

Lessons Learned:
**Developing Thermochemical Cycles
for Solar Heat Storage Applications**

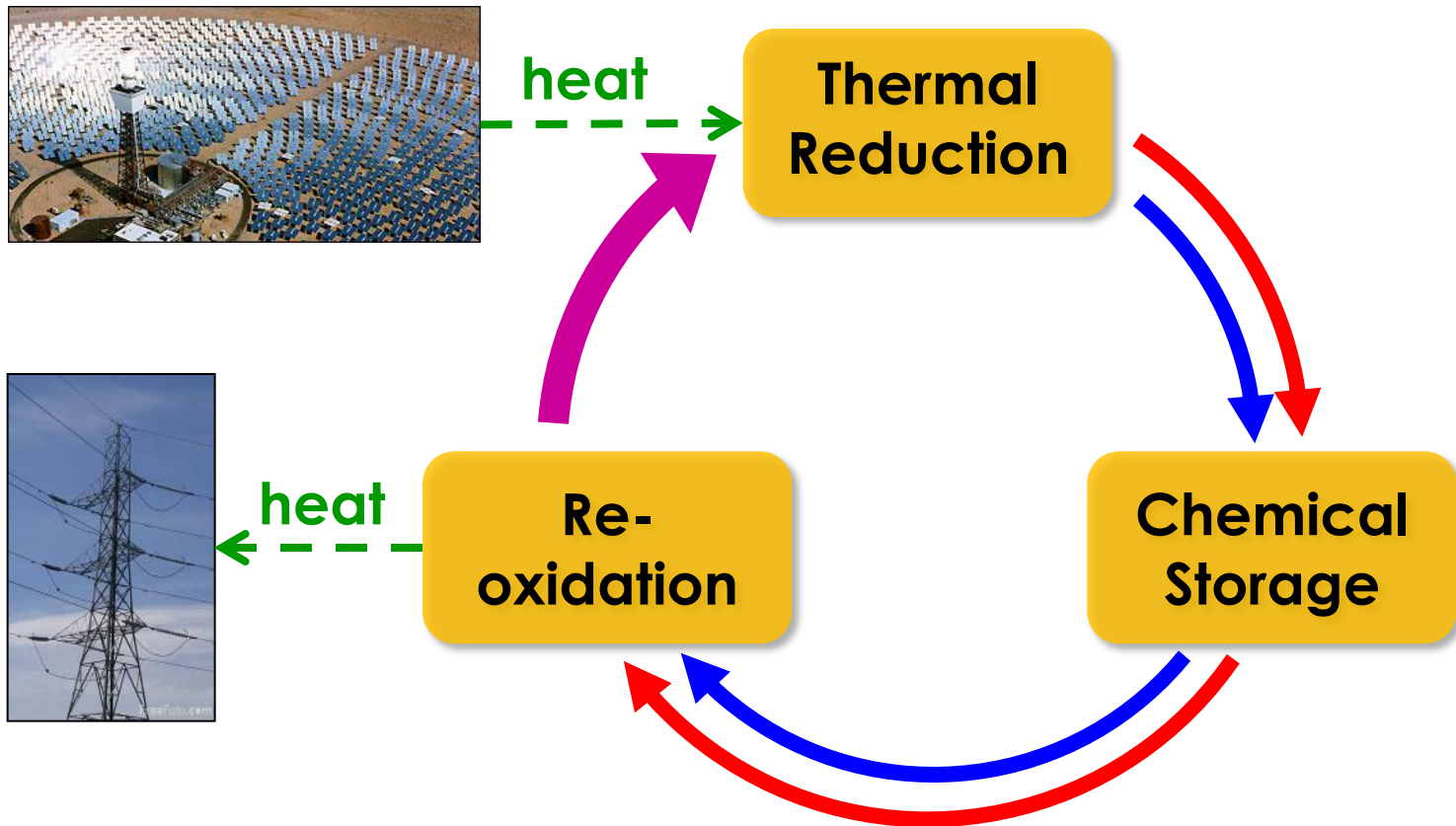
**General Atomics
Bunsen Wong**

IFT\ P2013-001

Outline

- Introduction
- Case Study I: **Solid Oxide Decomposition**
- Case Study II: **Sulfur Based Cycle**
- Conclusions

Solar heat is used to drive the reduction step of a thermochemical cycle



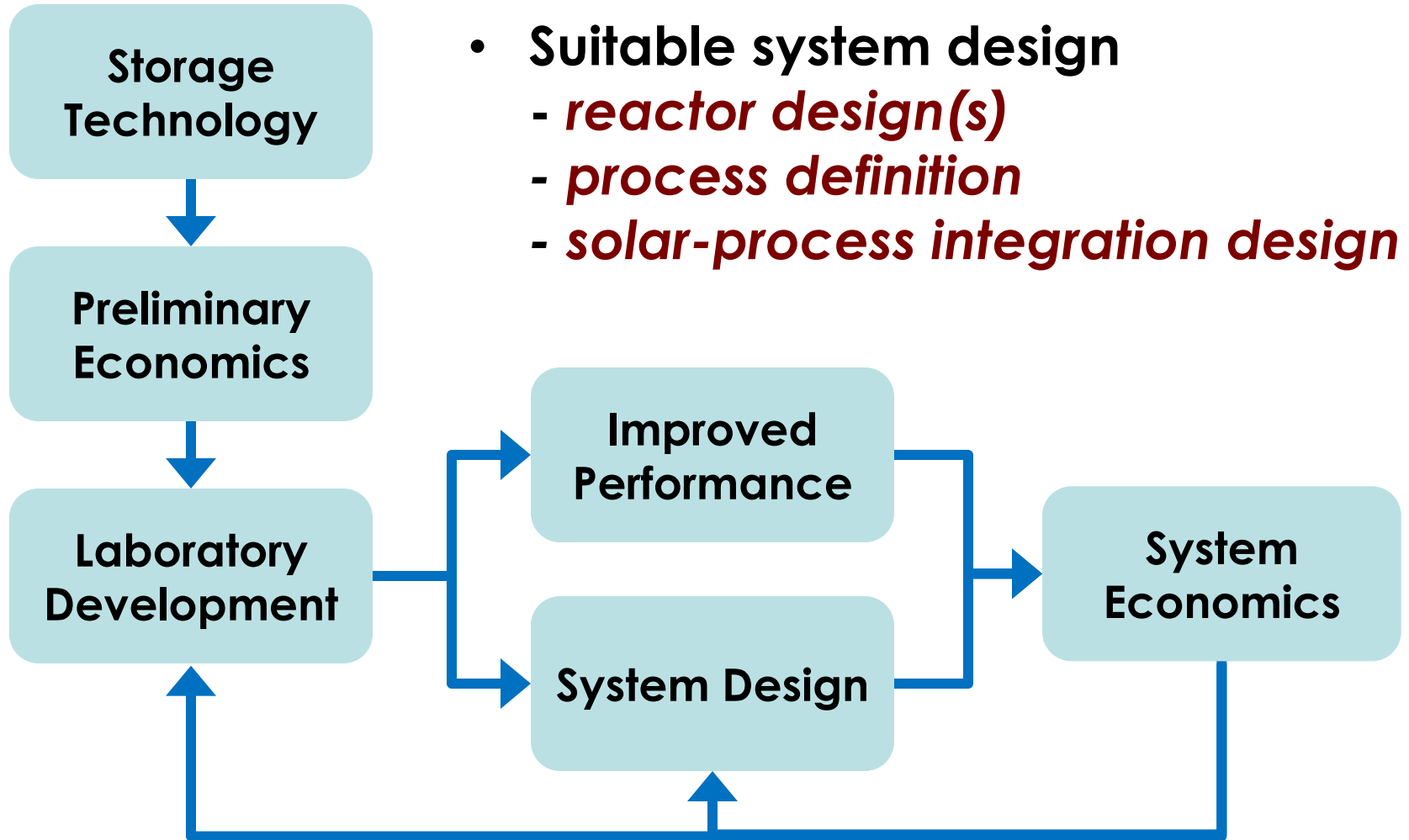
- Energy is stored in chemical bonds
- Energy is recovered upon chemical re-oxidation

