

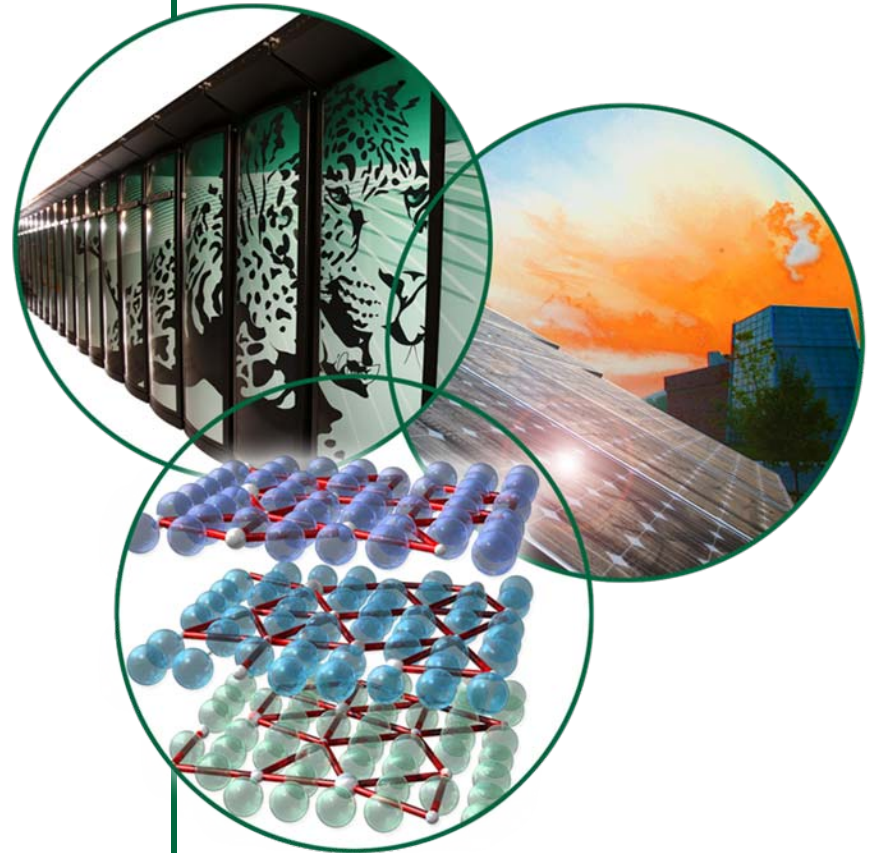
Durability of Diesel Engine Particulate Filters

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Merit Review and Peer Evaluation Meeting

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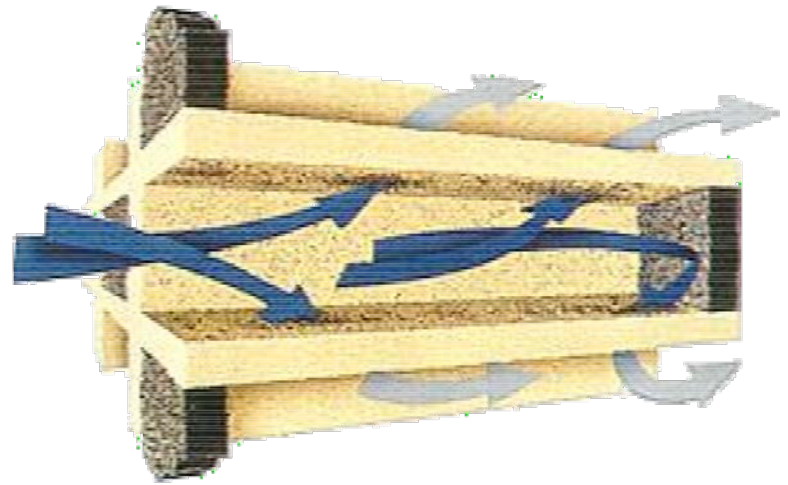
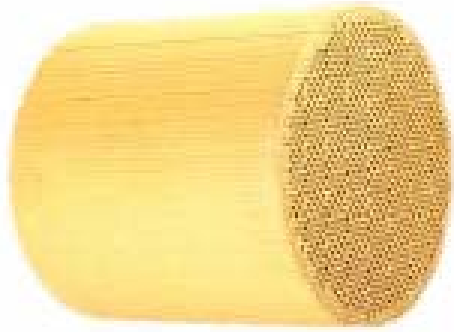
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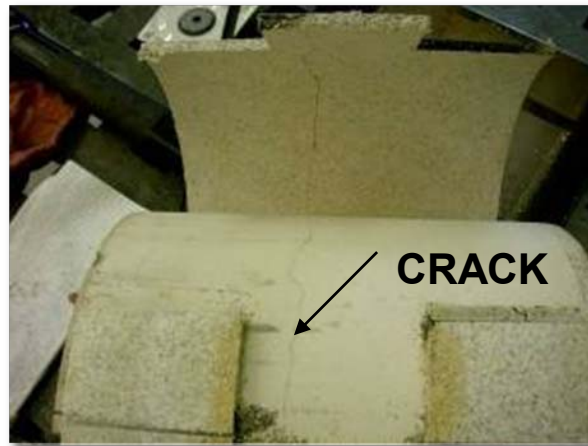


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Background



- Diesel Particulate Filters (DPFs) *already* play a key role in meeting stringent 2007 regulations and will continue to be key technology to meet the more stringent 2010 regulations.
- Reliable operation for 500,000 miles required. Reliability could be reduced due to thermal stresses induced in ceramic DPF during regeneration.
- Need for improved materials and designs along with life prediction models to optimize reliability and durability.



