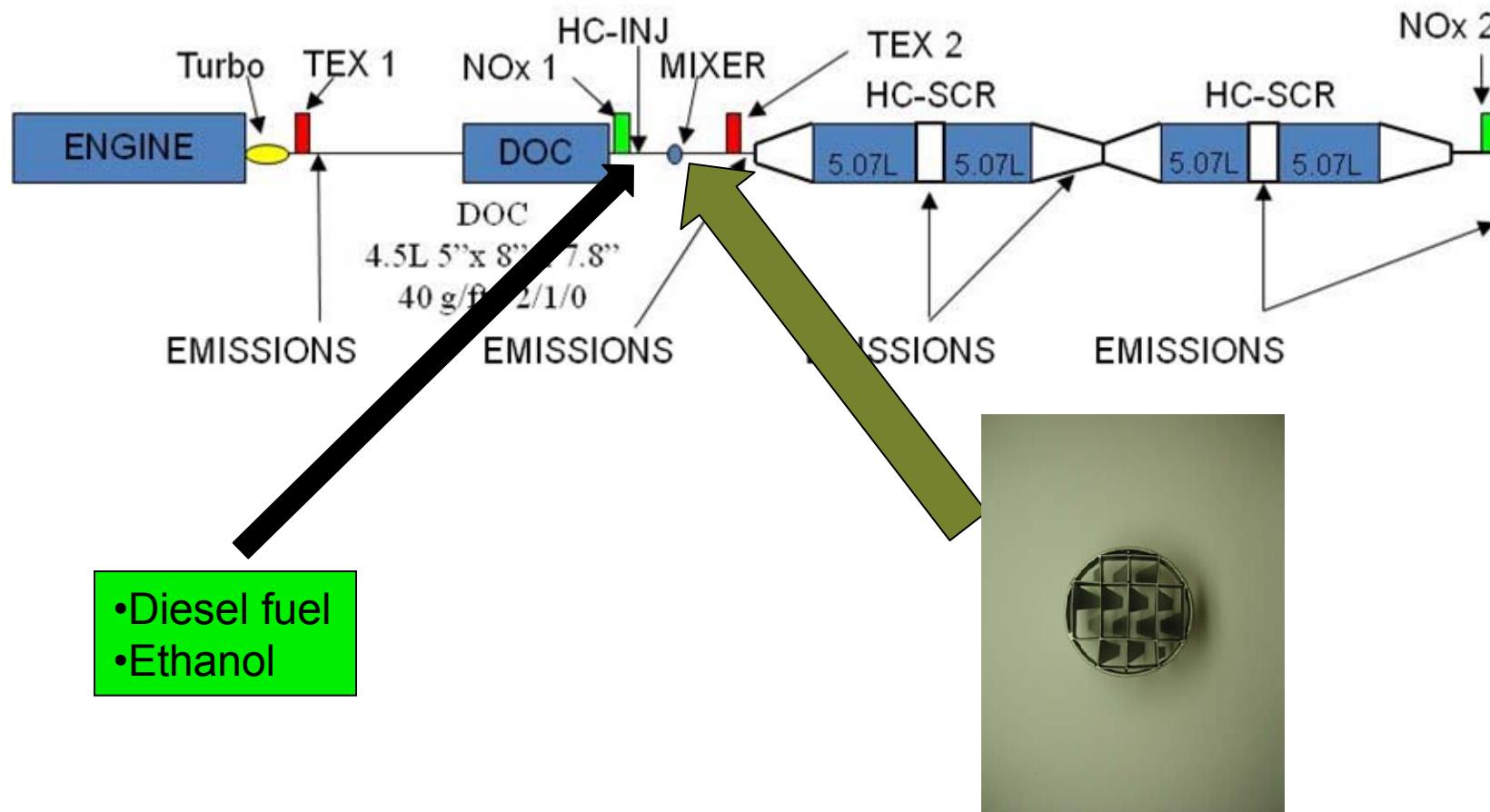
A_P = Modal average power, in brake horsepower. Any power measured during the idle mode (mode 1) is not included in this calculation.

WF = Weighting factor corresponding to each mode of the steady-state test cycle, as defined in paragraph (b)(1) of this section.