Thermochemical heat storage can provide very high energy storage densities

Technology	Energy Density (kJ/kg)
Gasoline	45000
Sulfur	12500
Cobalt Oxide	850
Molten Salt (Phase Change)	230
Molten Salt (Sensible)	155
Lithium Ion Battery	580
Elevated water Dam (100m)	1

- **High energy density with low storage cost**
- **Ambient and long term storage**
- **Transportability**

An approach to develop and determine whether a TC suitable for TES has been established

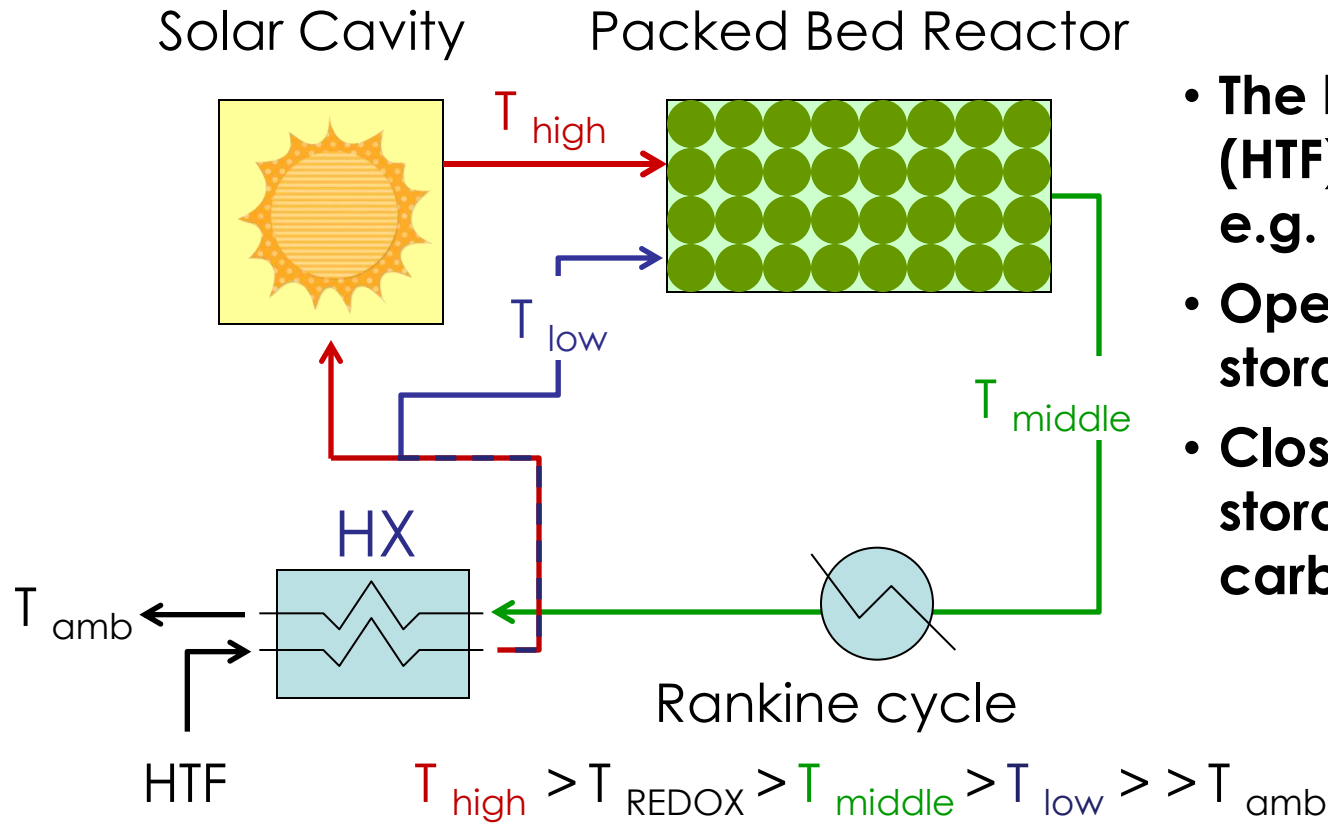


GA led two thermochemical energy storage projects that are supported by DOE

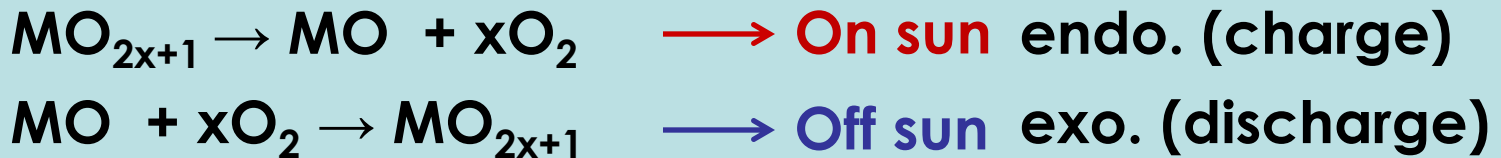
1. **Solid Oxide Based** Thermochemical Heat Storage*
(DOE Advance TES program DE-FG-36-08GO18145)
2. **Sulfur Based** Thermochemical Heat Storage for Baseload*
(DOE Baseload program DE-EE0003588)

* Project partner: German Aerospace Center (DLR)