Overview

Timeline

- Start: June 2004
- End: Sept. 2010
- 76% complete

Budget

- Total Project funding
 - DOE-\$1.55M
 - Contractor-\$1.7M
- Funding received:
 - FY08 \$300k
 - FY09 \$149k

Barriers^{*}

- Design data & modeling tools
 - New test methods needed: porosity
 - Lifetime = f(properties) for models
- Performance
 - Increased thermal stresses due to active filter regeneration forced by lower NO_x standard

Targets

- HD diesel engines compliant with 2010 EPA regulations

Partners

- Cummins Inc.
- Corning Inc.

Objective

- **Implement test techniques to characterize the physical and mechanical properties of ceramic diesel particulate filters (DPFs) and develop analysis and inspection tools for assessing their reliability and durability.**

Milestones

- **Milestone08: Determine the elastic moduli of *coated* DPFs as a function of time at temperature.**
- **Milestone09: Determine the change in thermal shock resistance of field tested DPFs and the thermal shock resistance of one alternate substrate DPF material.**

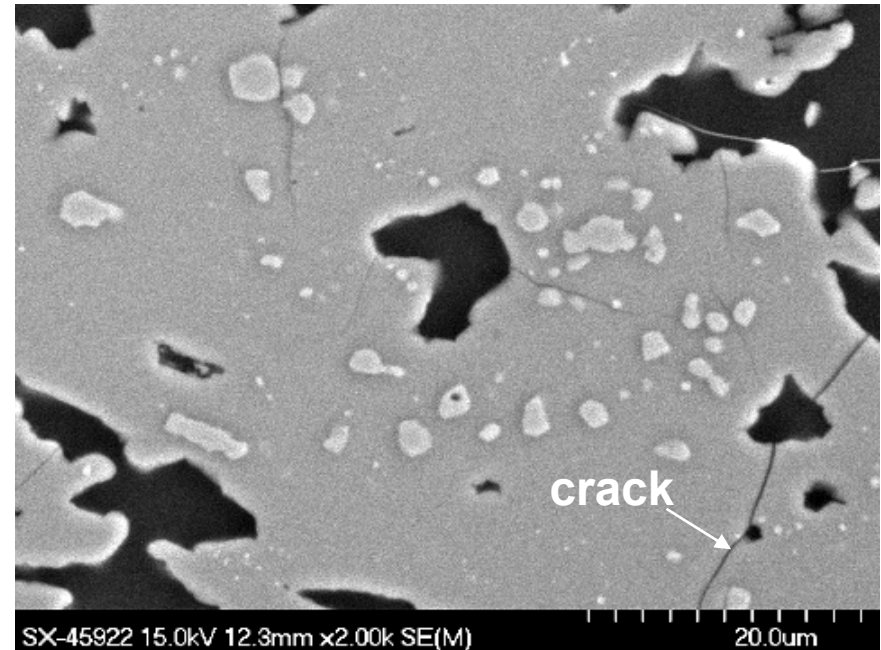
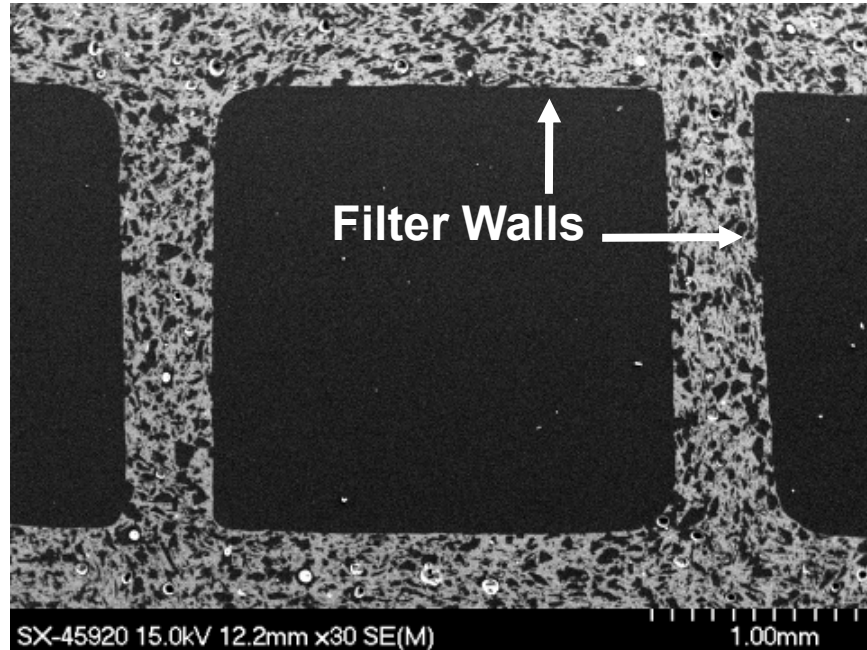
Approach

- **Rank the thermal shock resistance of candidate DPF substrates.**
- **Application of probabilistic design tools and non-destructive evaluation (NDE) techniques to DPF ceramic substrates.**
- **Refinement of DPF service lifetime prediction models based on characterization of field returned filters.**