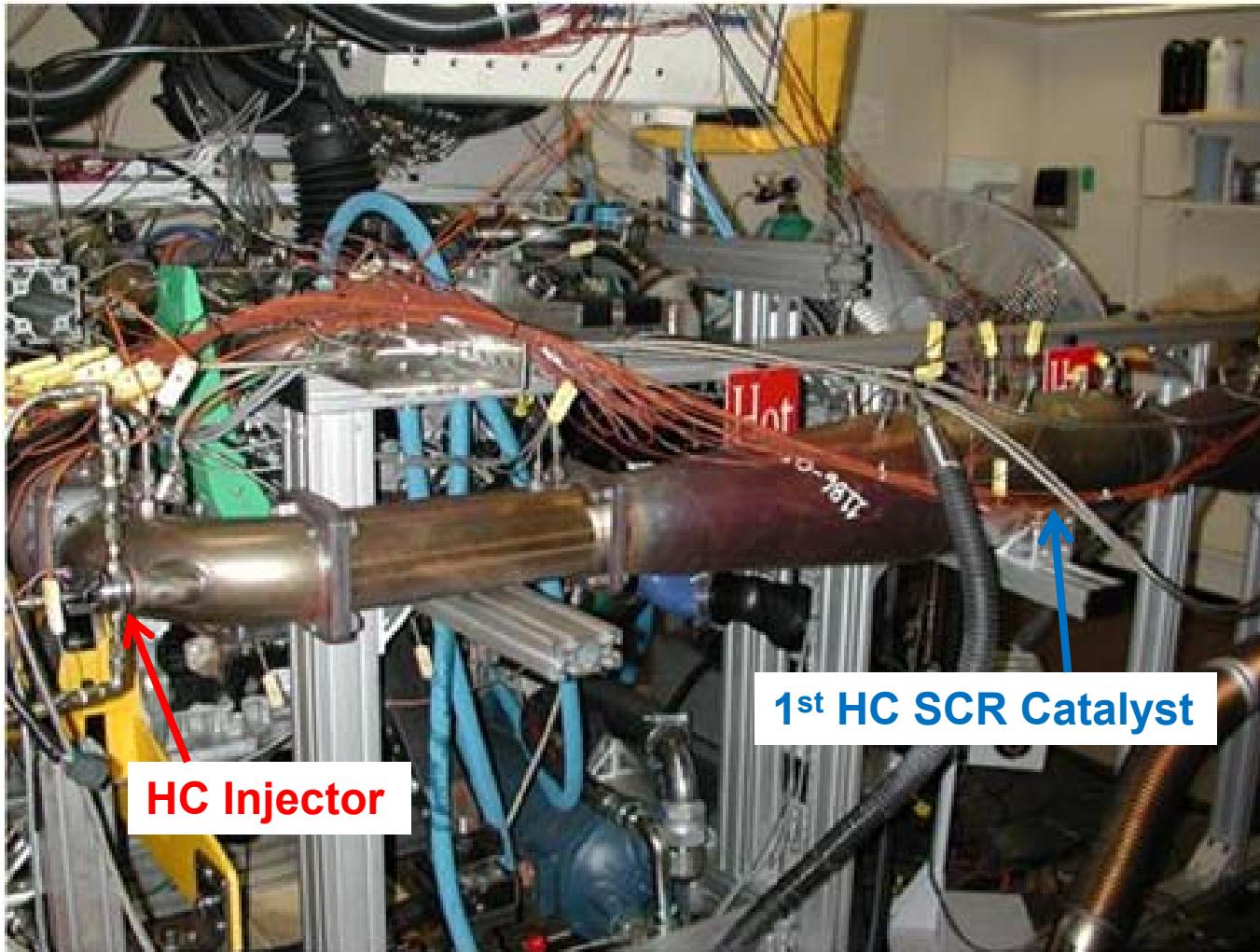
i = The modes of the steady-state test cycle, as defined in paragraph (b)(1) of this section.

$n = 13$, corresponding to the 13 modes of the steady-state test cycle, as defined in paragraph (b)(1) of this section.