A pair of solid oxide REDOX reactions were used to store and release heat

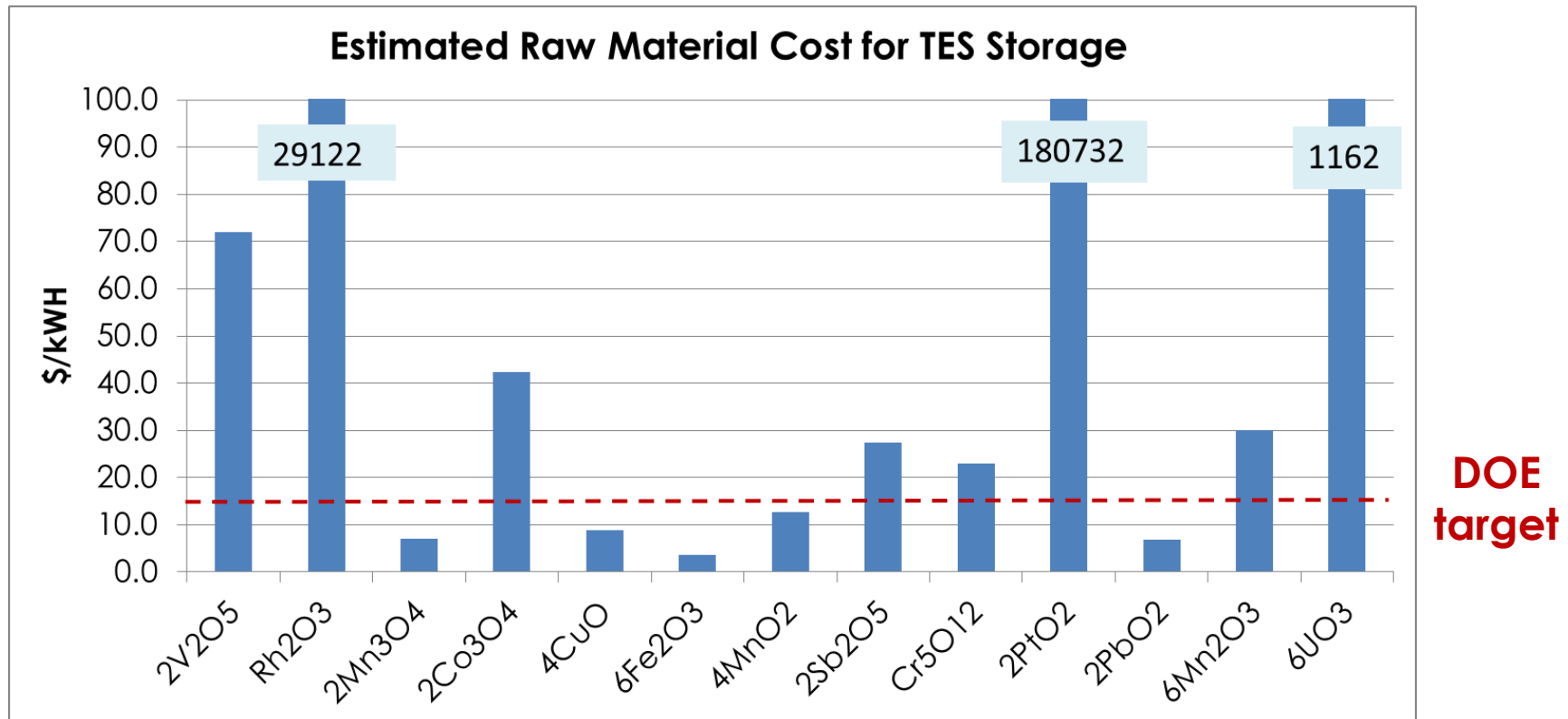


- The heat transfer fluid (HTF) is also the reactant e.g. Air (O_2), CO_2 & H_2O
- Open System – no storage of HTF: oxides
- Closed System – HTF storage required: carbonates, hydroxides



Preliminary economics can be estimated through energy related costs

- Energy related costs include raw materials, storage and process cost etc.



- Low raw material cost is required for large scale use

Thermal reduction takes place readily in all candidate oxides

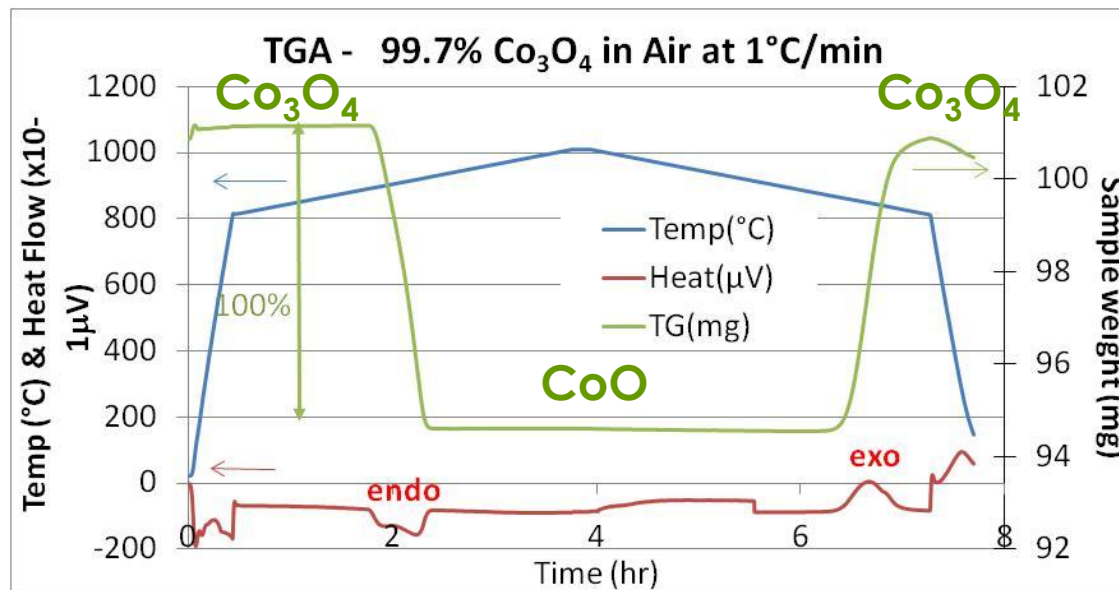
Reaction	HSC Temp (°C)	Exp Temp (°C)	Re-oxidation
$2\text{PbO}_2 \rightarrow 2\text{PbO} + \text{O}_2$	405	NA	NO
$2\text{Sb}_2\text{O}_5 \rightarrow 2\text{Sb}_2\text{O}_4 + \text{O}_2$	515	NA	NO
$4\text{MnO}_2 \rightarrow 2\text{Mn}_2\text{O}_3 + \text{O}_2$	530	NA	NO
$2\text{BaO}_2 \rightarrow 2\text{BaO} + \text{O}_2$	780	690	YES*
$2\text{Co}_3\text{O}_4 \rightarrow 6\text{CoO} + \text{O}_2$	900	870	YES
$6\text{Mn}_2\text{O}_3 \rightarrow 4\text{Mn}_3\text{O}_4 + \text{O}_2$	900	900	YES*
$4\text{CuO} \rightarrow 2\text{Cu}_2\text{O} + \text{O}_2$	1025	1030	YES
$6\text{Fe}_2\text{O}_3 \rightarrow 4\text{Fe}_3\text{O}_4 + \text{O}_2$	1300	1200	YES
$2\text{V}_2\text{O}_5 \rightarrow 2\text{V}_2\text{O}_4 + \text{O}_2$	1325	750*	YES*
$2\text{Mn}_3\text{O}_4 \rightarrow 6\text{MnO} + \text{O}_2$	1500	1400	YES

* incomplete

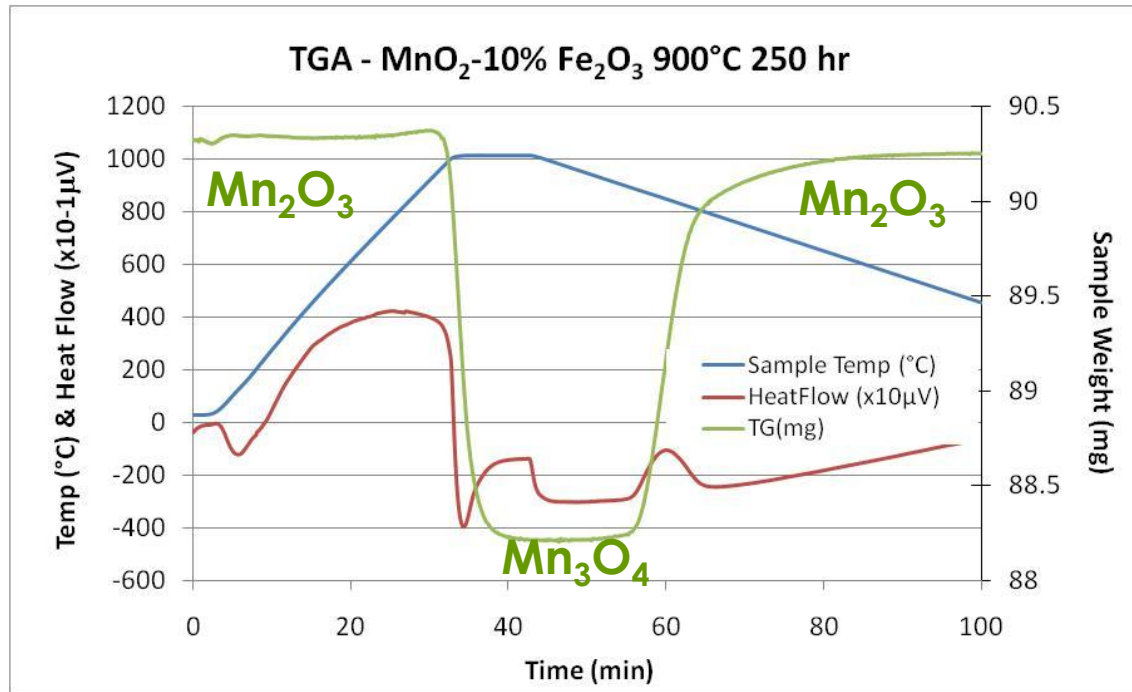
- Re-oxidation can be slow, especially at low temp
- **Reaction kinetics needed to be improved**