DPFs must withstand large temperature gradients associated w/ regeneration

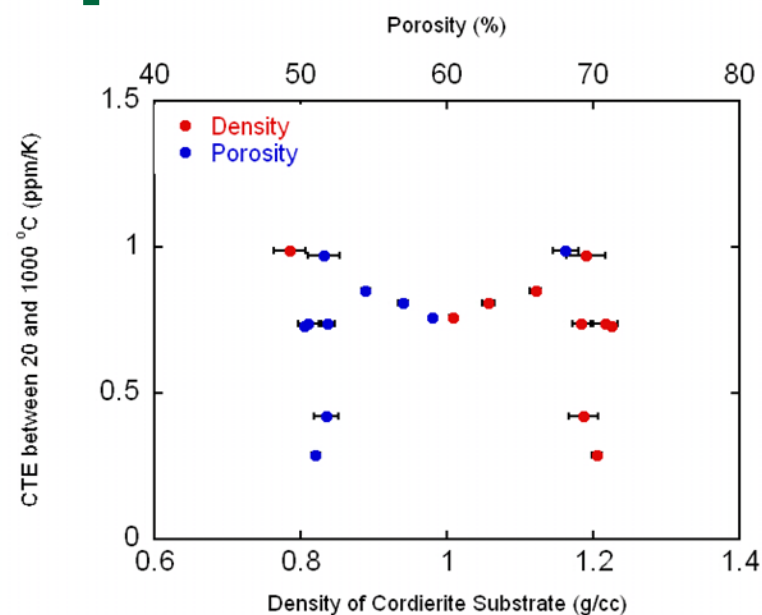
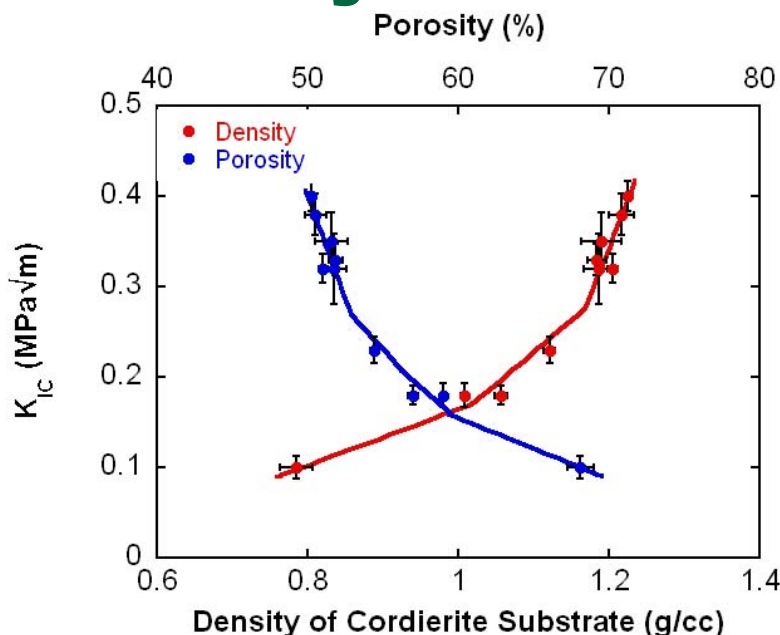
- Simple thermal shock parameter used for comparison
- Usual: $R_s = \sigma / \alpha E$, (σ = strength)
- Here: $R_K = K_{IC} / \alpha E$
 - Easier to perform fracture toughness tests than strength (less material and fewer samples)
- **Properties measured**
 - K_{IC} , Fracture Toughness (at room temperature) – Double Torsion
 - α , Coefficient of Thermal Expansion up to 1000°C – TMA
 - CTE analyzed parallel and perpendicular to extrusion
 - E , Elastic Modulus (up to 1000°C) – RUS

Microstructure: >50% porosity and microcracks

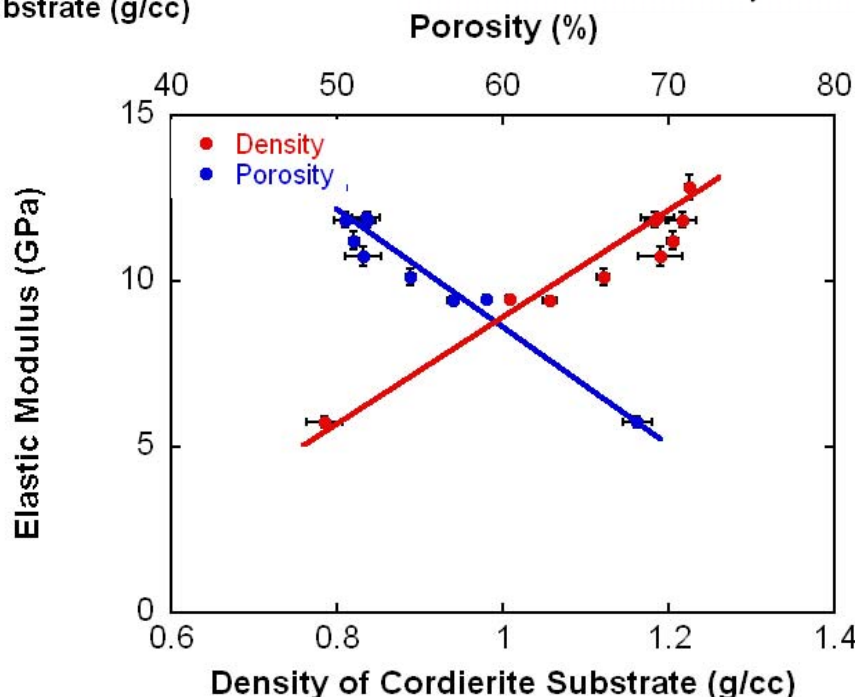


- Cordierite: $2\text{MgO} \cdot 2\text{Al}_2\text{O}_3 \cdot 5\text{SiO}_2$
- Anisotropic parallel and perpendicular to extrusion direction