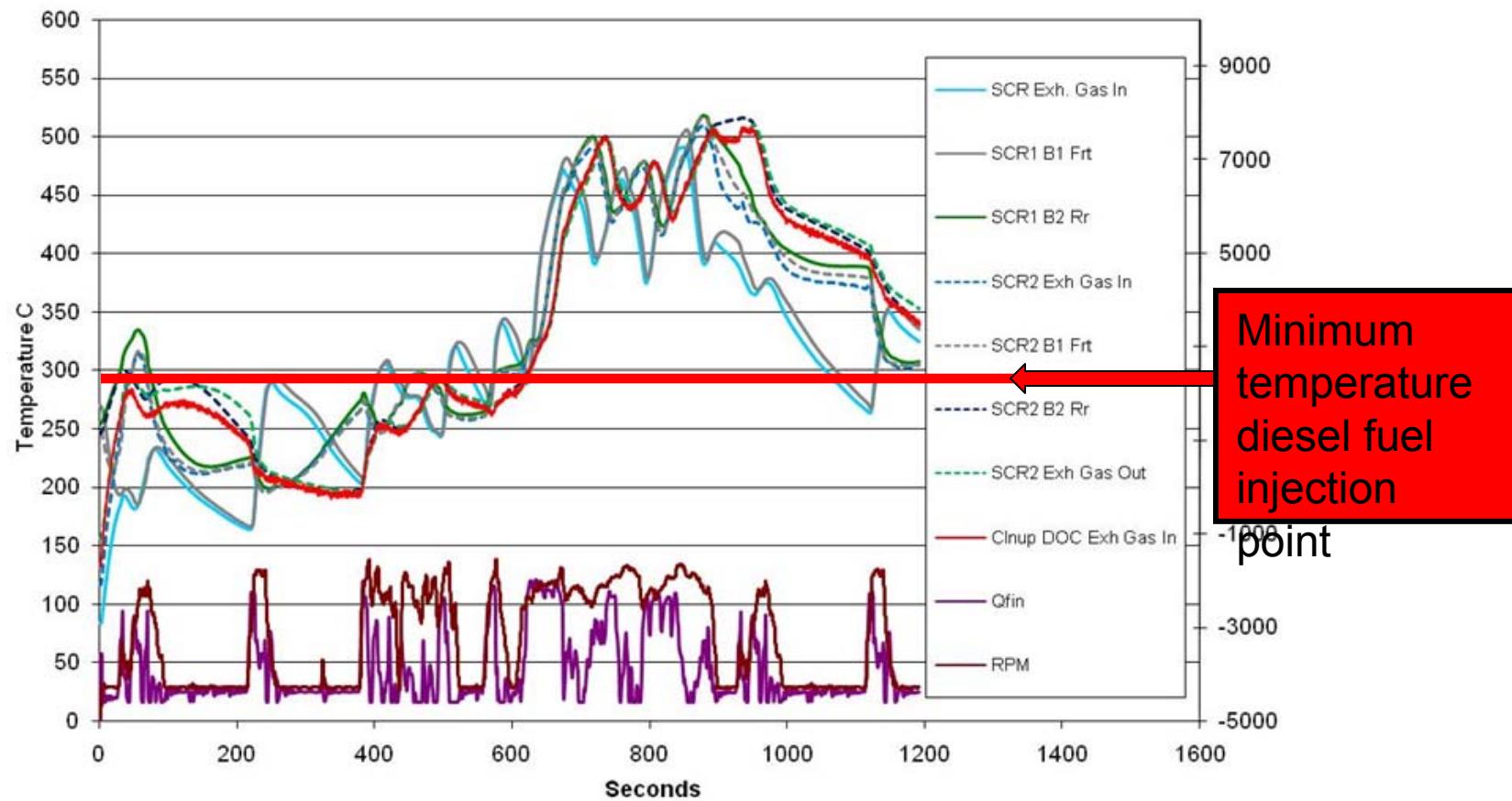
Diesel Aftertreatment testing architecture using 6.6 Duramax engine



Picture of Dyno Aftertreatment System, Injector and First Can.