Four oxides underwent REDOX between 700-1100°C but only CoO demonstrated full re-oxidation

Reaction	Full Re-oxidation	Cyclic Repeatability
$2\text{BaO}_2 \rightarrow 2\text{BaO} + \text{O}_2$	No	Yes
$2\text{Co}_3\text{O}_4 \rightarrow 6\text{CoO} + \text{O}_2$	Yes	Yes
$6\text{Mn}_2\text{O}_3 \rightarrow 4\text{Mn}_3\text{O}_4 + \text{O}_2$	No	No
$4\text{CuO} \rightarrow 2\text{Cu}_2\text{O} + \text{O}_2$	No	No



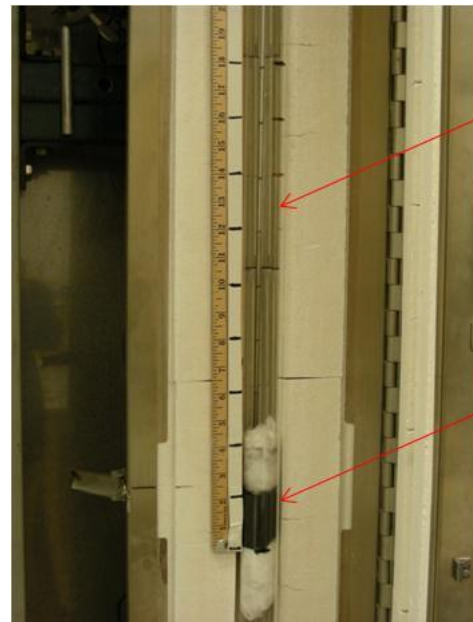
Secondary oxide addition was used to improve re-oxidation kinetics of manganese oxides



Doping	Max Re-oxidation (%)
Fe_2O_3	100
ZrO_2	42
CuO	25
None	6

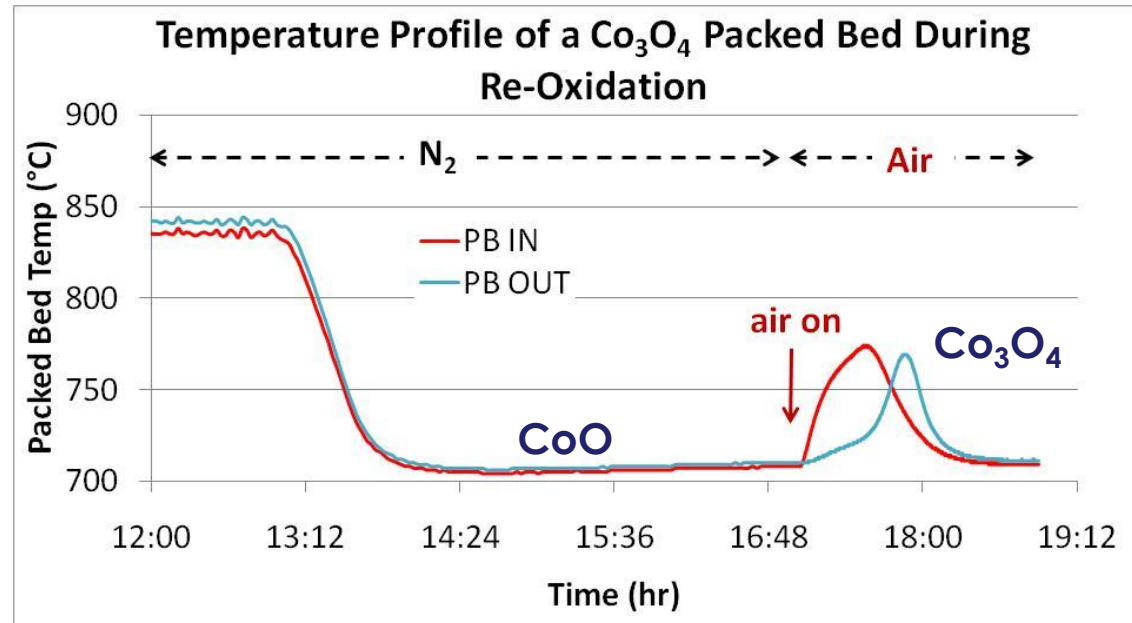
- Full re-oxidation and cyclic repeatability were achieved with a 10wt% Fe_2O_3 addition
- REDOX reaction kinetics were obtained from laboratory measurements

Thermal charging/discharging in a packed bed was demonstrated in the laboratory



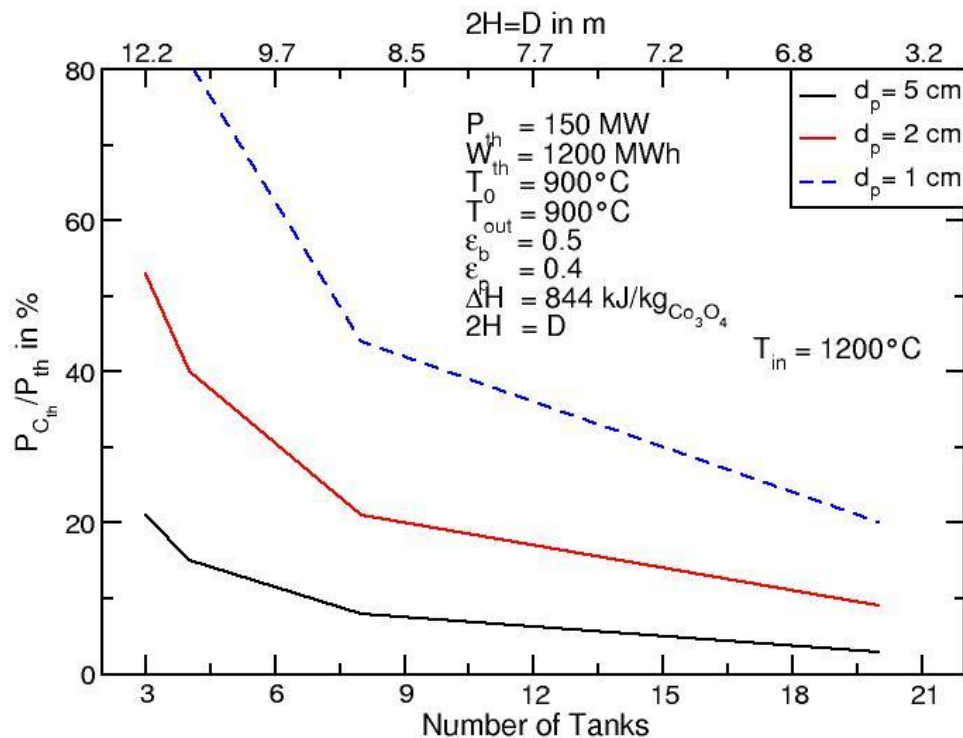
Quartz Tube

Packed Bed



- A materials compatibility study was carried out
- Process modeling was conducted using preliminary design and kinetics data
- Modeling data was used for final reactor design