Porosity dominates properties

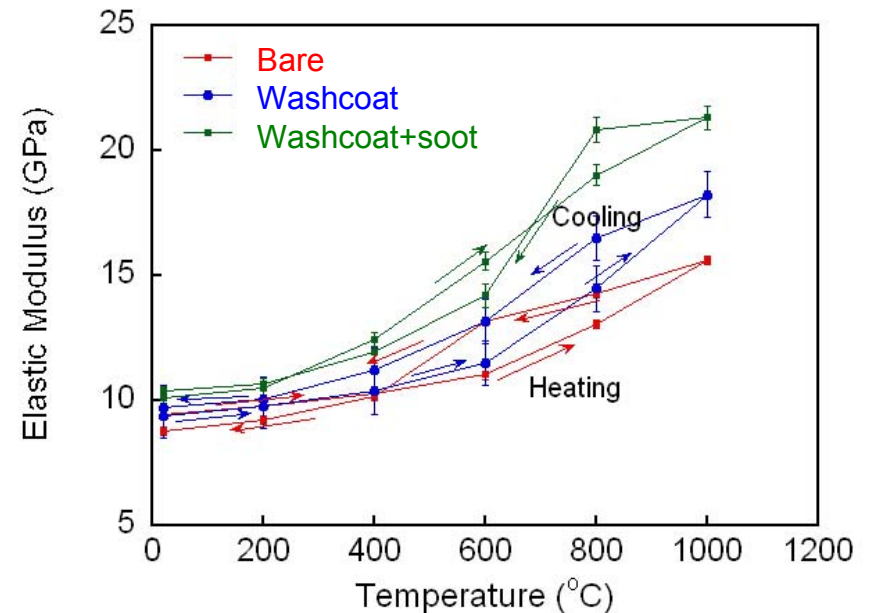
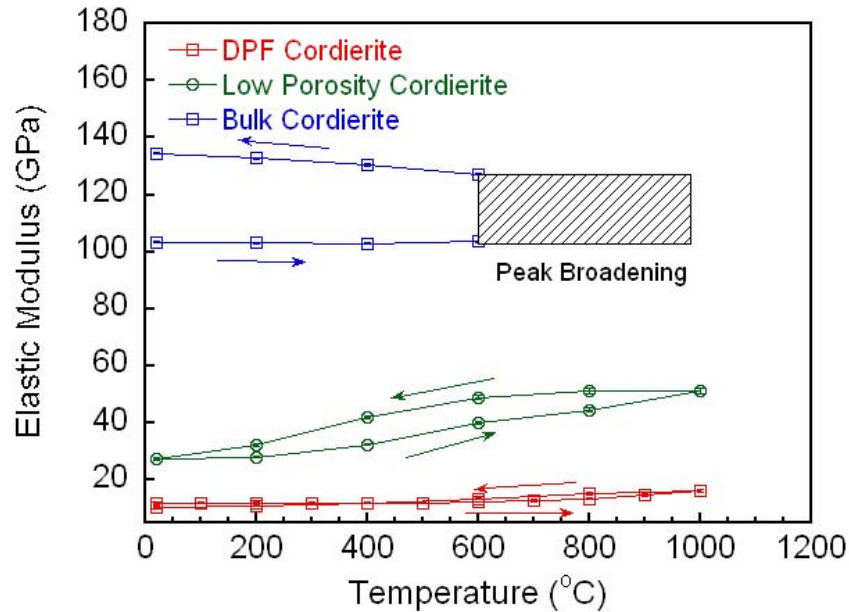


- Strong correlations with K_{IC} and E
- Porosity dominates all other conditions: bare, coated, field-tested, etc.