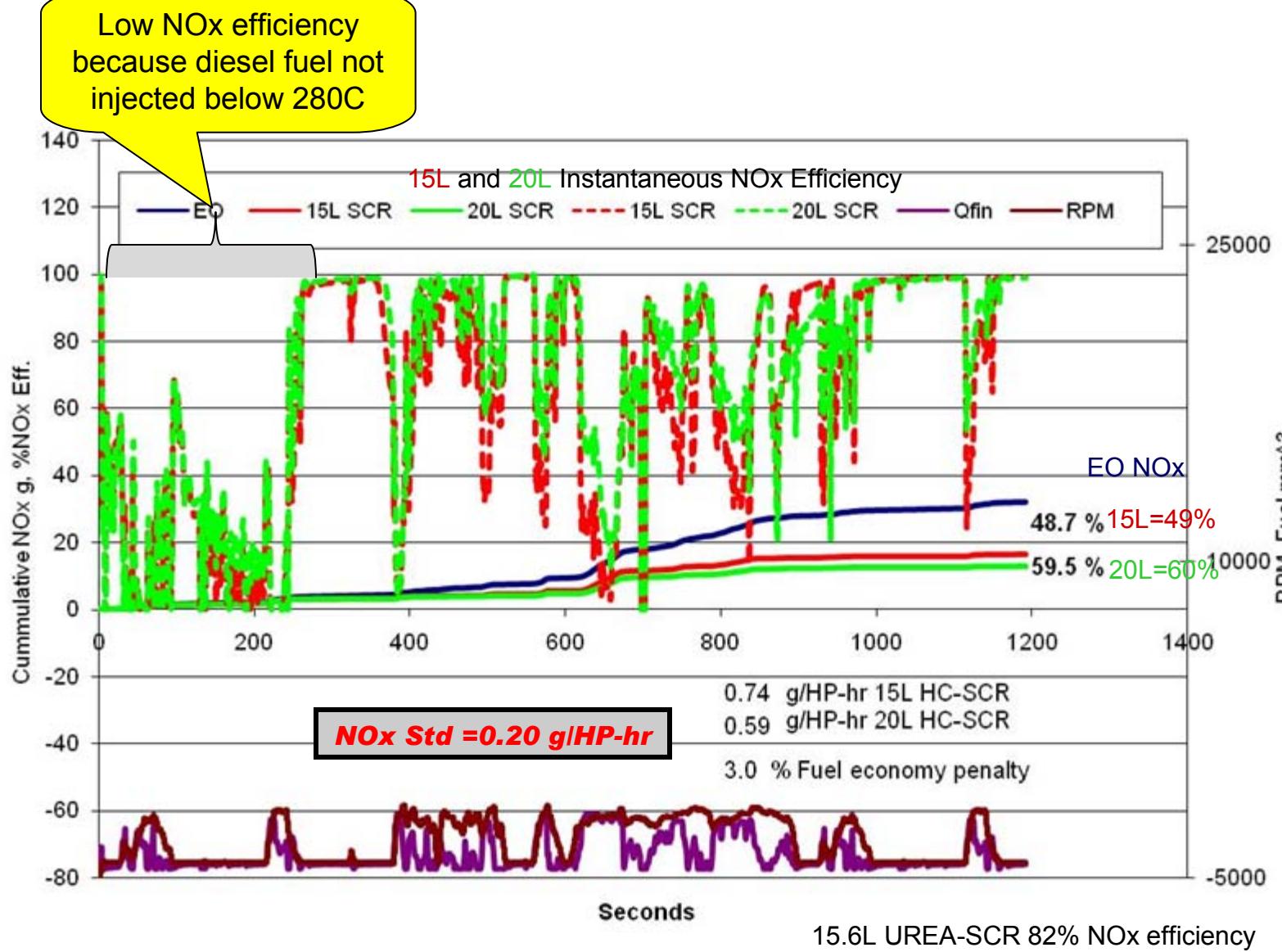


HDFTP Temperature Measurements



- Exhaust temperatures vary from 150 °C to 500 °C
- First 600 seconds show catalyst in temperatures no higher than 250 °C
- **Conclusion: Almost half the HDFTP is completed before the exhaust reaches the optimum NOx conversion temperature**