Modeling results show pressure drop has significant impact on efficiency, process and reactor designs

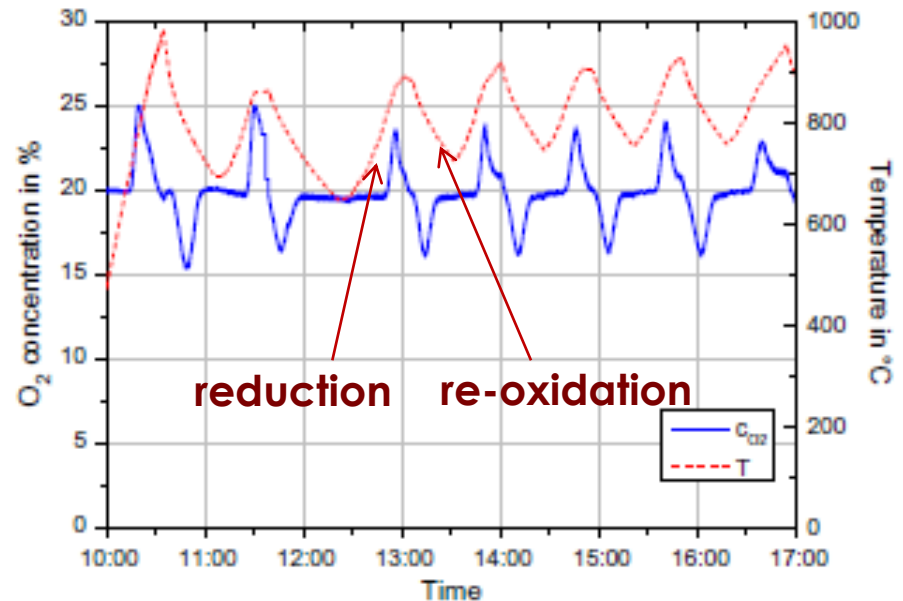
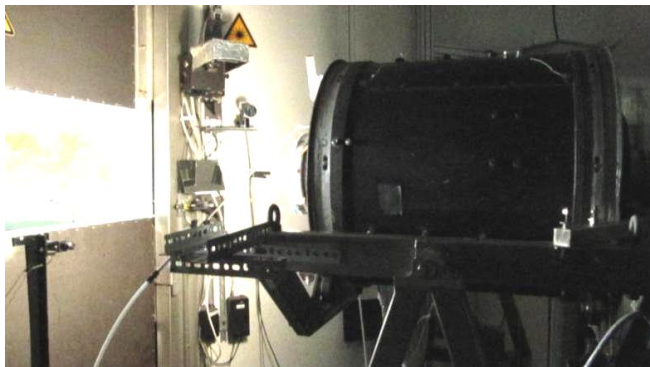
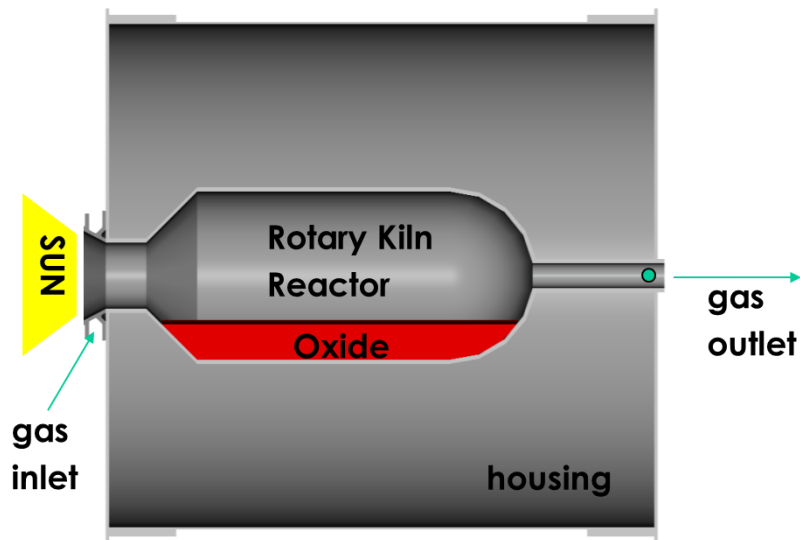


- Higher inlet air temp is required ($+300^\circ\text{C} > \text{eq}$)
- Larger pellets are necessary
- Multiple reactors are needed

- Indirect heat transfer is not suitable when high mass flow rates are required
- A directly irradiated design is preferred

F. Schaube in GA Report A27230

A directly irradiated moving bed reactor design was adapted



- REDOX kinetics was much faster in a moving bed
- **Maximize heat transfer rate to fully utilize solar heat**

A rotary kiln (moving bed) reactor

M. Neises et al, Solar Energy (2012)

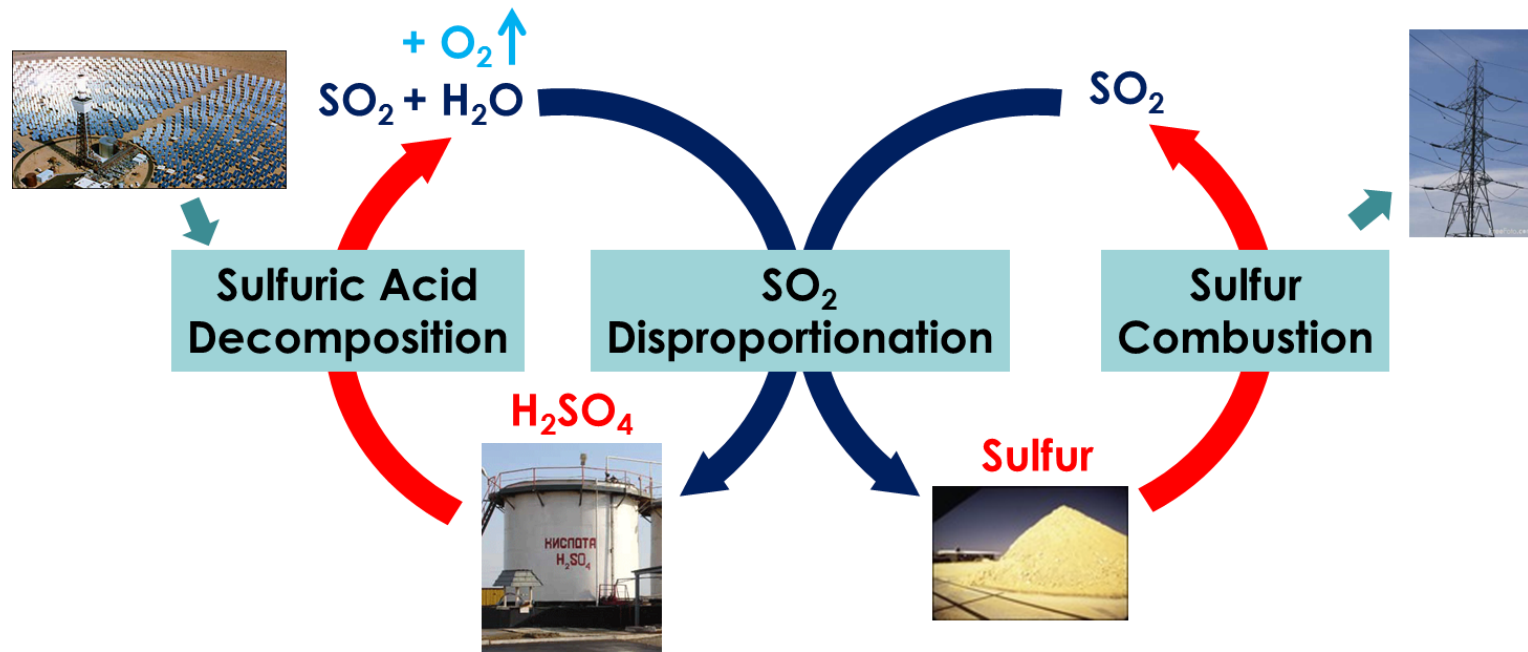
REDOX of solid oxide is applicable to thermochemical energy storage for CSP