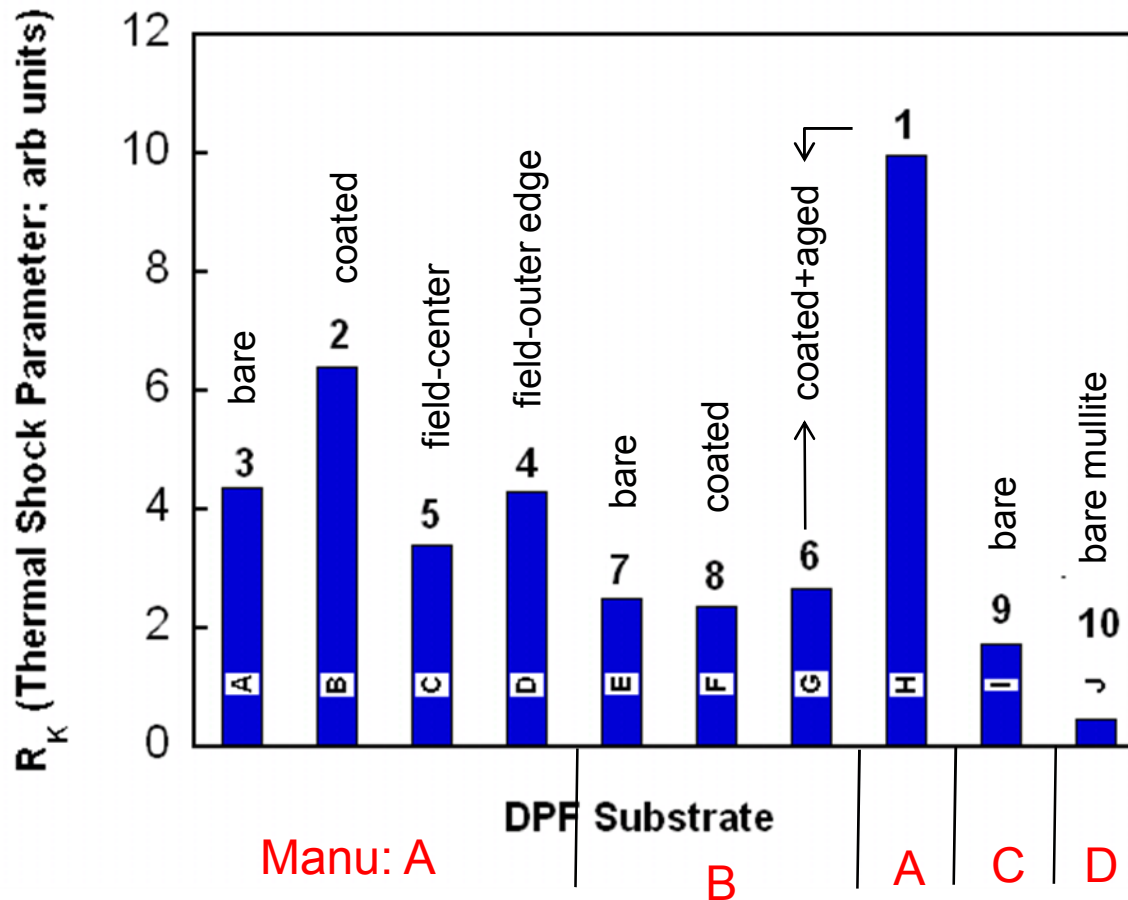
- CTE a function of crystal chemistry

Elastic moduli: hysteresis observed on heating & cooling



- Elastic moduli low relative to dense cordierite due to porosity
 - Measured using resonant ultrasound spectroscopy
- Hysteresis attributed to microcrack healing and re-cracking
- Washcoat and soot increase elastic moduli

Thermal shock ranking methodology developed

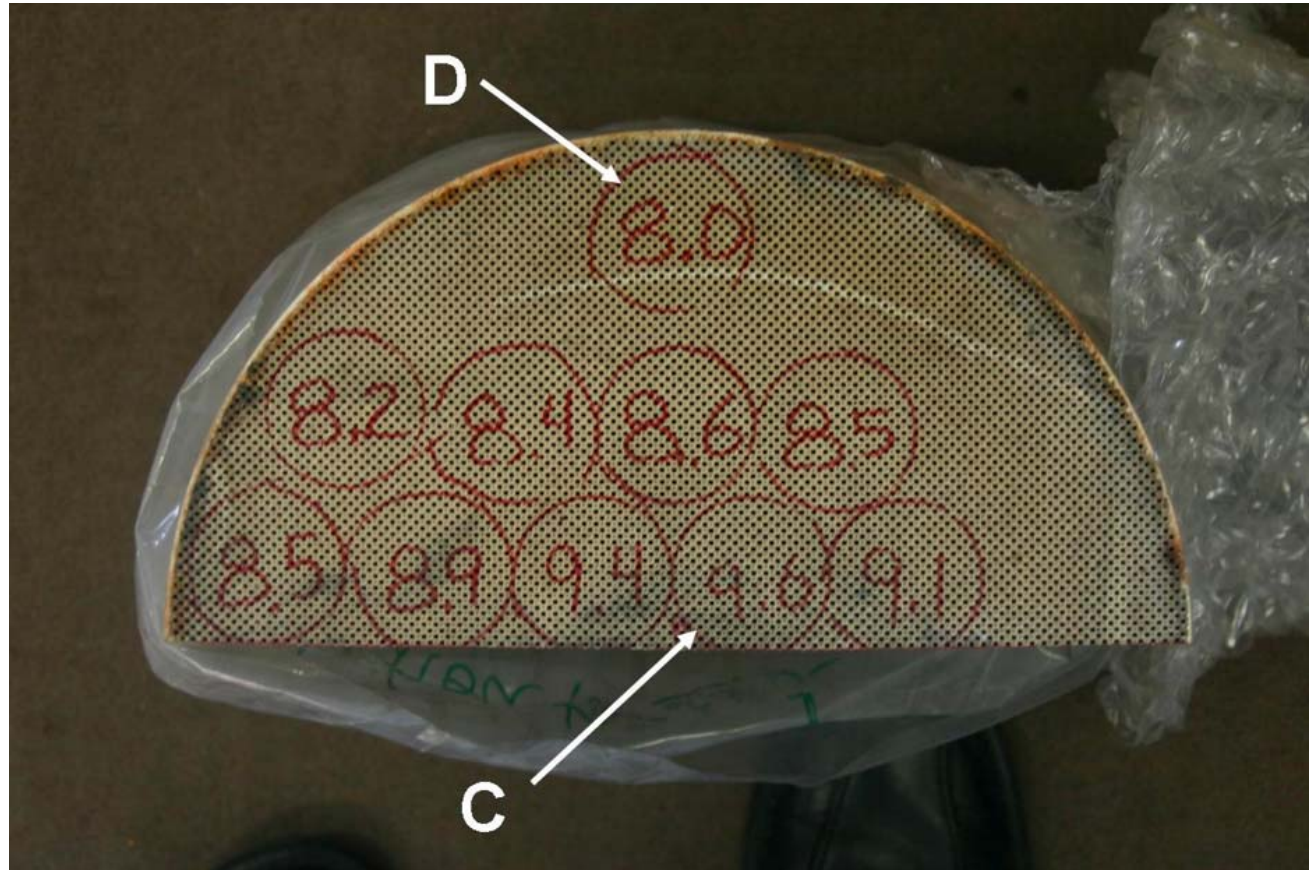


$$R_K = K_{IC} / \alpha E$$

- Note that the above analysis is highly simplified; assumes:
 - Homogeneity
 - Isotropy