HDFTP NOx Emissions Results with Diesel

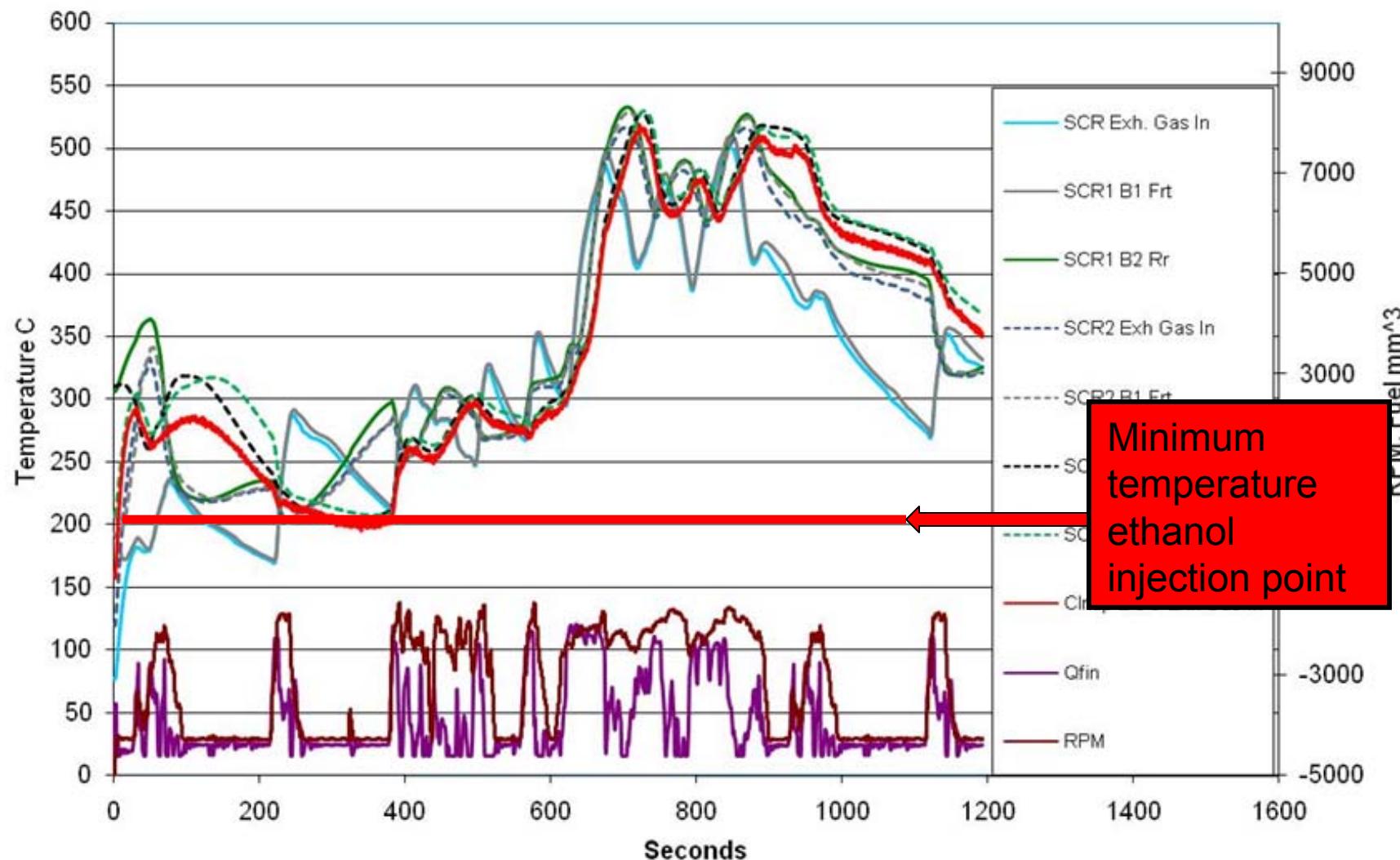


SET 13 NOx Emissions Results with Diesel

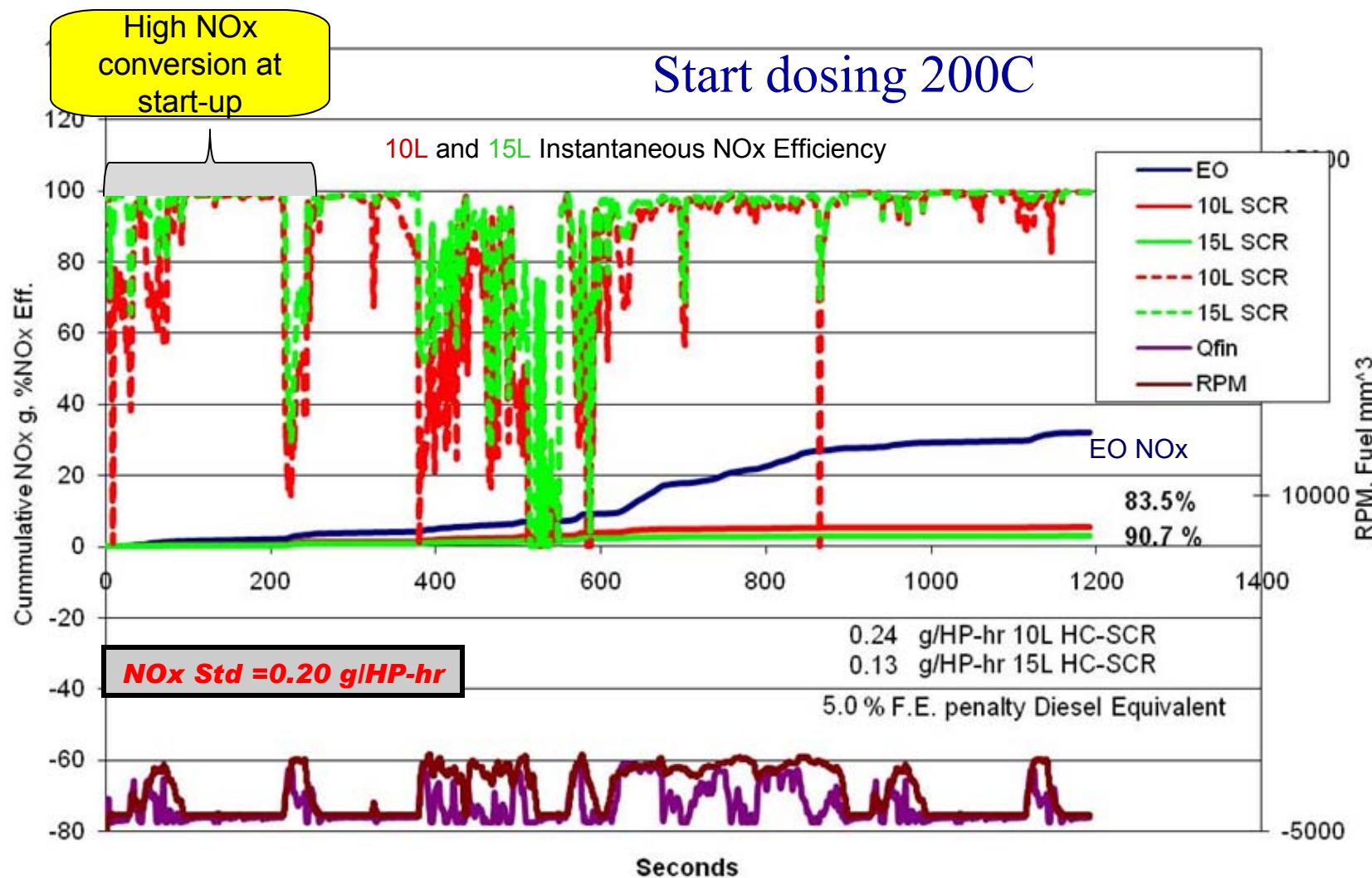


Space velocity, oxygen concentration and gas temperature each contribute to the NOx conversion at a give engine operating point