- **Material cost is the main driver of TES economics**
- **Mixed oxides greatly improve REDOX kinetics and cyclic repeatability**
- **A moving bed reactor is required to minimize parasitic cost**

DOE Metric	Unit	2015	Mn-Fe	Co-Al
Storage Cost	\$/kWh	15	15-35	50-100
LCOE	\$/kWh	0.06	0.09-0.11*	0.13-0.17*
Efficiency	%	93	>93	>93

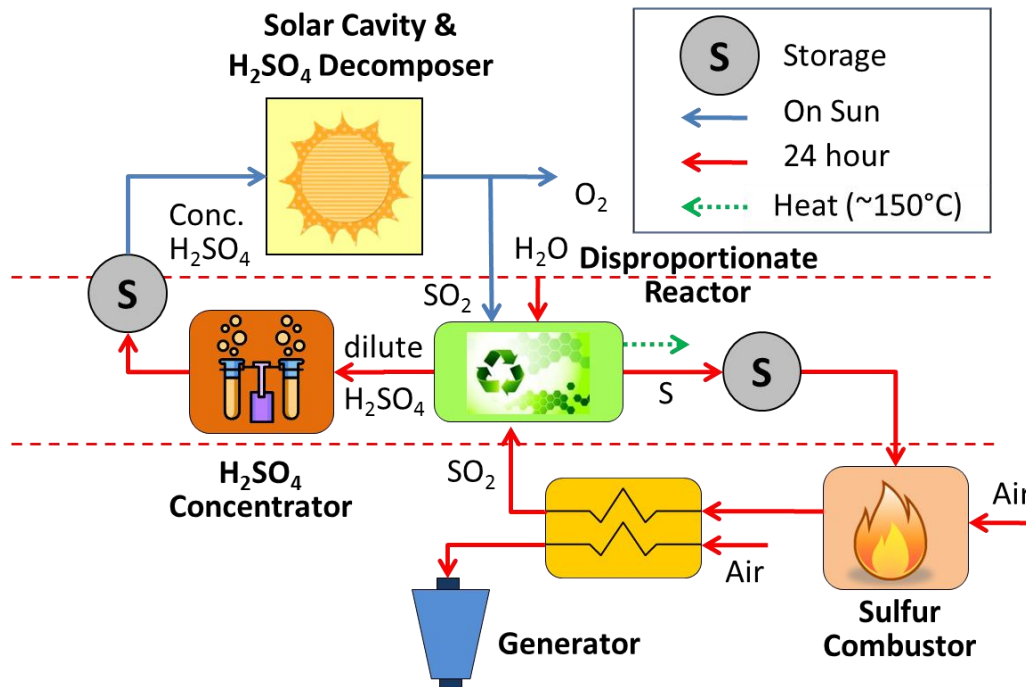
*SAM (NREL) using 2010 costs

Solar energy can be stored in elemental sulfur via a three step thermochemical cycle



	Reaction	Temp (C)
H_2SO_4 Decomposition	$2H_2SO_4 \rightarrow 2H_2O(g) + O_2(g) + 2SO_2(g)$	800
SO_2 Disproportionation	$2H_2O(l) + 3SO_2(g) \rightarrow 2H_2SO_4(aq) + S(l)$	150
Sulfur Combustion	$S(s,l) + O_2(g) \rightarrow SO_2(g)$	1200

Preliminary economics was assessed using a simplified process flowsheet

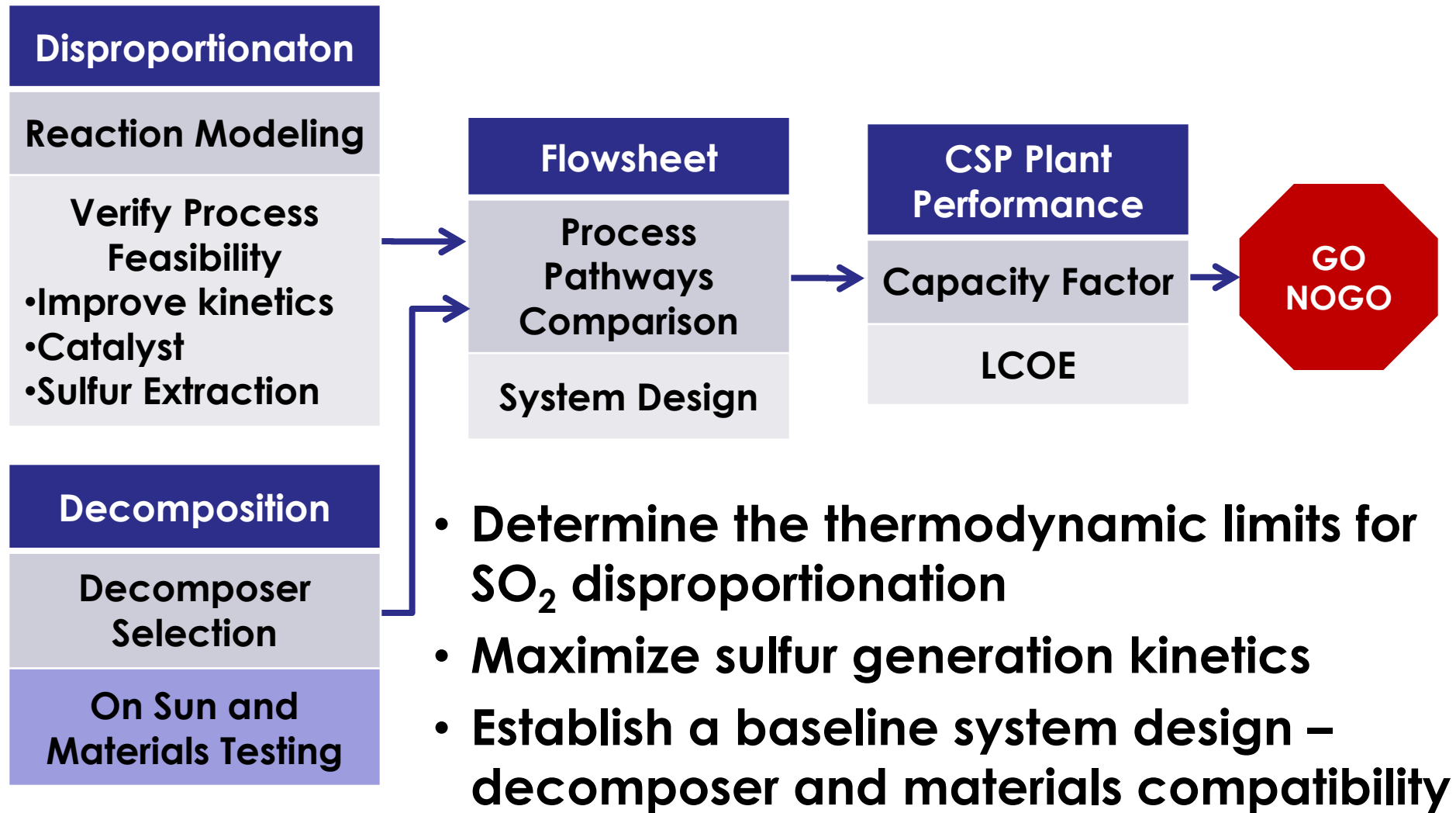


- **maximize solar capacity**
- **diurnal and seasonal energy storage**
- **constant daily/ year round power supply**
- **Brayton or combined cycle**
- **environmentally friendly**