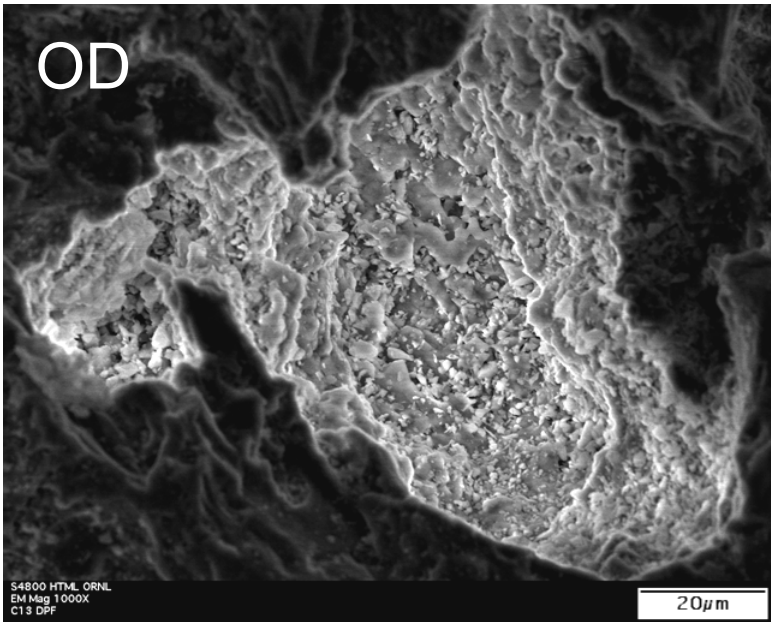
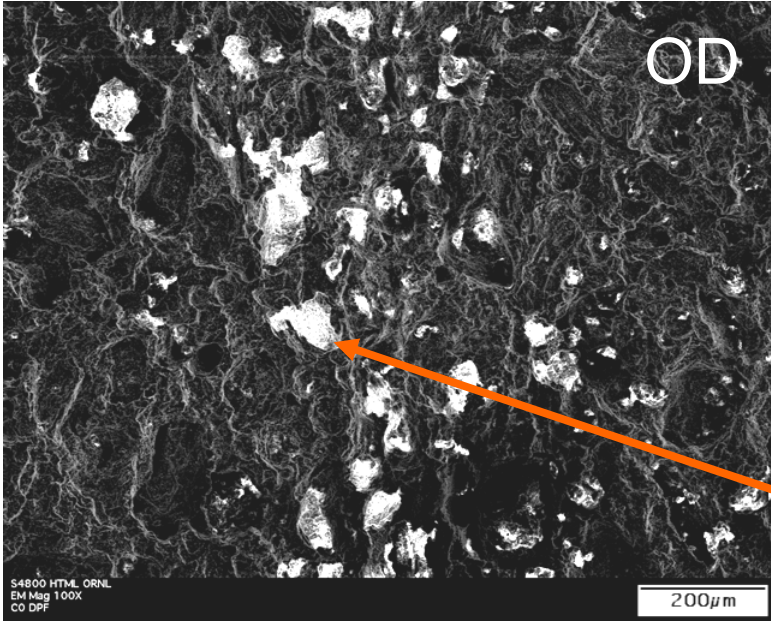
Cummins NDE: Pulse echo for variations from core to outside diameter; borescope for cracks

$$velocity^2 \propto \frac{E}{\rho}$$

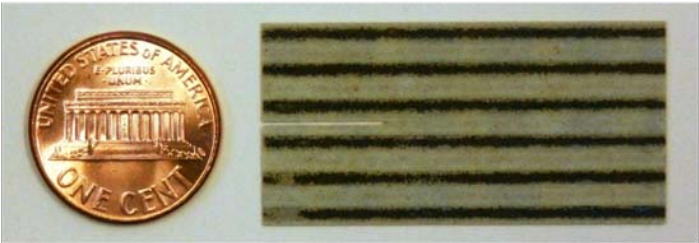
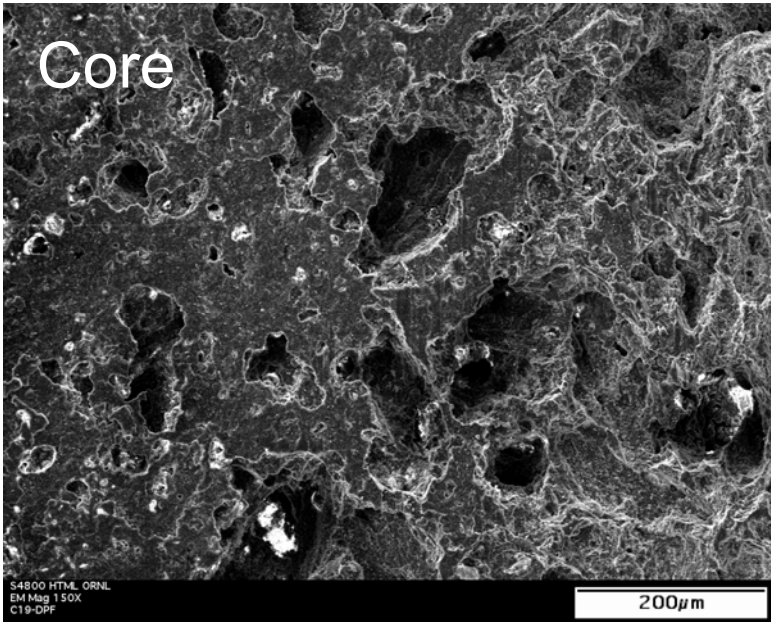