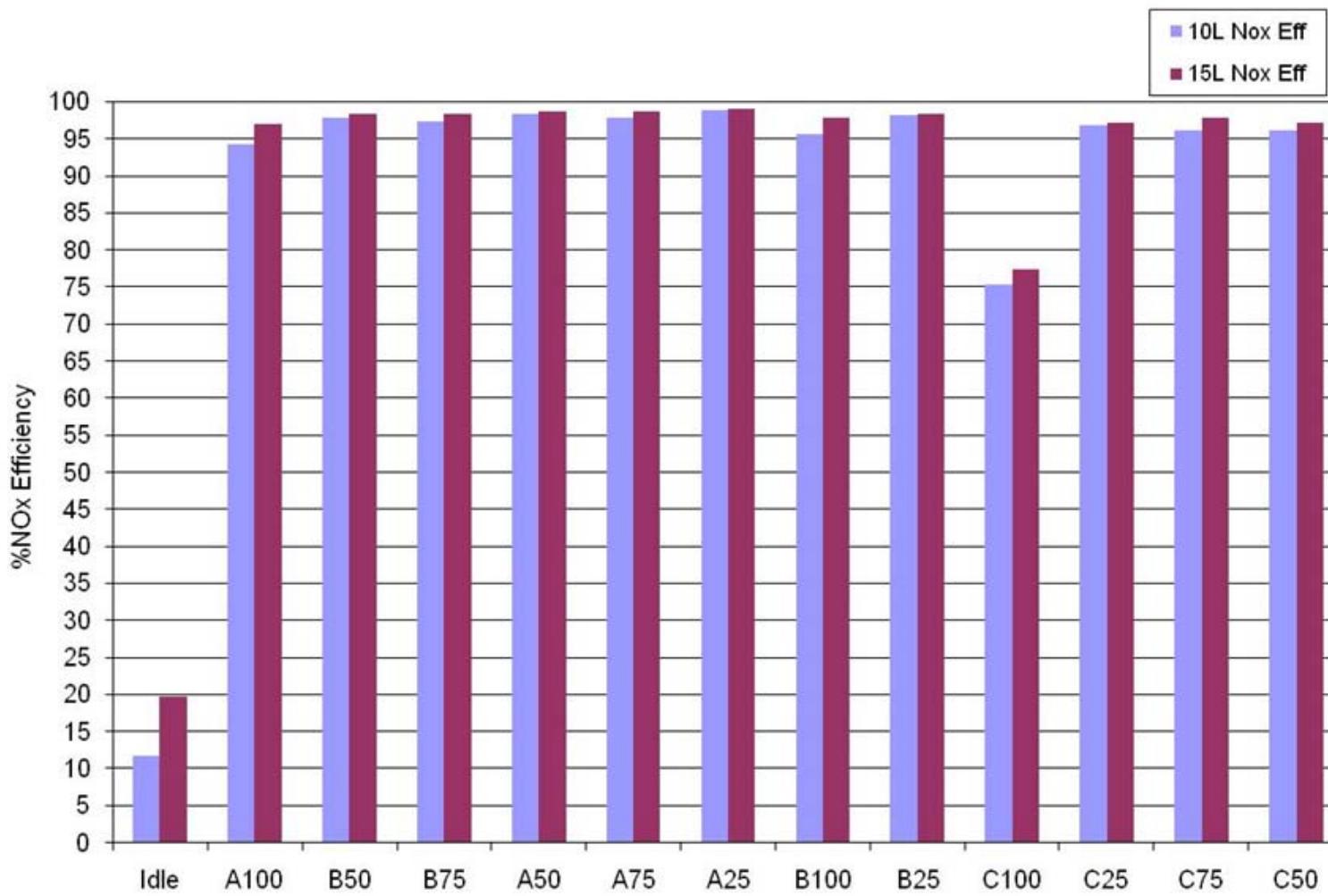
HDFTP NOx Emissions Results with EtOH



HDFTP NOx Emissions EtOH

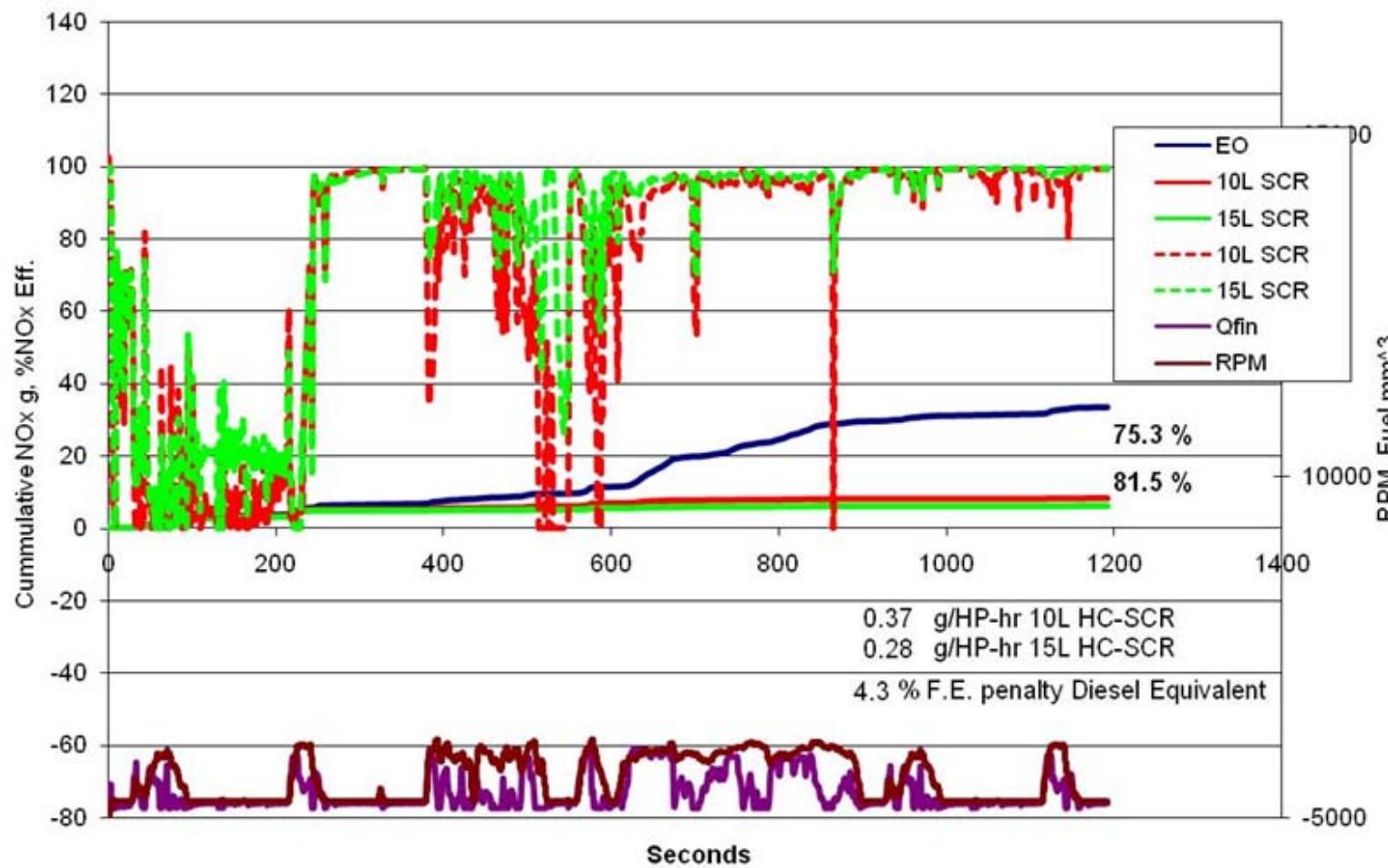


SET 13 NOx Emissions Results with EtOH



Conversions uniformly higher at each engine operating point

CHDFTP NOx Emissions EtOH



NOx conversions for cold start HDFTP are reasonable



Engine Dynamometer Test Results

Light-Duty w/ ULSD	Catalyst Volume	NOx Conversion	Fuel Economy Penalty	Weighted Emissions	Emission Standard
FTP75	20L	60%	3.1%	0.640 g/mi	0.070 g/mi
US06	20L	76%	2.6%	0.149 g/mi	0.400 g/mi
HWYFET	20L	92%	2.4%	0.024 g/mi	0.070 g/mi
Heavy-Duty w/ ULSD	Catalyst Volume	NOx Conversion	Fuel Economy Penalty	Weighted Emissions	Emission Standard
Hot HDFTP	20L	60%	3.0%	0.59 g/BHP-h	0.20 g/BHP-h
SET 13-Mode	20L	65%	2.7%	0.63 g/BHP-h	0.20 g/BHP-h
Heavy-Duty w/ Ethanol	Catalyst Volume	NOx Conversion	Fuel Economy Penalty	Weighted Emissions	Emission Standard
Hot HDFTP	15L	82%	4.3% (diesel eq.)	0.13 g/BHP-h	0.20 g/BHP-h
SET 13-Mode	15L	91%	4.7% (diesel eq.)	0.16 g/BHP-h	0.20 g/BHP-h
HDFTP (wtd. hot+cold)	15L	86%	4.7% (diesel eq.)	0.20 g/BHP-h	0.20 g/BHP-h