DOE Metric	Capacity Factor	LCOE (¢/kWh _e)
SunShot Target	75%	6.0
CSP w/Sulfur Storage	>75%	8.7*

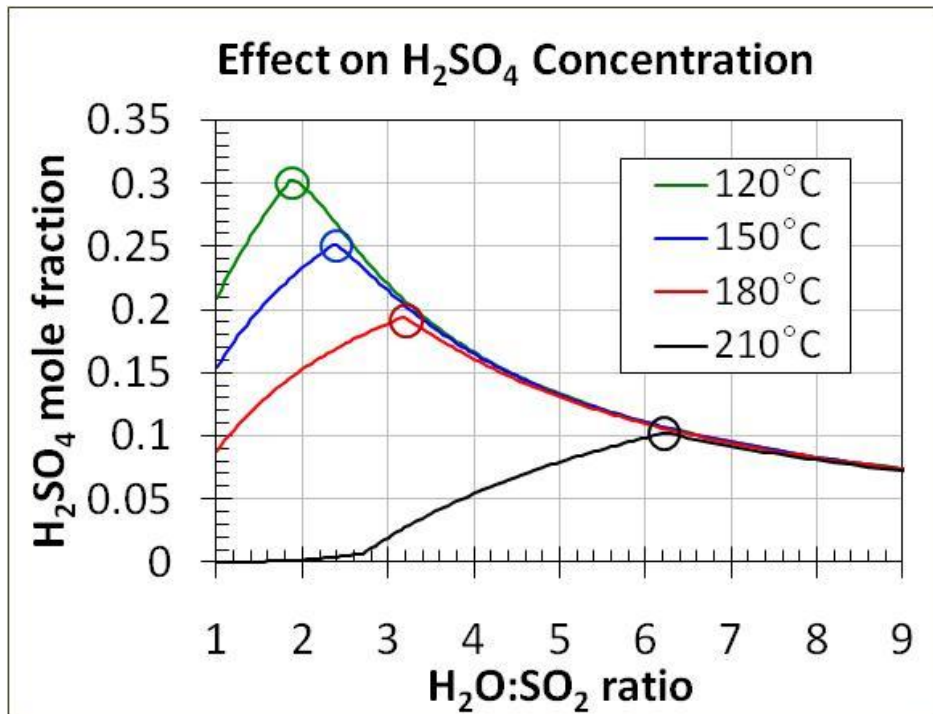
*SAM (NREL) using 2010 costs

Phase I – Determine the TC limits and address key process and design issues



Effect of temperature and pressure on sulfur generation and H_2SO_4 conc. was modeled

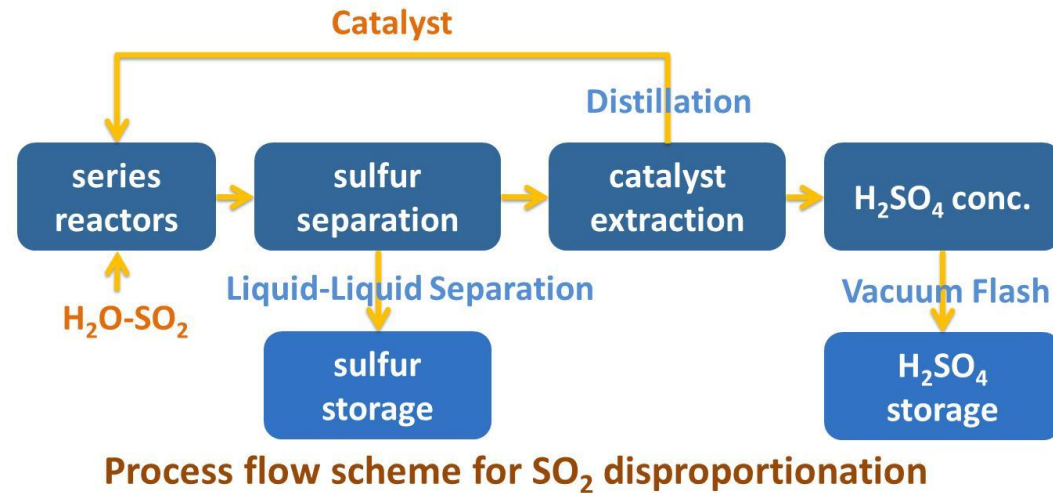
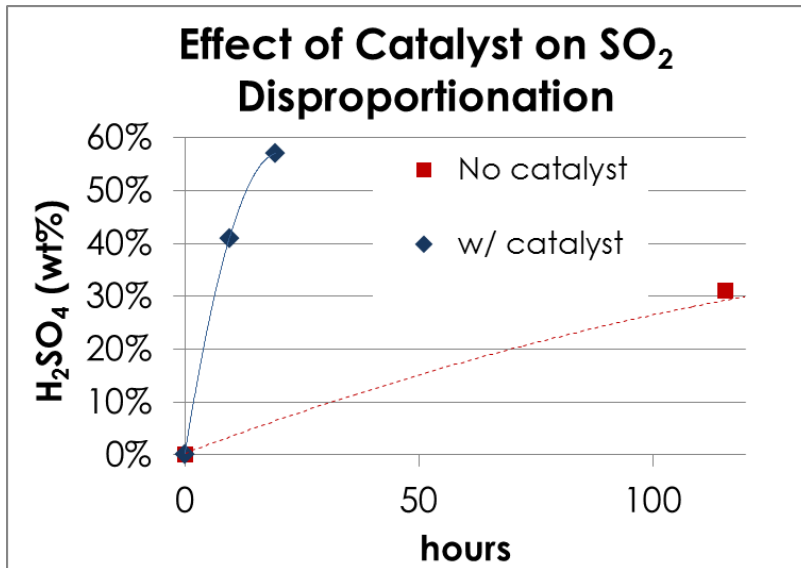
- Results guided experimental work
- Data used for process and flowsheet designs



- **Low temperature** and **high pressure** favor sulfur formation and high H_2SO_4 conc.