- Measured time ↓, velocity ↑, apparent length ↓
- E/ρ ↑ from core to OD

Modeling: Service changes apparent properties

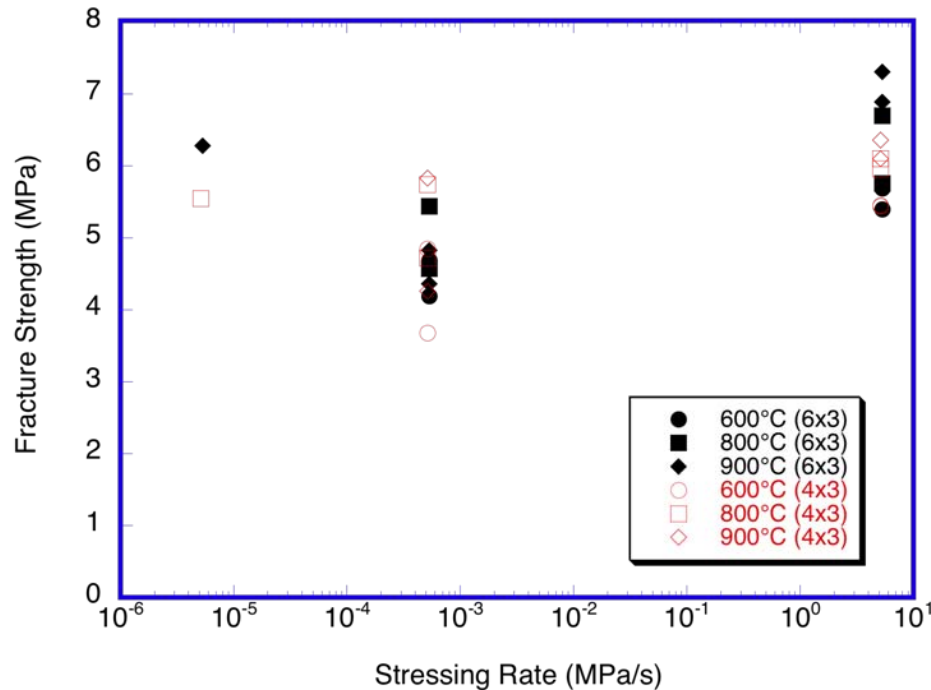


Material	Average CTE (ppm/K)	Elastic Modulus (GPa)	K _{IC} (MPa√m)	Density (g/cc)
Virgin (not coated)	0.42	11.91±0.15	0.32±0.04	1.19±0.02
C coated	0.97	10.74±0.29	0.35±0.03	1.19±0.03
D coated	0.73	12.84±0.37	0.40±0.02	1.23±0.02

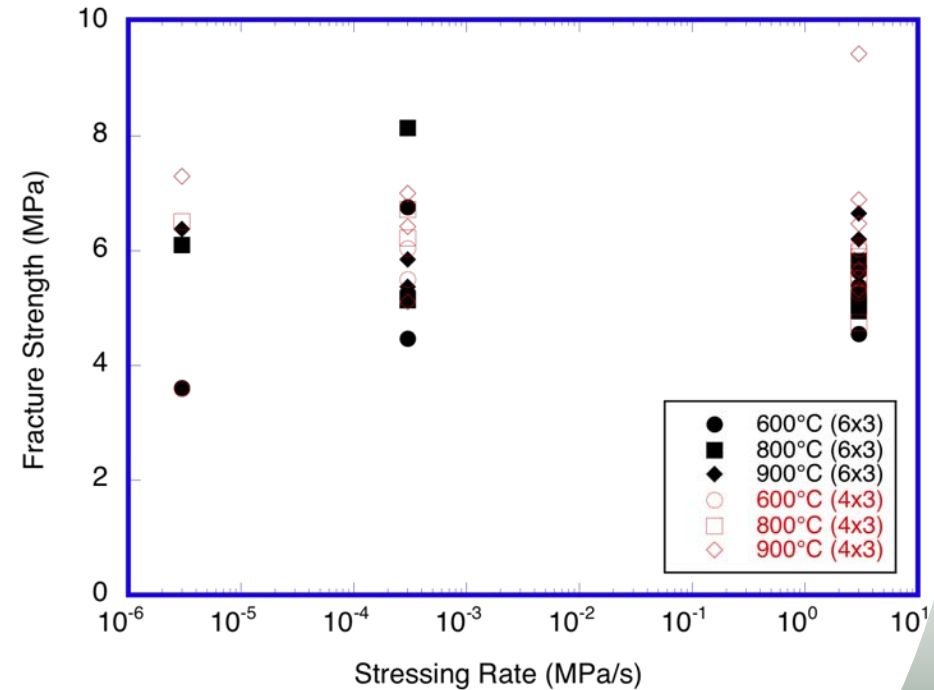


Probabilistic design: Dynamic Fatigue Response is not Influenced by the Applied Catalytic Coating