Light-Duty: [SAE 2008-01-2487](#) (M.B. Viola)

Heavy-Duty: [submitted SAE 2009](#) (M.B. Viola)



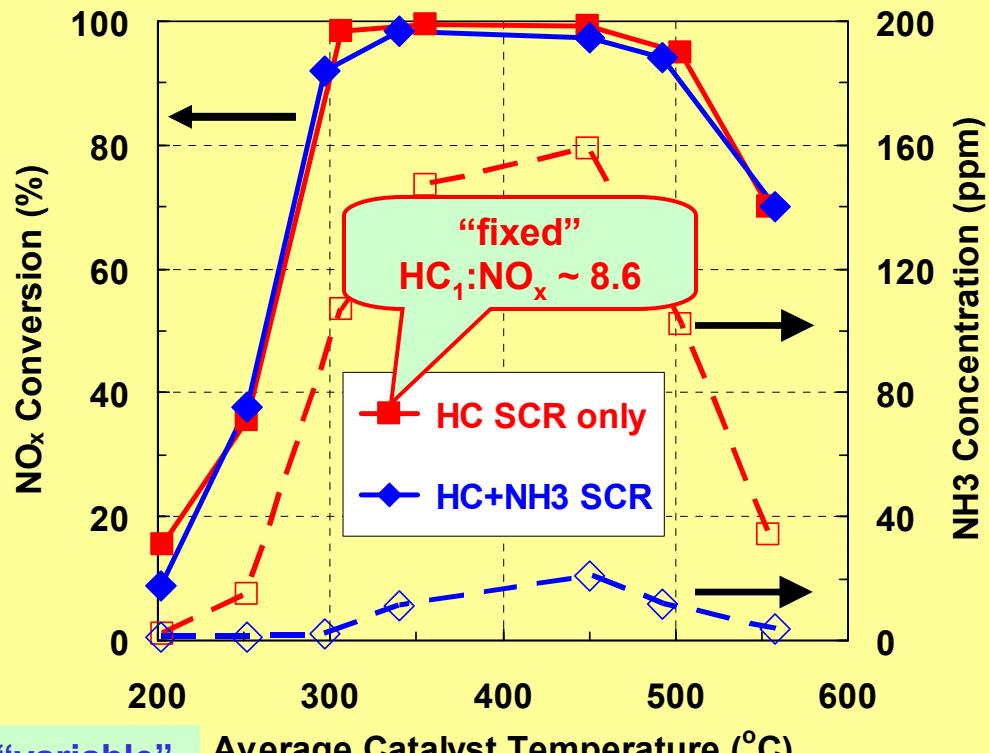
Dual-Catalyst Concept: HC-SCR+NH₃-SCR

SOLUTION: NO_x + C₂H₅OH → N₂ + NO_x + NH₃ → N₂

HC-SCR

NH₃-SCR

HC-SCR @ SV ~ 25,500 h⁻¹ +/- NH₃-SCR @ SV ~ 60,000 h⁻¹
 6% O₂ / 5% H₂O / 5% CO₂ / 750 ppm CO / 250 ppm H₂
 400 ppm NO / 431 - 1724 ppm C₂H₅OH (HC₁:NO_x ~ 2.2 to 8.6)



3.0 wt.% Ag₂O/Al₂O₃ + Cu-zeolite

- Tune ethanol injection amount to "balance" NO_x and NH₃ breakthrough
- High NO_x conversion levels maintained while lowering amount of ethanol injected
- System optimization still required

Engine Results Status

- With diesel as a reductant
 - HDFTP: 60% NOx reduction using 3x engine displacement (ED)
 - SET 13-Mode: 65% NOx reduction using 3x ED
- With EtOH as a reductant
 - HDFTP: 84% (1.5 ED), 91% (2.3 ED) NOx reduction
 - SET 13-Mode obtained 90% (1.5 ED) NOx reduction
 - Cold start HDFTP: 82% (2.3 ED)
- Poisoning and aging evaluations
 - Sulfur does poison, but is regenerable
 - Phosphorous does deposit, but does not appear to degrade performance abnormally
 - Heavy HC's do poison, but are also regenerable

Summary

- Accomplishments
 - High-throughput technology has optimized the HC-SCR catalyst formulation
 - Effectiveness of diesel fuel and ethanol demonstrated in both reactor and engine testing
 - HC-SCR control strategy has been developed
 - Dual bed technology demonstrated
 - All degradation mechanisms identified and redaction schemes devised
- Drawbacks
 - High SV significantly reduces the NO_x conversion efficiency
 - Poor diesel fuel vaporization at low T can limit reductant delivery
 - Degradation modes require close engine control
 - Hydrocarbon slip