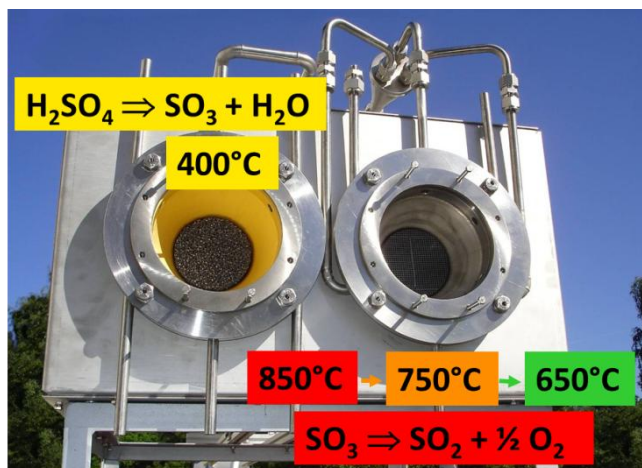
Parameters	Range
Temp	120-150°C
Pressure	>10 bar
$\text{H}_2\text{O}/\text{SO}_2$	2 to 4
H_2SO_4 conc.	62wt%

Disproportionation kinetics was greatly enhanced with the use of catalyst

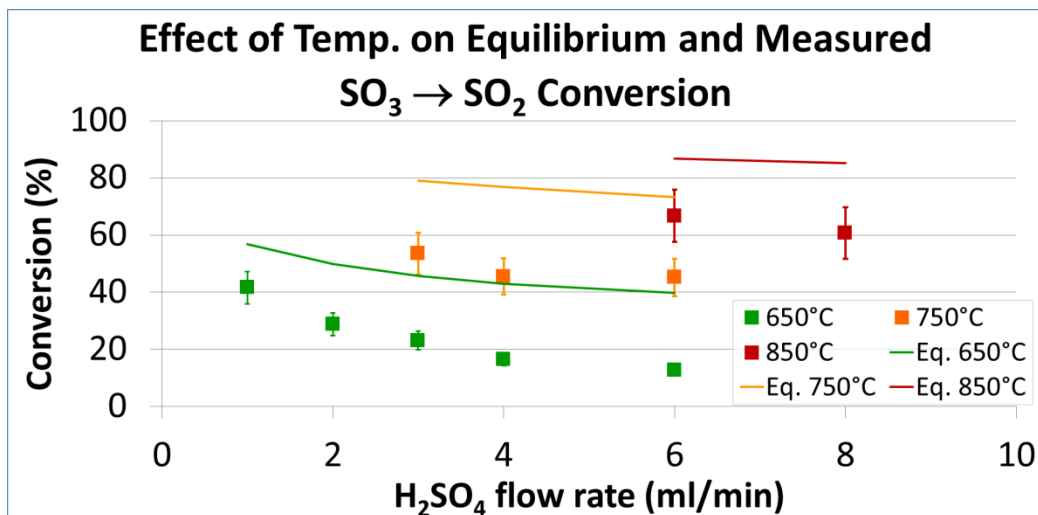


- Kinetics data defined reactor size and process cond.
- Means for sulfur extraction and catalyst recovery were established via laboratory work
- All processing steps for SO_2 disproportionation have been determined

Sulfuric acid decomposition was demonstrated on sun using a solar furnace

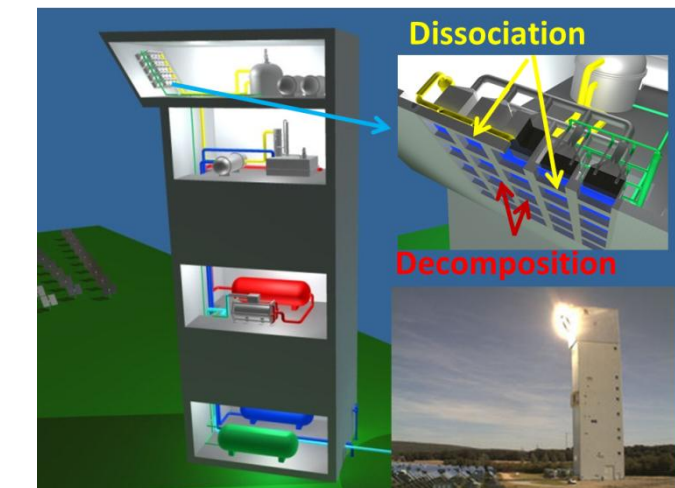


A dual chamber H_2SO_4 decomposer



- Process and decomposer refinement based on test data
- Lower decomp. temperature to reduce solar installation cost

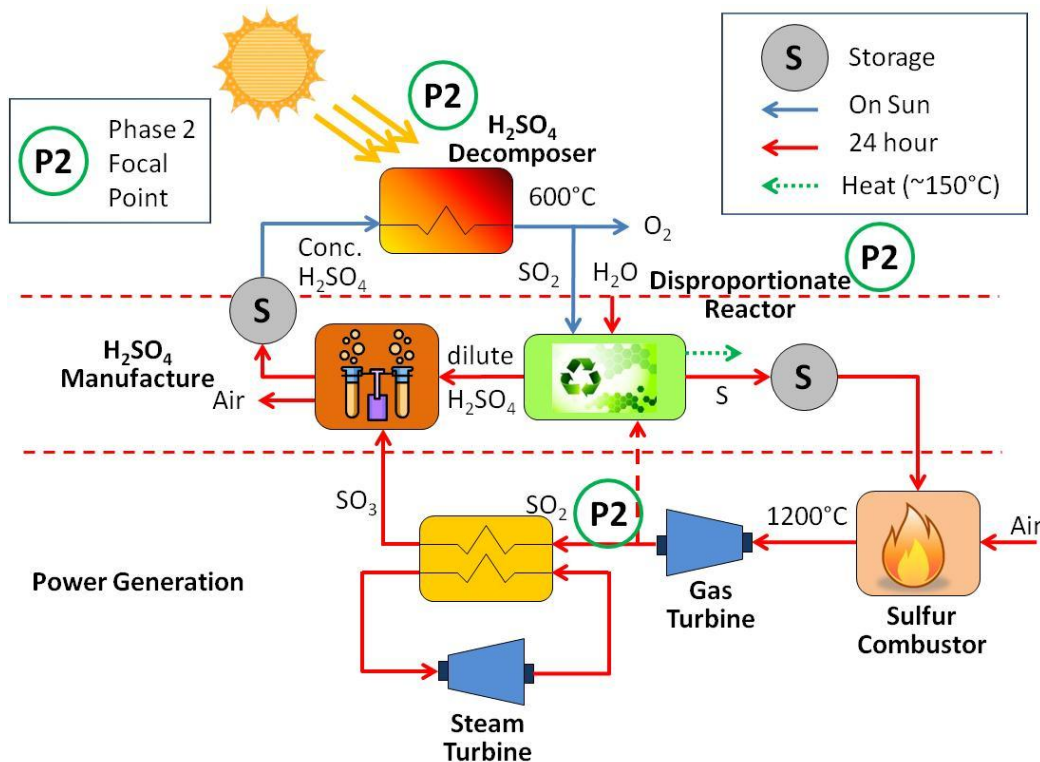
D. Thomey et al., Int. Journal of Hydrogen Energy (2012)



Conceptual scale up of a modular decomposer on a solar tower

A detailed flowsheet was established based on modeling and experimental data from Phase I

- Plant design incorporated established processes from sulfuric acid manufacturing plant



DOE Metric	LCOE ($\text{\$/kWh}_e$)
SunShot	6.0
CSP w/Sulfur Storage	8.1*

*SAM (NREL) using 2012 costs

- Storage cost is $< \$2/\text{kWh}$
- LCOE is $\sim 6\text{\$/kWh}_e$ based on proposed SunShot targets

Conclusions

- Chemical energy storage is well suited to CSP
- Energy related costs (materials and storage) need to be low
- Reaction kinetics of low temperature step can be a show stopper – improve kinetics
- Maximize process compatibility with solar reactor design – direct irradiation is preferred and always be beware of parasitic costs
- Maximize solar heat utilization and minimize solar installation cost in process and system designs
- When possible, incorporate established processes into your system design