Bare Cordierite DPF

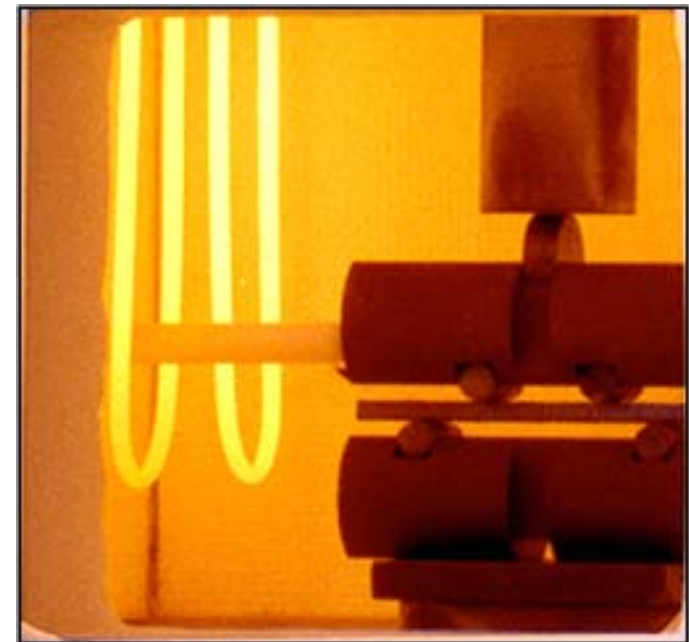
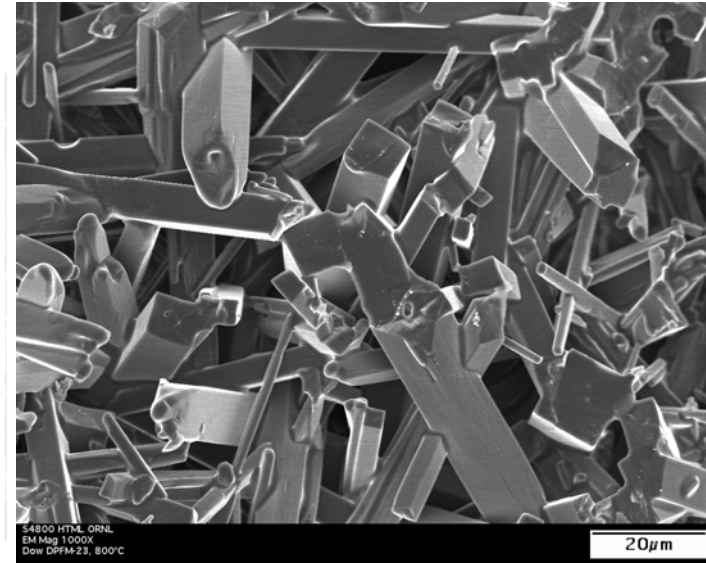
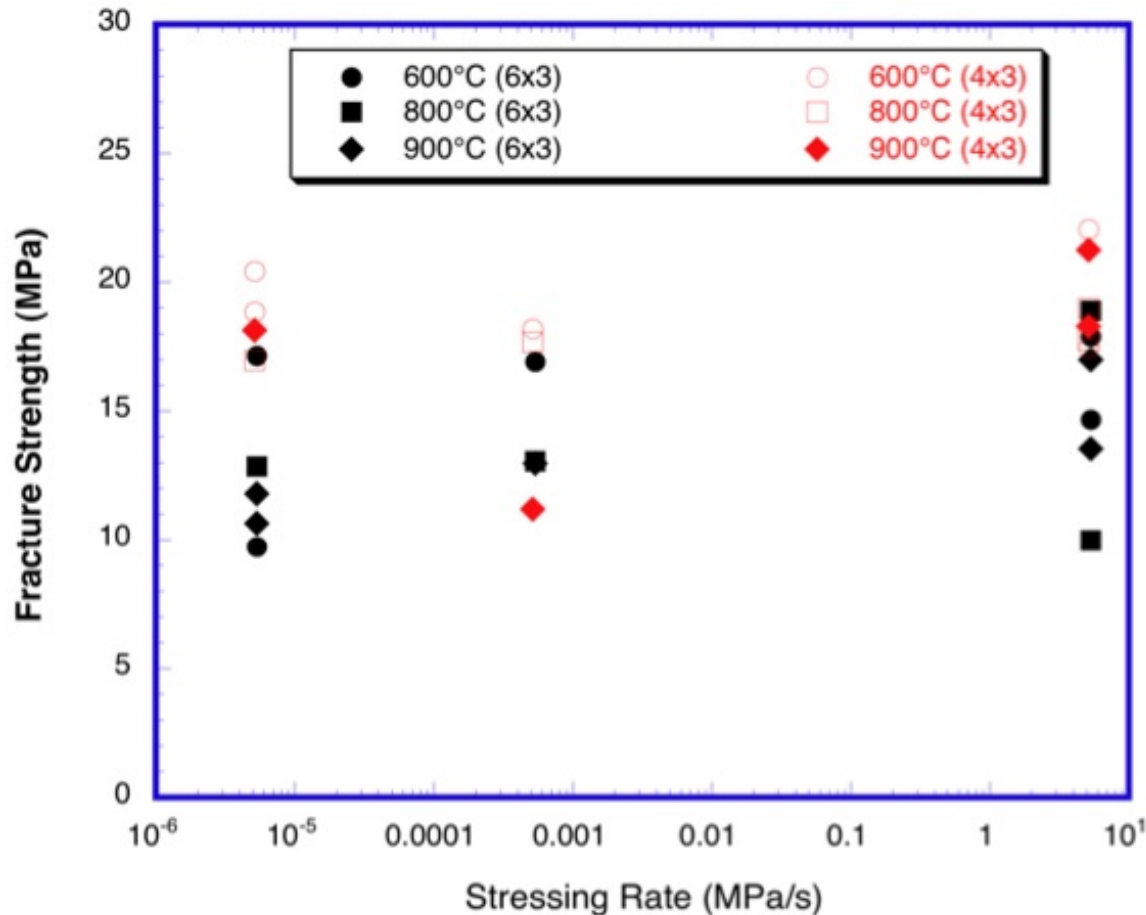


Coated Cordierite DPF



- Dynamic fatigue: $3 \times 10^{-5} - 3$ MPa/s, 600, 800 and 900°C, in air

Probabilistic design: Little Stress Rate Effect Observed in the Mullite DPF



However, there is a minor effect on the specimen size on the fracture strength due to the difference in flaw population

Future Work

- **Continue interaction of washcoat, soot and substrate on properties**
- **Continue determining properties as a function of location in DPF (core vs. outer)**
- **Collaborate with Dr. Sampath at SUNY-Stony Brook on further development of NDE technique**
- **Characterize the dynamic and static fatigue response Aluminum-titanate and SiC DPFs**

Summary

- Carried out physical and mechanical property measurements on several coated and uncoated substrates and ranked their relative thermal shock resistance (continued from FY2007).
- Identified the relationship between porosity and the elastic-fracture properties for diesel particulate filter substrates.
- Characterized field returned diesel particulate filters and compared their properties to virgin filters. This information would be utilized to refine the DPF service lifetime prediction models.